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MICROCOMPUTER ENHANCEMENT OF THE ARTICULATED TOTAL BODY (ATB)  
BIODYNAMIC MODELING SYSTEM

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This technical report has been reviewed and is approved for publication.

FOR THE COMMANDER

JAMES W. BRINKLEY  
Director  
Biodynamics and Bioengineering Division  
Harry G. Armstrong Aerospace Medical Research Laboratory

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## 1. INTRODUCTION

### 1.1 BACKGROUND

The *Articulated Total Body* (ATB) model was derived from the *Three Dimensional Crash Victim Simulation* (3DCVS) which was originally conceived as a research tool to enable investigation of driver or occupant and motor vehicle interaction under various restraint configurations and other initial conditions during automobile crashes. Researchers at the U.S. Air Force Harry G. Armstrong Aerospace Medical Research Laboratory (AAMRL) adopted this model for the study of aircrew members during ejections from aircraft, with the view of eliminating or reducing injuries in a high acceleration environment. The use of modeling in this area of study is particularly appropriate and attractive since it reduces the cost of testing (whether with manikins or human subjects) and eliminates the risks associated with human testing. The modeling approach also supports system evaluations under operating conditions that would otherwise be infeasible to test with human subjects, and where the biofidelity of manikins is inadequate.

The *Three Dimensional Crash Victim Simulation* was developed by J. A. Bartz at the Cornell Aeronautical Laboratory for the U.S. Department of Transportation (DoT). The original model is a system of over 180 simultaneous ordinary differential equations programmed for solution by numerical integration, on an IBM mainframe. The 3DCVS model was improved by Fleck, Butler, and Vogel under further DoT sponsorship. Air Force motivated enhancements include the modeling of significant g-blast forces during high speed ejections, and the modeling of complex, interacting-element restraint systems. Additional enhancements have included the development of significant graphic output capabilities to facilitate the analysis of results.

To facilitate the use of the model, additional application software has been written. These programs are GEBOD, VIEW, and CABS, which, together with ATB, comprise the ATB Modeling System (ATBMS). GEBOD prepares the body description for input to ATB using interactive inputs from the analyst. The VIEW program plots projected views of body position from the ATB simulation at constant time steps. CABS is used to compare tabular time history data files from

two ATB simulations.

The simulation, the numerical solution of the model, which was originally implemented on IBM mainframes, was adapted first to the CDC 6600 (another mainframe), and subsequently at AAMRL to the Perkin-Elmer 3250XP mini-computer.

## 1.2 OBJECTIVE

The ATB Modeling System is needed to address a variety of new technologies and challenges which are changing the operating environment of aircrews. These changes include increasing aircraft performance, which increase the need for expanding the safe ejection envelope. The increasing complexity of the weapon systems, cockpit, and missions have also stimulated the development of equipment to aid the aircrews -- night vision goggles, helmet mounted sights, and helmet mounted displays. Each of these devices has the potential for impacting the safe ejection envelope and increasing the injury potential of an ejection (as well as increasing the fatigue of normal flying). While microelectronics, fiber optic technology, and miniaturization can keep the equipment weight small, even these weights at 15 G ejection acceleration may pose a substantial injury hazard.

In view of the hazard potential of the technologies being introduced into the cockpit, exploration of their biodynamic effects is necessary. The use of the ATB Modeling System currently requires either costly mainframe computers, or a substantial minicomputer laboratory, which restricts its use at a time when computing technology is rapidly evolving, and is becoming available at the desktop level at an affordable cost. It is appropriate to reduce or eliminate the ATBMS analysis restrictions imposed by the present costly computer requirements in view of the needs of investigators in the DoD, industry, and the academic community to assess the consequences of new flightmission hardware developments.

Accordingly, this effort was undertaken with the objective of demonstrating the feasibility of using the Articulated Total Body Modeling System on readily available microcomputer systems.

### 1.3

#### REPORT OVERVIEW

Section 2 summarizes the results of this effort, with conclusions and recommendations. The system design criteria, hardware, operating system, and support software selections are described in Section 3. Section 4 discusses the software conversion and program execution. Supporting data are presented in the Appendices.

## 2. SUMMARY

### 2.1 RESULTS

The Articulated Total Body Modeling System was converted from the Perkin-Elmer 3250XP minicomputer to an Intel 80386/80387 microprocessor based personal computer under a Disk Operating System (DOS) environment. The design criteria, discussed in Section 3, were satisfied without compromises. The resulting hardware and software configuration suitable for using, or conducting further developmental work with, the ATBMS is also documented in Section 3. The results obtained on two sample cases using the microcomputer compare favorably with the results obtained from the Perkin-Elmer in terms of computational reproducibility. The results for comparison are presented in Appendices C3, C4, D3, and D4, respectively. The graphics capability presently in the ATBMS is also successfully replicated, as shown in Appendices E2, E3, F3, and G3.

The relevant hardware and performance characteristics of the computer systems used in this implementation are presented in Table 2-1. The significant differences between systems B and C are the presence of cache memory in system C and the clock frequencies of 20 vs 33 MHz. These two differences result in a three to one computational performance ratio, as indicated by both the Whetstone and Dhrystone measures. Two sample cases were used in comparing alternative hardware systems -- a basic sled test simulation (marked as example 1) and a dynamic joint test (example 2).

The execution timing results, summarized in Table 2-2, show that the 80386 system, operating with a 20 MHz clock, (80386/20, system B), is somewhat slower than the Perkin-Elmer. (System A is omitted from Table 2-2 due to insufficient memory for ATB execution.) However, the 80386/33 system (C) with cache memory is more than twice (2.17) the speed of the Perkin-Elmer. The comparison of two 80386 systems, at 20 and 33 MHz respectively, shows a performance ratio of slightly under three -- 2.79 and 2.95 for the two sample cases. These results are consistent with the systems' computational characteristics (3:1), which are slightly degraded by the I/O requirements. In view of the relatively high computation to I/O ratio of the ATB simulation the disk performance differences have only a slight impact.

Table 2-1. ATBMS Microcomputer System Comparisons

	<u>SYSTEM</u>		
	<u>A</u>	<u>B</u>	<u>C</u>
<u>HARDWARE CHARACTERISTICS</u>			
Clock frequency - MHz	16	20	33.35
Memory, main, kb	640	640	640
Memory, extended, kb	1024	3456	7552
Memory, cache, kb	0	0	64
<u>PROCESSOR PERFORMANCE<sup>1</sup></u>			
Dhrystones	3501	3793	11379
Whetstones, k	850.2	945.0	2933.8
<u>PROCESSOR PERFORMANCE</u> <u>RELATIVE to 20 MHz SYS.</u>			
Dhrystones	92	100	300
Whetstones	90	100	310
<u>DISK PERFORMANCE<sup>1</sup></u>			
capacity, mb	70	348	150
track to track seek, ms	3.42	5.32	5.36
average seek, ms	25.3	13.0	20.4
transfer rate, kb/sec	33.6	182.0	35.2

1: processor and disk performance were measured using *CheckIt*, Ver. 1.10, TouchStone Software Corporation, Seal Beach, CA 90740.

Table 2-2. ATB Execution Time Comparisons

<u>ATB</u> <u>PROBLEM</u>	<u>Perkin-Elmer</u> <u>3250XP</u>	<u>Intel 80386/80387</u>	
		<u>20 MHz</u> (B) <u>seconds</u>	<u>33 MHz</u> (C)
1	291.45	395.79	134.29
2	30.91	38.67	13.84
<u>percent, relative to 3250XP</u>			
1	100	136	46
2	100	125	45
<u>percent, relative to 80386/20</u>			
1	74	100	34
2	80	100	36



For program compilation and linking Table 2-3 shows the results for a 80386/7 at three different clock frequencies -- 16, 20, and 33 MHz. The data indicate that the 33 MHz system is approximately 1.7 times faster than the 20 MHz processor at this task. This speed ratio is much lower than the value (~2.9) for execution. The difference in compilation and linking performance is probably due to the relatively large volume of I/O which is slower with the disk installed on the 33 MHz system. This hypothesis is supported by the performance differences between compilation and linking, with linking being slower than compilation, due to more disk accesses to the library to resolve references.

Table 2-3. ATBMS Compilation and Link Time Comparisons

PROGRAM	16 MHz		20 MHz		33 MHz	
	(A)		(B)		(C)	
			<u>seconds</u>			
GEBOD	43	19	39	11	22	7
ATB	382	108	331	59	183	41
VIEW	41	54	35	32	19	22
<u>percent, relative to 80382/20</u>						
GEBOD	110	173	100	100	56	64
ATB	115	183	100	100	55	69
VIEW	117	154	100	100	54	69
<u>compilation + linking percent, relative to 80386/20</u>						
GEBOD	124		100		58	
ATB	126		100		57	
VIEW	142		100		61	

## 2.2 CONCLUSIONS

The results presented in Section 2.1 unquestionably demonstrate the capability of highly economical microcomputers for conducting both analytical and further developmental work with the ATBMS. The ATBMS conversion and execution results show that:

- (a) production hardware, commercially available disk operating systems and support software comprise a suitable host for the ATBMS work,
- (b) the demonstrated microcomputer host system performs without compromising the numerical accuracy or graphics capability of the ATBMS,
- (c) the high performance microcomputer (Intel 80386/80387 based, with 33 MHz clock rate and cache memory) offers execution times markedly superior

to that provided by the Perkin-Elmer 3250XP minicomputer, and

(d) based on the hardware and software requirements established in the course of this study, the microcomputer-based ATBMS use is considerably more economical than the minicomputer alternative.

## 2.3 RECOMMENDATIONS

In view of the demonstrated results, which show that the microcomputer based ATBMS is both technically and economically superior to its earlier-technology minicomputer implementation, further enhancement of the 386 ATBMS is recommended. Some specific enhancement areas are described below, while a fully developed set of recommended changes will be documented separately.

The principal areas for ATBMS enhancements are user interface improvements (UII) and performance upgrades (PU). UIIs include the extension of the program-files interface, which was implemented for this phase with the introduction of DIRECTORY files, described in Section 4.2.5. The extension will retain the DIRECTORY file concept, but expand it to take advantage of the full DOS path support, which is supported by the compiler and linker. This extension should also enable simplification of both file naming/moving rules and the ATBMS directory structure.

Since some simulations may require considerable processing time, when a large number of segments and joints are simulated for a long interval, a display of the simulation progress would be useful. The in-progress display might show the present time interval, the segment or joint number, indicators of integration convergence history, percent completed, as well as lower and upper bounds of the time required to complete execution.

An enhancement area which bridges both UII and PU is the interactive construction and testing of simulation input files. This capability, which is partially implemented by the GEBOD program, should reduce the time and effort required to prepare and test ATB inputs. The significant features of such an interactive program would naturally include accurate file construction in terms of data field and record placement, but more importantly would test data in terms of units of measure selected, perform conversions, and display options in menu

format in English and translate the responses into appropriate switch/flag settings. Upon completion the program would test the resulting file for completeness to ensure that all data related to explicitly or implicitly selected options were present. Discrepancies would be flagged, with an opportunity to correct faults on-line, until a satisfactory input file was ready for simulation.

The two significant performance upgrades recommended at this time include graphics capability enhancements and the development of a post-simulation analysis package. The graphics upgrade would take advantage of relatively recent hardware and software developments to provide the analyst with high quality graphs, plots, and pictures, optimized to control processing time.

Postsimulation data extraction, reduction, analysis, and display are necessary in view of the large quantity of data produced by a single simulation, and by the need to correlate and compare -- statistically and graphically -- the results of several simulations, or simulation and test results. Such data handling software's principal features include the ability to review large quantities of data rapidly, select data from various (similar or dissimilar) sources for comparison, with a choice of filters and display formats selected interactively by the user. References [7, 8] document data analysis packages with such functional characteristics. These are presently used on CDC Cyber and HP computers respectively.

### 3. DISCUSSION

#### 3.1 INTRODUCTION

This section of the report summarizes the technical issues relevant to the adaptation of the ATBMS to the microcomputer environment. Specific topics discussed include the design criteria, hardware configuration, operating systems, support software, and changes to the application software.

It should be noted that in the era of rapidly evolving microcomputer hardware and software, as well as peripherals (displays, bulk storage devices, hard copy devices), subjective judgements were made -- and revised -- which "date" this report as it is being written. Nevertheless, the *method* used in development will stand the test of time, while the specific recommendations may change with time.

#### 3.2 DESIGN CRITERIA

##### 3.2.1 Hardware

In view of the overall objective -- to make the ATBMS readily available to investigators having limited resources -- it was a design criterion to select a hardware configuration that would provide acceptable ATBMS performance at reasonable cost, using standard, commonly and readily available hardware components. Hardware selection was further oriented toward systems whose continued support could reasonably be expected.

##### 3.2.2 Operating System

An efficient, well known, commonly used operating system is desired that interacts with readily available support software, at an acceptable cost.

##### 3.2.3 Operating/developmental Environment

It was a design criterion that the combination of hardware, operating system, support software, and application software should jointly constitute an environment appropriate to investigators in biodynamics, rather than microcomputer specialists.

#### 3.2.4 Performance Times

In view of the computational intensity of the ATBMS, and particularly of the ATB simulation itself, an execution time not exceeding twice that of the Perkin-Elmer was desired.

### 3.3 HARDWARE CONFIGURATION

#### 3.3.1 Selection Criteria

##### 3.3.1.1 Processor, Memory, Clock

At the commencement of this project there were five classes of candidate microprocessor based systems potentially suited to the ATBMS application. These were the Intel 8000 based systems (IBM personal computers and their clones), the Motorola 68000 based Apple and Macintosh lines, microcomputers made by the Digital Equipment Corporation and by Hewlett-Packard (both using proprietary processors), and the various makes of "workstations".

The DEC and HP systems are not particularly common in general applications. The workstations, while offering the highest performance in the group, were significantly more expensive than other equipment. The Motorola 68000 based systems are not as common as the Intel systems and offer a smaller choice of support software.

Thus, by the process of elimination early in the project, the principal focus was on the Intel 8000 based systems. They appeared to be the most suitable due to their widespread use, which stimulates the commercial software vendors to develop and enhance the necessary support products. In view of the broad market base, continued hardware and software support can be reasonably expected. The Intel family of microprocessors also offers a range of performance capabilities through a choice between the 8086, 80286, and 80386 devices that are available at various clock frequencies, with their respective mathematical coprocessors. In view of the computational load posed by the ATB simulation, the Intel 80386/80387 processors are most suited to this application.

The ATBMS memory requirements are dictated by the ATB simulation, which is its largest component. Either sufficient memory has to be available to keep the program and data in memory during the entire execution, or a software

overlay approach has to be adopted. The in-memory alternative is preferred in view of the large volume of disk I/O needed for the overlay approach. Even with the substantial data transfer rates of high capacity disks, the system performance would suffer if overlays were used. The ATB simulation requires 4 Mb memory. The recommended processor supports up to 16 Mb of memory, which satisfies the preferred memory alternative.

The Intel 80386 processor is available in 16, 20, 25, and 33 MHz variants. It is clear from data presented above that increasing the clock frequency can significantly contribute to reducing execution times.

#### 3.3.1.2 Display

While a very high resolution CAD type display is highly effective for viewing graphic output, a good quality EGA display is satisfactory for the ATB application.

#### 3.3.1.3 Disk drives

Since most of the processing in ATBMS is computationally intensive, with a relatively low level of input/output activity, disk access time is not particularly critical. To accommodate the large output files, however, a disk of at least 70 Mb is recommended. Disks of that size typically are made with 28 ms access time, or less. Larger capacity disks would be recommended for high intensity analysis activity, particularly if frequent disk backups need to be avoided.

As software distribution and data handling media, floppy disks are the most common. User convenience would be well served if both common formats (5.25" and 3.5") were available.

#### 3.3.1.4 Printer/plotter

The ATBMS can produce a large quantity of tabular output, as well as graphs. While a wide variety of printers and plotters are available, a single device -- a laser type printer -- can serve both as a high volume printer and a plotter. A printer operating at or above eight pages per minute is recommended.

### 3.3.2 Recommended Hardware

The hardware configuration recommended for ATBMS is summarized in Table 3-1.

---

Table 3-1. Recommended ATBMS Hardware Configuration

<u>Item</u>	<u>Description</u>
Processor	Intel 80386
Coprocessor	Intel 80387
Clock	33 MHz desirable
Memory quantity	4 Mb required
Cache memory	64 Kb
Memory speed	80 ns or less
Display	EGA or VGA
Disk drive capacity	70 Mb
Disk drive access	28 ms or less
Floppy disks	1.2 Mb, 5.25" 1.4 Mb, 3.5"
Printer/plotter	Laser Jet type 8 pages/minute, minimum

---

If computer-to-computer data transfer is desired, a modem (internal or external) can be added to the system. In view of the volume of data that is often generated by ATBMS, the analyst may find a tape-based backup system quite useful for archiving, particularly with a small hard disk and high analysis or developmental activity level.

### 3.4 OPERATING SYSTEM

#### 3.4.1 Selection Criteria

Two operating systems are readily available for Intel microprocessor based systems -- the Disk Operating System, DOS, and variants of Bell Laboratories' UNIX system.

UNIX on a microcomputer offers two attractive features. First, all installed memory in the computer is directly available to the executing application. Second, microcomputer UNIX is available in a multiuser configuration.

This second feature is not of significant utility for the ATBMS implementation. In view of the computational load imposed by the simulation it is unlikely that the computer would be employed in a multiuser mode.

Since UNIX is not nearly as widely used as DOS, the quantity of available developmental software is somewhat limited, and is markedly more expensive than DOS software. Microcomputer users generally feel that UNIX based systems require more expertise and experience than DOS systems. Other attributes of the UNIX system will be discussed in Section 3.5, in conjunction with support software.

DOS presents two disadvantages in comparison with UNIX -- in conventional operations available application memory is limited to 640 Kb (regardless of amount installed), and the number of simultaneously open files within an application is limited to 15. These disadvantages, however, are alleviated by commercially available software packages which overcome DOS's built-in limits. Significant advantages to DOS are that it is well supported by a broad spectrum of commercially developed tools, which are typically less expensive than their UNIX counterparts -- when those counterparts exist. Furthermore DOS is well known not only to software developers, but also to application oriented computer users.

#### 3.4.2 Recommended Operating System

Based on the above discussion, and observations presented in Section 3.5, DOS is the operating system of choice for the ATBMS implementation.

### 3.5 SUPPORT SOFTWARE

The term support software is used to cover compilers, linkers, graphics packages, and DOS memory extenders. These are all commercially available products necessary to complete the software portion of the hardware-software environment for ATBMS operation.

#### 3.5.1 Selection Criteria

The support software selection was undertaken with the requirement to provide an efficient developmental/operating environment for the ATBMS. The



term efficient includes well documented, easy to use software, without the need for "work arounds" to solve potentially intractable problems. The operating environment has to be suitable to the problem-solving oriented application program user, rather than the dedicated, expert software developer.

It was also desired to minimize application software revisions, and to avoid new application development in order to fit the ATBMS to an operating environment.

#### 3.5.1.1 The UNIX environment

When using a UNIX family operating system, reference [1], we found that UNIX based compiler/linker would not accept standard FORTRAN labelled COMMON specifications unless they were of identical length in each subroutine and function throughout the entire program. (Most compilers and linkers will process code -- with a warning -- as long as the longest COMMON is declared on its first occurrence. Shorter subsequent declarations are accepted without error.) This problem can be eliminated by suitably padding each COMMON declaration.

The second challenge posed by the UNIX operating system was the unavailability of a graphics support package capable of handling the CalComp graphics calls. CalComp (California Computer Products) is an old, well established X-Y plotter, which was available to the scientific applications community through FORTRAN CALL statements, which were supported by a dedicated load-time library. Their use became sufficiently widespread that "after-market" support libraries have been written for several devices, such as the TEKTRONIX terminals, and more recently for microcomputers. Such a library was not available for a microcomputer operating under UNIX.

Thus the available choices were either to modify the ATBMS to run under UNIX outputting data to a file, which would be post-processed under UNIX or DOS. The UNIX option would have dictated the development of special application programs to handle ATBMS graphics. The DOS option would also have required some custom software development, and the use of two operating systems to run the ATBMS, with some data moving between the UNIX and DOS file systems.

Based on the above, it is clear that using the UNIX operating system would have violated the established selection criteria.

#### 3.5.1.2 The DOS environment

ATBMS implementation under DOS requires the simultaneously successful operation of the operating system and three support software elements. These are the compiler, the plotting library, and the DOS memory extender. The memory extender can be viewed as a memory driver that facilitates access to up to 4 Gb of installed memory, not only the first 640 Kb.

One support software collection included the *Phar Lap 386|ASM/LINK* memory extender, the *NDP Plot* plotter library, and the *NDP FORTRAN-386* compiler. The memory extender performed satisfactorily, while the plotting library failed to support its own demonstration example as documented. The significant deficiencies in the compiler included incorrect handling of real constants and incorrect handling of reserved keywords. Labelled COMMON is not checked for length, issues no diagnostic warnings, but misaligns COMMONs during execution. This software collection was deemed unacceptable for the ATBMS implementation. The software which satisfactorily supported the conversion effort is identified below.

#### 3.5.2 Recommended Support Software

The *Lahey* compiler-linker, with the *AI Architects'* DOS extender, and *Plotworks* library, reference [2], were found to provide the necessary ATBMS implementation environment.

The DOS limitation on the number of simultaneously open files is eliminated by the *Lahey DOS Interface Library*, reference [3].

## 4. ATBMS IMPLEMENTATION

### 4.1 INTRODUCTION

This section provides the details of the ATBMS implementation in terms of support software organization requirements, compilation and linking procedures, and specific program modifications. The procedures for executing the individual programs are given. Examples of outputs and modified source code listings are provided in appendices.

It is assumed that the reader of this section is proficient in using Intel microprocessor based personal computers under the disk operating system.

### 4.2 SYSTEM CONFIGURATION

#### 4.2.1 Hardware Configuration

The hardware configuration specified in Table 3-1 is assumed.

#### 4.2.2 Support Software Configuration

The work presented in this report was carried out under MS-DOS versions 3.3 or 4.01.

The support software used -- compiler, plotting library, and DOS extender -- are identified in Section 5, reference [2].

#### 4.2.3 Hard Disk Organization

The disk organization presented in this section was used to compile, link, and execute the ATBMS programs. While this is not the only possible organization, it follows a set of conventions that was used throughout the project. The conventions may be changed, but need to be kept consistent.

##### 4.2.3.1 The boot directory

The boot drive root directory, C:\, contains the user's AUTOEXEC.BAT and CONFIG.SYS files. The PATH established in the AUTOEXEC.BAT file must contain at least the following elements:

PATH=C:\;C:\DOS;D:\;D:\F77L3;D:\OS386;D:\PLOT88;D:\ATBM

#### 4.2.3.2 The working drive

The root directory of the working drive, D:\, must contain the AI DOS extender configuration file, CONFIG.AIA.

#### 4.2.3.3 The compiler directory

The Lahey FORTRAN-77 compiler is installed to directory D:\F77L3.

#### 4.2.3.4 The DOS extender directory

The DOS extender directory, D:\OS386, contains the files installed for A.I. Architects' OS/386. The DOS extender is a subset of the A.I. Developers Kit OS/386, and it may be packaged with the Lahey compiler. The complete Developers Kit is not required.

#### 4.2.3.5 The graphics directory

The plotting library is placed in directory D:\PLOT88.

#### 4.2.3.6 The working directory

The working directory employs the following naming conventions:

- .BAT are batch files, used for compilation and linking
- .FTN are FORTRAN source files
- .EXP are executable files generated by the compiler
- .DIR are directory files used for file handling by GEBOD, ATB, and VIEW discussed in Section 4.2.5

Also included in the working directory are:

- input files required for execution by GEBOD, ATB, and VIEW, specified in the corresponding .DIR file
- output files generated during program execution
- RPCSLAVE.EXE supplied with PLOT88, required for execution.

The object code, map, and listing files may be deleted or kept, at the discretion of the user.

#### 4.2.4 Compiling and Linking FORTRAN

The executable program, .EXP, is generated from the source code by

the compiler and linker programs. Two batch files have been prepared, their use depending on the presence or absence of graphics calls in the source code. In either case, compilation listings are generated with the same name as the source code file, using a .C extension. Following successful compilation, the batch files proceed by linking object modules, using the graphics libraries, as appropriate.

The GEBOD program, which does not utilize graphics, is compiled and linked by CL.BAT:

```
F77L3 %1.FTN %2 /7/nS > %1.C
UP L32 %1
```

The compilation/linking is invoked as:

```
CL GEBODII
```

The ATB and VIEW programs, both utilizing graphics, are compiled by CLL.BAT:

```
F77L3 %1.FTN %2 /7/nS > %1.C
UP L32 %1,,,\PLOT88\PLOT88+\PLOT88\DRIVE88+\F77L3\F77L3
```

The compilation/linking is invoked as:

```
CLL ATBIV or CLL VIEWPE
```

Additional compiler options, such as debug, cross reference listings, etc. may be added as a second element (without embedded blanks) following the program name for either batch file.

The ATB program source code, due to its large size, is usually transferred on floppy disks as four files. This also facilitates code modifications, since most conventional text editors will not process very large text files. The compilation and linking procedure (CLL.BAT) is, however, for a single source file. The user has the option of either developing multiple file compilation and linking procedures, or combining the four ATB source code files prior to compilation with the ACOPY.BAT procedure:

```
COPY ATBIV.FT1+ATBIV.FT2+ATBIV.FT3+ATBIV.FT4 ATBIV.FTN
```

Similarly, the large data file which is input to GEBOD, is stored in two segments on floppy disks. The segments are combined by the GCOPY.BAT procedure:

COPY GEBOD.DT1+GEBOD.DT2 GEBOD.DAT

#### 4.2.5 ATBMS DIRECTORY Files

The purpose of the DIRECTORY files in the 386-ATBMS implementation is to identify the input files, provide names for the output files, and initialize hardware devices -- displays, printers, and plotters. The alternative of having fixed file names and hardware devices embedded in the FORTRAN source code would have been unacceptably inflexible.

The file name records in the directory file follow the format:

- field 1: characters 1-12, left justified, valid DOS filename, required
- field 2: characters 15-21, FORTRAN logical unit designator, optional, recommended
- field 3: characters 25-80, file use description or comments, optional, recommended

The device initialization records in the directory file follow the following format:

- field 1: characters 1-4, right justified, numeric, PLOT88 PLOTS parameter value, required for device parameter initialization
- field 2: characters 7-12, alphanumeric, PLOTS parameter name, optional, recommended
- field 3: characters 15-21, alphanumeric, FORTRAN logical unit designator (when used), optional, recommended
- field 4: characters 25-80, alphanumeric, comments, optional, recommended

The following are the general rules for all DIRECTORY files:

- (1) The names of the DIRECTORY files may not be changed, they are GEBODII.DIR, ATBIV.DIR, and VIEWPE.DIR, respectively.
- (2) The SEQUENCE of records in the DIRECTORY files is critical.  
Records MUST NOT be deleted! Records MUST NOT be interchanged!
- (3) All output files are conservatively opened with STATUS=NEW.  
This prevents these files from being overwritten. To obtain a second or subsequent execution, the analyst has the following options, one of which MUST be exercised:

- (a) delete the output files,
- (b) rename the output files,
- (c) move the output files to a different DOS directory,
- (d) copy the output files to a different DOS directory, then delete the originals, or
- (e) edit the DIRECTORY file, assigning new names to the output files.

The DIRECTORY files specific to each program are described in Section 4.3.

#### 4.2.6 Executing Programs

An executable file (.EXP) is produced by the compilation and link steps for each ATBMS program. Each program has its corresponding DIRECTORY (.DIR) file which identifies input/output file names and hardware device parameters. The .DIR file is prepared or modified by using any ASCII text editor. With the executable (.EXP), directory (.DIR), and input files in the current working directory, the programs are executed by the command

UP GEBODII, UP ATBIV, or UP VIEWPE

### 4.3 PROGRAM IMPLEMENTATION

The specific changes incorporated into each program, their DIRECTORY files, and sample outputs for each are described in the balance of this section. All source code modifications are identified by the string 80386 starting in character position 73.

#### 4.3.1 The GEBOD Program

The modified GEBOD program (reference [4]) source code is provided in Appendix H.

##### 4.3.1.1 Source code modifications

The following source code changes were made for the 386-GEBOD implementation.

- (1) Changes to COMMONs, to achieve equal length across all subprograms
  - (a) /DIMS/ in MAIN, CONTAC, SEGMAS, TORSO, FEET, RESULTS, CNVERT

- (b) /FLOAT/ in MAIN, CONTAC, SGINER, TORSO, FEET
- (c) /NAMES/ in BLOCK DATA, PFILE, RESULTS, RESULTZ
- (d) /JNTS/ in CONTAC, SEGMA, CNVRT
- (e) /SGMNTS/ in SGINER

(2) Accessed the directory file GEBODII.DIR and opened the appropriate files in MAIN and DIALOG.

(3) Reduced real constant exponent from E+74 to E+38 in subprogram NDTRI.

(4) Modified EXTERNAL calls to ELLIP in subprogram SEGMA,

(5) Modified EXTERNAL calls to ELLPMI in subprogram SGINER, and

(6) Modified ABEVAL calls in subprograms ELLIP and ELLPMI. Changes 4 through 6 were necessary since the present version of the compiler does not support the EXTERNAL statement.

(7) Removed case sensitivity from user responses in subprograms DIALOG, RESULTS, and RESULTZ.

#### 4.3.1.2 The GEBODII.DIR file

The general rules discussed in Section 4.2.5 apply to GEBODII.DIR.

A sample if this directory file is shown below.

##### GEBODII.DIR

GEBOD.DAT	UNIT 2	GEBOD INPUT
GEBOD.AIN	UNIT 3	GEBOD BODY DESCRIPTION OUTPUT, INPUT TO ATB
GEBOD.TAB	UNIT 9	GEBOD BODY DESCRIPTION TABULAR OUTPUT
GEBODIN.USR	UNIT 1	USER-SUPPLIED GEBOD INPUT, 4(8F10.3) RECORDS

##### Comments:

(a) The body description tabular output file (unit 9) contains carriage control characters and may be printed directly.

(b) The user supplied input file (unit 1) is opened only if the appropriate option is selected during program execution. If this file is not used, then the corresponding field may be left blank, but the record must be present.

#### 4.3.1.3 Sample outputs

The GEBOD program outputs, which is the body description in tabular form (GEBOD.TAB) and in ATB input form (GEBOD.AIN), are shown in Appendices A and B, respectively.



#### 4.3.2 The ATB Program

The modified ATB program (reference [5]) source code is provided in Appendix I.

##### 4.3.2.1 Source code modifications

The following source code changes were made for the 386-ATB implementation.

- (1) Changes to COMMONs, to achieve equal length across all subprograms

- (a) /CDINT/ in BLOCK DATA, ADJUST, CMPUTE, DINT, HICCSI, POSTPR, RSTART, TRIGFS.

- (b) /TEMPVS/ in

BLOCK DATA,	AIRBAG,	AIRBGG,	AIRBG1,	AIRBG3,
BELTG,	BELTRT,	BGG,	BINPUT,	BLKDTA,
CHAIN,	CINPUT,	DAUX,	DAUX11,	DAUX12,
DAUX22,	DAUX31,	DAUX32,	DAUX33,	DAUX44,
DAUX55,	DRIFT,	EJOINT,	EQUILB,	FDINIT,
FINPUT,	FLXSEG,	HBELT,	HBPLAY,	HEDING,
HINPUT,	HPTURB,	HSETC,	HYEST,	HYLPX,
HYNTR,	IMPLS2,	INITAL,	KINPUT,	OUTPUT,
PDAUX,	PLEDG,	PLELP,	PLSEGF,	PLTXYZ,
POSTPR,	PRINT,	PRIPLT,	ROTATE,	SEGSEG,
SETUP1,	SETUP2,	SINPUT,	SPDAMP,	UNIT1,
VINPUT,	VISPR,	WINDY,		

- (c) /TITLES/ in KINPUT.

- (d) /CNSNTS/ in POSTPR.

- (2) Accessed the directory file ATBIV.DIR and opened the appropriate files in MAIN.

- (3) Removed Perkin-Elmer CARCON command in subprograms MAIN, HEDING, and OUTPUT.

- (4) Modified system clock calls in subprogram ELTIME.

- (5) Modified PLOTS call in subprogram POSTPR, and

- (6) In subprogram SLPLOT modified the declaration of COMMON /TEMPVS/ variables passed as arguments from subprogram POSTPR. Changes 5 and 6 were necessary for compatibility with the PLOT88 package.

- (7) Modified SYMBOL call in subprogram SLPLOT.

#### 4.3.2.2 The ATBIV.DIR file

The general rules discussed in Section 4.2.5 apply to GEBODII.DIR.

A sample of this directory file is shown below.

##### ATBIV.DIR

ATB.TP1	UNIT 1	ATB OUTPUT, VIEW BODY ELEMENT AND CONTACT PLANE INPUT
ATB.PRP	UNIT 2	ATB PRINTER PLOTS
ATB.ROU	UNIT 3	ATB RESTART RUN OUTPUT FILE
ATB.RIN	UNIT 4	ATB RESTART RUN INPUT FILE
ATB.AIN	UNIT 5	ATB INPUT, GEBOD BODY DESCRIPTION OUTPUT
ATB.AOU	UNIT 6	ATB PRIMARY OUTPUT FILE
ATB.TP8	UNIT 8	ATB SUBROUTINE POSTPR OUTPUT FILE
0 IDEF	UNIT 10	DRAWING OPTION SEE PLOT88, 3.1
91 IOPORT	UNIT 10	HARDWARE INTERFACE 91/ 1 SEE PLOT88, 3.1
91 MODEL	UNIT 10	OUTPUT DEVICE 91/64 SEE PLOT88, 3.1
ATB.T24	21 - 85	LAST ATB TABULAR TIME HISTORY OUTPUT FILE (21-85)

##### Comments:

(a) The ATB printer plots, primary output file, and tabular time history files (units 2, 6, and 21-85) contain carriage control characters and may be printed directly.

(b) Optional files are not OPENed during execution unless the corresponding features have been selected in the input file. When optional files are not used, their name fields in the .DIR file may be left blank. However, the record position in the file must be retained! The following files are optional during ATB execution:

<u>UNIT</u>	<u>APPLICATION</u>
1	VIEW input
2	printer plots
3	RESTART run output
4	RESTART run input
8	POSTPR output
10	X-Y plots
21-85	tabular time history output

(c) When tabular time history output files (units 21-85) are selected, the last ATB directory entry must contain a valid DOS file name, with a three character extension. The second and third characters of the extension are used to specify the last logical output unit (21-85) used for tabular time history data. As an example, if tabular time history data are to be output on logical units 21 through 46, then the last entry should read ccccccc.c46, where

"c" represents any legal DOS file name character.

#### 4.3.2.3 Sample outputs

Two sample cases, provided by AAMRL/BBM were used to test the 386-ATB implementation, and to develop the performance statistics presented in Table 2-1. Appendix C presents the inputs and outputs for the Basic Sled Test Simulation, with C1 and C2 listing the input and directory files, and Appendix C3 showing the 386 output. To facilitate comparison between the 386-ATB results and those obtained on the Perkin-Elmer, Appendix C4, showing the Perkin-Elmer results is provided. Similar appendices (D1-D4) are used for presenting example 2, the Dynamic Joint Test.

The input file for example 2 was modified to demonstrate both the X-Y plot and the printer plot capability of the 386-ATB. Appendix E1 shows the modified input file, while samples of the resulting plots are in appendices E2 and E3, respectively. The output is identical to the one shown in Appendix D3, with an increase in execution time to 43 seconds, due to the plotting options.

#### 4.3.3 The VIEW Program

The modified VIEW program (reference [6]) source code is provided in Appendix J.

##### 4.3.3.1 Source code modifications

The following source code changes were made for the 386-VIEW implementation.

- (1) Changes to COMMONs, to achieve equal length across all subprograms
  - (a) /PLTT/ in EXTEND, PLPLN, PNTPLT.
  - (b) /DEBUG/ in INPUT.
- (2) Modified hexadecimal constant assignments in subprogram NFRAME.
- (3) Accessed the directory file VIEWPE.DIR and opened the appropriate files in MAIN.
- (4) Moved code blocks following the statement numbers 200 and 400 within the DO-100 loop in subprogram PNTPLT to avoid external transfer into the DO-loop range.
- (5) Changed NEWPEN calls to COLOR calls in subprograms MAIN, PLPLN, and

TITLE for compatibility with the PLOT88 package.

(6) Modified the MAIN program to ignore device flag, DEVFLG, specified on record 1 of the control data input file. The device flag is now set to 4, for a multicolor graphics terminal.

(7) Added a scale factor in the MAIN program to allow display of the 20-character title on the graphics screen.

(8) Modified calls to SYMBOL and NUMBER in program MAIN to display frame titles on the graphics screen.

(9) Inserted a test on variable TEMP in subprogram ELIPSN. This test is needed due to differences in precision between computers.

(10) Replaced PLOTS call with PLOT call in subprogram NFRAME for compatibility with the PLOT88 package.

#### 4.3.3.2 The VIEWPE.DIR file

The general rules discussed in Section 4.2.5 apply to VIEWPE.DIR. The output listing file (unit 6) contains carriage control characters and may be directly printed. A sample of this directory file is shown below.

##### VIEWPE.DIR

VIEW.TP1	UNIT 1	VIEW BODY ELEMENT AND CONTACT PLANE INPUT, ATB OUTPUT	
VIEW.VIN	UNIT 5	VIEW CONTROL DATA INPUT	
VIEW.VOU	UNIT 6	VIEW LISTING OUTPUT	
0 IDEF		DRAWING OPTION	SEE PLOT88, 3.1
91 IOPORT		HARDWARE INTERFACE 91/ 1	SEE PLOT88, 3.1
91 MODEL		OUTPUT DEVICE 91/64	SEE PLOT88, 3.1

#### 4.3.3.3 Sample outputs

The two samples used for testing the 386-VIEW program implementation are ATB course examples 1 and 2. The input files, the output listings, and the resulting graphics are shown in Appendices F and G, respectively.

## 5. REFERENCES

1. Microport System V/386 Runtime System, Version 3.0e  
LPI-FORTRAN for Intel 80386 UNIX System V, Version 3.02
2. Lahey compiler-linker F77L-EM/32  
    Lahey Computer Systems, Inc., Incline Village, NV  
AI Architects' DOS extender OS/386  
    Lahey Computer Systems, Inc., Incline Village, NV  
Plotworks PLOT88 library  
    Plotworks Inc., Ramona, CA
3. Lahey Spindrift Utility Library (for F77L-EM/32)
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6. Leetch, B.D. and Bowman, W.L., *Articulated Total Body (ATB) "VIEW" Program Software Report, Parts I and II*, Technical Report AFAMRL-TR-81-111, WPAFB, OH, June 1983.
7. D'Aulerio, L.A., Frisch, G.D., and Fender, D.A., *Ejection Test Data Analysis Package (ETDAP) User's Guide*, Report No. NADC-84133-60, Warminster, PA, October 1984.
8. Hyslop, R.L., *Horizontal Accelerator Data Acquisition System Enhancements*, KETRON Technical Report 4658-25, Warminster, PA, March 1989.

## APPENDIX A

GEBOD Body Description Tabular Output (GEBOD.TAB)

01/10/90  
ADULT HUMAN MALE  
SELECTED BODY DIMENSIONS

COMPUTED BODY DIMENSIONS		WEIGHT	75.00	%-TILE
0	WEIGHT		188.0	LB.
1	STANDING HEIGHT		70.66	IN.
2	SHOULDER HEIGHT		58.01	IN.
3	ARMPIT HEIGHT		51.78	IN.
4	WAIST HEIGHT		42.44	IN.
5	SEATED HEIGHT		37.07	IN.
6	HEAD LENGTH		7.869	IN.
7	HEAD BREADTH		6.186	IN.
8	HEAD TO CHIN HEIGHT		9.011	IN.
9	NECK CIRCUMFERENCE		15.44	IN.
10	SHOULDER BREADTH		16.27	IN.
11	CHEST DEPTH		10.04	IN.
12	CHEST BREADTH		13.33	IN.
13	WAIST DEPTH		9.216	IN.
14	WAIST BREADTH		12.73	IN.
15	BUTTOCK DEPTH		9.879	IN.
16	HIP BREADTH, STANDING		14.29	IN.
17	SHOULDER TO ELBOW LENGTH		14.33	IN.
18	FOREARM-HAND LENGTH		19.68	IN.
19	BICEPS CIRCUMFERENCE		12.89	IN.
20	ELBOW CIRCUMFERENCE		12.57	IN.
21	FOREARM CIRCUMFERENCE		11.39	IN.
22	WRIST CIRCUMFERENCE		7.067	IN.
23	KNEE HEIGHT, SEATED		22.31	IN.
24	THIGH CIRCUMFERENCE		24.16	IN.
25	UPPER LEG CIRCUMFERENCE		15.69	IN.
26	KNEE CIRCUMFERENCE		15.95	IN.
27	CALF CIRCUMFERENCE		15.11	IN.
28	ANKLE CIRCUMFERENCE		9.054	IN.
29	ANKLE HEIGHT, OUTSIDE		5.462	IN.
30	FOOT BREADTH		3.904	IN.
31	FOOT LENGTH		10.79	IN.
WEIGHT CORRECTION FACTOR =		1.099		

01/10/90  
CRASH VICTIM PARAMETERS (3-D)

SEGMENT NO. SYM PLOT	WEIGHT (LB. )	SEGMENT MOMENT OF INERTIA (LB-SEC**2-IN)			SEGMENT CONTACT ELLIPSOID SEMIAXIS (IN)			CENTER (IN)		
		X	Y	Z	X	Y	Z	X	Y	Z
1 LT 1	31.18	1.34822	0.83419	1.47922	4.94	7.14	3.65	0.00	0.00	-0.07
2 CT 2	11.63	0.33664	0.18749	0.47497	4.61	6.36	4.01	0.00	0.00	-0.01
3 UT 3	48.11	2.84603	2.29042	1.94681	5.02	6.66	7.01	0.00	0.00	-0.83
4 N 4	3.06	0.02435	0.07435	0.01918	2.46	2.46	3.05	0.00	0.00	0.00
5 H 5	11.61	0.25522	0.79078	0.15060	3.93	3.09	5.73	0.00	0.00	0.00
6 RUL 6	20.12	1.61197	1.61197	0.20966	3.17	3.17	12.03	0.00	0.00	0.00
7 RLL 7	8.80	0.40723	0.070723	0.05271	2.41	2.41	9.14	0.00	0.00	0.00
8 RF 8	1.89	0.03583	0.03461	0.00470	2.73	1.95	5.40	0.00	0.00	1.40
9 LUL 9	20.12	1.61197	1.61197	0.20966	3.17	3.17	12.03	0.00	0.00	0.00
10 LLL A	8.80	0.40723	0.40723	0.05271	2.41	2.41	9.14	0.00	0.00	0.00
11 LF B	1.89	0.03583	0.03461	0.00470	2.73	1.95	5.40	0.00	0.00	1.40
12 RUA C	5.01	0.14425	0.14425	0.02185	2.05	2.05	7.17	0.00	0.00	0.00
13 RLA D	5.38	0.27886	0.27886	0.01830	1.81	1.81	9.84	0.00	0.00	0.00
14 LUA E	5.01	0.14425	0.14425	0.02185	2.05	2.05	7.17	0.00	0.00	0.00
15 LLA F	5.38	0.27886	0.27886	0.01830	1.81	1.81	9.84	0.00	0.00	0.00

JOINT J SYM PLOT JNT PIN	LOCATION(IN) - SEG(JNT)			LOCATION(IN) - SEG(J+1)			PRIN. AXIS(DEG) - SEG(JNT)			PRIN. AXIS(DEG) - SEG(J+1)		
	X	Y	Z	X	Y	Z	YAW	PITCH	ROLL	YAW	PITCH	ROLL
1 P M 1 0	0.00	0.00	-3.72	0.00	0.00	1.55	0.00	0.00	0.00	0.00	0.00	0.00
2 W N 2 0	0.00	0.00	-1.57	0.00	0.00	6.18	0.00	0.00	0.00	0.00	0.00	0.00
3 WP O 3 0	0.00	0.00	-7.83	0.00	0.00	0.59	0.00	0.00	0.00	0.00	20.00	0.00
4 HP P 4 0	0.00	0.00	-0.59	0.00	0.00	5.73	0.00	0.00	0.00	0.00	0.00	0.00
5 RH Q 1 0	0.00	3.30	-0.27	0.00	0.00	-8.18	0.00	0.00	0.00	8.10	-44.40	14.50
6 RK R 6 1	0.00	0.00	9.49	0.00	0.00	-6.60	0.00	0.00	0.00	0.00	65.60	-3.30
7 RA S 7 0	0.00	0.00	7.70	2.73	0.00	-2.55	0.00	0.00	0.00	-8.10	-80.00	0.00
8 LH T 1 0	0.00	-3.30	-0.27	0.00	0.00	-8.18	0.00	0.00	0.00	-8.10	-44.40	-14.50
9 LK U 9 1	0.00	0.00	9.49	0.00	0.00	-6.60	0.00	0.00	0.00	0.00	65.60	3.30
10 LA V 10 0	0.00	0.00	7.70	2.73	0.00	-2.55	0.00	0.00	0.00	8.10	-80.00	0.00
11 RS W 3 0	0.00	6.08	-5.00	0.00	0.00	-5.11	0.00	0.00	0.00	28.80	-39.60	63.30
12 RE X 12 1	0.00	0.00	5.16	0.00	0.00	-7.84	0.00	0.00	0.00	80.00	-70.00	0.00
13 LS Y 3 0	0.00	-6.08	-5.00	0.00	0.00	-5.11	0.00	0.00	0.00	-28.80	-39.60	-63.30
14 LE Z 14 1	0.00	0.00	5.16	0.00	0.00	-7.84	0.00	0.00	0.00	-80.00	-70.00	0.00

JOINTS RA, LA, RE, & LE ARE ORDERED PITCH, YAW, ROLL



APPENDIX B

GEBOD Body Description File Output (GEBOD.AIN)

15	14	01/10/90											CARD 8.1
LT	1	31.181.34820.83421.4792	4.940	7.144	3.645	0.000	0.000	0.000	0.000	0.000	0.000	CARD 8.2	
CT	2	11.630.33660.18750.4750	4.608	6.363	4.015	0.000	0.000	0.000	0.000	0.000	0.010	CARD 8.2	
UT	3	48.112.84602.29041.9468	5.020	6.663	7.006	0.000	0.000	0.000	0.000	0.000	0.826	CARD 8.2	
N	4	3.060.02430.02430.0192	2.458	3.458	3.049	0.000	0.000	0.000	0.000	0.000	0.000	CARD 8.2	
H	5	11.610.25520.29080.1506	3.935	3.093	5.734	0.000	0.000	0.000	0.000	0.000	0.000	CARD 8.2	
RU	6	20.121.61201.61200.2097	3.172	3.172	3.172	0.000	0.000	0.000	0.000	0.000	0.000	CARD 8.2	
RL	7	8.800.40720.40720.0527	2.405	2.405	9.143	0.000	0.000	0.000	0.000	0.000	0.000	CARD 8.2	
RF	8	1.890.03580.03460.0047	2.731	1.952	5.395	0.000	0.000	0.000	0.000	0.000	1.401	CARD 8.2	
LU	9	20.121.61201.61200.2097	3.172	3.172	3.172	0.000	0.000	0.000	0.000	0.000	0.000	CARD 8.2	
LL	A	8.800.40720.40720.0527	2.405	2.405	9.143	0.000	0.000	0.000	0.000	0.000	0.000	CARD 8.2	
LF	B	1.890.03580.03460.0047	2.731	1.952	5.395	0.000	0.000	0.000	0.000	0.000	1.401	CARD 8.2	
RU	C	5.010.14420.14420.0218	2.051	2.051	7.166	0.000	0.000	0.000	0.000	0.000	0.000	CARD 8.2	
LA	D	5.380.27890.27890.0183	1.813	1.813	9.841	0.000	0.000	0.000	0.000	0.000	0.000	CARD 8.2	
LU	E	5.010.14420.14420.0218	2.051	2.051	7.166	0.000	0.000	0.000	0.000	0.000	0.000	CARD 8.2	
LL	F	5.380.27890.27890.0183	1.813	1.813	9.841	0.000	0.000	0.000	0.000	0.000	0.000	CARD 8.2	
P	H	1 0 0.00 0.00 -3.72	0.00	0.00	1.55							CARD 8.3	
		0.00 0.00 0.00 0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0 0 0	
W	N	2 0 0.00 0.00 -1.57	0.00	0.00	6.18							CARD 8.3	
		0.00 0.00 0.00 0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0 0 0	
NP	O	3 0 0.00 0.00 -7.83	0.00	0.00	0.59							CARD 8.3	
		0.00 0.00 0.00 0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0 0 0	
HP	P	4 0 0.00 0.00 -0.59	0.00	0.00	5.73							CARD 8.3	
		0.00 0.00 0.00 0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0 0 0	
RH	Q	1 0 0.00 3.30 -0.27	0.00	0.00	-8.18							CARD 8.3	
		0.00 0.00 0.00 0.00 0.00	0.00	0.00	8.10	-44.40	14.50					0 0 0	
RK	R	6 1 0.00 0.00 9.49	0.00	0.00	-6.60							CARD 8.3	
		0.00 0.00 0.00 0.00 0.00	0.00	0.00	65.60	-3.30						0 0 0	
RA	S	7 0 0.00 0.00 7.70	2.73	0.00	-2.55							CARD 8.3	
		0.00 0.00 0.00 0.00 0.00	0.00	0.00	-8.10	-80.00	0.00					2 3 1	
LH	T	1 0 0.00 -3.30 -0.27	0.00	0.00	-8.18							CARD 8.3	
		0.00 0.00 0.00 0.00 0.00	0.00	0.00	-8.10	-44.40	14.50					0 0 0	
LK	U	9 1 0.00 0.00 9.49	0.00	0.00	-6.60							CARD 8.3	
		0.00 0.00 0.00 0.00 0											

## APPENDIX C1

Example 1, ATB Basic Sled Test Simulation  
Input File (EX1.AIN)



0.1	0.0	30.0	0.0	0.0				0.0	0.0		CARD B5
0.1	0.0	30.0	0.0	0.0				0.0	0.0		CARD B5
0.1	0.0	30.0	0.0	0.0				0.0	0.0		CARD B5
0.1	0.0	30.0	0.0	0.0				0.0	0.0		CARD B5
0.1	0.0	30.0	0.0	0.0				0.0	0.0		CARD B5
0.1	0.0	30.0	0.0	0.0				0.0	0.0		CARD B5
0.1	0.0	30.0	0.0	0.0				0.0	0.0		CARD B5
0.1	0.0	30.0	0.0	0.0				0.0	0.0		CARD B5
0.1	0.0	30.0	0.0	0.0				0.0	0.0		CARD B5
0.1	0.0	30.0	0.0	0.0				0.0	0.0		CARD B5
0.1	0.0	30.0	0.0	0.0				0.0	0.0		CARD B5
0.1	0.0	30.0	0.0	0.0				0.0	0.0		CARD B5
.01	.01	.01	.01	.01	.01	.10	.10	.10	.10	.10	.01CARD B6
.01	.01	.01	.00	.00	.00	.10	.10	.10	.00	.00	.00CARD B6
.01	.01	.01	.00	.00	.00	.10	.10	.10	.00	.00	.00CARD B6
.01	.01	.01	.00	.00	.00	.10	.10	.10	.00	.00	.00CARD B6
.01	.01	.01	.00	.00	.00	.10	.10	.10	.00	.00	.00CARD B6
.01	.01	.01	.00	.00	.00	.10	.10	.10	.00	.00	.00CARD B6
.01	.01	.01	.00	.00	.00	.10	.10	.10	.00	.00	.00CARD B6
.01	.01	.01	.00	.00	.00	.10	.10	.10	.00	.00	.00CARD B6
.01	.01	.01	.00	.00	.00	.10	.10	.10	.00	.00	.00CARD B6
.01	.01	.01	.00	.00	.00	.10	.10	.10	.00	.00	.00CARD B6
.01	.01	.01	.00	.00	.00	.10	.10	.10	.00	.00	.00CARD B6
.01	.01	.01	.00	.00	.00	.10	.10	.10	.00	.00	.00CARD B6
.01	.01	.01	.00	.00	.00	.10	.10	.10	.00	.00	.00CARD B6
.01	.01	.01	.00	.00	.00	.10	.10	.10	.00	.00	.00CARD B6
.01	.01	.01	.00	.00	.00	.10	.10	.10	.00	.00	.00CARD B6
.01	.01	.01	.00	.00	.00	.10	.10	.10	.00	.00	.00CARD B6
.01	.01	.01	.00	.00	.00	.10	.10	.10	.00	.00	.00CARD B6
SLED ACCELERATION - 20G PEAK											
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	15	0.0	0.010	0CARD G2A
0.0	5.0	10.0	15.0	20.0	15.0	10.0	5.0	0.0	0.0	0.0	0.0CARD C3
0.0	0.0	0.0									CARD C3
12	0	0	3	0	0	1	0	0	0		CARD D1
1	SEAT. 6 DEGREE OFF HORIZONTAL.										CARD D2A
	10.0		8.0		-10.0						CARD D2B
	28.01		8.0		-11.89						CARD D2C
	10.0		-8.0		-10.0						CARD D2D
2	BACK PANEL. 13 DEGREE OFF VERTICAL.										CARD D2A
	1.0		9.0		-48.97						CARD D2B
	10.0		9.0		-10.0						CARD D2C
	1.0		-9.0		-48.97						CARD D2D
3	FLOOR.										CARD D2A
	0.0		12.0		-1.3						CARD D2B
	60.0		12.0		-1.3						CARD D2C
	0.0		-12.0		-1.3						CARD D2D
4	HEAD PAD. 13 DEGR										CARD D2A
	2.48		7.5		-47.26						CARD D2B
	4.96		7.5		-36.55						CARD D2C
	2.48		-7.5		-47.26						CARD D2D
5	SEAT FRONT PANEL.										CARD D2A
	28.01		8.0		-11.89						CARD D2B
	26.65		8.0		-4.40						CARD D2C
	28.01		-8.0		-11.89						CARD D2D
6	BACK PANEL2. 13 DEGREE OFF VERTICAL.										CARD D2A
	1.0		9.0		-48.97						CARD D2B
	10.0		9.0		-10.0						CARD D2C
	1.0		-9.0		-48.97						CARD D2D
7	FIREWALL.										CARD D2A
	60.0		12.0		-25.0						CARD D2B
	60.0		-12.0		-25.0						CARD D2C
	60.0		12.0		-0.75						CARD D2D
8	RIGHT SIDE SEAT/IN.										CARD D2A
	8.41		8.1		-6.66						CARD D2B
	8.70		8.1		-14.73						CARD D2C
	30.58		8.1		-6.64						CARD D2D
9	LEFT SIDE SEAT/IN.										CARD D2A
	8.41		-8.1		-6.66						CARD D2B

	30.58	-8.1	-6.64	CARD D2C						
	8.70	-8.1	-14.73	CARD D2D						
10	RUDDER PEDALS.			CARD D2A						
	49.992	9.0	-2.239222	CARD D2B						
	52.992	9.0	-4.7565222	CARD D2C						
	49.992	-9.0	-2.239222	CARD D2D						
11	LEFT SIDE PANEL.			CARD D2A						
	1.0	-9.0	-48.97	CARD D2B						
	10.9	-9.0	-6.10	CARD D2C						
	-7.77	-9.0	-46.95	CARD D2D						
12	RIGHT SIDE PANEL.			CARD D2A						
	1.0	9.0	-48.97	CARD D2B						
	-7.77	9.0	-46.95	CARD D2C						
	10.9	9.0	-6.10	CARD D2D						
22	4.5	3.0	3.0	0.0	4.0	-3.5	0.0	0.0	0.0	CARD D5
23	3.2	6.0	8.0	0.0	0.0	-7.0	0.0	0.0	0.0	CARD D5
24	6.0	15.0	5.0	38.0	0.0	-28.0	0.0	0.0	0.0	20. 20. 20. CARD D5
0	0	0	0	0	0	0	0	0	0	CARD D7
3	SEGMENT-SEGMENT FCN.			CARD E1						
	0.0	-5.0	0.0	0.0	1.0	CARD E2				
6				CARD E4A						
	0.0	0.0	1.0	470.0	2.0	890.0	CARD E4B			
	3.0	1220.0	4.0	1470.0	5.0	1580.0	CARD E4B			
6	CONSTANT, F=0.0			CARD E1						
	0.0	0.0	0.0	0.0	0.0	CARD E2				
7	R FACTOR.			CARD E1						
	0.0	0.0	0.7	0.0	0.0	CARD E2				
13	STIFF SURFACES			CARD E1						
	0.0	-4.0	0.0	0.0	1.0	CARD E2				
8				CARD E4A						
	0.0	0.0	0.1	5.0	0.2	20.0	CARD E4B			
	0.3	40.0	0.4	60.0	1.0	860.0	CARD E4B			
	2.0	2400.0	3.0	4000.0	CARD E4B					
14	FRICTION FUNC.			CARD E1						
	0.0	0.0	0.5	0.0	1.0	CARD E2				
19	CF=.25,CREST=.25			CARD E1						
	0.0	0.0	0.25	0.0	0.0	CARD E2				
20	DAMPING COEFF. C=900			CARD E1						
	0.0	1.00	0.0	0.0	1.0	CARD E2				
	0.0	900.0	0.0	0.0	0.0	0.0	CARD E3			
21	RATE OF DEFLEC.			CARD E1						
	-40.0	-150.00	0.0	0.0	1.0	CARD E2				
21				CARD E4A						
	-40.0	0.000	-30.0	0.000	-20.0	0.000	CARD E4B			
	-10.0	0.000	0.0	0.000	5.0	1.000	CARD E4B			
	10.0	1.000	20.0	0.990	30.0	0.965	CARD E4B			
	40.0	0.928	50.0	0.860	60.0	0.690	CARD E4B			
	70.0	0.475	80.0	0.340	90.0	0.260	CARD E4B			
	100.0	0.200	110.0	0.180	120.0	0.090	CARD E4B			
	130.0	0.060	140.0	0.025	150.0	0.000	CARD E4B			
22	DAMPING COEFF. C=35			CARD E1						
	0.0	1.00	0.0	0.0	1.0	CARD E2				
	0.0	35.0	0.0	0.0	0.0	0.0	CARD E3			
24	DAMPING COEFF. C=0.8			CARD E1						
	-1000.0	-1000.0	0.0	0.0	1.0	CARD E2				
4				CARD E4A						
	-1000.0	0.6	-1.0	0.6	0.0	1.0	CARD E4B			
	1000.0	1.0	CARD E4B							
25	DAMPING COEFF C=1100			CARD E1						
	0.0	1.00	0.0	0.0	1.0	CARD E2				
	0.0	1100.0	0.0	0.0	0.0	0.0	CARD E3			
26	STIFF SURFACES-LL			CARD E1						
	0.0	-4.0	0.0	0.0	1.0	CARD E2				
8				CARD E4A						
	0.0	0.0	0.1	5.0	0.2	20.0	CARD E4B			
	0.3	40.0	0.4	60.0	2.0	860.0	CARD E4B			

[illegible]

1	23	0	1	0	0	0	0	0	0.00	-5.7	3.80	CRD F8D1				
1	1	0	1	0	0	0	0	32	0.01	-4.0	-4.50	CRD F8D2				
2	2	0	1	0	0	0	0	32	1.818	-5.439	-1.820	CRD F8D1				
2	2	0	1	0	0	0	0	32	2.50	-2.5	-1.50	CRD F8D2				
3	3	0	1	0	0	0	0	32	3.00	-1.5	6.50	CRD F8D1				
3	3	0	1	0	0	0	0	32	4.487	-0.133	3.734	CRD F8D2				
3	3	0	1	0	0	0	0	32	4.421	3.319	-1.662	CRD F8D1				
3	3	0	1	0	0	0	0	32	0.879	4.202	-5.672	CRD F8D2				
3	22	0	0	0	0	0	0	32	0.30	0.2	-2.80	CRD F8D1				
3	3	0	1	0	0	0	0	32	-1.00	4.3	-6.00	CRD F8D2				
3	3	0	1	0	0	0	0	32	-2.50	4.3	-4.00	CRD F8D1				
16	0	1	1	0	0	0	0	0	0.000	5.00	-35.200	CRD F8D2				
									0.7	17.5	-21.3	CRD F8D1				
	0.0		0.0		0.0	0	0	0	0			CARD G1A				
14.3810			0.0		-13.7500		0.0		0.0	0.0		CARD G2				
	0.0		12.90		0.0		0.0		0.0	0.0	3	2	1	O	CARD G3A	
	0.0		12.95		0.0		0.0		0.0	0.0	0.0	3	2	1	O	CARD G3A
	0.0		13.28		0.0		0.0		0.0	0.0	0.0	3	2	1	O	CARD G3A
	0.0		13.46		0.0		0.0		0.0	0.0	0.0	3	2	1	O	CARD G3A
	0.0		13.46		0.0		0.0		0.0	0.0	0.0	3	2	1	O	CARD G3A
	0.0		92.900		0.0		0.0		0.0	0.0	0.0	3	2	1	O	CARD G3A
	0.0		48.650		0.0		0.0		0.0	0.0	0.0	3	2	1	O	CARD G3A
	0.0		128.80		0.0		0.0		0.0	0.0	0.0	3	2	1	O	CARD G3A
	0.0		92.900		0.0		0.0		0.0	0.0	0.0	3	2	1	O	CARD G3A
	0.0		48.650		0.0		0.0		0.0	0.0	0.0	3	2	1	O	CARD G3A
	0.0		128.80		0.0		0.0		0.0	0.0	0.0	3	2	1	O	CARD G3A
	0.0		24.50		0.0		0.0		0.0	0.0	0.0	3	2	1	O	CARD G3A
	0.0		85.00		0.0		0.0		0.0	0.0	0.0	3	2	1	O	CARD G3A
	0.0		24.50		0.0		0.0		0.0	0.0	0.0	3	2	1	O	CARD G3A
	0.0		85.00		0.0		0.0		0.0	0.0	0.0	3	2	1	O	CARD G3A
3		3			0.0		0.0		0.0							CARD H1A
	1	-5			0.0		0.0		0.0							CARD H1B
	16	5			0.0		0.0		0.0							CARD H1B
3		3			0.0		0.0		0.0							CARD H2A
		5			0.0		0.0		0.0							CARD H2B
	3	5			0.0		0.0		0.0							CARD H2B
3		3			0.0		0.0		0.0							CARD H3A
		5			0.0		0.0		0.0							CARD H3B
	3	5			0.0		0.0		0.0							CARD H3B
3		3		5	16	5										CARD H4
3		3		5	5	5	</									



## APPENDIX C2

Example 1, ATB Basic Sled Test Simulation  
386 Directory File (ATBIV1.DIR)

EXP1.TP1	UNIT 1	ATB OUTPUT, VIEW BODY ELEMENT AND CONTACT PLANE INPUT
EXP1.PRP	UNIT 2	ATB PRINTER PLOTS
ATB.ROU	UNIT 3	ATB RESTART RUN OUTPUT FILE
ATB.3IN	UNIT 4	ATB RESTART RUN INPUT FILE
EX1.AIN	UNIT 5	ATB INPUT, GEBOO BODY DESCRIPTION OUTPUT
EXP1.AOU	UNIT 6	ATB PRIMARY OUTPUT FILE
EXP1.TP8	UNIT 8	ATB SUBROUTINE POSTPR OUTPUT FILE
0 IDEF	UNIT 10	DRAWING OPTION SEE PLOTWORKS, PLOT88, 3.1
91 IOPORT	UNIT 10	HARDWARE INTERFACE 91/ 1 SEE PLOTWORKS, PLOT88, 3.1
91 MODEL	UNIT 10	OUTPUT DEVICE 91/64 SEE PLOTWORKS, PLOT88, 3.1
EXP1.T24	21 - 85	LAST ATB TABULAR TIME HISTORY OUTPUT FILE (21-85)

### APPENDIX C3

Example 1, ATB Basic Sled Test Simulation  
386 Output File (EXP1.AOU)

DEVELOPED BY CALSPAN CORP., P.O. BOX 400, BUFFALO NY 14225  
AND BY J&J TECHNOLOGIES INC., ORCHARD PARK, NY 14127

FOR THE AIR FORCE ARMSTRONG AEROSPACE MEDICAL RESEARCH  
LABORATORY, WRIGHT PATTERSON AIR FORCE BASE  
UNDER CONTRACTS F33615-75C-5002,-78C-0516 AND -80C-0517

AND FOR THE NATIONAL HIGHWAY TRAFFIC SAFETY ADMINISTRATION,  
U.S. DEPARTMENT OF TRANSPORTATION, UNDER CONTRACTS  
FH-11-7592, HS-053-2-485, HS-6-01300 AND HS-6-01410.

PROGRAM DOCUMENTATION: NHTSA REPORT NOS. DOT-HS-801-507 THROUGH 510 (FORMERLY CALSPAN REPORT NO. ZG-5180-L-1), AVAILABLE FROM NTIS (ACCESSION NOS. PB-241692,3,4 AND 5), APPENDIXES A-J TO THE ABOVE (AVAILABLE FROM CALSPAN), AND REPORT NOS. AMRL-TR-75-14 (NTIS NO. AD-A014 816), AFAMRL-TR-80-14 (NTIS NO. AD-A088 029), AND AFAMRL-TR-83-073 (NTIS NO. AD-8079 184).

PROGRAM ATB-IV 80386 IMPLEMENTATION COMPLETED BY KETRON,  
OCTOBER 31, 1989, UNDER CONTRACT F33615-88-C-0543

2 SEPT 1988 IRSIN= 0 IRSOUT= 0 RSTIME = 0.0000

**CARDS A**

EXAMPLE 1: BASIC SLED TEST SIMULATION  
TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

[illegible]

CARD 8.1

CARDS 8.2

SEGMENT			WEIGHT ( LB.)	PRINCIPAL MOMENTS OF INERTIA ( LB.-SEC.**2- IN.)			SEGMENT CONTACT ELLIPSOID SEMIAXES ( IN.)			CENTER ( IN.)			PRINCIPAL AXES (DEG)		
I	SYM	PLOT		X	Y	Z	X	Y	Z	X	Y	Z	YAW	PITCH	ROLL
1	LT	1	34.772	1.6280	1.0101	1.7954	5.168	7.436	3.778	0.000	0.000	-0.072	0.00	0.00	0.00
2	CT	2	13.099	0.4160	0.2301	0.5857	4.809	6.673	4.145	0.000	0.000	-0.011	0.00	0.00	0.00
3	UT	3	53.673	3.4525	2.7832	2.3509	5.220	6.906	7.314	0.000	0.000	-0.872	0.00	0.00	0.00
4	N	4	3.289	0.0278	0.0278	0.0216	2.520	2.520	3.156	0.000	0.000	0.000	0.00	0.00	0.00
5	H	5	11.927	0.2708	0.3085	0.1584	3.984	3.125	5.836	0.000	0.000	0.000	0.00	0.00	0.00
6	RUL	6	22.725	2.0130	2.0130	0.2576	3.308	3.308	12.652	0.000	0.000	0.000	0.00	0.00	0.00
7	RLL	7	9.763	0.4989	0.4989	0.0626	2.487	2.487	9.616	0.000	0.000	0.000	0.00	0.00	0.00
8	RF	8	2.079	0.0426	0.0412	0.0055	2.866	2.016	5.617	0.000	0.000	1.462	0.00	0.00	0.00
9	LUL	9	22.725	2.0130	2.0130	0.2576	3.308	3.308	12.652	0.000	0.000	0.000	0.00	0.00	0.00
10	LLL	A	9.763	0.4989	0.4989	0.0626	2.487	2.487	9.616	0.000	0.000	0.000	0.00	0.00	0.00
11	LF	B	2.079	0.0426	0.0412	0.0055	2.866	2.016	5.617	0.000	0.000	1.462	0.00	0.00	0.00
12	RUA	C	5.542	0.1743	0.1743	0.0259	2.122	2.122	7.497	0.000	0.000	0.000	0.00	0.00	0.00
13	RLA	D	5.901	0.3331	0.3331	0.0214	1.871	1.871	10.269	0.000	0.000	0.000	0.00	0.00	0.00
14	LUA	E	5.542	0.1743	0.1743	0.0259	2.122	2.122	7.497	0.000	0.000	0.000	0.00	0.00	0.00
15	LLA	F	5.901	0.3331	0.3331	0.0214	1.871	1.871	10.269	0.000	0.000	0.000	0.00	0.00	0.00

CARDS 8.3

JOINT				LOCATION( IN.) - SEG(JNT)			LOCATION( IN.) - SEG(J+1)			PRIN. AXIS(DEG) - SEG(JNT)			PRIN. AXIS(DEG) - SEG(J+1)		
J	SYM	PLOT	JNT PIN	X	Y	Z	X	Y	Z	YAW	PITCH	ROLL	YAW	PITCH	ROLL
1	P	M	1 0	0.000	0.000	-3.850	0.000	0.000	1.610	0.00	0.00	0.00	0.00	5.00	0.00
2	W	N	2 0	0.000	0.000	-1.640	0.000	0.000	6.440	0.00	0.00	0.00	0.00	5.00	0.00
3	NP	O	3 0	0.000	0.000	-8.190	0.000	0.000	0.640	0.00	0.00	0.00	0.00	10.00	0.00
4	HP	P	4 0	0.000	0.000	-0.640	0.000	0.000	5.840	0.00	0.00	0.00	0.00	10.00	0.00
5	RH	Q	1 0	0.000	3.420	-0.310	0.000	0.000	-8.640	0.00	0.00	0.00	0.00	-45.00	0.00
6	RK	R	6 1	0.000	0.000	10.000	0.000	0.000	-6.970	0.00	0.00	0.00	0.00	60.00	0.00
7	RA	S	7 0	0.000	0.000	8.120	2.870	0.000	-2.660	0.00	90.00	0.00	0.00	10.00	0.00
8	LH	T	1 0	0.000	-3.420	-0.310	0.000	0.000	-8.640	0.00	0.00	0.00	0.00	-45.00	0.00
9	LK	U	9 1	0.000	0.000	10.000	0.000	0.000	-6.970	0.00	0.00	0.00	0.00	60.00	0.00
10	LA	V	10 0	0.000	0.000	8.120	2.870	0.000	-2.660	0.00	90.00	0.00	0.00	10.00	0.00
11	RS	W	3 0	0.000	6.240	-5.220	0.000	0.000	-5.370	0.00	0.00	0.00	0.00	-4.10	0.00
12	RE	X	12 1	0.000	0.000	5.420	0.000	0.000	-8.200	0.00	0.00	0.00	0.00	-70.00	0.00
13	LS	Y	3 0	0.000	-6.240	-5.220	0.000	0.000	-5.370	0.00	0.00	0.00	0.00	-4.10	0.00
14	LE	Z	14 1	0.000	0.000	5.420	0.000	0.000	-8.200	0.00	0.00	0.00	0.00	-70.00	0.00

## FLEXURAL SPRING CHARACTERISTICS

## TORSIONAL SPRING CHARACTERISTICS

JOINT	FLEXURAL SPRING CHARACTERISTICS					TORSIONAL SPRING CHARACTERISTICS				
	SPRING COEF. ( IN. LB./DEG**J)			ENERGY	JOINT	SPRING COEF. ( IN. LB./DEG**J)			ENERGY	JOINT
	LINEAR	QUADRATIC	CUBIC	DISSIPATION	STOP	LINEAR	QUADRATIC	CUBIC	DISSIPATION	STOP
	(J=1)	(J=2)	(J=3)	COEF.	(DEG)	(J=1)	(J=2)	(J=3)	COEF.	(DEG)
1 P	0.000	10.000	0.000	0.700	20.000	0.000	10.000	0.000	0.700	5.000
2 W	0.000	10.000	0.000	0.700	20.000	0.000	10.000	0.000	0.700	35.000
3 NP	0.000	5.000	0.000	0.700	25.000	0.000	10.000	0.000	0.700	35.000
4 HP	0.000	5.000	0.000	0.700	25.000	0.000	10.000	0.000	0.700	35.000
5 RH	0.000	10.000	0.000	0.700	70.000	0.000	0.800	0.000	0.700	40.000
6 RK	0.000	1.800	0.000	0.700	60.000	0.000	0.000	0.000	0.000	0.000
7 RA	0.000	7.000	0.000	0.700	35.000	0.000	10.000	0.000	0.700	26.000
8 LH	0.000	10.000	0.000	0.700	70.000	0.000	0.800	0.000	0.700	40.000
9 LK	0.000	1.800	0.000	0.700	60.000	0.000	0.000	0.000	0.000	0.000
10 LA	0.000	7.000	0.000	0.700	35.000	0.000	10.000	0.000	0.700	26.000
11 RS	0.000	10.000	0.000	0.700	122.500	0.000	10.000	0.000	0.700	65.000
12 RE	0.000	1.800	0.000	0.700	70.000	0.000	0.000	0.000	0.000	0.000
13 LS	0.000	10.000	0.000	0.700	122.500	0.000	10.000	0.000	0.700	65.000
14 LE	0.000	1.800	0.000	0.700	70.000	0.000	0.000	0.000	0.000	0.000

CARDS 8.5

## JOINT VISCOUS CHARACTERISTICS AND LOCK-UNLOCK CONDITIONS

JOINT	VISCOUS	COULOMB	FULL FRICTION	MAX TORQUE FOR	MIN TORQUE FOR	MIN. ANG. VELOCITY	IMPULSE
	COEFFICIENT	FRICTION COEF.	ANGULAR VELOCITY	A LOCKED JOINT	UNLOCKED JOINT	FOR UNLOCKED JOINT	RESTITUTION
	( IN. LB.SEC./DEG)	( IN. LB.)	(DEG./SEC.)	( IN. LB.)	( IN. LB.)	(RAD/SEC.)	COEFFICIENT
1 P	0.100	0.00	30.00	0.00	0.00	0.00	0.000
2 W	0.100	0.00	30.00	0.00	0.00	0.00	0.000
3 NP	0.100	0.00	30.00	0.00	0.00	0.00	0.000
4 HP	0.100	0.00	30.00	0.00	0.00	0.00	0.000
5 RH	0.100	0.00	30.00	0.00	0.00	0.00	0.000
6 RK	0.100	0.00	30.00	0.00	0.00	0.00	0.000
7 RA	0.100	0.00	30.00	0.00	0.00	0.00	0.000
8 LH	0.100	0.00	30.00	0.00	0.00	0.00	0.000
9 LK	0.100	0.00	30.00	0.00	0.00	0.00	0.000
10 LA	0.100	0.00	30.00	0.00	0.00	0.00	0.000
11 RS	0.100	0.00	30.00	0.00	0.00	0.00	0.000
12 RE	0.100	0.00	30.00	0.00	0.00	0.00	0.000
13 LS	0.100	0.00	30.00	0.00	0.00	0.00	0.000
14 LE	0.100	0.00	30.00	0.00	0.00	0.00	0.000

SEGMENT INTEGRATION CONVERGENCE TEST INPUT

SEGMENT NO. SYM	ANGULAR VELOCITIES (RAD/SEC.)			LINEAR VELOCITIES ( IN./SEC.)			ANGULAR ACCELERATIONS (RAD/SEC.**2)			LINEAR ACCELERATIONS ( IN./SEC.**2)		
	MAG. TEST	ABS. ERROR	REL. ERROR	MAG. TEST	ABS. ERROR	REL. ERROR	MAG. TEST	ABS. ERROR	REL. ERROR	MAG. TEST	ABS. ERROR	REL. ERROR
1 LT	0.010	0.010	0.0100	0.010	0.010	0.0100	0.100	0.100	0.1000	0.100	0.100	0.0100
2 CT	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
3 UT	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
4 N	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
5 H	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
6 RUL	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
7 RLL	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
8 RF	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
9 LUL	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
10 LLL	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
11 LF	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
12 RUA	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
13 RLA	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
14 LUA	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
15 LLA	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000

## VEHICLE DECELERATION INPUTS

PAGE 5  
CARDS C

## SLED ACCELERATION - 20G PEAK

YAW	PITCH	ROLL	VIPS	VTIME	X0(X)	X0(Y)	X0(Z)	NATAB	ATO	ADT	MSEG
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	15	0.000000	0.010000	0

## UNIDIRECTIONAL VEHICLE POSITION TABLES

TIME (MSEC)	ACC (G)	VELOCITY ( IN./SEC.)	POSITION ( IN.)	TIME (MSEC)	ACC (G)	VELOCITY ( IN./SEC.)	POSITION ( IN.)
0.00000	0.00	0.0000	0.00000				
10.00000	5.00	-9.6522	-0.03217				
20.00000	10.00	-38.6088	-0.25739				
30.00000	15.00	-86.8698	-0.86870				
40.00000	20.00	-154.4352	-2.05914				
50.00000	15.00	-222.0006	-3.95740				
60.00000	10.00	-270.2616	-6.43480				
70.00000	5.00	-299.2182	-9.29829				
80.00000	0.00	-308.8704	-12.35482				
90.00000	0.00	-308.8704	-15.44352				
100.00000	0.00	-308.8704	-18.53222				
110.00000	0.00	-308.8704	-21.62093				
120.00000	0.00	-308.8704	-24.70963				
130.00000	0.00	-308.8704	-27.79834				
140.00000	0.00	-308.8704	-30.88704				



NPI	NBLT	NBAG	NELP	NQ	NSD	NHRNSS	NWINDF	NJNTF	NFORCE
12	0	0	3	0	0	1	0	0	0

PAGE 6  
CARD D.1  
CARDS D.2

PLANE INITS

PLANE NO. 1 SEAT. 6 DEGREE OFF H

	X	Y	Z
POINT 1	10.0000	8.0000	-10.0000
POINT 2	28.0100	8.0000	-11.8900
POINT 3	10.0000	-8.0000	-10.0000

PLANE NO. 2 BACK PANEL. 13 DEGR

	X	Y	Z
POINT 1	1.0000	9.0000	-48.9700
POINT 2	10.0000	9.0000	-10.0000
POINT 3	1.0000	-9.0000	-48.9700

PLANE NO. 3 FLOOR.

	X	Y	Z
POINT 1	0.0000	12.0000	-1.3000
POINT 2	60.0000	12.0000	-1.3000
POINT 3	0.0000	-12.0000	-1.3000

PLANE NO. 4 HEAD PAD. 13 DEGR

	X	Y	Z
POINT 1	2.4800	7.5000	-47.2600
POINT 2	4.9600	7.5000	-36.5500
POINT 3	2.4800	-7.5000	-47.2600

PLANE NO. 5 SEAT FRONT PANEL.

	X	Y	Z
POINT 1	28.0100	8.0000	-11.8900
POINT 2	26.6600	8.0000	-4.4000
POINT 3	28.0100	-8.0000	-11.8900

PLANE NO. 6 BACK PANEL2. 13 DEGR

	X	Y	Z
POINT 1	1.0000	9.0000	-48.9700
POINT 2	10.0000	9.0000	-10.0000
POINT 3	1.0000	-9.0000	-48.9700

PLANE NO. 7 FIREWALL.

	X	Y	Z
POINT 1	60.0000	12.0000	-25.0000
POINT 2	60.0000	-12.0000	-25.0000
POINT 3	60.0000	12.0000	-0.7500

## PLANE NO. 8 RIGHT SIDE SEAT/IN.

	X	Y	Z
POINT 1	8.4100	8.1000	-6.6600
POINT 2	8.7000	8.1000	-14.7300
POINT 3	30.5800	8.1000	-6.6400

## PLANE NO. 9 LEFT SIDE SEAT/IN.

	X	Y	Z
POINT 1	8.4100	-8.1000	-6.6600
POINT 2	30.5800	-8.1000	-6.6400
POINT 3	8.7000	-8.1000	-14.7300

## PLANE NO. 10 RUDDER PEDALS.

	X	Y	Z
POINT 1	49.9920	9.0000	-2.2392
POINT 2	52.9920	9.0000	-4.7565
POINT 3	49.9920	-9.0000	-2.2392

## PLANE NO. 11 LEFT SIDE PANEL.

	X	Y	Z
POINT 1	1.0000	-9.0000	-48.9700
POINT 2	10.9000	-9.0000	-6.1000
POINT 3	-7.7700	-9.0000	-46.9500

## PLANE NO. 12 RIGHT SIDE PANEL.

	X	Y	Z
POINT 1	1.0000	9.0000	-48.9700
POINT 2	-7.7700	9.0000	-46.9500
POINT 3	10.9000	9.0000	-6.1000

PAGE 8  
CARDS D.5

[illegible]

FUNCTION NO. 3 SEGMENT-SEGMENT FCN. NT1( 3) = 1

D0	D1	D2	D3	D4
0.0000	-5.0000	0.0000	0.0000	1.0000

FIRST PART OF FUNCTION - 6 TABULAR POINTS

D	F(D)
0.000000	0.0000
1.000000	470.0000
2.000000	890.0000
3.000000	1220.0000
4.000000	1470.0000
5.000000	1580.0000

FUNCTION NO. 6 CONSTANT, F=0.0 NT1( 6) = 19

CARDS E

D0	D1	D2	D3	D4
0.0000	0.0000	0.0000	0.0000	0.0000

FUNCTION IS CONSTANT 0.000000

FUNCTION NO. 7 R FACTOR.

NT1( 7) = 24

D0	D1	D2	D3	D4
0.0000	0.0000	0.7000	0.0000	0.0000

FUNCTION IS CONSTANT 0.700000

FUNCTION NO. 13 STIFF SURFACES

NT1(13) = 29

CARDS E

D0	D1	D2	D3	D4
0.0000	-4.0000	0.0000	0.0000	1.0000

FIRST PART OF FUNCTION - 8 TABULAR POINTS

D	F(D)
0.000000	0.0000
0.100000	5.0000
0.200000	20.0000
0.300000	40.0000
0.400000	60.0000
1.000000	860.0000
2.000000	2400.0000
3.000000	4000.0000

FUNCTION NO. 14 FRICTION FUNC. NTI(14) = 51

D0	D1	D2	D3	D4
0.0000	0.0000	0.5000	0.0000	1.0000

FUNCTION IS CONSTANT 0.500000

FUNCTION NO. 19 CF=.25,CREST=.25 NTI(19) = 56

CARDS E

D0	D1	D2	D3	D4
0.0000	0.0000	0.2500	0.0000	0.0000

FUNCTION IS CONSTANT 0.250000

FUNCTION NO. 20 DAMPING COEFF. C=900 NTI(20) = 61

D0	D1	D2	D3	D4
0.0000	1.0000	0.0000	0.0000	1.0000

FIRST PART OF FUNCTION - 5TH DEGREE POLYNOMIAL

A0	A1	A2	A3	A4	A5
0.000000	900.000000	0.000000	0.000000	0.000000	0.000000

FUNCTION NO. 21 RATE OF DEFLEC. NTI(21) = 72

CARDS E

D0	D1	D2	D3	D4
-40.0000	-150.0000	0.0000	0.0000	1.0000

FIRST PART OF FUNCTION - 21 TABULAR POINTS

D	F(D)
-40.000000	0.0000
-30.000000	0.0000
-20.000000	0.0000
-10.000000	0.0000
0.000000	0.0000
5.000000	1.0000
10.000000	1.0000
20.000000	0.9900
30.000000	0.9650
40.000000	0.9280
50.000000	0.8600
60.000000	0.6900
70.000000	0.4750
80.000000	0.3400
90.000000	0.2600
100.000000	0.2000
110.000000	0.1800
120.000000	0.0900
130.000000	0.0600
140.000000	0.0250
150.000000	0.0000

FUNCTION NO. 22 DAMPING COEFF. C=35 NTI(22) = 120

D0	D1	D2	D3	D4
0.0000	1.0000	0.0000	0.0000	1.0000

FIRST PART OF FUNCTION - 5TH DEGREE POLYNOMIAL

A0	A1	A2	A3	A4	A5
0.000000	35.000000	0.000000	0.000000	0.000000	0.000000

FUNCTION NO. 24 DAMPING COEFF. C=0.8 NTI(24) = 131

CARDS E

D0	D1	D2	D3	D4
-1000.0000	-1000.0000	0.0000	0.0000	1.0000

FIRST PART OF FUNCTION - 4 TABULAR POINTS

D	F(D)
-1000.000000	0.6000
-1.000000	0.6000
0.000000	1.0000
1000.000000	1.0000



FUNCTION NO. 25 DAMPING COEFF C=1100 NTI(25) = 145

D0	D1	D2	D3	D4
0.0000	1.0000	0.0000	0.0000	1.0000

FIRST PART OF FUNCTION - 5TH DEGREE POLYNOMIAL

A0	A1	A2	A3	A4	A5
0.000000	1100.000000	0.000000	0.000000	0.000000	0.000000

FUNCTION NO. 26 STIFF SURFACES-LL NTI(26) = 156

CARDS E

D0	D1	D2	D3	D4
0.0000	-4.0000	0.0000	0.0000	1.0000

FIRST PART OF FUNCTION - 8 TABULAR POINTS

D	F(D)
0.000000	0.0000
0.100000	5.0000
0.200000	20.0000
0.300000	40.0000
0.400000	60.0000
2.000000	860.0000
3.000000	2400.0000
4.000000	4000.0000

FUNCTION NO. 31 HARNESS FDF NT1(31) = 178

D0	D1	D2	D3	D4
0.0000	-4.0000	0.0000	0.0000	0.0000

FIRST PART OF FUNCTION - 8 TABULAR POINTS

D	F(D)
0.000000	0.0000
0.010000	150.0000
0.020000	300.0000
0.030000	450.0000
0.050000	850.0000
0.100000	3500.0000
1.000000	35000.0000
4.000000	140000.0000

FUNCTION NO. 32 HARNESS FRICTION NT1(32) = 200

CARDS E

D0	D1	D2	D3	D4
0.0000	0.0000	0.2000	0.0000	0.2000

FUNCTION IS CONSTANT 0.200000

FUNCTION NO. 34 HARNESS FRICTION

NTI(34) = 205

D0	D1	D2	D3	D4
0.0000	0.0000	0.9000	0.0000	0.2000

FUNCTION IS CONSTANT 0.900000

# ALLOWED CONTACTS AND ASSOCIATED FUNCTIONS

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CARDS F.1

PLANE	SEGMENT	FORCE DEFLECTION	INERTIAL SPIKE	R FACTOR	G FACTOR	FRICTION COEF. OPT
1- 16	1- 1	13	-20	-21	0	14 1
SEAT. 6 DEGREE OFF H	LT	STIFF SURFACES	DAMPING COEFF. C=900	RATE OF DEFLEC.		FRICTION FUNC.
1- 16	6- 6	13	-25	-21	0	14 1
SEAT. 6 DEGREE OFF H	RUL	STIFF SURFACES	DAMPING COEFF C=1100	RATE OF DEFLEC.		FRICTION FUNC.
1- 16	9- 9	13	-25	-21	0	14 1
SEAT. 6 DEGREE OFF H	LUL	STIFF SURFACES	DAMPING COEFF C=1100	RATE OF DEFLEC.		FRICTION FUNC.
2- 16	1- 1	13	-20	-21	0	14 1
BACK PANEL. 13 DEGR	LT	STIFF SURFACES	DAMPING COEFF. C=900	RATE OF DEFLEC.		FRICTION FUNC.
2- 16	2- 2	13	-20	-21	0	14 1
BACK PANEL. 13 DEGR	CT	STIFF SURFACES	DAMPING COEFF. C=900	RATE OF DEFLEC.		FRICTION FUNC.
2- 16	3- 3	13	-20	-21	0	14 1
BACK PANEL. 13 DEGR	UT	STIFF SURFACES	DAMPING COEFF. C=900	RATE OF DEFLEC.		FRICTION FUNC.
3- 16	8- 8	13	-22	-21	0	14 -1
FLOOR.	RF	STIFF SURFACES	DAMPING COEFF. C=35	RATE OF DEFLEC.		FRICTION FUNC.
3- 16	11- 11	13	-22	-21	0	14 -1
FLOOR.	LF	STIFF SURFACES	DAMPING COEFF. C=35	RATE OF DEFLEC.		FRICTION FUNC.
4- 16	5- 5	13	-22	-21	0	14 1
HEAD PAD. 13 DEGR	H	STIFF SURFACES	DAMPING COEFF. C=35	RATE OF DEFLEC.		FRICTION FUNC.
10- 16	8- 8	13	-22	-21	0	14 1
RUDDER PEDALS.	RF	STIFF SURFACES	DAMPING COEFF. C=35	RATE OF DEFLEC.		FRICTION FUNC.
10- 16	11- 11	13	-22	-21	0	14 1
RUDDER PEDALS.	LF	STIFF SURFACES	DAMPING COEFF. C=35	RATE OF DEFLEC.		FRICTION FUNC.

CARDS F.3

SEGMENT	SEGMENT	FORCE DEFLECTION	INERTIAL SPIKE	R FACTOR	G FACTOR	FRICTION COEF. OPT
2- 2	13- 13	3	0	7	0	19 0
CT	RLA	SEGMENT-SEGMENT FCN.		R FACTOR.		CF=.25,CREST=.25
2- 2	15- 15	3	0	7	0	19 0
CT	LLA	SEGMENT-SEGMENT FCN.		R FACTOR.		CF=.25,CREST=.25
6- 6	13- 13	3	0	7	0	19 0
RUL	RLA	SEGMENT-SEGMENT FCN.		R FACTOR.		CF=.25,CREST=.25
9- 9	15- 15	3	0	7	0	19 0
LUL	LLA	SEGMENT-SEGMENT FCN.		R FACTOR.		CF=.25,CREST=.25
13- 13	16- 24	13	-22	-21	0	14 0
RLA	VEH	STIFF SURFACES	DAMPING COEFF. C=35	RATE OF DEFLEC.		FRICTION FUNC.
15- 15	16- 24	13	-22	-21	0	14 0
LLA	VEH	STIFF SURFACES	DAMPING COEFF. C=35	RATE OF DEFLEC.		FRICTION FUNC.

## HARNESS-BELT SYSTEM INPUT

PAGE 18  
CARDS F.8

NO. OF HARNESSES = 1

NO. OF BELTS PER HARNESS = 2

FOR HARNESS NO. 1 NO. OF POINTS PER BELT = 12 15

HARNESS NO. 1 BELT NO. 1 FUNCTION NOS. 31 0 0 0 0 REFERENCE SLACK = 0.000 IN.

K	KS	KE	NT	NPD	NDR	FUNCTION NOS.				
1	16	0	109	1	1	0	0	0	0	0
2	1	1	115	0	1	0	0	0	0	34
3	1	1	121	0	1	0	0	0	0	34
4	1	1	127	0	1	0	0	0	0	34
5	1	1	133	0	1	0	0	0	0	34
6	1	23	139	0	1	0	0	0	0	0
7	1	1	145	0	1	0	0	0	0	34
8	1	1	151	0	1	0	0	0	0	34
9	1	1	157	0	1	0	0	0	0	34
10	1	1	163	0	1	0	0	0	0	34
11	1	1	169	0	1	0	0	0	0	34
12	16	0	175	1	1	0	0	0	0	0

CARDS F.8.D

K	BASE REFERENCE ( IN. )			ADJUSTED REFERENCE ( IN. )			OFFSET ( IN. )			PREFERRED DIRECTION ( IN. )		
	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z
1	13.000	8.000	-10.300	13.000	8.000	-10.300	0.000	0.000	0.000	2.400	22.000	-0.300
2	-1.178	7.075	-0.781	-1.178	7.075	-0.781	0.000	0.000	-0.072	0.000	0.000	0.000
3	-0.029	6.796	-1.534	-0.029	6.795	-1.534	0.000	0.000	-0.072	0.000	0.000	0.000
4	0.910	5.778	-2.283	0.910	5.778	-2.283	0.000	0.000	-0.072	0.000	0.000	0.000
5	2.228	2.355	-3.192	2.228	2.355	-3.192	0.000	0.000	-0.072	0.000	0.000	0.000
6	2.957	0.000	3.059	2.957	0.000	3.059	0.000	0.000	-7.000	0.000	0.000	0.000
7	3.070	-0.080	-4.410	2.344	-0.061	-3.367	0.000	0.000	-0.072	0.000	0.000	0.000
8	1.785	-2.325	-3.343	1.785	-2.325	-3.343	0.000	0.000	-0.072	0.000	0.000	0.000
9	0.011	-5.145	-2.728	0.011	-5.145	-2.728	0.000	0.000	-0.072	0.000	0.000	0.000
10	-0.880	-5.789	-2.282	-0.880	-5.789	-2.282	0.000	0.000	-0.072	0.000	0.000	0.000
11	-2.460	-6.099	-1.200	-2.460	-6.098	-1.200	0.000	0.000	-0.072	0.000	0.000	0.000
12	13.000	-8.000	-10.300	13.000	-8.000	-10.300	0.000	0.000	0.000	2.400	22.000	-0.300

HARNESS NO. 1 BELT NO. 2 FUNCTION NOS. 31 0 0 0 0 REFERENCE SLACK = 0.000 IN.

K	KS	KE	NT	NPD	NDR	FUNCTION NOS.				
13	16	0	187	1	1	0	0	0	0	0
14	1	1	193	0	1	0	0	0	0	32
15	1	1	199	0	1	0	0	0	0	32
16	1	23	205	0	1	0	0	0	0	0
17	1	1	211	0	1	0	0	0	0	32
18	2	2	217	0	1	0	0	0	0	32
19	2	2	223	0	1	0	0	0	0	32
20	3	3	229	0	1	0	0	0	0	32
21	3	3	235	0	1	0	0	0	0	32
22	3	3	241	0	1	0	0	0	0	32
23	3	3	247	0	1	0	0	0	0	32
24	3	22	253	0	0	0	0	0	0	32
25	3	3	259	0	1	0	0	0	0	32
26	3	3	265	0	1	0	0	0	0	32
27	16	0	271	1	1	0	0	0	0	0

CARDS F.8.D

K	BASE REFERENCE ( IN. )			ADJUSTED REFERENCE ( IN. )			OFFSET ( IN. )			PREFERRED DIRECTION ( IN. )		
	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z
13	13.000	-8.000	-10.300	13.000	-8.000	-10.300	0.000	0.000	0.000	0.700	17.500	-21.300
14	-2.445	-6.101	-1.213	-2.445	-6.101	-1.213	0.000	0.000	-0.072	0.000	0.000	0.000
15	-0.960	-6.000	-2.500	-0.906	-5.661	-2.359	0.000	0.000	-0.072	0.000	0.000	0.000
16	0.000	-5.700	3.800	0.000	-5.367	3.578	0.000	0.000	-7.000	0.000	0.000	0.000
17	0.010	-4.000	-4.500	0.008	-3.061	-3.443	0.000	0.000	-0.072	0.000	0.000	0.000
18	1.818	-5.439	-1.820	1.818	-5.439	-1.820	0.000	0.000	-0.011	0.000	0.000	0.000
19	2.500	-2.500	-1.500	3.397	-3.397	-2.038	0.000	0.000	-0.011	0.000	0.000	0.000

20	3.000	-1.500	6.500	2.777	-1.388	6.016	0.000	0.000	-0.872	0.000	0.000	0.000
21	4.487	-0.133	3.734	4.487	-0.133	3.734	0.000	0.000	-0.872	0.000	0.000	0.000
22	4.421	3.319	-1.662	4.421	3.319	-1.662	0.000	0.000	-0.872	0.000	0.000	0.000
23	0.879	4.202	-5.672	0.879	4.202	-5.672	0.000	0.000	-0.872	0.000	0.000	0.000
24	0.300	0.200	-2.800	0.320	0.213	-2.985	0.000	4.000	-3.500	0.000	0.000	0.000
25	-1.000	4.300	-6.000	-0.955	4.105	-5.728	0.000	0.000	-0.872	0.000	0.000	0.000
26	-2.500	4.300	-4.000	-2.612	4.492	-4.179	0.000	0.000	-0.872	0.000	0.000	0.000
27	0.000	5.000	-35.200	0.000	5.000	-35.200	0.000	0.000	0.000	0.700	17.500	-21.300

ZPLT(X)	ZPLT(Y)	ZPLT(Z)	I1	J1	I2	J2	I3	SPLT(1)	SPLT(2)	SPLT(3)
0.	0.	0.	0	0	0	0	0	10.00	6.00	1.00

INITIAL POSITIONS (INERTIAL REFERENCE)

CARDS G.2

SEGMENT NO. SEG	LINEAR POSITION ( IN.)			LINEAR VELOCITY ( IN./SEC.)		
	X	Y	Z	X	Y	Z
1 LT	14.38100	0.00000	-13.75000	0.00000	0.00000	0.00000
2 CT	13.16068	0.00000	-19.07188	0.00000	0.00000	0.00000
3 UT	11.31383	0.00000	-26.93796	0.00000	0.00000	0.00000
4 N	9.28353	0.00000	-35.53137	0.00000	0.00000	0.00000
5 H	7.77521	0.00000	-41.83338	0.00000	0.00000	0.00000
6 RUL	22.94073	3.42000	-14.48930	0.00000	0.00000	0.00000
7 RLL	38.16022	3.42000	-10.39045	0.00000	0.00000	0.00000
8 RF	48.12719	3.42000	-4.45598	0.00000	0.00000	0.00000
9 LUL	22.94073	-3.42000	-14.48930	0.00000	0.00000	0.00000
10 LLL	38.16022	-3.42000	-10.39045	0.00000	0.00000	0.00000
11 LF	48.12719	-3.42000	-4.45598	0.00000	0.00000	0.00000
12 RUA	12.34164	6.24000	-27.13188	0.00000	0.00000	0.00000
13 RLA	22.75808	6.24000	-21.48521	0.00000	0.00000	0.00000
14 LUA	12.34164	-6.24000	-27.13188	0.00000	0.00000	0.00000
15 LLA	22.75808	-6.24000	-21.48521	0.00000	0.00000	0.00000

INITIAL ANGULAR ROTATION AND VELOCITY

CARDS G.3

SEGMENT NO. SEG	ANGULAR ROTATION (DEG)			ANGULAR VELOCITY (DEG/SEC.)			IYPR
	YAW	PITCH	ROLL	X	Y	Z	
1 LT	0.00000	12.90000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
2 CT	0.00000	12.95000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
3 UT	0.00000	13.28000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
4 N	0.00000	13.46000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
5 H	0.00000	13.46000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
6 RUL	0.00000	92.90000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
7 RLL	0.00000	48.65000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
8 RF	0.00000	128.80000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
9 LUL	0.00000	92.90000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
10 LLL	0.00000	48.65000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
11 LF	0.00000	128.80000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
12 RUA	0.00000	24.50000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
13 RLA	0.00000	85.00000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
14 LUA	0.00000	24.50000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
15 LLA	0.00000	85.00000	0.00000	0.00000	0.00000	0.00000	3 2 1 0

LINEAR AND ANGULAR VELOCITIES HAVE BEEN SET EQUAL TO THE INITIAL VEHICLE VELOCITIES.

HBPLAY TIME = 0.000 MSEC. NH,NB,NPTS NT= 1 1 11 103

NL(1)= 1 2 3 4 5 6 8 9 10 11 12

BB = 4.124 1.402 1.574 3.779 2.557 2.656 3.388 1.187 1.940 4.738

HBPLAY TIME = 0.000 MSEC. NH,NB,NPTS NT= 1 2 7 181

NL(1)= 13 14 18 21 22 23 27

BB = 4.748 7.394 6.842 6.406 5.423 10.829

TABULAR TIME HISTORY CONTROL PARAMETERS

TYPE KSG SELECTED SEGMENTS OR JOINTS

H.1 3 3 5 5

REF 0 1 16

H.2 3 3 5 5

REF 0 0 3

H.3 3 3 5 5

REF 0 0 3

H.4 3 3 5 5

REF 0 0 16

H.5 3 3 5 5

REF 0 0 5

H.6 3 3 5 5

REF 0 0 3

H.7 2 3 4

REF 0 0

H.8 0

REF

H.9 1 4

REF 5

H.10 15 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15

REF 16



SEGMENT	(INERTIAL)			(LOCAL)			(LOCAL)		
	ANGULAR ROTATION (DEG)			ANGULAR VELOCITY (RAD/SEC.)			ANGULAR ACCELERATION (RAD/SEC.**2)		
	YAW	PITCH	ROLL	X	Y	Z	X	Y	Z
1 LT	0.0000	12.9000	0.0000	0.00000	0.00000	0.00000	0.000000	-26.834649	0.000000
2 CY	0.0000	12.9500	0.0000	0.00000	0.00000	0.00000	0.000000	40.304245	0.000000
3 UT	0.0000	13.2800	0.0000	0.00000	0.00000	0.00000	0.000000	-0.859459	0.000000
4 N	0.0000	13.4600	0.0000	0.00000	0.00000	0.00000	0.000000	13.637948	0.000000
5 H	0.0000	13.4600	0.0000	0.00000	0.00000	0.00000	0.000000	-1.165343	0.000000
6 RUL	0.0000	92.9000	0.0000	0.00000	0.00000	0.00000	0.000000	-2.405246	0.000000
7 RLL	0.0000	48.6500	0.0000	0.00000	0.00000	0.00000	0.000000	-12.215669	0.000000
8 RF	0.0000	128.8000	0.0000	0.00000	0.00000	0.00000	0.000000	56.318297	0.000000
9 LUL	0.0000	92.9000	0.0000	0.00000	0.00000	0.00000	0.000000	-2.405246	0.000000
10 LLL	0.0000	48.6500	0.0000	0.00000	0.00000	0.00000	0.000000	-12.215669	0.000000
11 LF	0.0000	128.8000	0.0000	0.00000	0.00000	0.00000	0.000000	56.318297	0.000000
12 RUA	0.0000	24.5000	0.0000	0.00000	0.00000	0.00000	0.000000	-6.917594	0.000000
13 RLA	0.0000	85.0000	0.0000	0.00000	0.00000	0.00000	0.000000	-34.722447	0.000000
14 LUA	0.0000	24.5000	0.0000	0.00000	0.00000	0.00000	0.000000	-6.917594	0.000000
15 LLA	0.0000	85.0000	0.0000	0.00000	0.00000	0.00000	0.000000	-34.722447	0.000000
16 VEH	0.0000	0.0000	0.0000	0.00000	0.00000	0.00000	0.000000	0.000000	0.000000

SEGMENT	(INERTIAL)			(INERTIAL)			(INERTIAL)		
	LINEAR POSITION ( IN.)			LINEAR VELOCITY ( IN./SEC.)			LINEAR ACCELERATIONS (G'S)		
	X	Y	Z	X	Y	Z	X	Y	Z
1 LT	14.3810	0.0000	-13.7500	0.00000	0.00000	0.00000	0.017822	0.000000	-0.088444
2 CT	13.1607	0.0000	-19.0719	0.00000	0.00000	0.00000	0.114863	0.000000	-0.110519
3 UT	11.3138	0.0000	-26.9380	0.00000	0.00000	0.00000	-0.038031	0.000000	-0.075446
4 N	9.2835	0.0000	-35.5314	0.00000	0.00000	0.00000	-0.042274	0.000000	-0.074372
5 H	7.7752	0.0000	-41.8334	0.00000	0.00000	0.00000	-0.047117	0.000000	-0.073212
6 RUL	22.9407	3.4200	-14.4893	0.00000	0.00000	0.00000	0.041548	0.000000	-0.039498
7 RLL	38.1602	3.4200	-10.3904	0.00000	0.00000	0.00000	-0.100994	0.000000	0.188268
8 RF	48.1272	3.4200	-4.4560	0.00000	0.00000	0.00000	-0.187590	0.000000	-0.183587
9 LUL	22.9407	-3.4200	-14.4893	0.00000	0.00000	0.00000	0.041548	0.000000	-0.039498
10 LLL	38.1602	-3.4200	-10.3904	0.00000	0.00000	0.00000	-0.100994	0.000000	0.188268
11 LF	48.1272	-3.4200	-4.4560	0.00000	0.00000	0.00000	-0.187590	0.000000	-0.183587
12 RUA	12.3416	6.2400	-27.1319	0.00000	0.00000	0.00000	-0.114274	0.000000	-0.038215
13 RLA	22.7581	6.2400	-21.4852	0.00000	0.00000	0.00000	-0.266915	0.000000	0.736709
14 LUA	12.3416	-6.2400	-27.1319	0.00000	0.00000	0.00000	-0.114274	0.000000	-0.038215
15 LLA	22.7581	-6.2400	-21.4852	0.00000	0.00000	0.00000	-0.266915	0.000000	0.736709
16 VEH	0.0000	0.0000	0.0000	0.00000	0.00000	0.00000	0.000000	0.000000	0.000000

SEGMENT	(INERTIAL)			(LOCAL)			KINETIC ENERGY		
	U1 ARRAY ( IN./SEC.**2)			U2 ARRAY (RAD/SEC.**2)			( LB.- IN.)		
	EXTERNAL LINEAR ACCELERATIONS			EXTERNAL ANGULAR ACCELERATIONS			LINEAR	ANGULAR	TOTAL
	X	Y	Z	X	Y	Z			
1 LT	-0.1289E+03	0.0000E+00	-0.1135E+04	-0.63845E-15	-0.48015E+02	-0.60266E-16	0.00000E+00	0.00000E+00	0.00000E+00
2 CT	0.0000E+00	0.0000E+00	0.3861E+03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
3 UT	0.6940E+02	0.0000E+00	0.3701E+03	-0.43592E-20	-0.31861E+01	0.13303E-17	0.00000E+00	0.00000E+00	0.00000E+00
4 N	0.0000E+00	0.0000E+00	0.3861E+03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
5 H	0.7822E+02	0.0000E+00	0.3680E+03	-0.18372E-18	-0.26721E+00	0.42601E-16	0.00000E+00	0.00000E+00	0.00000E+00
6 RUL	-0.5309E+02	0.0000E+00	-0.1198E+03	0.46503E-17	0.21827E+02	0.67300E-15	0.00000E+00	0.00000E+00	0.00000E+00
7 RLL	0.0000E+00	0.0000E+00	0.3861E+03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
8 RF	-0.9511E+01	0.0000E+00	-0.5210E+03	0.62882E-20	-0.17610E+03	0.23251E-17	0.00000E+00	0.00000E+00	0.00000E+00
9 LUL	-0.5309E+02	0.0000E+00	-0.1198E+03	0.46503E-17	0.21827E+02	0.67300E-15	0.00000E+00	0.00000E+00	0.00000E+00
10 LLL	0.0000E+00	0.0000E+00	0.3861E+03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
11 LF	-0.9511E+01	0.0000E+00	-0.5210E+03	0.62882E-20	-0.17610E+03	0.23251E-17	0.00000E+00	0.00000E+00	0.00000E+00
12 RUA	0.0000E+00	0.0000E+00	0.3861E+03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
13 RLA	0.0000E+00	0.0000E+00	0.3861E+03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
14 LUA	0.0000E+00	0.0000E+00	0.3861E+03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
15 LLA	0.0000E+00	0.0000E+00	0.3861E+03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
							TOTAL BODY KINETIC ENERGY		
							0.00000E+00	0.00000E+00	0.00000E+00

JOINT	IPIN	(INERTIAL)			(INERTIAL)			RELATIVE ANGULAR VELCCITY (RAD/SEC.)	
		JOINT FORCES ( LB.)			JOINT TORQUES ( IN. LB.)				
		X	Y	Z	X	Y	Z		
1	P	0	-0.177E+02	0.000E+00	-0.100E+03	0.0000E+00	0.0000E+00	0.0000E+00	0.000
2	W	0	-0.192E+02	0.000E+00	-0.859E+02	0.0000E+00	0.0000E+00	0.0000E+00	0.000
3	NP	0	-0.312E+01	0.000E+00	-0.158E+02	0.0000E+00	0.0000E+00	0.0000E+00	0.000
4	HP	0	-0.298E+01	0.000E+00	-0.122E+02	0.0000E+00	0.0000E+00	0.0000E+00	0.000
5	SH	0	0.274E+01	0.000E+00	0.653E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.000
6	RK	1	-0.132E+01	0.000E+00	-0.550E+01	0.0000E+00	0.0000E+00	0.0000E+00	0.000
7	RA	0	-0.339E+00	0.000E+00	0.242E+01	0.0000E+00	0.0000E+00	0.0000E+00	0.000
8	LH	0	0.274E+01	0.000E+00	0.653E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.000
9	LK	1	-0.132E+01	0.000E+00	-0.550E+01	0.0000E+00	0.0000E+00	0.0000E+00	0.000
10	LA	0	-0.339E+00	0.000E+00	0.242E+01	0.0000E+00	0.0000E+00	0.0000E+00	0.000
11	RS	0	-0.221E+01	0.000E+00	-0.731E+01	0.0000E+00	0.0000E+00	0.0000E+00	0.000
12	RE	1	-0.158E+01	0.000E+00	-0.155E+01	0.0000E+00	0.0000E+00	0.0000E+00	0.000
13	LS	0	-0.221E+01	0.000E+00	-0.731E+01	0.0000E+00	0.0000E+00	0.0000E+00	0.000
14	LE	1	-0.158E+01	0.000E+00	-0.155E+01	0.0000E+00	0.0000E+00	0.0000E+00	0.000

POINT NO.	POINT INDEX	SEGMENT NO.	LENGTH ( IN. )	BELT STRAIN ENERGY LOSS ( IN. LB. )	(LOCAL OR ELLIPSOID)			(INERTIAL)			PENETRATION ENERGY LOSS ( IN. LB. )
					REFERENCE POINT ( IN. )			BELT FORCES ( LB. )			
					X	Y	Z	X	Y	Z	
BELT NO. 1 OF HARNESS NO. 1											
1	1	16	0.000	0.000	13.000	8.000	-10.300	0.000	0.000	0.000	0.000
2	2	1	4.124	0.000	-1.178	7.075	-0.781	0.000	0.000	0.000	0.000
3	3	1	1.402	0.000	-0.029	6.795	-1.534	0.000	0.000	0.000	0.000
4	4	1	1.574	0.000	0.910	5.778	-2.283	0.000	0.000	0.000	0.000
5	5	1	3.779	0.000	2.228	2.355	-3.192	0.000	0.000	0.000	0.000
6	6	1	2.557	0.000	2.957	0.000	3.059	0.000	0.000	0.000	0.000
7	8	1	2.656	0.000	1.785	-2.325	-3.343	0.000	0.000	0.000	0.000
8	9	1	3.388	0.000	0.011	-5.145	-2.728	0.000	0.000	0.000	0.000
9	10	1	1.187	0.000	-0.880	-5.789	-2.282	0.000	0.000	0.000	0.000
10	11	1	1.940	0.000	-2.460	-6.098	-1.200	0.000	0.000	0.000	0.000
11	12	16	4.738	0.000	13.000	-8.000	-10.300	0.000	0.000	0.000	0.000
TOTAL BELT ENERGY LOSS				0.000							
BELT NO. 2 OF HARNESS NO. 1											
12	13	16	0.000	0.000	13.000	-8.000	-10.300	0.000	0.000	0.000	0.000
13	14	1	4.748	0.000	-2.445	-6.101	-1.213	0.000	0.000	0.000	0.000
14	18	2	7.394	0.000	1.818	-5.439	-1.820	0.000	0.000	0.000	0.000
15	21	3	6.842	0.000	4.487	-0.133	3.734	0.000	0.000	0.000	0.000
16	22	3	6.406	0.000	4.421	3.319	-1.662	0.000	0.000	0.000	0.000
17	23	3	5.423	0.000	0.879	4.202	-5.672	0.000	0.000	0.000	0.000
18	27	16	10.829	0.000	0.000	5.000	-35.200	0.000	0.000	0.000	0.000
TOTAL BELT ENERGY LOSS				0.000							
TOTAL HARNESS ENERGY LOSS				0.000							
HPTURB ITER = 10 AT TIME = 16.000 MSEC. DELMAX = 0.010537 SCALE = 1.000000											
HPTURB ITER = 10 AT TIME = 18.000 MSEC. DELMAX = 0.009232 SCALE = 1.000000											
HPTURB ITER = 10 AT TIME = 19.000 MSEC. DELMAX = 0.009627 SCALE = 1.000000											
HPTURB ITER = 10 AT TIME = 20.000 MSEC. DELMAX = 0.010050 SCALE = 1.000000											
HPTURB ITER = 10 AT TIME = 21.000 MSEC. DELMAX = 0.010116 SCALE = 1.000000											
HBPLAY TIME = 22.000 MSEC. NH,NB,NPTS NT= 1 2 8 181											
NL(1)= 13 14 18 21 22 23 24 27											
BB = 4.748 7.394 6.842 6.406 5.423 0.491 10.338											
HPTURB ITER = 10 AT TIME = 22.000 MSEC. DELMAX = 0.012849 SCALE = 1.000000											
HPTURB ITER = 10 AT TIME = 23.000 MSEC. DELMAX = 0.011517 SCALE = 1.000000											
HPTURB ITER = 10 AT TIME = 24.000 MSEC. DELMAX = 0.011234 SCALE = 1.000000											
HPTURB ITER = 10 AT TIME = 25.000 MSEC. DELMAX = 0.011569 SCALE = 1.000000											
HPTURB ITER = 10 AT TIME = 26.000 MSEC. DELMAX = 0.012320 SCALE = 1.000000											
HPTURB ITER = 10 AT TIME = 28.000 MSEC. DELMAX = 0.010639 SCALE = 1.000000											
HPTURB ITER = 10 AT TIME = 29.000 MSEC. DELMAX = 0.012461 SCALE = 1.000000											
HPTURB ITER = 10 AT TIME = 30.000 MSEC. DELMAX = 0.014987 SCALE = 1.000000											
HBPLAY TIME = 31.000 MSEC. NH,NB,NPTS NT= 1 2 7 181											
NL(1)= 13 14 18 21 22 24 27											
BB = 4.748 7.394 6.842 6.406 5.572 10.679											
HPTURB ITER = 10 AT TIME = 31.000 MSEC. DELMAX = 0.021341 SCALE = 1.000000											
HBPLAY TIME = 32.000 MSEC. NH,NB,NPTS NT= 1 2 8 181											
NL(1)= 13 14 18 21 22 23 24 27											
BB = 4.748 7.394 6.842 6.406 5.066 0.260 10.926											
HPTURB											

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HBPLAY TIME = 36.000 MSEC. NH,NB,NPTS NT= 1 2 8 181
NL(1)= 13 14 18 21 22 23 24 27
BB = 4.748 7.394 6.842 6.406 4.847 0.195 11.210
HPTURB ITER = 10 AT TIME = 36.000 MSEC. DELMAX = 0.012648 SCALE = 1.000000
HPTURB ITER = 10 AT TIME = 37.000 MSEC. DELMAX = 0.015643 SCALE = 1.000000
HPTURB ITER = 10 AT TIME = 38.000 MSEC. DELMAX = 0.011152 SCALE = 1.000000
HPTURB ITER = 10 AT TIME = 39.000 MSEC. DELMAX = 0.014391 SCALE = 1.000000
HPTURB ITER = 10 AT TIME = 40.000 MSEC. DELMAX = 0.017690 SCALE = 1.000000
HPTURB ITER = 10 AT TIME = 41.000 MSEC. DELMAX = 0.015081 SCALE = 1.000000
HPTURB ITER = 10 AT TIME = 42.000 MSEC. DELMAX = 0.017005 SCALE = 1.000000
HBPLAY TIME = 43.000 MSEC. NH,NB,NPTS NT= 1 2 7 181
NL(1)= 13 14 18 21 22 24 27
BB = 4.748 7.394 6.842 6.406 4.910 11.342
HPTURB ITER = 10 AT TIME = 43.000 MSEC. DELMAX = 0.053120 SCALE = 1.000000
HBPLAY TIME = 44.000 MSEC. NH,NB,NPTS NT= 1 2 8 181
NL(1)= 13 14 18 21 22 23 24 27
BB = 4.748 7.394 6.842 6.406 4.496 0.075 11.681
HPTURB ITER = 10 AT TIME = 44.000 MSEC. DELMAX = 0.013932 SCALE = 1.000000
HPTURB ITER = 10 AT TIME = 45.000 MSEC. DELMAX = 0.012674 SCALE = 1.000000
HBPLAY TIME = 46.000 MSEC. NH,NB,NPTS NT= 1 2 7 181
NL(1)= 13 18 21 22 23 24 27
BB = 12.143 6.842 6.406 4.496 0.055 11.701
HPTURB ITER = 10 AT TIME = 46.000 MSEC. DELMAX = 0.014891 SCALE = 1.000000
HBPLAY TIME = 47.000 MSEC. NH,NB,NPTS NT= 1 1 10 103
NL(1)= 1 3 4 5 6 8 9 10 11 12
BB = 5.526 1.574 3.779 2.557 2.656 3.388 1.187 1.940 4.738
HPTURB ITER = 10 AT TIME = 47.000 MSEC. DELMAX = 0.018982 SCALE = 1.000000
HBPLAY TIME = 48.000 MSEC. NH,NB,NPTS NT= 1 2 6 181
NL(1)= 13 18 21 22 24 27
BB = 12.143 6.842 6.406 4.534 11.718
HPTURB ITER = 10 AT TIME = 48.000 MSEC. DELMAX = 0.064777 SCALE = 1.000000
HBPLAY TIME = 49.000 MSEC. NH,NB,NPTS NT= 1 2 7 181
NL(1)= 13 18 21 22 23 24 27
BB = 12.143 6.842 6.406 4.192 0.045 12.015
HPTURB ITER = 10 AT TIME = 49.000 MSEC. DELMAX = 0.010077 SCALE = 1.000000
HPTURB ITER = 10 AT TIME = 50.000 MSEC. DELMAX = 0.010283 SCALE = 1.000000
HPTURB ITER = 10 AT TIME = 51.000 MSEC. DELMAX = 0.012303 SCALE = 1.000000
HBPLAY TIME = 52.000 MSEC. NH,NB,NPTS NT= 1 2 6 181
NL(1)= 13 18 21 22 24 27
BB = 12.143 6.842 6.406 4.222 12.029
HPTURB ITER = 10 AT TIME = 52.000 MSEC. DELMAX = 0.055553 SCALE = 1.000000
HPTURB ITER = 10 AT TIME = 53.000 MSEC. DELMAX = 0.035482 SCALE = 1.000000
HBPLAY TIME = 54.000 MSEC. NH,NB,NPTS NT= 1 1 9 103
NL(1)= 1 3 4 5 6 8 9 10 12
BB = 5.526 1.574 3.779 2.557 2.656 3.388 1.187 6.678
HPTURB ITER = 10 AT TIME = 54.000 MSEC. DELMAX = 0.024287 SCALE = 1.000000
HPTURB ITER = 10 AT TIME = 55.000 MSEC. DELMAX = 0.015678 SCALE = 1.000000
HPTURB ITER = 10 AT TIME = 56.000 MSEC. DELMAX = 0.011486 SCALE = 1.000000
HBPLAY TIME = 57.000 MSEC. NH,NB,NPTS NT= 1 2 7 181
NL(1)= 13 18 19 21 22 24 27
BB = 12.143 1.887 4.955 6.406 3.880 12.372
HPTURB ITER = 10 AT TIME = 57.000 MSEC. DELMAX = 0.385309 SCALE = 0.259532
HBPLAY TIME = 58.000 MSEC. NH,NB,NPTS NT= 1 2 8 181
NL(1)= 13 18 19 20 21 22 24 27
BB = 12.143 1.887 1.817 3.139 6.406 3.880 12.372
HPTURB ITER = 10 AT TIME = 58.000 MSEC. DELMAX = 0.443658 SCALE = 0.225399
HBPLAY TIME = 59.000 MSEC. NH,NB,NPTS NT= 1 2 9 181
NL(1)= 13 16 18 19 20 21 22 24 27
BB = 7.889 4.253 1.887 1.817 3.139 6.406 3.974 12.277
HPTURB ITER = 10 AT TIME = 59.000 MSEC. DELMAX = 0.052001 SCALE = 1.000000
HBPLAY TIME = 60.000 MSEC. NH,NB,NPTS NT= 1 2 8 181
NL(1)= 13 18 19 20 21 22 24 27
BB = 12.143 1.887 1.817 3.139 6.406 4.086 12.165
HPTURB ITER = 10 AT TIME = 60.000 MSEC. DELMAX = 0.057808 SCALE = 1.000000
HBPLAY TIME = 61.000 MSEC. NH,NB,NPTS NT= 1 2 7 181
NL(1)= 13 18 20 21 22 24 27

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BB = 12.143 3.703 3.139 6.406 4.156 12.096  
 HPTURB ITER = 10 AT TIME = 61.000 MSEC. DELMAX = 0.015872 SCALE = 1.000000  
 HPTURB ITER = 10 AT TIME = 62.000 MSEC. DELMAX = 0.022130 SCALE = 1.000000  
 HPTURB ITER = 10 AT TIME = 63.000 MSEC. DELMAX = 0.015337 SCALE = 1.000000  
 HBPLAY TIME = 64.000 MSEC. NH,NB,NPTS NT= 1 2 6 181  
 NL(1)= 13 18 20 21 22 27

BB = 12.143 3.703 3.139 6.406 16.252  
 HPTURB ITER = 10 AT TIME = 64.000 MSEC. DELMAX = 0.011067 SCALE = 1.000000  
 HBPLAY TIME = 66.000 MSEC. NH,NB,NPTS NT= 1 1 8 103  
 NL(1)= 1 3 4 5 6 8 9 12

BB = 5.526 1.574 3.779 2.557 2.656 3.388 7.865  
 HPTURB ITER = 10 AT TIME = 67.000 MSEC. DELMAX = 0.011853 SCALE = 1.000000  
 HPTURB ITER = 10 AT TIME = 69.000 MSEC. DELMAX = 0.013454 SCALE = 1.000000

DINT CONV. TEST 72.000 N ANG VEL 22.55 0.2652E-02 0.1176E-03 0.1000E-03 0.1000E-03 0.1000E-03  
 TEST FAILED AT TIME = 0.072000 FOR H = 0.001000  
 DINT CONV. TEST 73.000 N ANG VEL 23.86 0.3624E-02 0.1518E-03 0.1000E-03 0.1000E-03 0.1000E-03  
 TEST FAILED AT TIME = 0.073000 FOR H = 0.001000  
 DINT CONV. TEST 74.000 N ANG VEL 26.11 0.3039E-02 0.1164E-03 0.1000E-03 0.1000E-03 0.1000E-03  
 TEST FAILED AT TIME = 0.074000 FOR H = 0.001000

SEGMENT	(INERTIAL)			(LOCAL)			(LOCAL)		
	ANGULAR ROTATION (DEG)			ANGULAR VELOCITY (RAD/SEC.)			ANGULAR ACCELERATION (RAD/SEC.**2)		
	YAW	PITCH	ROLL	X	Y	Z	X	Y	Z
1 LT	10.9078	40.4616	-2.5237	-3.50101	6.77176	3.01702	-712.525840	-923.312215	-344.896206
2 CT	5.8648	8.3877	-35.0629	-28.78011	38.13662	26.32712	2669.823693	4863.705047	714.436127
3 UT	22.6603	16.1876	4.2073	-4.55898	-8.33212	11.28470	-833.189016	-740.536145	24.730106
4 N	9.4134	-28.3216	9.0212	3.10468	-11.10456	11.62142	-474.529280	-2359.202266	525.452345
5 H	-14.7037	-62.0894	29.6482	16.06835	-58.33883	6.84809	321.909906	-351.659928	252.225950
6 RUL	11.0166	100.4701	10.5736	-0.26043	-3.94123	-2.59116	-82.766870	-780.201793	66.972956
7 RLL	-2.0078	53.9069	-3.2449	-2.05452	9.15294	-1.60027	12.275725	-89.117047	79.212811
8 RF	-1.2125	146.0433	2.4774	3.41634	1.03537	-1.56581	-92.295830	747.087282	-23.919556
9 LUL	4.3688	101.7927	4.4680	-0.37199	-3.33541	-0.44435	-290.296221	-679.956632	528.292675
10 LLL	-0.9289	45.3497	-1.2981	-0.57596	5.97768	0.06395	278.790376	-4.508497	528.778813
11 LF	-0.5610	155.8698	1.6050	1.79239	0.13205	-0.59660	-177.520463	1209.576341	196.625307
12 RUA	-75.0950	70.5657	-80.2833	-6.23227	-4.14211	-1.63954	244.397026	-3261.631888	-168.345676
13 RLA	-21.0534	51.2884	-31.6271	-6.18955	1.21106	1.79408	113.635227	2487.522772	-303.100898
14 LUA	-17.8558	62.4794	-23.3643	-2.95595	-0.00123	5.46149	322.014085	-2838.181404	888.201239
15 LLA	-16.0460	60.3973	-21.7744	-2.73881	-15.25083	5.57354	441.700348	4146.746554	916.611637
16 VEH	0.0000	0.0000	0.0000	0.00000	0.00000	0.00000	0.000000	0.000000	0.000000

SEGMENT	(INERTIAL)			(INERTIAL)			(INERTIAL)		
	LINEAR POSITION ( IN. )			LINEAR VELOCITY ( IN./SEC. )			LINEAR ACCELERATIONS (G'S)		
	X	Y	Z	X	Y	Z	X	Y	Z
1 LT	6.0377	0.0702	-13.0395	-334.65671	-2.92122	-92.21272	1.118456	-3.419755	-24.241372
2 CT	3.5221	-1.5083	-17.2697	-403.89532	-63.36301	-39.55188	-7.411998	0.308363	-23.341359
3 UT	1.5893	-2.7194	-24.7657	-399.28403	-115.11128	-20.63141	-8.535068	3.408484	-20.077252
4 N	-0.4641	-2.8941	-33.1662	-319.46157	-121.58509	-38.64033	16.009901	-4.901599	-22.093312
5 H	4.8868	-1.0902	-36.0984	-178.47710	-69.83431	287.80272	-29.256214	-10.703850	8.134162
6 RUL	13.6013	3.3950	-14.9332	-345.17072	-4.32318	-59.80904	2.896528	-1.986709	-14.025632
7 RLL	29.0739	3.6383	-12.6201	-300.76311	12.64266	-73.16830	3.883535	0.620604	6.154392
8 RF	39.4986	3.6714	-8.4455	-258.02278	23.08008	-137.61724	0.173190	0.601745	-0.915789
9 LUL	15.0441	-3.3466	-14.9210	-314.88548	2.85212	-60.25035	6.374569	3.680291	-3.334002
10 LLL	29.7934	-3.3024	-12.0614	-278.81100	10.63011	-57.36381	9.156247	6.479980	13.521611
11 LF	39.2761	-3.3229	-7.6097	-244.93381	11.69052	-92.38042	4.608846	0.164379	1.561647
12 RUA	3.1574	3.4023	-29.0240	-426.99852	-109.61718	-32.04897	-2.643843	6.759738	6.506879
13 RLA	15.1710	5.9986	-24.3530	-429.54688	-25.03050	-46.34975	23.116917	3.958924	9.885922
14 LUA	7.1965	-8.0306	-27.9271	-282.38560	-78.35066	-29.72059	-9.173876	2.088389	27.959874
15 LLA	19.2594	-6.2444	-21.8664	-343.80786	-23.50199	71.96752	11.107168	-20.329519	-12.311189
16 VEH	-12.3548	0.0000	0.0000	-308.87040	0.00000	0.00000	0.000000	0.000000	0.000000



## POSTPROCESSOR CONTROL PARAMETERS

	HIC & HSI POINT	CSI POINT
N.11	2	1



DATE: 2 SEPT 1988

PAGE 26

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 21.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

## POINT TOTAL ACCELERATION (G'S)

TIME (MSEC)	POINT ( 0.00, 0.00, 0.00) ON SEGMENT NO. 3 - UT				POINT ( 0.00, 0.00, 0.00) ON SEGMENT NO. -5 - H				POINT ( 0.00, 0.00, 0.00) ON SEGMENT NO. 5 - H			
	IN UT REFERENCE				ACCELEROMETER (1G)				IN VEH REFERENCE			
	X	Y	Z	RES	X	Y	Z	RES	X	Y	Z	RES
0.000	-0.020	0.000	-0.082	0.084	-0.262	0.000	0.890	0.928	-0.047	0.000	-0.073	0.087
2.000	-0.014	0.000	-0.107	0.108	-0.260	0.000	0.865	0.903	-0.051	0.000	-0.098	0.111
4.000	-0.007	0.000	-0.179	0.179	-0.258	0.000	0.793	0.834	-0.067	0.000	-0.168	0.181
6.000	-0.006	-0.003	-0.247	0.247	-0.269	0.000	0.725	0.774	-0.093	0.000	-0.232	0.250
8.000	-0.019	-0.012	-0.314	0.315	-0.306	-0.002	0.658	0.725	-0.144	-0.002	-0.289	0.323
10.000	-0.061	-0.023	-0.386	0.391	-0.379	-0.005	0.586	0.698	-0.233	-0.005	-0.342	0.413
12.000	-0.091	-0.032	-0.464	0.474	-0.475	-0.008	0.507	0.695	-0.344	-0.008	-0.396	0.525
14.000	-0.099	-0.023	-0.547	0.556	-0.487	-0.006	0.425	0.646	-0.375	-0.006	-0.474	0.604
16.000	-0.132	-0.024	-0.623	0.638	-0.506	-0.007	0.348	0.614	-0.411	-0.007	-0.544	0.682
18.000	-0.111	-0.005	-0.719	0.727	-0.510	-0.003	0.253	0.570	-0.437	-0.003	-0.635	0.771
20.000	-0.133	-0.001	-0.791	0.802	-0.525	-0.002	0.181	0.555	-0.468	-0.002	-0.702	0.844
22.000	-0.197	-0.016	-0.854	0.876	-0.551	-0.005	0.119	0.564	-0.509	-0.006	-0.756	0.911
24.000	-0.382	-0.063	-1.317	1.373	-0.662	-0.179	-0.342	0.767	-0.724	-0.179	-1.179	1.395
26.000	-0.390	-0.112	-1.296	1.358	-0.685	-0.231	-0.314	0.788	-0.739	-0.231	-1.147	1.384
28.000	-0.357	0.556	-1.166	1.340	-0.682	-0.014	-0.181	0.705	-0.705	-0.014	-1.019	1.239
30.000	-0.438	0.816	-1.246	1.553	-0.702	0.035	-0.256	0.748	-0.742	0.035	-1.087	1.317
32.000	-2.733	-0.835	-0.461	2.895	-1.271	-0.218	0.576	1.412	-1.106	-0.220	-0.149	1.137
34.000	-2.186	-0.420	-0.403	2.263	-1.208	-0.216	0.667	1.397	-1.025	-0.219	-0.076	1.051
36.000	-3.145	-0.474	-0.313	3.196	-1.481	-0.353	0.849	1.743	-1.252	-0.357	0.159	1.312
38.000	-4.178	-0.580	-1.221	4.391	-1.843	-0.709	0.133	1.979	-1.769	-0.710	-0.467	1.963
40.000	-5.137	0.364	-1.250	5.299	-2.004	-0.530	0.280	2.092	-1.897	-0.533	-0.297	1.993
42.000	-6.838	1.397	-2.254	7.334	-2.388	-0.543	-0.390	2.479	-2.417	-0.540	-0.885	2.630
44.000	-14.419	-3.743	0.830	14.920	-4.097	-1.242	3.893	5.787	-3.227	-1.300	3.624	5.024
46.000	-16.621	-1.760	-0.518	16.722	-4.375	-1.075	3.474	5.689	-3.633	-1.143	3.226	4.991
48.000	-21.535	0.772	0.632	21.558	-4.411	-0.608	5.515	7.088	-3.372	-0.744	5.190	6.234
50.000	-41.704	-14.755	6.467	44.707	-8.393	-3.295	18.145	20.262	-5.470	-3.858	18.124	19.321
52.000	-46.097	-12.754	8.809	48.633	-8.850	-2.015	24.198	25.844	-5.684	-2.996	24.033	24.877
54.000	-59.506	-18.177	14.142	63.807	-11.972	-2.812	40.775	42.589	-8.224	-4.949	40.493	41.615
56.000	-60.433	-15.422	13.472	63.808	-11.763	-2.643	48.226	49.710	-9.706	-5.876	47.398	48.737
58.000	-73.471	-17.978	-2.410	75.677	-11.839	-4.818	45.094	46.871	-12.593	-8.610	43.319	45.927
60.000	-93.922	-15.685	14.909	96.382	-10.687	1.243	64.829	65.716	-16.338	-5.515	62.414	64.752
62.000	-39.398	-7.543	-3.263	40.247	-8.458	0.385	50.073	50.783	-16.781	-5.749	46.585	49.848
64.000	-13.416	-3.242	-10.799	17.525	-4.985	0.413	34.219	34.583	-13.561	-4.374	30.511	33.674
66.000	2.837	-2.587	-20.041	20.406	-4.396	-0.971	17.138	17.719	-9.978	-3.581	13.198	16.929
68.000	12.171	-3.027	-29.353	31.921	-6.574	-2.288	10.559	12.647	-10.367	-3.898	5.106	12.195
70.000	12.817	-4.431	-27.755	30.891	-6.991	-2.721	11.812	13.993	-11.904	-4.656	4.693	13.617
72.000	8.827	-2.877	-26.335	27.924	-5.142	-2.316	12.679	13.876	-11.519	-4.665	5.172	13.461
74.000	3.362	-1.720	-32.445	32.664	-5.688	-2.458	13.892	15.211	-13.307	-5.198	4.223	14.897
76.000	-2.984	1.218	-32.702	32.861	-6.355	-2.850	21.202	22.317	-19.656	-7.488	6.458	22.003
78.000	-4.104	3.348	-30.967	31.417	-5.758	-2.791	26.452	27.215	-24.295	-9.144	7.173	26.932
80.000	-0.706	4.868	-21.526	22.081	-3.903	-2.154	32.157	32.464	-29.256	-10.704	8.134	32.197

DATE: 2 SEPT 1988

PAGE 27

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 22.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

POINT REL. VELOCITY ( IN./SEC.)

TIME (MSEC)	POINT ( 0.00, 0.00, 0.00) ON SEGMENT NO. 3 - UT				POINT ( 0.00, 0.00, 0.00) ON SEGMENT NO. 5 - H				POINT ( 0.00, 0.00, 0.00) ON SEGMENT NO. 5 - H			
	IN VEH REFERENCE				IN VEH REFERENCE				IN UT REFERENCE			
	X	Y	Z	RES	X	Y	Z	RES	X	Y	Z	RES
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2.000	0.357	0.000	-0.064	0.362	0.349	0.000	-0.062	0.355	-0.008	0.000	0.000	0.008
4.000	1.482	0.000	-0.168	1.491	1.463	0.000	-0.163	1.472	-0.020	0.000	0.000	0.020
6.000	3.368	-0.002	-0.329	3.384	3.332	0.000	-0.320	3.347	-0.037	0.002	0.000	0.037
8.000	6.010	-0.010	-0.534	6.034	5.944	-0.002	-0.519	5.967	-0.067	0.008	0.000	0.068
10.000	9.392	-0.024	-0.792	9.425	9.275	-0.005	-0.764	9.307	-0.120	0.019	0.000	0.121
12.000	13.502	-0.048	-1.096	13.546	13.296	-0.010	-1.048	13.338	-0.211	0.038	0.000	0.214
14.000	18.360	-0.073	-1.462	18.418	18.037	-0.016	-1.386	18.090	-0.332	0.057	0.000	0.336
16.000	23.966	-0.096	-1.885	24.040	23.526	-0.022	-1.782	23.593	-0.452	0.074	-0.001	0.458
18.000	30.318	-0.118	-2.369	30.411	29.761	-0.028	-2.239	29.845	-0.572	0.090	-0.001	0.579
20.000	37.426	-0.138	-2.913	37.539	36.747	-0.034	-2.754	36.851	-0.697	0.104	-0.001	0.704
22.000	45.254	-0.173	-3.495	45.389	44.477	-0.043	-3.312	44.601	-0.798	0.130	-0.001	0.808
24.000	53.624	-0.222	-4.417	53.806	52.814	-0.157	-4.225	52.983	-0.832	0.065	-0.001	0.835
26.000	62.779	-0.294	-5.297	63.002	61.919	-0.307	-5.089	62.128	-0.885	-0.012	0.003	0.885
28.000	72.709	-0.176	-6.137	72.968	71.793	-0.419	-5.907	72.037	-0.945	-0.242	0.010	0.975
30.000	83.403	0.352	-6.915	83.690	82.451	-0.398	-6.666	82.721	-0.986	-0.749	0.019	1.238
32.000	94.080	0.535	-7.240	94.360	93.727	-0.423	-7.110	93.997	-0.376	-0.957	0.041	1.029
34.000	104.889	0.071	-7.234	105.138	105.604	-0.633	-7.306	105.859	0.710	-0.706	0.097	1.006
36.000	116.510	-0.408	-7.277	116.737	118.233	-0.984	-7.495	118.474	1.722	-0.585	0.197	1.830
38.000	127.722	-1.024	-7.102	127.923	131.306	-1.474	-7.573	131.533	3.590	-0.474	0.404	3.643
40.000	139.233	-1.201	-6.715	139.400	145.087	-1.867	-7.440	145.290	5.849	-0.719	0.720	5.937
42.000	149.450	-0.660	-6.479	149.592	158.571	-2.237	-7.528	158.765	9.079	-1.685	1.225	9.315
44.000	155.812	-0.836	-4.740	155.887	170.774	-2.712	-6.337	170.913	14.855	-2.106	2.198	15.163
46.000	157.720	-3.088	-1.115	157.754	181.675	-3.707	-3.283	181.743	23.690	-1.112	4.061	24.061
48.000	156.096	-4.584	3.913	156.213	191.901	-4.378	0.957	191.953	35.308	-0.762	6.593	35.927
50.000	141.126	-13.942	16.832	142.808	199.739	-6.638	13.452	200.301	57.525	5.185	12.814	59.163
52.000	122.195	-24.412	32.266	128.719	206.670	-9.011	29.910	209.017	82.311	11.324	21.803	85.900
54.000	94.373	-38.752	54.224	115.535	211.079	-12.280	56.971	218.976	112.157	18.960	37.279	119.701
56.000	63.940	-52.830	78.311	114.069	213.707	-16.371	91.124	232.899	141.171	23.677	58.599	154.673
58.000	27.937	-68.681	99.258	123.894	214.085	-21.715	126.806	249.767	171.680	26.531	86.244	193.948
60.000	-48.785	-89.387	132.584	167.178	209.556	-25.937	169.668	270.875	238.362	28.911	120.368	268.591
62.000	-77.547	-101.219	145.352	193.355	203.606	-30.570	209.855	293.988	252.303	25.298	154.604	296.984
64.000	-88.016	-107.303	145.939	201.393	199.040	-34.244	238.403	312.451	249.362	19.440	183.655	310.304
66.000	-87.056	-109.586	135.436	194.758	196.297	-37.048	254.173	323.279	237.429	13.587	207.586	315.673
68.000	-81.208	-110.824	115.623	179.570	193.532	-39.896	261.153	327.486	220.628	9.256	230.063	318.891
70.000	-73.848	-112.242	90.482	161.984	189.212	-43.176	264.497	328.061	200.518	6.746	252.981	322.881
72.000	-68.106	-113.520	68.202	148.919	183.289	-46.872	268.296	328.290	181.488	4.619	273.349	328.145
74.000	-67.903	-114.780	45.146	140.795	177.090	-50.470	271.958	328.435	167.908	1.761	295.644	340.002
76.000	-74.122	-116.052	20.340	139.197	166.505	-55.141	276.103	327.105	156.313	-2.407	320.292	356.408
78.000	-83.506	-116.413	-2.649	143.291	150.797	-61.731	281.259	325.049	143.815	-8.988	343.115	372.145
80.000	-90.414	-115.111	-20.631	147.820	130.393	-69.834	287.803	323.589	126.450	-16.916	360.086	382.017

DATE: 2 SEPT 1988

PAGE 28

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 23.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

POINT REL. LINEAR DISPLACEMENT ( IN.)

TIME (MSEC)	POINT ( 0.00, 0.00, 0.00) ON SEGMENT NO. 3 - UT				POINT ( 0.00, 0.00, 0.00) ON SEGMENT NO. 5 - H				POINT ( 0.00, 0.00, 0.00) ON SEGMENT NO. 5 - H			
	IN VEH		REFERENCE		IN VEH		REFERENCE		IN UT		REFERENCE	
	X	Y	Z	RES	X	Y	Z	RES	X	Y	Z	RES
0.000	11.314	0.000	-26.938	29.217	7.775	0.000	-41.833	42.550	-0.022	0.000	-15.310	15.310
2.000	11.314	0.000	-26.938	29.218	7.775	0.000	-41.833	42.550	-0.022	0.000	-15.310	15.310
4.000	11.315	0.000	-26.938	29.218	7.777	0.000	-41.834	42.550	-0.022	0.000	-15.310	15.310
6.000	11.320	0.000	-26.939	29.221	7.782	0.000	-41.834	42.552	-0.023	0.000	-15.310	15.310
8.000	11.330	0.000	-26.940	29.225	7.791	0.000	-41.835	42.554	-0.023	0.000	-15.310	15.310
10.000	11.345	0.000	-26.941	29.232	7.806	0.000	-41.836	42.558	-0.022	0.000	-15.310	15.310
12.000	11.368	0.000	-26.943	29.243	7.828	0.000	-41.838	42.564	-0.022	0.000	-15.310	15.310
14.000	11.400	0.000	-26.945	29.257	7.860	0.000	-41.840	42.572	-0.021	0.000	-15.310	15.310
16.000	11.442	0.000	-26.949	29.277	7.901	0.000	-41.844	42.583	-0.020	0.001	-15.310	15.310
18.000	11.496	-0.001	-26.953	29.302	7.954	0.000	-41.848	42.597	-0.017	0.001	-15.310	15.310
20.000	11.564	-0.001	-26.958	29.334	8.021	0.000	-41.853	42.614	-0.015	0.001	-15.310	15.310
22.000	11.646	-0.001	-26.965	29.372	8.102	0.000	-41.859	42.636	-0.011	0.002	-15.310	15.310
24.000	11.745	-0.002	-26.972	29.419	8.199	0.000	-41.866	42.661	-0.005	0.004	-15.310	15.310
26.000	11.861	-0.002	-26.982	29.474	8.314	-0.001	-41.876	42.693	0.003	0.008	-15.310	15.310
28.000	11.996	-0.003	-26.994	29.539	8.447	-0.002	-41.887	42.730	0.014	0.016	-15.310	15.310
30.000	12.152	-0.003	-27.007	29.615	8.601	-0.003	-41.899	42.773	0.027	0.024	-15.310	15.310
32.000	12.330	-0.001	-27.021	29.701	8.777	-0.003	-41.913	42.822	0.044	0.032	-15.310	15.310
34.000	12.529	-0.001	-27.036	29.798	8.977	-0.004	-41.928	42.878	0.069	0.042	-15.310	15.310
36.000	12.750	-0.001	-27.050	29.905	9.200	-0.006	-41.943	42.940	0.102	0.058	-15.309	15.309
38.000	12.995	-0.003	-27.065	30.023	9.450	-0.008	-41.958	43.009	0.147	0.081	-15.308	15.309
40.000	13.262	-0.005	-27.079	30.152	9.726	-0.012	-41.973	43.085	0.206	0.112	-15.306	15.308
42.000	13.551	-0.007	-27.092	30.292	10.030	-0.016	-41.988	43.169	0.279	0.149	-15.303	15.306
44.000	13.857	-0.007	-27.104	30.441	10.360	-0.021	-42.002	43.261	0.371	0.191	-15.298	15.303
46.000	14.171	-0.011	-27.110	30.590	10.712	-0.027	-42.012	43.356	0.499	0.245	-15.288	15.298
48.000	14.486	-0.019	-27.107	30.735	11.086	-0.035	-42.014	43.452	0.659	0.307	-15.273	15.290
50.000	14.784	-0.037	-27.087	30.859	11.478	-0.046	-42.001	43.541	0.868	0.380	-15.247	15.276
52.000	15.048	-0.075	-27.039	30.944	11.884	-0.062	-41.958	43.609	1.144	0.470	-15.201	15.252
54.000	15.266	-0.138	-26.953	30.976	12.302	-0.083	-41.873	43.643	1.497	0.561	-15.128	15.212
56.000	15.424	-0.230	-26.821	30.940	12.727	-0.111	-41.726	43.624	1.939	0.645	-15.010	15.148
58.000	15.520	-0.349	-26.641	30.834	13.156	-0.149	-41.507	43.543	2.449	0.714	-14.836	15.054
60.000	15.493	-0.507	-26.412	30.624	13.579	-0.197	-41.214	43.394	2.991	0.751	-14.606	14.928
62.000	15.361	-0.699	-26.130	30.319	13.993	-0.253	-40.832	43.164	3.548	0.697	-14.323	14.772
64.000	15.193	-0.909	-25.837	29.987	14.395	-0.318	-40.382	42.872	4.108	0.585	-13.976	14.579
66.000	15.017	-1.126	-25.554	29.661	14.790	-0.390	-39.887	42.543	4.633	0.439	-13.579	14.354
68.000	14.848	-1.347	-25.302	29.368	15.180	-0.466	-39.371	42.199	5.107	0.285	-13.141	14.101
70.000	14.693	-1.569	-25.096	29.123	15.563	-0.549	-38.845	41.851	5.528	0.131	-12.660	13.815
72.000	14.552	-1.795	-24.938	28.929	15.936	-0.639	-38.313	41.500	5.887	-0.018	-12.144	13.496
74.000	14.417	-2.024	-24.824	28.778	16.297	-0.737	-37.772	41.145	6.179	-0.156	-11.604	13.147
76.000	14.275	-2.255	-24.759	28.668	16.641	-0.842	-37.225	40.784	6.409	-0.281	-11.038	12.767
78.000	14.118	-2.487	-24.742	28.595	16.959	-0.959	-36.667	40.411	6.577	-0.392	-10.451	12.355
80.000	13.944	-2.719	-24.766	28.551	17.242	-1.090	-36.098	40.019	6.684	-0.491	-9.851	11.915

DATE: 2 SEPT 1988

PAGE 29

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPOID FOR DASH BOARD

PAGE: 24.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

## SEGMENT ANGULAR ACCELERATION (REV/SEC.\*\*2)

TIME (MSEC)	SEGMENT NO. 3 - UT				SEGMENT NO. 5 - H				SEGMENT NO. 5 - H			
	IN	UT	REFERENCE	RES	IN	H	REFERENCE	RES	IN	VEH	REFERENCE	RES
	X	Y	Z		X	Y	Z		X	Y	Z	
0.000	0.000	-0.137	0.000	0.137	0.000	-0.185	0.000	0.185	0.000	-0.185	0.000	0.185
2.000	0.001	-0.042	0.002	0.043	-0.001	-0.052	0.000	0.052	-0.001	-0.052	0.000	0.052
4.000	0.006	0.040	0.015	0.043	-0.006	-0.067	0.000	0.067	-0.006	-0.067	0.002	0.067
6.000	-0.004	0.247	0.049	0.252	0.021	-0.177	-0.001	0.178	0.020	-0.177	-0.005	0.178
8.000	-0.039	0.665	0.129	0.678	0.107	-0.365	-0.002	0.380	0.104	-0.365	-0.027	0.380
10.000	-0.080	1.188	0.277	1.223	0.221	-0.482	0.002	0.530	0.215	-0.482	-0.050	0.530
12.000	-0.118	1.611	0.416	1.669	0.332	-0.264	0.016	0.424	0.326	-0.264	-0.062	0.424
14.000	-0.083	1.943	0.457	1.997	0.283	-0.730	0.029	0.784	0.282	-0.730	-0.038	0.784
16.000	-0.087	2.460	0.635	2.542	0.302	-1.430	0.043	1.462	0.303	-1.430	-0.029	1.462
18.000	0.008	2.589	0.664	2.673	0.141	-1.610	0.060	1.617	0.151	-1.610	0.026	1.617
20.000	0.037	2.973	0.948	3.120	0.102	-2.115	0.080	2.119	0.118	-2.115	0.054	2.119
22.000	-0.010	3.607	1.429	3.879	0.244	-3.094	0.108	3.106	0.262	-3.094	0.048	3.106
24.000	-8.600	7.157	4.790	12.171	7.768	-7.307	0.183	10.666	7.598	-7.307	-1.626	10.666
26.000	-9.914	7.450	4.950	13.353	10.014	-8.144	0.309	12.911	9.812	-8.143	-2.022	12.911
28.000	-1.602	6.837	5.335	8.819	0.731	-7.928	0.450	7.974	0.814	-7.928	0.260	7.974
30.000	-2.418	7.045	5.092	9.022	-1.971	-8.546	0.594	8.791	-1.785	-8.548	1.017	8.791
32.000	-5.518	18.566	11.214	22.381	8.491	-29.792	0.788	30.988	8.434	-29.793	-1.243	30.988
34.000	-5.789	14.342	10.997	18.977	8.985	-28.116	1.107	29.537	8.988	-28.117	-1.045	29.537
36.000	-10.236	20.115	12.679	25.887	15.101	-38.011	1.455	40.927	15.018	-38.013	-2.127	40.927
38.000	-27.100	26.891	17.134	41.846	30.178	-51.830	1.903	60.006	29.806	-51.828	-5.111	60.006
40.000	-22.699	24.663	16.092	37.182	22.068	-57.722	2.414	61.843	21.998	-57.727	-2.878	61.843
42.000	-30.498	28.252	24.219	48.113	21.827	-71.925	2.986	75.223	21.854	-71.937	-2.442	75.223
44.000	-32.187	56.105	49.690	81.565	50.733	-136.186	3.903	145.381	50.213	-136.179	-8.335	145.381
46.000	-28.042	37.572	48.859	67.714	44.955	-148.639	5.635	155.391	44.854	-148.665	-5.761	155.391
48.000	-20.702	-4.036	40.577	45.731	24.155	-149.938	7.474	152.055	24.678	-150.038	-0.423	152.055
50.000	-48.385	37.032	81.432	101.704	139.703	-302.279	11.206	333.190	138.788	-302.255	-19.874	333.190
52.000	20.899	8.412	77.489	80.698	86.870	-320.679	15.481	332.598	87.017	-320.899	-8.573	332.598
54.000	21.075	54.615	169.909	179.711	120.265	-438.481	21.646	455.190	120.241	-438.852	-12.223	455.190
56.000	15.799	22.276	164.884	167.130	113.182	-428.843	29.299	444.494	113.279	-429.795	-4.359	444.494
58.000	-70.850	-73.615	-213.885	237.035	205.076	-427.001	36.749	475.117	204.444	-428.864	3.808	475.117
60.000	213.357	-282.895	320.674	477.894	-54.947	-386.329	39.469	392.209	-56.394	-388.083	-6.237	392.209
62.000	88.426	-23.362	27.240	95.430	-20.082	-300.005	42.593	303.679	-23.448	-302.770	1.119	303.679
64.000	44.445	-34.608	-63.285	84.723	-20.168	-163.484	40.696	169.676	-26.390	-167.272	10.665	169.676
66.000	-14.123	-63.981	-141.182	155.645	35.355	-125.898	37.342	135.996	24.564	-131.014	26.957	135.996
68.000	-37.438	-24.558	-71.335	84.222	82.975	-179.967	36.180	201.450	67.795	-186.059	36.984	201.450
70.000	-38.031	-65.178	-38.947	84.920	90.968	-166.521	37.777	193.473	68.935	-174.339	47.809	193.473
72.000	-58.153	-115.779	-40.978	135.889	65.468	-76.947	39.363	108.427	34.892	-86.935	54.600	108.427
74.000	-73.956	-128.701	-33.634	152.200	71.790	-104.065	35.913	131.427	39.042	-114.114	52.218	131.427
76.000	-108.913	-153.734	-12.238	188.802	85.877	-134.273	35.927	163.386	46.823	-145.589	57.501	163.386
78.000	-133.289	-152.796	3.154	202.787	80.966	-120.334	37.667	149.849	34.375	-133.462	58.829	149.849
80.000	-132.606	-117.860	3.936	177.457	51.234	-55.968	40.143	85.842	-0.345	-70.727	48.645	85.842

DATE: 2 SEPT 1988

PAGE 30

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 25.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

## SEGMENT REL. ANGULAR VELOCITY (REV/SEC.)

TIME (MSEC)	SEGMENT NO. 3 - UT				SEGMENT NO. 5 - H				SEGMENT NO. 5 - H			
	IN VEH REFERENCE				IN VEH REFERENCE				IN H REFERENCE			
	X	Y	Z	RES	X	Y	Z	RES	X	Y	Z	RES
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
4.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
6.000	0.000	0.000	0.000	0.000	0.000	-0.001	0.000	0.001	0.000	-0.001	0.000	0.001
8.000	0.000	0.001	0.000	0.001	0.000	-0.001	0.000	0.001	0.000	-0.001	0.000	0.001
10.000	0.000	0.003	0.001	0.003	0.001	-0.002	0.000	0.002	0.001	-0.002	0.000	0.002
12.000	0.000	0.006	0.002	0.006	0.001	-0.003	0.000	0.003	0.001	-0.003	0.000	0.003
14.000	0.000	0.009	0.003	0.010	0.002	-0.004	0.000	0.004	0.002	-0.004	0.000	0.004
16.000	0.000	0.014	0.004	0.014	0.002	-0.006	0.000	0.006	0.002	-0.006	0.000	0.006
18.000	0.000	0.019	0.005	0.019	0.003	-0.009	0.000	0.009	0.003	-0.009	0.000	0.009
20.000	0.000	0.024	0.006	0.025	0.004	-0.013	0.000	0.013	0.004	-0.013	0.000	0.013
22.000	0.001	0.031	0.009	0.032	0.005	-0.018	-0.001	0.019	0.005	-0.018	0.001	0.019
24.000	-0.012	0.044	0.021	0.050	0.016	-0.031	-0.003	0.035	0.017	-0.031	0.001	0.035
26.000	-0.026	0.058	0.033	0.072	0.033	-0.046	-0.007	0.057	0.034	-0.046	0.001	0.057
28.000	-0.036	0.072	0.046	0.093	0.046	-0.062	-0.009	0.077	0.047	-0.062	0.002	0.077
30.000	-0.036	0.085	0.055	0.108	0.044	-0.078	-0.007	0.089	0.044	-0.078	0.003	0.089
32.000	-0.037	0.112	0.075	0.139	0.045	-0.114	-0.006	0.123	0.045	-0.114	0.004	0.123
34.000	-0.049	0.146	0.102	0.185	0.067	-0.174	-0.010	0.187	0.067	-0.174	0.006	0.187
36.000	-0.076	0.180	0.132	0.236	0.105	-0.236	-0.016	0.258	0.106	-0.236	0.009	0.258
38.000	-0.114	0.231	0.174	0.311	0.158	-0.331	-0.025	0.367	0.159	-0.331	0.012	0.367
40.000	-0.139	0.277	0.212	0.376	0.200	-0.436	-0.031	0.481	0.202	-0.436	0.017	0.481
42.000	-0.172	0.326	0.260	0.452	0.239	-0.565	-0.035	0.614	0.240	-0.565	0.022	0.614
44.000	-0.196	0.409	0.348	0.571	0.285	-0.766	-0.041	0.818	0.287	-0.766	0.029	0.818
46.000	-0.235	0.504	0.469	0.728	0.385	-1.056	-0.056	1.125	0.388	-1.056	0.038	1.125
48.000	-0.229	0.530	0.567	0.809	0.447	-1.355	-0.060	1.428	0.449	-1.355	0.051	1.428
50.000	-0.241	0.669	0.811	1.079	0.652	-1.933	-0.092	2.042	0.655	-1.933	0.069	2.042
52.000	-0.192	0.728	0.993	1.246	0.850	-2.558	-0.116	2.698	0.854	-2.558	0.096	2.698
54.000	-0.059	0.902	1.343	1.618	1.071	-3.411	-0.144	3.578	1.075	-3.411	0.132	3.578
56.000	0.073	1.021	1.706	1.989	1.296	-4.299	-0.161	4.493	1.300	-4.297	0.183	4.493
58.000	0.050	0.985	1.756	2.014	1.581	-5.149	-0.162	5.389	1.586	-5.144	0.249	5.389
60.000	0.638	0.350	2.155	2.274	1.585	-6.117	-0.179	6.321	1.591	-6.109	0.325	6.321
62.000	0.889	0.383	2.284	2.480	1.553	-6.864	-0.186	7.040	1.563	-6.852	0.408	7.040
64.000	0.999	0.342	2.217	2.456	1.491	-7.290	-0.171	7.443	1.512	-7.271	0.492	7.443
66.000	0.984	0.240	2.039	2.276	1.477	-7.552	-0.134	7.696	1.514	-7.524	0.570	7.696
68.000	0.901	0.147	1.885	2.095	1.563	-7.860	-0.072	8.014	1.626	-7.821	0.642	8.014
70.000	0.823	0.060	1.817	1.996	1.708	-8.236	0.012	8.412	1.807	-8.184	0.716	8.412
72.000	0.766	-0.148	1.772	1.936	1.824	-8.529	0.116	8.722	1.975	-8.458	0.794	8.722
74.000	0.692	-0.414	1.729	1.908	1.879	-8.677	0.222	8.881	2.095	-8.586	0.868	8.881
76.000	0.606	-0.733	1.717	1.963	1.971	-8.960	0.328	9.180	2.256	-8.849	0.939	9.180
78.000	0.491	-1.104	1.763	2.138	2.058	-9.256	0.445	9.492	2.428	-9.120	1.013	9.492
80.000	0.353	-1.429	1.829	2.347	2.089	-9.448	0.553	9.692	2.557	-9.285	1.090	9.692

DATE: 2 SEPT 1988

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RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPTOID FOR DASH BOARD

PAGE: 26.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

## SEGMENT REL. ANGULAR DISPLACEMENT (DEG)

TIME (MSEC)	SEGMENT NO. 3 - UT				SEGMENT NO. 5 - H				SEGMENT NO. 5 - H			
	IN VEH	REFERENCE			IN VEH	REFERENCE			IN UT	REFERENCE		
	YAW	PITCH	ROLL	RES	YAW	PITCH	ROLL	RES	YAW	PITCH	ROLL	RES
0.000	0.000	13.280	0.000	13.280	0.000	13.460	0.000	13.460	0.000	0.180	0.000	0.180
2.000	0.000	13.280	0.000	13.280	0.000	13.460	0.000	13.460	0.000	0.180	0.000	0.180
4.000	0.000	13.280	0.000	13.280	0.000	13.460	0.000	13.460	0.000	0.180	0.000	0.180
6.000	0.000	13.280	0.000	13.280	0.000	13.459	0.000	13.459	0.000	0.180	0.000	0.180
8.000	0.000	13.280	0.000	13.280	0.000	13.459	0.000	13.459	0.000	0.179	0.000	0.179
10.000	0.001	13.281	0.000	13.281	0.000	13.458	0.000	13.458	-0.001	0.176	0.000	0.176
12.000	0.001	13.284	0.000	13.284	0.000	13.456	0.001	13.456	-0.001	0.171	0.001	0.172
14.000	0.003	13.290	0.000	13.290	0.000	13.454	0.002	13.454	-0.003	0.164	0.003	0.164
16.000	0.005	13.298	0.000	13.298	0.000	13.450	0.003	13.450	-0.005	0.152	0.005	0.152
18.000	0.008	13.310	0.000	13.310	0.000	13.445	0.005	13.445	-0.008	0.135	0.007	0.136
20.000	0.012	13.325	0.000	13.325	0.000	13.437	0.008	13.437	-0.011	0.112	0.010	0.113
22.000	0.018	13.345	0.001	13.345	0.001	13.426	0.011	13.426	-0.016	0.081	0.014	0.084
24.000	0.027	13.372	-0.003	13.372	0.001	13.409	0.018	13.409	-0.025	0.037	0.027	0.052
26.000	0.043	13.409	-0.017	13.409	0.002	13.381	0.036	13.382	-0.040	-0.027	0.063	0.079
28.000	0.067	13.456	-0.042	13.456	0.003	13.343	0.067	13.343	-0.062	-0.113	0.124	0.179
30.000	0.097	13.513	-0.069	13.513	0.005	13.293	0.101	13.293	-0.089	-0.220	0.191	0.305
32.000	0.136	13.582	-0.095	13.583	0.008	13.227	0.132	13.228	-0.126	-0.354	0.257	0.455
34.000	0.193	13.675	-0.127	13.677	0.011	13.123	0.173	13.124	-0.178	-0.552	0.343	0.673
36.000	0.265	13.791	-0.175	13.795	0.017	12.978	0.237	12.980	-0.245	-0.813	0.471	0.970
38.000	0.359	13.939	-0.243	13.946	0.023	12.775	0.333	12.779	-0.332	-1.162	0.657	1.374
40.000	0.476	14.123	-0.336	14.136	0.032	12.500	0.466	12.508	-0.443	-1.620	0.910	1.907
42.000	0.617	14.341	-0.449	14.354	0.042	12.140	0.628	12.156	-0.579	-2.196	1.220	2.572
44.000	0.797	14.601	-0.582	14.638	0.055	11.672	0.813	11.700	-0.757	-2.920	1.583	3.398
46.000	1.052	14.935	-0.739	14.997	0.068	11.017	1.061	11.067	-1.018	-3.903	2.055	4.511
48.000	1.383	15.315	-0.905	15.414	0.082	10.149	1.367	10.240	-1.367	-5.141	2.620	5.902
50.000	1.837	15.754	-1.063	15.912	0.093	8.975	1.755	9.144	-1.860	-6.738	3.301	7.683
52.000	2.445	16.263	-1.213	16.515	0.095	7.361	2.304	7.712	-2.548	-8.837	4.197	10.024
54.000	3.262	16.853	-1.279	17.247	0.077	5.221	2.994	6.017	-3.499	-11.531	5.240	12.994
56.000	4.376	17.548	-1.225	18.167	0.024	2.443	3.846	4.556	-4.830	-14.954	6.468	16.740
58.000	5.730	18.282	-1.076	19.232	-0.080	-0.956	4.867	4.960	-6.520	-19.021	7.925	21.188
60.000	7.198	18.725	-0.796	20.112	-0.263	-5.032	6.043	7.858	-8.457	-23.473	9.510	26.030
62.000	9.010	18.894	-0.167	20.927	-0.545	-9.713	7.216	12.079	-10.799	-28.287	10.903	31.183
64.000	10.887	19.035	0.596	21.863	-0.927	-14.811	8.405	16.984	-13.329	-33.526	12.297	36.700
66.000	12.684	19.097	1.389	22.806	-1.407	-20.134	9.632	22.235	-15.925	-38.944	13.770	42.339
68.000	14.326	19.070	2.120	23.692	-2.012	-25.641	10.994	27.755	-18.620	-44.470	15.523	48.056
70.000	15.868	18.985	2.772	24.554	-2.808	-31.383	12.610	33.588	-21.668	-50.163	17.827	53.960
72.000	17.346	18.800	3.344	25.369	-3.876	-37.343	14.579	39.712	-25.358	-55.941	20.942	60.003
74.000	18.753	18.447	3.806	26.080	-5.305	-43.404	16.970	46.004	-30.054	-61.584	25.198	66.009
76.000	20.091	17.906	4.127	26.679	-7.292	-49.559	19.979	52.473	-36.534	-66.989	31.360	71.966
78.000	21.384	17.148	4.271	27.175	-10.213	-55.825	23.994	59.178	-46.425	-71.980	41.030	77.911
80.000	22.660	16.188	4.207	27.614	-14.704	-62.089	29.648	66.073	-62.537	-76.081	56.973	83.815

DATE: 2 SEPT 1988

PAGE 32

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 27.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

## JOINT PARAMETERS

TIME (MSEC)	STATE IPIN	JOINT NO. 3 - NP						STATE IPIN	JOINT NO. 4 - HP					
		JOINT ANGLES (DEG)			TOTAL TORQUE ( IN. LB.)				JOINT ANGLES (DEG)			TOTAL TORQUE ( IN. LB.)		
		FLEXURE	AZIMUTH	TORSION	SPRING	VISCOUS	RES.		FLEXURE	AZIMUTH	TORSION	SPRING	VISCOUS	RES.
0.000	0.	10.180	0.000	0.000	0.000	0.000	0.000	0.	10.000	0.000	0.000	0.000	0.000	0.000
2.000	0.	10.181	0.000	0.000	0.000	0.118	0.118	0.	9.999	0.000	0.000	0.000	0.118	0.118
4.000	0.	10.184	0.000	0.000	0.000	0.190	0.190	0.	9.996	0.000	0.000	0.000	0.194	0.194
6.000	0.	10.189	0.000	0.000	0.000	0.241	0.241	0.	9.991	0.000	0.000	0.000	0.263	0.263
8.000	0.	10.194	-0.001	0.000	0.000	0.224	0.224	0.	9.985	0.001	0.000	0.000	0.303	0.303
10.000	0.	10.197	-0.005	0.000	0.000	0.115	0.115	0.	9.979	0.002	0.000	0.000	0.284	0.284
12.000	0.	10.197	-0.013	-0.001	0.000	0.166	0.166	0.	9.974	0.005	0.000	0.000	0.187	0.187
14.000	0.	10.192	-0.026	-0.002	0.000	0.401	0.401	0.	9.971	0.009	-0.001	0.000	0.112	0.112
16.000	0.	10.182	-0.042	-0.003	0.000	0.680	0.680	0.	9.970	0.012	-0.002	0.000	0.069	0.069
18.000	0.	10.166	-0.061	-0.004	0.000	0.977	0.977	0.	9.969	0.013	-0.003	0.000	0.072	0.072
20.000	0.	10.144	-0.081	-0.006	0.000	1.281	1.281	0.	9.968	0.012	-0.004	0.000	0.104	0.104
22.000	0.	10.115	-0.104	-0.009	0.000	1.728	1.728	0.	9.967	0.009	-0.006	0.000	0.122	0.122
24.000	0.	10.068	-0.222	-0.013	0.000	3.586	3.586	0.	9.970	0.046	-0.009	0.000	0.771	0.771
26.000	0.	9.997	-0.530	-0.019	0.000	5.256	5.256	0.	9.977	0.134	-0.016	0.000	0.981	0.981
28.000	0.	9.907	-0.984	-0.026	0.000	6.009	6.009	0.	9.981	0.211	-0.024	0.000	0.458	0.458
30.000	0.	9.805	-1.332	-0.039	0.000	6.012	6.012	0.	9.978	0.136	-0.034	0.000	1.331	1.331
32.000	0.	9.671	-1.592	-0.058	0.000	9.657	9.657	0.	9.978	-0.039	-0.045	0.000	1.704	1.704
34.000	0.	9.440	-2.129	-0.084	0.000	14.463	14.463	0.	10.014	-0.105	-0.062	0.000	2.267	2.267
36.000	0.	9.152	-3.083	-0.113	0.000	18.782	18.782	0.	10.046	-0.075	-0.088	0.000	2.371	2.371
38.000	0.	8.767	-4.576	-0.147	0.000	26.352	26.352	0.	10.095	-0.005	-0.122	0.000	3.606	3.606
40.000	0.	8.280	-6.692	-0.188	0.000	31.362	31.362	0.	10.149	0.007	-0.163	0.000	3.348	3.348
42.000	0.	7.699	-9.366	-0.240	0.000	37.757	37.757	0.	10.197	-0.171	-0.212	0.000	4.202	4.202
44.000	0.	6.972	-12.870	-0.317	0.000	52.652	52.652	0.	10.265	-0.573	-0.269	0.000	7.887	7.887
46.000	0.	5.966	-19.595	-0.430	0.000	71.325	71.325	0.	10.445	-0.726	-0.352	0.000	11.132	11.132
48.000	0.	4.869	-30.859	-0.581	0.000	80.360	80.360	0.	10.627	-1.060	-0.464	0.000	10.999	10.999
50.000	0.	3.822	-54.577	-0.804	0.000	125.388	125.388	0.	10.957	-1.213	-0.617	0.000	25.143	25.143
52.000	0.	4.001	-95.947	-1.088	0.000	150.487	150.487	0.	11.421	-0.891	-0.839	0.000	25.934	25.934
54.000	0.	6.124	-127.683	-1.502	0.000	193.882	193.882	0.	11.949	-0.784	-1.122	0.000	32.618	32.618
56.000	0.	9.668	-143.883	-2.084	0.000	220.529	220.529	0.	12.423	-0.721	-1.497	0.000	27.056	27.056
58.000	0.	13.878	-152.083	-2.748	0.000	235.094	235.094	0.	12.563	-0.690	-1.964	0.000	26.095	26.095
60.000	0.	18.379	-157.625	-3.482	0.000	234.042	234.042	0.	12.544	-1.090	-2.446	0.000	28.518	28.518
62.000	0.	22.709	-162.883	-4.505	0.000	238.449	238.449	0.	12.127	-2.354	-2.954	0.000	43.769	43.769
64.000	0.	26.899	-167.023	-5.484	18.036	216.552	233.247	0.	11.096	-3.358	-3.457	0.000	73.428	73.428
66.000	0.	30.558	-170.082	-6.297	154.456	176.484	324.673	0.	9.293	-4.188	-3.894	0.000	115.796	115.796
68.000	0.	33.331	-172.228	-6.882	347.062	123.565	462.542	0.	6.439	-6.114	-4.250	0.000	175.281	175.281
70.000	0.	35.027	-173.783	-7.296	502.714	67.615	559.233	0.	2.361	-19.607	-4.534	0.000	244.357	244.357
72.000	0.	35.552	-174.978	-7.592	493.636	30.690	494.729	0.	3.448	-162.475	-4.760	0.000	303.225	303.225
74.000	0.	35.540	-177.910	-7.807	466.062	24.286	466.652	0.	9.415	-172.198	-4.909	0.000	300.392	300.392
76.000	0.	35.544	-175.681	-7.960	539.761	20.915	540.627	0.	15.394	-174.585	-4.988	0.000	299.780	299.780
78.000	0.	35.568	-177.364	-8.079	558.450	19.211	561.920	0.	21.358	-175.662	-5.027	0.000	295.975	295.975
80.000	0.	35.764	-178.027	-8.198	579.271	26.658	596.493	0.	27.109	-176.275	-5.046	22.243	278.693	300.921

DATE: 2 SEPT 1988

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RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 28.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

## HP JOINT FORCES &amp; TORQUES ON H IN H REFERENCE

TIME (MSEC)	JOINT FORCE ( LB. 10**2)			JOINT TORQUE ( IN.- LB. 10**2)		
	X	Y	Z	X	Y	Z
0.000	0.000	0.000	-0.126	0.000E+00	0.000E+00	0.000E+00
2.000	0.000	0.000	-0.129	-0.119E-06	0.118E-02	0.232E-07
4.000	0.001	0.000	-0.136	-0.939E-07	0.194E-02	0.765E-06
6.000	0.002	0.000	-0.142	0.273E-04	0.263E-02	0.587E-05
8.000	0.002	0.000	-0.148	0.116E-03	0.303E-02	0.258E-04
10.000	0.001	-0.001	-0.158	0.238E-03	0.283E-02	0.725E-04
12.000	-0.001	-0.001	-0.171	0.385E-03	0.183E-02	0.160E-03
14.000	-0.003	-0.001	-0.181	0.383E-03	0.101E-02	0.284E-03
16.000	-0.005	-0.001	-0.190	0.297E-03	0.458E-03	0.427E-03
18.000	-0.005	0.000	-0.202	0.148E-03	0.370E-03	0.601E-03
20.000	-0.007	0.000	-0.210	0.503E-05	0.665E-03	0.800E-03
22.000	-0.010	-0.001	-0.218	0.670E-04	0.574E-03	0.107E-02
24.000	-0.024	-0.021	-0.273	0.675E-02	-0.325E-02	0.181E-02
26.000	-0.027	-0.028	-0.270	0.883E-02	-0.301E-02	0.305E-02
28.000	-0.026	-0.002	-0.254	0.106E-02	-0.444E-03	0.444E-02
30.000	-0.029	0.004	-0.263	-0.115E-01	0.330E-02	0.586E-02
32.00	-0.097	-0.027	-0.164	-0.105E-01	-0.109E-01	0.776E-02
34.00	-0.090	-0.026	-0.153	-0.180E-02	-0.198E-01	0.108E-01
36.000	-0.123	-0.043	-0.131	0.560E-02	-0.182E-01	0.141E-01
38.000	-0.167	-0.086	-0.217	0.121E-01	-0.287E-01	0.182E-01
40.000	-0.187	-0.065	-0.200	-0.435E-02	-0.242E-01	0.227E-01
42.000	-0.235	-0.067	-0.280	-0.207E-01	-0.239E-01	0.277E-01
44.000	-0.440	-0.151	0.231	-0.200E-01	-0.675E-01	0.356E-01
46.000	-0.476	-0.133	0.180	-0.666E-02	-0.992E-01	0.500E-01
48.000	-0.484	-0.078	0.423	-0.409E-01	-0.785E-01	0.653E-01
50.000	-0.964	-0.400	1.929	0.475E-01	-0.229E+00	0.927E-01
52.000	-1.025	-0.250	2.650	0.333E-01	-0.227E+00	0.122E+00
54.000	-1.406	-0.348	4.626	0.417E-01	-0.281E+00	0.161E+00
56.000	-1.393	-0.331	5.514	0.379E-01	-0.168E+00	0.208E+00
58.000	-1.416	-0.595	5.141	0.910E-01	0.106E-01	0.244E+00
60.000	-1.296	0.123	7.496	-0.979E-01	0.101E+00	0.248E+00
62.000	-1.049	0.016	5.739	-0.807E-01	0.339E+00	0.264E+00
64.000	-0.656	0.016	3.853	-0.406E-01	0.692E+00	0.241E+00
66.000	-0.606	-0.153	1.823	-0.400E-01	0.114E+01	0.202E+00
68.000	-0.887	-0.314	1.048	-0.123E+00	0.174E+01	0.171E+00
70.000	-0.958	-0.369	1.210	-0.259E+00	0.242E+01	0.156E+00
72.000	-0.758	-0.324	1.329	-0.380E+00	0.300E+01	0.143E+00
74.000	-0.842	-0.344	1.491	-0.344E+00	0.298E+01	0.897E-01
76.000	-0.939	-0.393	2.383	-0.340E+00	0.298E+01	0.605E-01
78.000	-0.884	-0.387	3.033	-0.337E+00	0.294E+01	0.453E-01
80.000	-0.676	-0.312	3.738	-0.352E+00	0.299E+01	0.461E-01



DATE: 2 SEPT 1988

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RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 29.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

BODY PROPERTIES - REFERENCE SEGMENT NO. 16 (VEH)

INCLUDED SEGMENT NOS: 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15

TIME (MSEC)	CENTER OF GRAVITY ( IN. )			LINEAR MOMENTUM ( LB.-SEC. )			ANGULAR MOMENTUM ( IN.- LB.-SEC. )			KINETIC ENERGY ( LB.- IN. )		
	X	Y	Z	X	Y	Z	X	Y	Z	LINEAR	ANGULAR	TOTAL
0.000	18.183	0.000	-20.231	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
2.000	18.183	0.000	-20.231	-0.252E-01	0.287E-06	0.723E-04	-0.699E-04	0.197E-01	0.304E-03	0.382E-01	0.495E-02	0.431E-01
4.000	18.185	0.000	-20.231	-0.121E+00	-0.220E-04	-0.665E-02	-0.641E-03	0.993E+00	0.158E-02	0.505E+00	0.344E-01	0.539E+00
6.000	18.189	0.000	-20.231	-0.299E+00	-0.442E-03	-0.326E-01	-0.121E-01	0.341E+01	0.154E-02	0.242E+01	0.137E+00	0.256E+01
8.000	18.197	0.000	-20.231	-0.543E+00	-0.201E-02	-0.842E-01	-0.554E-01	0.730E+01	-0.472E-02	0.754E+01	0.391E+00	0.793E+01
10.000	18.210	0.000	-20.232	-0.841E+00	-0.497E-02	-0.167E+00	-0.138E+00	0.127E+02	-0.181E-01	0.184E+02	0.862E+00	0.192E+02
12.000	18.230	0.000	-20.233	-0.118E+01	-0.991E-02	-0.283E+00	-0.275E+00	0.194E+02	-0.448E-01	0.384E+02	0.155E+01	0.399E+02
14.000	18.257	0.000	-20.234	-0.155E+01	-0.150E-01	-0.435E+00	-0.416E+00	0.274E+02	-0.749E-01	0.717E+02	0.247E+01	0.742E+02
16.000	18.294	0.000	-20.236	-0.195E+01	-0.197E-01	-0.622E+00	-0.546E+00	0.366E+02	-0.995E-01	0.123E+03	0.365E+01	0.127E+03
18.000	18.342	0.000	-20.239	-0.239E+01	-0.243E-01	-0.844E+00	-0.671E+00	0.469E+02	-0.121E+00	0.200E+03	0.515E+01	0.205E+03
20.000	18.402	0.000	-20.242	-0.287E+01	-0.286E-01	-0.110E+01	-0.789E+00	0.584E+02	-0.134E+00	0.307E+03	0.698E+01	0.314E+03
22.000	18.476	0.000	-20.247	-0.340E+01	-0.356E-01	-0.140E+01	-0.982E+00	0.713E+02	-0.157E+00	0.451E+03	0.923E+01	0.461E+03
24.000	18.564	-0.001	-20.253	-0.401E+01	-0.350E-01	-0.183E+01	-0.164E+01	0.880E+02	0.204E+00	0.641E+03	0.118E+02	0.653E+03
26.000	18.669	-0.001	-20.260	-0.463E+01	-0.365E-01	-0.227E+01	-0.252E+01	0.105E+03	0.607E+00	0.886E+03	0.146E+02	0.901E+03
28.000	18.792	-0.001	-20.270	-0.528E+01	-0.204E-02	-0.270E+01	-0.226E+01	0.122E+03	0.141E+01	0.120E+04	0.179E+02	0.122E+04
30.000	18.933	-0.001	-20.280	-0.598E+01	0.973E-01	-0.311E+01	0.463E+00	0.139E+03	0.286E+01	0.158E+04	0.216E+02	0.160E+04
32.000	19.095	0.000	-20.292	-0.691E+01	0.132E+00	-0.341E+01	0.168E+01	0.160E+03	0.401E+01	0.204E+04	0.264E+02	0.206E+04
34.000	19.278	0.000	-20.306	-0.820E+01	0.583E-01	0.369E+01	-0.240E+00	0.189E+03	0.455E+01	0.256E+04	0.343E+02	0.259E+04
36.000	19.481	0.000	-20.320	-0.988E+01	0.265E-01	-0.410E+01	-0.155E+01	0.226E+03	0.628E+01	0.315E+04	0.483E+02	0.320E+04
38.000	19.704	0.001	-20.336	-0.122E+02	0.801E-01	-0.454E+01	-0.166E-01	0.277E+03	0.101E+02	0.379E+04	0.721E+02	0.386E+04
40.000	19.948	0.001	-20.354	-0.149E+02	0.324E+00	-0.494E+01	0.272E+01	0.333E+03	0.171E+02	0.449E+04	0.104E+03	0.460E+04
42.000	20.212	0.003	-20.373	-0.180E+02	0.767E+00	-0.541E+01	0.108E+02	0.400E+03	0.278E+02	0.520E+04	0.136E+03	0.533E+04
44.000	20.492	0.007	-20.393	-0.220E+02	0.103E+01	-0.537E+01	0.138E+02	0.483E+03	0.377E+02	0.576E+04	0.166E+03	0.593E+04
46.000	20.782	0.010	-20.412	-0.272E+02	0.825E+00	-0.462E+01	0.280E+01	0.583E+03	0.427E+02	0.611E+04	0.192E+03	0.631E+04
48.000	21.078	0.014	-20.426	-0.336E+02	0.103E+01	-0.313E+01	-0.118E+01	0.699E+03	0.510E+02	0.623E+04	0.206E+03	0.644E+04
50.000	21.369	0.015	-20.431	-0.431E+02	-0.477E+00	0.120E+01	-0.558E+02	0.860E+03	0.409E+02	0.588E+04	0.251E+03	0.614E+04
52.000	21.644	0.010	-20.416	-0.545E+02	-0.246E+01	0.687E+01	-0.122E+03	0.104E+04	0.198E+02	0.539E+04	0.363E+03	0.575E+04
54.000	21.894	-0.005	-20.377	-0.685E+02	-0.545E+01	0.145E+02	-0.211E+03	0.126E+04	-0.927E+01	0.491E+04	0.673E+03	0.558E+04
56.000	22.111	-0.030	-20.309	-0.834E+02	-0.852E+01	0.720E+02	-0.295E+03	0.151E+04	-0.346E+02	0.471E+04	0.104E+04	0.574E+04
58.000	22.290	-0.069	-20.216	-0.991E+02	-0.135E+02	0.279E+02	-0.411E+03	0.179E+04	-0.797E+02	0.476E+04	0.128E+04	0.604E+04
60.000	22.406	-0.126	-20.096	-0.125E+03	-0.182E+02	0.375E+02	-0.524E+03	0.227E+04	-0.120E+03	0.581E+04	0.201E+04	0.782E+04
62.000	22.463	-0.202	-19.952	-0.140E+03	-0.221E+02	0.392E+02	-0.608E+03	0.259E+04	-0.146E+03	0.655E+04	0.226E+04	0.881E+04
64.000	22.487	-0.287	-19.810	-0.150E+03	-0.237E+02	0.370E+02	-0.647E+03	0.284E+04	-0.148E+03	0.673E+04	0.223E+04	0.896E+04
66.000	22.490	-0.376	-19.683	-0.158E+03	-0.241E+02	0.311E+02	-0.659E+03	0.306E+04	-0.145E+03	0.640E+04	0.206E+04	0.846E+04
68.000	22.476	-0.465	-19.584	-0.166E+03	-0.239E+02	0.220E+02	-0.658E+03	0.329E+04	-0.144E+03	0.579E+04	0.189E+04	0.768E+04
70.000	22.446	-0.552	-19.523	-0.171E+03	-0.235E+02	0.114E+02	-0.651E+03	0.348E+04	-0.141E+03	0.524E+04	0.177E+04	0.700E+04
72.000	22.406	-0.640	-19.495	-0.175E+03	-0.237E+02	0.416E+01	-0.648E+03	0.360E+04	-0.142E+03	0.484E+04	0.164E+04	0.648E+04
74.000	22.358	-0.728	-19.490	-0.180E+03	-0.238E+02	-0.130E+01	-0.646E+03	0.369E+04	-0.147E+03	0.453E+04	0.150E+04	0.604E+04
76.000	22.298	-0.816	-19.505	-0.183E+03	-0.240E+02	-0.635E+01	-0.648E+03	0.377E+04	-0.156E+03	0.443E+04	0.143E+04	0.587E+04
78.000	22.233	-0.905	-19.537	-0.185E+03	-0.242E+02	-0.114E+02	-0.655E+03	0.383E+04	-0.166E+03	0.456E+04	0.146E+04	0.602E+04
80.000	22.165	-0.995	-19.588	-0.186E+03	-0.244E+02	-0.161E+02	-0.659E+03	0.386E+04	-0.170E+03	0.477E+04	0.155E+04	0.632E+04

DATE: 2 SEPT 1988

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 30.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

CONTACT FORCES - SEGMENT PANELS VS. SEGMENTS

TIME (MSEC)	PANEL 1 (SEAT. 6 DEGREE OFF H) VS. SEGMENT 1 ( LT )							PANEL 1 (SEAT. 6 DEGREE OFF H) VS. SEGMENT 6 ( RUL )						
	DEFL- ECTION ( IN. )	NORMAL FORCE ( LB. )	FRICTION FORCE ( LB. )	RESULTANT FORCE ( LB. )	CONTACT (VEH REFERENCE)	LOCATION ( IN. )		DEFL- ECTION ( IN. )	NORMAL FORCE ( LB. )	FRICTION FORCE ( LB. )	RESULTANT FORCE ( LB. )	CONTACT (VEH REFERENCE)	LOCATION ( IN. )	
					X	Y	Z					X	Y	Z
0.000	0.458	137.10	0.00	137.10	14.372	0.000	-10.459	0.250	29.94	0.00	29.94	24.725	3.420	-11.545
2.000	0.458	137.02	8.94	137.31	14.373	0.000	-10.459	0.250	31.22	4.99	31.62	24.725	3.420	-11.545
4.000	0.458	136.86	27.51	139.60	14.375	0.000	-10.459	0.250	36.69	15.37	39.79	24.726	3.420	-11.545
6.000	0.458	136.72	46.60	144.44	14.380	0.000	-10.460	0.250	44.22	22.11	49.44	24.727	3.420	-11.545
8.000	0.457	138.78	64.83	153.18	14.390	0.000	-10.461	0.251	51.70	25.85	57.80	24.729	3.420	-11.546
10.000	0.458	144.58	72.29	161.65	14.407	0.000	-10.462	0.251	58.35	29.18	65.24	24.732	3.420	-11.546
12.000	0.458	152.48	76.24	170.48	14.431	0.000	-10.465	0.252	63.83	31.91	71.36	24.737	3.420	-11.546
14.000	0.458	161.71	80.85	180.80	14.464	0.000	-10.468	0.253	68.37	34.18	76.44	24.744	3.420	-11.547
16.000	0.459	172.39	86.19	192.73	14.508	0.000	-10.473	0.254	72.13	36.06	80.64	24.755	3.420	-11.548
18.000	0.459	184.02	92.01	205.74	14.565	-0.001	-10.479	0.255	75.12	37.56	83.99	24.770	3.420	-11.550
20.000	0.460	196.74	98.37	219.96	14.635	-0.001	-10.486	0.256	76.24	38.12	85.24	24.790	3.420	-11.552
22.000	0.461	211.45	105.72	236.41	14.720	-0.001	-10.495	0.257	74.47	37.23	83.26	24.816	3.420	-11.555
24.000	0.463	200.50	100.25	224.17	14.822	-0.001	-10.506	0.257	66.45	33.22	74.29	24.849	3.420	-11.558
26.000	0.464	199.45	99.72	222.99	14.942	-0.001	-10.519	0.257	58.64	29.32	65.56	24.891	3.420	-11.563
28.000	0.465	207.89	103.94	232.42	15.081	0.000	-10.533	0.256	49.90	24.95	55.79	24.942	3.420	-11.568
30.000	0.466	228.27	114.13	255.21	15.242	0.001	-10.550	0.255	45.48	22.74	50.85	25.002	3.420	-11.574
32.000	0.468	279.53	139.76	312.52	15.424	0.006	-10.569	0.253	53.74	26.87	60.08	25.069	3.421	-11.581
34.000	0.472	356.68	178.34	398.78	15.630	0.016	-10.591	0.251	53.97	26.99	60.35	25.138	3.421	-11.589
36.000	0.478	448.62	224.31	501.57	15.859	0.038	-10.615	0.248	38.40	19.20	42.93	25.207	3.421	-11.596
38.000	0.485	560.72	280.36	626.90	16.111	0.079	-10.641	0.244	37.83	18.91	42.29	25.272	3.422	-11.603
40.000	0.496	634.27	317.14	709.14	16.385	0.146	-10.670	0.239	65.17	32.59	72.87	25.325	3.424	-11.608
42.000	0.510	664.96	332.48	743.44	16.679	0.237	-10.701	0.234	89.40	44.70	99.96	25.364	3.428	-11.612
44.000	0.527	703.41	351.70	786.43	16.985	0.346	-10.733	0.230	119.38	59.69	133.47	25.391	3.434	-11.615
46.000	0.551	756.42	378.21	845.71	17.293	0.460	-10.765	0.227	157.62	78.81	176.23	25.402	3.441	-11.616
48.000	0.585	828.62	414.31	926.43	17.592	0.567	-10.797	0.225	201.14	100.57	224.88	25.394	3.451	-11.615
50.000	0.634	922.91	461.45	1031.84	17.867	0.638	-10.826	0.225	230.71	115.35	257.94	25.366	3.464	-11.613
52.000	0.705	1043.08	521.54	1166.20	18.102	0.630	-10.850	0.225	229.76	114.88	256.88	25.326	3.480	-11.608
54.000	0.806	1090.42	545.21	1219.13	18.285	0.526	-10.869	0.227	275.31	137.65	307.80	25.267	3.497	-11.602
56.000	0.942	1085.51	542.75	1213.64	18.410	0.360	-10.883	0.237	287.36	143.68	321.28	25.149	3.514	-11.590
58.000	1.113	1255.01	627.50	1403.14	18.483	0.194	-10.890	0.263	319.11	159.55	356.77	24.927	3.526	-11.567
60.000	1.323	1450.74	725.37	1621.98	18.497	0.037	-10.892	0.312	369.55	184.78	413.17	24.589	3.526	-11.531
62.000	1.576	1827.33	913.67	2043.02	18.468	-0.132	-10.889	0.373	440.16	220.08	492.11	24.222	3.511	-11.493
64.000	1.825	2293.38	1146.69	2564.07	18.450	-0.237	-10.887	0.443	571.58	285.79	639.04	23.850	3.487	-11.453
66.000	2.046	2723.02	1361.51	3044.43	18.439	-0.287	-10.886	0.512	745.66	372.83	833.68	23.509	3.460	-11.418
68.000	2.217	3434.09	1717.05	3839.43	18.418	-0.298	-10.883	0.565	895.39	447.69	1001.07	23.230	3.435	-11.388
70.000	2.318	3801.87	1900.93	4250.62	18.370	-0.288	-10.878	0.584	304.97	152.49	340.97	23.046	3.419	-11.369
72.000	2.356	2969.04	1484.52	3319.48	18.300	-0.277	-10.871	0.565	279.61	139.80	312.61	22.958	3.408	-11.360
74.000	2.342	2947.61	1473.80	3295.52	18.218	-0.271	-10.862	0.515	213.84	106.92	239.08	22.945	3.400	-11.359
76.000	2.282	2851.26	210.71	2859.04	18.125	-0.274	-10.853	0.436	108.38	54.19	121.18	23.013	3.395	-11.366
78.000	2.180	2688.19	119.57	2690.85	18.036	-0.252	-10.843	0.328	45.26	22.78	50.93	23.161	3.390	-11.381
80.000	2.039	2461.74	235.32	2472.96	17.954	-0.332	-10.835	0.191	18.66	9.33	20.85	23.244	3.381	-11.390

DATE: 2 SEPT 1988

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 31.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

CONTACT FORCES - SEGMENT PANELS VS. SEGMENTS

TIME (MSEC)	PANEL 1 (SEAT. 6 DEGREE OFF H) VS. SEGMENT 9 ( LUL )							PANEL 2 (BACK PANEL. 13 DEGR) VS. SEGMENT 1 ( LT )						
	DEFL- ECTION ( IN. )	NORMAL FORCE ( LB. )	FRICTION FORCE ( LB. )	RESULTANT FORCE ( LB. )	CONTACT LOCATION ( IN. ) (VEH REFERENCE)			DEFL- ECTION ( IN. )	NORMAL FORCE ( LB. )	FRICTION FORCE ( LB. )	RESULTANT FORCE ( LB. )	CONTACT LOCATION ( IN. ) (VEH REFERENCE)		
					X	Y	Z					X	Y	Z
0.000	0.250	29.94	0.00	29.94	24.725	-3.420	-11.545	0.055	2.77	0.00	2.77	9.382	0.000	-12.674
2.000	0.250	31.23	5.00	31.62	24.725	-3.420	-11.545	0.055	2.76	0.40	2.79	9.382	0.000	-12.674
4.000	0.250	36.71	15.41	39.81	24.726	-3.420	-11.545	0.054	2.68	0.97	2.85	9.382	0.000	-12.675
6.000	0.250	44.24	22.12	49.46	24.727	-3.420	-11.545	0.050	2.51	1.25	2.80	9.382	0.000	-12.676
8.000	0.251	51.74	25.87	57.84	24.729	-3.420	-11.546	0.044	2.18	1.09	2.44	9.382	0.000	-12.677
10.000	0.251	58.41	29.21	65.30	24.732	-3.420	-11.546	0.033	1.65	0.83	1.85	9.381	0.000	-12.680
12.000	0.252	63.91	31.95	71.45	24.737	-3.420	-11.546	0.017	0.86	0.43	0.96	9.380	0.000	-12.684
14.000	0.253	68.45	34.23	76.53	24.744	-3.420	-11.547	-0.006	0.00	0.00	0.00	0.000	0.000	0.000
16.000	0.254	72.21	36.10	80.73	24.755	-3.420	-11.548	-0.036	0.00	0.00	0.00	0.000	0.000	0.000
18.000	0.255	75.19	37.60	84.07	24.770	-3.420	-11.550	-0.077	0.00	0.00	0.00	0.000	0.000	0.000
20.000	0.256	76.31	38.16	85.32	24.790	-3.420	-11.552	-0.128	0.00	0.00	0.00	0.000	0.000	0.000
22.000	0.257	74.63	37.31	83.43	24.815	-3.420	-11.555	-0.192	0.00	0.00	0.00	0.000	0.000	0.000
24.000	0.257	65.18	32.59	72.87	24.849	-3.420	-11.558	-0.269	0.00	0.00	0.00	0.000	0.000	0.000
26.000	0.257	56.40	28.20	63.06	24.891	-3.420	-11.563	-0.362	0.00	0.00	0.00	0.000	0.000	0.000
28.000	0.256	47.59	23.79	53.20	24.943	-3.420	-11.568	-0.472	0.00	0.00	0.00	0.000	0.000	0.000
30.000	0.254	34.68	17.34	38.78	25.005	-3.420	-11.575	-0.601	0.00	0.00	0.00	0.000	0.000	0.000
32.000	0.252	30.42	15.21	34.01	25.079	-3.419	-11.582	-0.749	0.00	0.00	0.00	0.000	0.000	0.000
34.000	0.248	29.66	14.83	33.16	25.168	-3.419	-11.592	-0.918	0.00	0.00	0.00	0.000	0.000	0.000
36.000	0.241	28.14	14.07	31.46	25.280	-3.419	-11.604	-1.198	0.00	0.00	0.00	0.000	0.000	0.000
38.000	0.227	25.44	12.72	28.44	25.426	-3.418	-11.619	-1.317	0.00	0.00	0.00	0.000	0.000	0.000
40.000	0.206	21.30	10.65	23.81	25.615	-3.415	-11.639	-1.546	0.00	0.00	0.00	0.000	0.000	0.000
42.000	0.179	16.89	8.45	18.89	25.850	-3.411	-11.663	-1.794	0.00	0.00	0.00	0.000	0.000	0.000
44.000	0.147	12.03	6.01	13.45	26.130	-3.405	-11.693	-2.056	0.00	0.00	0.00	0.000	0.000	0.000
46.000	0.112	6.87	3.43	7.68	26.435	-3.396	-11.725	-2.328	0.00	0.00	0.00	0.000	0.000	0.000
48.000	0.080	3.99	1.99	4.46	26.760	-3.386	-11.759	-2.601	0.00	0.00	0.00	0.000	0.000	0.000
50.000	0.056	2.78	1.39	3.11	27.008	-3.372	-11.785	-2.864	0.00	0.00	0.00	0.000	0.000	0.000
52.000	0.051	58.93	29.46	65.88	27.020	-3.355	-11.786	-3.104	0.00	0.00	0.00	0.000	0.000	0.000
54.000	0.076	84.08	42.04	94.01	26.648	-3.335	-11.747	-3.311	0.00	0.00	0.00	0.000	0.000	0.000
56.000	0.137	138.11	69.06	154.41	26.015	-3.313	-11.681	-3.479	0.00	0.00	0.00	0.000	0.000	0.000
58.000	0.228	165.60	82.80	185.14	25.312	-3.292	-11.607	-3.609	0.00	0.00	0.00	0.000	0.000	0.000
60.000	0.353	148.11	74.06	165.60	24.605	-3.280	-11.533	-3.695	0.00	0.00	0.00	0.000	0.000	0.000
62.000	0.522	357.14	178.57	399.30	23.920	-3.280	-11.461	-3.747	0.00	0.00	0.00	0.000	0.000	0.000
64.000	0.684	686.47	343.24	767.50	23.448	-3.290	-11.411	-3.784	0.00	0.00	0.00	0.000	0.000	0.000
66.000	0.819	1246.33	623.16	1393.44	23.155	-3.301	-11.380	-3.811	0.00	0.00	0.00	0.000	0.000	0.000
68.000	0.905	1699.87	849.94	1900.52	22.994	-3.313	-11.364	-3.828	0.00	0.00	0.00	0.000	0.000	0.000
70.000	0.924	758.55	379.27	848.08	22.932	-3.322	-11.357	-3.837	0.00	0.00	0.00	0.000	0.000	0.000
72.000	0.888	710.46	355.23	794.31	22.936	-3.329	-11.358	-3.838	0.00	0.00	0.00	0.000	0.000	0.000
74.000	0.814	611.98	305.99	684.21	22.992	-3.333	-11.363	-3.831	0.00	0.00	0.00	0.000	0.000	0.000
76.000	0.713	477.86	238.93	534.26	23.096	-3.334	-11.374	-3.811	0.00	0.00	0.00	0.000	0.000	0.000
78.000	0.591	314.21	157.11	351.30	23.266	-3.333	-11.392	-3.793	0.00	0.00	0.00	0.000	0.000	0.000
80.000	0.450	126.56	63.28	141.50	23.529	-3.333	-11.420	-3.762	0.00	0.00	0.00	0.000	0.000	0.000

DATE: 2 SEPT 1988

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RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 32.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

CONTACT FORCES - SEGMENT PANELS VS. SEGMENTS

TIME (MSEC)	PANEL 2 (BACK PANEL. 13 DEGR) VS. SEGMENT 2 ( CT )							PANEL 2 (BACK PANEL. 13 DEGR) VS. SEGMENT 3 ( UT )						
	DEFL- ECTION	NORMAL FORCE	FRICTION FORCE	RESULTANT FORCE	CONTACT LOCATION ( IN. )			DEFL- ECTION	NORMAL FORCE	FRICTION FORCE	RESULTANT FORCE	CONTACT LOCATION ( IN. )		
	( IN. )	( LB. )	( LB. )	( LB. )	(VEH X	REFERENCE Y	Z	( IN. )	( LB. )	( LB. )	( LB. )	(VEH X	REFERENCE Y	Z
0.000	-0.312	0.00	0.00	0.00	0.000	0.000	0.000	0.133	9.90	0.00	9.90	6.151	0.000	-26.665
2.000	-0.312	0.00	0.00	0.00	0.000	0.000	0.000	9.132	9.87	0.06	9.87	6.151	0.000	-26.665
4.000	-0.314	0.00	0.00	0.00	0.000	0.000	0.000	0.131	9.61	0.75	9.64	6.151	0.000	-26.665
6.000	-0.320	0.00	0.00	0.00	0.000	0.000	0.000	0.126	8.90	1.74	9.07	6.151	0.000	-26.664
8.000	-0.330	0.00	0.00	0.00	0.000	0.000	0.000	0.117	7.52	2.55	7.94	6.152	0.000	-26.663
10.000	-0.347	0.00	0.00	0.00	0.000	0.000	0.000	0.102	5.25	2.42	5.77	6.152	0.000	-26.661
12.000	-0.372	0.00	0.00	0.00	0.000	0.000	0.000	0.079	3.95	1.98	4.42	6.153	0.000	-26.658
14.000	-0.406	0.00	0.00	0.00	0.000	0.000	0.000	0.048	2.38	1.19	2.66	6.154	0.000	-26.654
16.000	-0.452	0.00	0.00	0.00	0.000	0.000	0.000	0.006	0.30	0.15	0.33	6.155	0.000	-26.649
18.000	-0.510	0.00	0.00	0.00	0.000	0.000	0.000	-0.048	0.00	0.00	0.00	0.000	0.000	0.000
20.000	-0.583	0.00	0.00	0.00	0.000	0.000	0.000	-0.114	0.00	0.00	0.00	0.000	0.000	0.000
22.000	-0.671	0.00	0.00	0.00	0.000	0.000	0.000	-0.196	0.00	0.00	0.00	0.000	0.000	0.000
24.000	-0.776	0.00	0.00	0.00	0.000	0.000	0.000	-0.294	0.00	0.00	0.00	0.000	0.000	0.000
26.000	-0.901	0.00	0.00	0.00	0.000	0.000	0.000	-0.409	0.00	0.00	0.00	0.000	0.000	0.000
28.000	-1.045	0.00	0.00	0.00	0.000	0.000	0.000	-0.542	0.00	0.00	0.00	0.000	0.000	0.000
30.000	-1.211	0.00	0.00	0.00	0.000	0.000	0.000	-0.696	0.00	0.00	0.00	0.000	0.000	0.000
32.000	-1.400	0.00	0.00	0.00	0.000	0.000	0.000	-0.872	0.00	0.00	0.00	0.000	0.000	0.000
34.000	-1.612	0.00	0.00	0.00	0.000	0.000	0.000	-1.067	0.00	0.00	0.00	0.000	0.000	0.000
36.000	-1.849	0.00	0.00	0.00	0.000	0.000	0.000	-1.284	0.00	0.00	0.00	0.000	0.000	0.000
38.000	-2.110	0.00	0.00	0.00	0.000	0.000	0.000	-1.523	0.00	0.00	0.00	0.000	0.000	0.000
40.000	-2.397	0.00	0.00	0.00	0.000	0.000	0.000	-1.783	0.00	0.00	0.00	0.000	0.000	0.000
42.000	-2.707	0.00	0.00	0.00	0.000	0.000	0.000	-2.064	0.00	0.00	0.00	0.000	0.000	0.000
44.000	-3.034	0.00	0.00	0.00	0.000	0.000	0.000	-2.361	0.00	0.00	0.00	0.000	0.000	0.000
46.000	-3.370	0.00	0.00	0.00	0.000	0.000	0.000	-2.662	0.00	0.00	0.00	0.000	0.000	0.000
48.000	-3.702	0.00	0.00	0.00	0.000	0.000	0.000	-2.960	0.00	0.00	0.00	0.000	0.000	0.000
50.000	-4.012	0.00	0.00	0.00	0.000	0.000	0.000	-3.238	0.00	0.00	0.00	0.000	0.000	0.000
52.000	-4.276	0.00	0.00	0.00	0.000	0.000	0.000	-3.473	0.00	0.00	0.00	0.000	0.000	0.000
54.000	-4.477	0.00	0.00	0.00	0.000	0.000	0.000	-3.652	0.00	0.00	0.00	0.000	0.000	0.000
56.000	-4.606	0.00	0.00	0.00	0.000	0.000	0.000	-3.757	0.00	0.00	0.00	0.000	0.000	0.000
58.000	-4.661	0.00	0.00	0.00	0.000	0.000	0.000	-3.787	0.00	0.00	0.00	0.000	0.000	0.000
60.000	-4.582	0.00	0.00	0.00	0.000	0.000	0.000	-3.687	0.00	0.00	0.00	0.000	0.000	0.000
62.000	-4.378	0.00	0.00	0.00	0.000	0.000	0.000	-3.478	0.00	0.00	0.00	0.000	0.000	0.000
64.000	-4.177	0.00	0.00	0.00	0.000	0.000	0.000	-3.225	0.00	0.00	0.00	0.000	0.000	0.000
66.000	-3.915	0.00	0.00	0.00	0.000	0.000	0.000	-2.965	0.00	0.00	0.00	0.000	0.000	0.000
68.000	-3.689	0.00	0.00	0.00	0.000	0.000	0.000	-2.720	0.00	0.00	0.00	0.000	0.000	0.000
70.000	-3.476	0.00	0.00	0.00	0.000	0.000	0.000	-2.499	0.00	0.00	0.00	0.000	0.000	0.000
72.000	-3.281	0.00	0.00	0.00	0.000	0.000	0.000	-2.303	0.00	0.00	0.00	0.000	0.000	0.000
74.000	-3.098	0.00	0.00	0.00	0.000	0.000	0.000	-2.127	0.00	0.00	0.00	0.000	0.000	0.000
76.000	-2.921	0.00	0.00	0.00	0.000	0.000	0.000	-1.960	0.00	0.00	0.00	0.000	0.000	0.000
78.000	-2.744	0.00	0.00	0.00	0.000	0.000	0.000	-1.791	0.00	0.00	0.00	0.000	0.000	0.000
80.000	-2.561	0.00	0.00	0.00	0.000	0.000	0.000	-1.618	0.00	0.00	0.00	0.000	0.000	0.000

DATE: 2 SEPT 1988

PAGE 38

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 33.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

CONTACT FORCES - SEGMENT PANELS VS. SEGMENTS

TIME (MSEC)	PANEL 3 (FLOOR.) VS. SEGMENT 8 ( RF )							PANEL 3 (FLOOR.) VS. SEGMENT 11 ( LF )						
	DEFL- ECTION	NORMAL FORCE	FRICTION FORCE	RESULTANT FORCE	CONTACT (VEH	LOCATION ( IN.) REFERENCE)		DEFL- ECTION	NORMAL FORCE	FRICTION FORCE	RESULTANT FORCE	CONTACT (VEH	LOCATION ( IN.) REFERENCE)	
	( IN.)	( LB.)	( LB.)	( LB.)	X	Y	Z	( IN.)	( LB.)	( LB.)	( LB.)	X	Y	Z
0.000	0.096	4.82	0.00	4.82	46.596	3.420	-1.300	0.096	4.82	0.00	4.82	46.596	-3.420	-1.300
2.000	0.097	4.88	0.97	4.98	46.596	3.420	-1.300	0.097	4.88	0.97	4.98	46.596	-3.420	-1.300
4.000	0.097	4.97	2.11	5.40	46.597	3.420	-1.300	0.097	4.98	2.11	5.40	46.597	-3.420	-1.300
6.000	0.097	5.05	2.52	5.64	46.601	3.420	-1.300	0.097	5.05	2.52	5.64	46.601	-3.420	-1.300
8.000	0.098	5.02	2.51	5.62	46.609	3.420	-1.300	0.098	5.03	2.52	5.62	46.609	-3.420	-1.300
10.000	0.098	4.90	2.45	5.48	46.620	3.420	-1.300	0.098	4.91	2.46	5.49	46.620	-3.420	-1.300
12.000	0.098	4.88	2.44	5.46	46.638	3.420	-1.300	0.098	4.89	2.44	5.46	46.638	-3.420	-1.300
14.000	0.097	4.83	2.42	5.41	46.662	3.420	-1.300	0.097	4.84	2.42	5.41	46.662	-3.420	-1.300
16.000	0.095	4.75	2.37	5.31	46.693	3.420	-1.300	0.095	4.76	2.38	5.32	46.694	-3.420	-1.300
18.000	0.092	4.61	2.31	5.16	46.734	3.420	-1.300	0.093	4.63	2.31	5.17	46.734	-3.420	-1.300
20.000	0.088	4.42	2.21	4.94	46.784	3.420	-1.300	0.089	4.44	2.22	4.97	46.784	-3.420	-1.300
22.000	0.083	4.17	2.00	4.66	46.844	3.420	-1.300	0.084	4.19	2.10	4.69	46.845	-3.420	-1.300
24.000	0.077	3.85	1.92	4.30	46.915	3.420	-1.300	0.078	3.88	1.94	4.34	46.916	-3.420	-1.300
26.000	0.069	3.46	1.73	3.86	46.998	3.420	-1.300	0.070	3.50	1.75	3.91	46.999	-3.420	-1.300
28.000	0.060	2.99	1.50	3.35	47.092	3.420	-1.300	0.061	3.05	1.52	3.41	47.093	-3.420	-1.300
30.000	0.049	2.46	1.23	2.75	47.199	3.420	-1.300	0.051	2.54	1.27	2.83	47.201	-3.420	-1.300
32.000	0.037	1.85	0.93	2.07	47.318	3.420	-1.300	0.040	1.98	0.99	2.21	47.322	-3.420	-1.300
34.000	0.022	1.12	0.56	1.26	47.448	3.420	-1.300	0.027	1.36	0.68	1.52	47.456	-3.420	-1.300
36.000	0.004	0.19	0.10	0.21	47.583	3.420	-1.300	0.013	0.65	0.32	0.73	47.597	-3.420	-1.300
38.000	-0.021	0.00	0.00	0.00	0.000	0.000	0.000	-0.004	0.00	0.00	0.00	0.000	0.000	0.000
40.000	-0.052	0.00	0.00	0.00	0.000	0.000	0.000	-0.024	0.00	0.00	0.00	0.000	0.000	0.000
42.000	-0.092	0.00	0.00	0.00	0.000	0.000	0.000	-0.047	0.00	0.00	0.00	0.000	0.000	0.000
44.000	-0.140	0.00	0.00	0.00	0.000	0.000	0.000	-0.072	0.00	0.00	0.00	0.000	0.000	0.000
46.000	-0.199	0.00	0.00	0.00	0.000	0.000	0.000	-0.101	0.00	0.00	0.00	0.000	0.000	0.000
48.000	-0.268	0.00	0.00	0.00	0.000	0.000	0.000	-0.137	0.00	0.00	0.00	0.000	0.000	0.000
50.000	-0.348	0.00	0.00	0.00	0.000	0.000	0.000	-0.183	0.00	0.00	0.00	0.000	0.000	0.000
52.000	-0.40	0.00	0.00	0.00	0.000	0.000	0.000	-0.245	0.00	0.00	0.00	0.000	0.000	0.000
54.000	-0.543	0.00	0.00	0.00	0.000	0.000	0.000	-0.330	0.00	0.00	0.00	0.000	0.000	0.000
56.000	-0.661	0.00	0.00	0.00	0.000	0.000	0.000	-0.434	0.00	0.00	0.00	0.000	0.000	0.000
58.000	-0.798	0.00	0.00	0.00	0.000	0.000	0.000	-0.554	0.00	0.00	0.00	0.000	0.000	0.000
60.000	-0.960	0.00	0.00	0.00	0.000	0.000	0.000	-0.686	0.00	0.00	0.00	0.000	0.000	0.000
62.000	-1.145	0.00	0.00	0.00	0.000	0.000	0.000	-0.830	0.00	0.00	0.00	0.000	0.000	0.000
64.000	-1.351	0.00	0.00	0.00	0.000	0.000	0.000	-0.974	0.00	0.00	0.00	0.000	0.000	0.000
66.000	-1.576	0.00	0.00	0.00	0.000	0.000	0.000	-1.122	0.00	0.00	0.00	0.000	0.000	0.000
68.000	-1.817	0.00	0.00	0.00	0.000	0.000	0.000	-1.277	0.00	0.00	0.00	0.000	0.000	0.000
70.000	-2.071	0.00	0.00	0.00	0.000	0.000	0.000	-1.446	0.00	0.00	0.00	0.000	0.000	0.000
72.000	-2.335	0.00	0.00	0.00	0.000	0.000	0.000	-1.625	0.00	0.00	0.00	0.000	0.000	0.000
74.000	-2.606	0.00	0.00	0.00	0.000	0.000	0.000	-1.812	0.00	0.00	0.00	0.000	0.000	0.000
76.000	-2.883	0.00	0.00	0.00	0.000	0.000	0.000	-2.005	0.00	0.00	0.00	0.000	0.000	0.000
78.000	-3.160	0.00	0.00	0.00	0.000	0.000	0.000	-2.199	0.00	0.00	0.00	0.000	0.000	0.000
80.000	-3.434	0.00	0.00	0.00	0.000	0.000	0.000	-2.387	0.00	0.00	0.00	0.000	0.000	0.000

DATE: 2 SEPT 1988

PAGE 39

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 34.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

CONTACT FORCES - SEGMENT PANELS VS. SEGMENTS

TIME (MSEC)	PANEL 4 (HEAD PAD. 13 DEGR ) VS. SEGMENT 5 ( H )							PANEL 10 (RUDDER PEDALS. ) VS. SEGMENT 8 ( RF )						
	DEFL- ECTION	NORMAL FORCE	FRICTION FORCE	RESULTANT FORCE	CONTACT LOCATION ( IN. )			DEFL- ECTION	NORMAL FORCE	FRICTION FORCE	RESULTANT FORCE	CONTACT LOCATION ( IN. )		
	( IN. )	( LB. )	( LB. )	( LB. )	(VEH X	REFERENCE) Y	Z	( IN. )	( LB. )	( LB. )	( LB. )	(VEH X	REFERENCE) Y	Z
0.000	0.050	2.48	0.00	2.48	3.935	0.000	-40.978	0.002	0.08	0.00	0.08	51.239	3.420	-3.286
2.000	0.049	2.47	0.02	2.47	3.935	0.000	-40.978	0.001	0.07	0.01	0.07	51.239	3.420	-3.286
4.000	0.048	2.38	0.19	2.39	3.935	0.000	-40.978	0.002	0.11	0.04	0.12	51.239	3.420	-3.285
6.000	0.043	2.15	0.41	2.19	3.935	0.000	-40.977	0.005	0.29	0.14	0.32	51.240	3.420	-3.287
8.000	0.034	1.70	0.55	1.78	3.935	0.000	-40.976	0.010	0.75	0.37	0.83	51.245	3.420	-3.291
10.000	0.019	0.95	0.41	1.03	3.936	0.000	-40.974	0.019	1.59	0.80	1.78	51.254	3.420	-3.298
12.000	-0.003	0.00	0.00	0.00	0.000	0.000	0.000	0.031	2.66	1.33	2.98	51.266	3.420	-3.309
14.000	-0.034	0.00	0.00	0.00	0.000	0.000	0.000	0.048	4.09	2.05	4.58	51.284	3.420	-3.323
16.000	-0.075	0.00	0.00	0.00	0.000	0.000	0.000	0.070	5.92	2.96	6.62	51.306	3.420	-3.342
18.000	-0.128	0.00	0.00	0.00	0.000	0.000	0.000	0.096	8.17	4.08	9.13	51.334	3.420	-3.365
20.000	-0.194	0.00	0.00	0.00	0.000	0.000	0.000	0.128	13.66	6.83	15.28	51.367	3.420	-3.393
22.000	-0.274	0.00	0.00	0.00	0.000	0.000	0.000	0.165	20.41	10.21	22.82	51.406	3.420	-3.426
24.000	-0.371	0.00	0.00	0.00	0.000	0.000	0.000	0.205	28.17	14.09	31.50	51.464	3.420	-3.474
26.000	-0.484	0.00	0.00	0.00	0.000	0.000	0.000	0.249	38.47	19.24	43.01	51.490	3.420	-3.496
28.000	-0.617	0.00	0.00	0.00	0.000	0.000	0.000	0.296	49.29	24.64	55.10	51.503	3.420	-3.507
30.000	-0.770	0.00	0.00	0.00	0.000	0.000	0.000	0.343	60.44	30.22	67.58	51.511	3.420	-3.514
32.000	-0.945	0.00	0.00	0.00	0.000	0.000	0.000	0.392	71.83	35.92	80.31	51.516	3.420	-3.518
34.000	-1.142	0.00	0.00	0.00	0.000	0.000	0.000	0.440	128.19	64.09	143.32	51.520	3.420	-3.521
36.000	-1.363	0.00	0.00	0.00	0.000	0.000	0.000	0.477	178.75	89.37	199.85	51.521	3.420	-3.522
38.000	-1.610	0.00	0.00	0.00	0.000	0.000	0.000	0.496	204.92	102.46	229.11	51.519	3.420	-3.521
40.000	-1.882	0.00	0.00	0.00	0.000	0.000	0.000	0.498	191.03	95.51	213.58	51.515	3.420	-3.517
42.000	-2.181	0.00	0.00	0.00	0.000	0.000	0.000	0.492	182.60	91.30	204.15	51.508	3.419	-3.511
44.000	-2.505	0.00	0.00	0.00	0.000	0.000	0.000	0.482	168.82	84.41	188.75	51.501	3.418	-3.505
46.000	-2.849	0.00	0.00	0.00	0.000	0.000	0.000	0.470	153.91	76.96	172.08	51.494	3.417	-3.499
48.000	-3.211	0.00	0.00	0.00	0.000	0.000	0.000	0.460	139.82	69.91	156.32	51.489	3.415	-3.495
50.000	-3.584	0.00	0.00	0.00	0.000	0.000	0.000	0.450	126.65	63.33	141.60	51.488	3.413	-3.495
52.000	-3.960	0.00	0.00	0.00	0.000	0.000	0.000	0.441	114.28	57.14	127.77	51.494	3.410	-3.499
54.000	-4.328	0.00	0.00	0.00	0.000	0.000	0.000	0.430	100.59	50.30	112.47	51.507	3.406	-3.510
56.000	-4.675	0.00	0.00	0.00	0.000	0.000	0.000	0.415	79.36	39.68	88.73	51.531	3.402	-3.531
58.000	-4.989	0.00	0.00	0.00	0.000	0.000	0.000	0.388	57.60	28.80	64.40	51.577	3.398	-3.569
60.000	-5.254	0.00	0.00	0.00	0.000	0.000	0.000	0.346	49.17	24.59	54.98	51.679	3.394	-3.654
62.000	-5.458	0.00	0.00	0.00	0.000	0.000	0.000	0.289	37.73	18.86	42.18	51.812	3.392	-3.767
64.000	-5.609	0.00	0.00	0.00	0.000	0.000	0.000	0.215	23.04	11.52	25.75	51.976	3.393	-3.904
66.000	-5.724	0.00	0.00	0.00	0.000	0.000	0.000	0.125	8.82	4.41	9.86	52.183	3.400	-4.077
68.000	-5.817	0.00	0.00	0.00	0.000	0.000	0.000	0.020	0.99	0.49	1.10	52.440	3.417	-4.294
70.000	-5.894	0.00	0.00	0.00	0.000	0.000	0.000	-0.101	0.00	0.00	0.00	0.000	0.000	0.000
72.000	-5.963	0.00	0.00	0.00	0.000	0.000	0.000	-0.231	0.00	0.00	0.00	0.000	0.000	0.000
74.000	-6.032	0.00	0.00	0.00	0.000	0.000	0.000	-0.367	0.00	0.00	0.00	0.000	0.000	0.000
76.000	-6.105	0.00	0.00	0.00	0.000	0.000	0.000	-0.510	0.00	0.00	0.00	0.000	0.000	0.000
78.000	-6.178	0.00	0.00	0.00	0.000	0.000	0.000	-0.655	0.00	0.00	0.00	0.000	0.000	0.000
80.000	-6.252	0.00	0.00	0.00	0.000	0.000	0.000	-0.800	0.00	0.00	0.00	0.000	0.000	0.000

DATE: 2 SEPT 1988

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 35.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

CONTACT FORCES - SEGMENT PANELS VS. SEGMENTS

PANEL 10 (RUDDER PEDALS. ) VS. SEGMENT 11 ( LF )							
TIME (MSEC)	DEFL- ECTION ( IN.)	NORMAL FORCE ( LB.)	FRICTION FORCE ( LB.)	RESULTANT FORCE ( LB.)	CONTACT LOCATION ( IN.) (VEH REFERENCE)		
					X	Y	Z
0.000	0.002	0.08	0.00	0.08	51.239	-3.420	-3.286
2.000	0.001	0.07	0.01	0.07	51.239	-3.420	-3.286
4.000	0.002	0.11	0.04	0.12	51.239	-3.420	-3.285
6.000	0.005	0.29	0.14	0.32	51.240	-3.420	-3.287
8.000	0.010	0.75	0.37	0.83	51.245	-3.420	-3.291
10.000	0.019	1.60	0.80	1.78	51.254	-3.420	-3.298
12.000	0.031	2.67	1.33	2.98	51.266	-3.420	-3.308
14.000	0.048	4.10	2.05	4.58	51.284	-3.420	-3.323
16.000	0.070	5.93	2.96	6.63	51.306	-3.420	-3.342
18.000	0.096	8.18	4.09	9.15	51.334	-3.420	-3.365
20.000	0.128	13.70	6.85	15.32	51.366	-3.420	-3.393
22.000	0.165	20.47	10.23	22.88	51.406	-3.420	-3.425
24.000	0.206	28.26	14.13	31.59	51.464	-3.420	-3.474
26.000	0.250	38.58	19.29	43.14	51.489	-3.420	-3.496
28.000	0.296	49.45	24.73	55.29	51.503	-3.420	-3.507
30.000	0.344	60.69	30.34	67.85	51.511	-3.420	-3.513
32.000	0.394	72.29	36.14	80.82	51.516	-3.420	-3.518
34.000	0.444	133.60	66.80	149.37	51.519	-3.420	-3.520
36.000	0.483	188.09	94.05	210.29	51.519	-3.420	-3.520
38.000	0.507	219.74	109.87	245.68	51.515	-3.420	-3.518
40.000	0.514	216.05	108.03	241.55	51.508	-3.420	-3.511
42.000	0.515	213.02	106.51	238.16	51.497	-3.421	-3.502
44.000	0.514	212.01	106.00	237.03	51.482	-3.422	-3.490
46.000	0.514	211.89	105.95	236.90	51.465	-3.423	-3.475
48.000	0.514	212.07	106.04	237.10	51.446	-3.425	-3.459
50.000	0.511	207.70	103.85	232.22	51.425	-3.427	-3.441
52.000	0.498	190.37	95.18	212.83	51.399	-3.430	-3.420
54.000	0.472	155.61	77.80	173.97	51.361	-3.432	-3.388
56.000	0.436	107.92	53.96	120.66	51.306	-3.435	-3.342
58.000	0.395	59.01	29.50	65.97	51.268	-3.437	-3.310
60.000	0.353	50.53	25.27	56.50	51.259	-3.438	-3.302
62.000	0.307	41.43	20.72	46.32	51.288	-3.438	-3.327
64.000	0.268	33.64	16.82	37.61	51.387	-3.436	-3.409
66.000	0.234	26.90	13.45	30.07	51.514	-3.432	-3.516
68.000	0.200	20.05	10.02	22.41	51.657	-3.425	-3.637
70.000	0.159	13.90	6.95	15.54	51.813	-3.413	-3.767
72.000	0.112	6.75	3.37	7.55	51.972	-3.393	-3.901
74.000	0.056	2.80	1.40	3.13	52.128	-3.366	-4.032
76.000	-0.008	0.00	0.00	0.00	0.000	0.000	0.000
78.000	-0.077	0.00	0.00	0.00	0.000	0.000	0.000
80.000	-0.141	0.00	0.00	0.00	0.000	0.000	0.000

DATE: 2 SEPT 1988

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RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 36.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

HARNESS SYSTEM BELT ENDPOINT FORCES

TIME (MSEC)	BELT NO. 1 OF HARNESS NO. 1				BELT NO. 2 OF HARNESS NO. 1			
	POINT NO. 1		POINT NO. 12		POINT NO. 13		POINT NO. 27	
	STRAIN ( IN./ IN.)	FORCE ( LB.)	STRAIN ( IN./ IN.)	FORCE ( LB.)	STRAIN ( IN./ IN.)	FORCE ( LB.)	STRAIN ( IN./ IN.)	FORCE ( LB.)
0.000	0.000000	0.00	0.000000	0.00	0.000000	0.00	0.000000	0.00
2.000	0.000025	0.37	0.000017	0.25	0.000014	0.21	0.000018	0.27
4.000	0.000119	1.79	0.000065	0.98	0.000057	0.85	0.000152	2.27
6.000	0.000281	4.22	0.000150	2.25	0.000124	1.86	0.000470	7.04
8.000	0.000523	7.85	0.000276	4.15	0.000219	3.29	0.001018	15.27
10.000	0.000854	12.81	0.000438	6.57	0.000336	5.04	0.001803	27.04
12.000	0.001023	15.34	0.000481	7.21	0.000344	5.16	0.002454	36.81
14.000	0.001320	19.80	0.000515	7.72	0.000433	6.50	0.003168	47.52
16.000	0.001672	25.08	0.000551	8.27	0.000496	7.44	0.003856	57.84
18.000	0.001420	21.30	0.000400	6.00	0.000404	6.06	0.003427	51.41
20.000	0.001831	27.40	0.000484	7.26	0.000498	7.46	0.004276	64.13
22.000	0.002363	35.45	0.000617	9.26	0.000643	9.65	0.005479	82.19
24.000	0.003085	46.27	0.000877	13.15	0.000921	13.81	0.019008	285.12
26.000	0.004040	60.61	0.001215	18.22	0.001284	19.26	0.021036	315.53
28.000	0.006003	90.05	0.001724	25.85	0.001768	26.52	0.027340	410.10
30.000	0.009472	142.08	0.002256	33.83	0.002429	36.44	0.035707	564.14
32.000	0.013979	209.69	0.003249	48.73	0.004372	65.58	0.023671	355.06
34.000	0.019790	296.85	0.004754	71.30	0.008401	126.02	0.020865	312.97
36.000	0.026146	392.20	0.007124	106.86	0.018334	275.01	0.025025	375.38
38.000	0.032200	494.00	0.010831	162.46	0.030199	453.97	0.039302	636.04
40.000	0.037809	606.17	0.021023	315.35	0.040241	654.82	0.056200	1178.59
42.000	0.043063	711.27	0.036025	570.49	0.050245	863.00	0.075150	2182.96
44.000	0.048343	816.85	0.053858	1054.46	0.060539	1408.57	0.064897	1639.53
46.000	0.053827	1052.84	0.071518	1990.44	0.072248	2029.17	0.084525	2679.84
48.000	0.055271	1129.35	0.087363	2830.23	0.056456	1192.15	0.103767	3631.84
50.000	0.058800	1316.42	0.098307	3410.27	0.065766	1685.60	0.093883	3175.81
52.000	0.064710	1629.61	0.098688	3430.48	0.068526	1831.86	0.107224	3752.85
54.000	0.072120	2022.35	0.087992	2863.56	0.074577	2152.58	0.092638	3109.84
56.000	0.076068	2231.59	0.071069	1966.67	0.075155	2183.20	0.089018	2917.94
58.000	0.074497	2148.32	0.049516	840.31	0.069789	1898.82	0.084438	2675.23
60.000	0.061993	1485.61	0.026359	395.38	0.082583	2576.88	0.093363	3148.22
62.000	0.047024	790.48	0.005156	77.34	0.032040	490.80	0.086107	2763.69
64.000	0.028177	422.66	0.000000	0.00	0.024499	367.48	0.065353	1663.72
66.000	0.007038	105.57	0.000000	0.00	0.006231	93.46	0.051787	944.69
68.000	0.000000	0.00	0.000000	0.00	0.000000	0.00	0.037962	609.25
70.000	0.000000	0.00	0.000000	0.00	0.000000	0.00	0.022501	337.51
72.000	0.000000	0.00	0.000000	0.00	0.000000	0.00	0.012711	190.67
74.000	0.000000	0.00	0.000000	0.00	0.000000	0.00	0.006159	92.39
76.000	0.000000	0.00	0.000000	0.00	0.000000	0.00	0.000000	0.00
78.000	0.000000	0.00	0.000000	0.00	0.000000	0.00	0.000000	0.00
80.000	0.000000	0.00	0.000000	0.00	0.000000	0.00	0.000000	0.00



DATE: 2 SEPT 1988

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPTOID FOR DASH BOARD

PAGE: 37.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

CONTACT FORCES - SEGMENT NO. 2 ( CT ) VS. SEGMENT NO. 13 ( RLA)

TIME (MSEC)	DEFL- ECTION ( IN. )	NORMAL FORCE ( LB. )	FRICTION FORCE ( LB. )	RESULTANT FORCE ( LB. )	CONTACT LOCATION ( IN. )					
					SEG. 2	LOCAL REFERENCE		SEG. 13	LOCAL REFERENCE	
					X	Y	Z	X	Y	Z
0.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
2.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
4.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
6.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
8.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
10.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
12.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
14.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
16.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
18.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
20.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
22.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
24.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
26.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
28.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
30.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
32.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
34.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
36.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
38.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
40.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
42.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
44.000	0.009	4.39	1.10	4.52	2.018	5.365	-1.749	-0.875	-0.809	-7.906
46.000	0.010	3.62	0.90	3.73	2.036	5.360	-1.739	-0.881	-0.803	-7.903
48.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
50.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
52.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
54.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
56.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
58.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
60.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
62.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
64.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
66.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
68.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
70.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
72.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
74.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
76.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
78.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
80.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000

**RUN DESCRIPTION:**    **EXAMPLE 1:  BASIC SLED TEST SIMULATION**  
                           **TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD**

**PAGE: 38.01**

**VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK**

**CRASH VICTIM: 95TH PERCENTILE MALE**

CONTACT FORCES - SEGMENT NO. 2 ( CT ) VS. SEGMENT NO. 15 ( LLA)

TIME (MSEC)	DEFL-	NORMAL	FRICTION	RESULTANT	CONTACT LOCATION ( IN. )						
	ECTION	FORCE	FORCE	FORCE	SEG. 2	LOCAL REFERENCE			SEG. 15	LOCAL REFERENCE	
	( IN. )	( LB. )	( LB. )	( LB. )	X	Y	Z	X	Y	Z	
0.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
2.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
4.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
6.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
8.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
10.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
12.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
14.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
16.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
18.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
20.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
22.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
24.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
26.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
28.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
30.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
32.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
34.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
36.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
38.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
40.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
42.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
44.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
46.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
48.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
50.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
52.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
54.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
56.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
58.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
60.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
62.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
64.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
66.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
68.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
70.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
72.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
74.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
76.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
78.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	
80.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	

PAGE: 39.01

TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

**CRASH VICTIM: 95TH PERCENTILE MALE**

CONTACT FORCES - SEGMENT NO. 6 ( RUL ) VS. SEGMENT NO. 13 ( RLA )

TIME (MSEC)	DEFL- ECTION ( IN.)	NORMAL FORCE ( LB.)	FRICTION FORCE ( LB.)	RESULTANT FORCE ( LB.)	CONTACT LOCATION ( IN.)					
					SEG. 6 X	LOCAL Y	REFERENCE Z	SEG. 13 X	LOCAL Y	REFERENCE Z
0.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
2.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
4.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
6.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
8.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
10.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
12.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
14.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
16.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
18.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
20.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
22.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
24.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
26.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
28.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
30.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
32.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
34.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
36.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
38.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
40.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
42.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
44.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
46.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
48.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
50.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
52.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
54.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
56.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
58.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
60.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
62.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
64.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
66.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
68.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
70.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
72.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
74.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
76.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
78.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
80.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000

DATE: 2 SEPT 1988

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 40.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

CONTACT FORCES - SEGMENT NO. 9 ( L'L) VS. SEGMENT NO. 15 ( LLA)

TIME (MSEC)	DEFL- ECTION ( IN.)	NORMAL FORCE ( LB.)	FRICTION FORCE ( LB.)	RESULTANT FORCE ( LB.)	CONTACT LOCATION ( IN.)					
					SEG. 9 LOCAL REFERENCE			SEG. 15 LOCAL REFERENCE		
					X	Y	Z	X	Y	Z
0.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
2.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
4.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
6.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
8.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
10.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
12.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
14.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
16.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
18.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
20.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
22.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
24.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
26.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
28.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
30.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
32.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
34.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
36.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
38.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
40.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
42.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
44.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
46.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
48.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
50.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
52.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
54.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
56.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
58.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
60.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
62.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
64.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
66.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
68.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
70.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
72.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
74.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
76.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
78.000	0.282	132.75	33.19	136.84	1.229	-1.146	10.441	-1.121	0.658	6.935
80.000	0.685	321.84	80.46	331.75	1.096	-1.142	10.037	-1.019	0.683	6.725

DATE: 2 SEPT 1988

PAGE 46

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 41.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

CONTACT FORCES - SEGMENT NO. 13 ( RLA ) VS. SEGMENT NO. 16 ( VEH )

TIME (MSEC)	DEFL- ECTION ( IN. )	NORMAL FORCE ( LB. )	FRICTION FORCE ( LB. )	RESULTANT FORCE ( LB. )	CONTACT LOCATION ( IN. )					
					SEG. 13 LOCAL REFERENCE			SEG. 16 LOCAL REFERENCE		
					X	Y	Z	X	Y	Z
0.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
2.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
4.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
6.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
8.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
10.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
12.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
14.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
16.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
18.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
20.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
22.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
24.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
26.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
28.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
30.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
32.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
34.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
36.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
38.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
40.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
42.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
44.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
46.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
48.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
50.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
52.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
54.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
56.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
58.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
60.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
62.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
64.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
66.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
68.000	0.217	24.79	12.39	27.71	1.714	0.433	2.758	32.371	6.599	-23.212
70.000	0.496	193.03	96.51	215.81	1.651	0.426	3.110	32.482	6.706	-23.329
72.000	0.671	444.83	222.41	497.33	1.602	0.408	3.504	32.546	6.820	-23.401
74.000	0.627	362.71	181.36	405.53	1.587	0.388	3.859	32.512	6.921	-23.391
76.000	0.420	87.00	43.50	97.27	1.600	0.370	4.164	32.409	7.003	-23.320
78.000	0.219	23.90	11.95	26.72	1.612	0.354	4.449	32.311	7.076	-23.249
80.000	0.103	5.46	2.73	6.10	1.608	0.342	4.722	32.256	7.143	-23.206

DATE: 2 SEPT 1988

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 42.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

CONTACT FORCES - SEGMENT NO. 15 ( LLA ) VS. SEGMENT NO. 16 (VEH )

TIME (MSEC)	DEFL- ECTION ( IN. )	NORMAL FORCE ( LB. )	FRICTION FORCE ( LB. )	RESULTANT FORCE ( LB. )	CONTACT LOCATION ( IN. )					
					SEG. 15 LOCAL REFERENCE			SEG. 16 LOCAL REFERENCE		
					X	Y	Z	X	Y	Z
0.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
2.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
4.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
6.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
8.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
10.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
12.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
14.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
16.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
18.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
20.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
22.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
24.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
26.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
28.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
30.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
32.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
34.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
36.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
38.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
40.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
42.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
44.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
46.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
48.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
50.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
52.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
54.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
56.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
58.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
60.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
62.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
64.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
66.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
68.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
70.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
72.000	0.524	226.73	113.37	253.49	1.755	0.307	0.651	32.615	-6.119	-23.311
74.000	0.804	610.21	305.10	682.23	1.712	0.298	0.537	32.732	-6.130	-23.436
76.000	0.907	736.13	368.06	823.02	1.699	0.281	0.427	32.764	-6.147	-23.486
78.000	0.798	590.20	295.10	659.86	1.720	0.263	0.294	32.694	-6.176	-23.450
80.000	0.583	303.74	151.87	339.60	1.758	0.244	0.157	32.574	-6.224	-23.368

HIC, HSI AND CSI RESULTS  
HEAD INJURY CRITERION

PAGE 48

HIC = 192.44      TIME DURATION = 52.000 TO 65.000 MSEC  
                     WITH HEAD RESULTANTS = 25.844 AND 23.464 G'S

                     AVERAGE HEAD RESULTANT FOR TIME DURATION = 46.574 G'S  
HEAD SEVERITY INDEX

HSI = 245.20

MAX HEAD RESULTANT = 65.716 G'S AT 60.000 MSEC  
CHEST SEVERITY INDEX

CSI = 733.64

MAX CHEST RESULTANT = 146.473 G'S AT 59.000 MSEC

SUB	CALLS	TIME	%
MAIN3D	1	213	1.69
INPUT	1	220	1.74
CHAIN	484	306	2.42
EJOINT	484	17	0.13
DINT	41	496	3.92
PDAUX	568	434	3.43
DAUX	483	520	4.11
SETUP1	483	236	1.87
CONTC	483	235	1.86
PLELP	5313	901	7.13
SEGSEG	2898	886	7.01
HBELT	1072	1434	11.35
VISPR	483	758	6.00
SETUP2	483	89	0.70
DAUX11	483	629	4.98
DAUX12	483	181	1.43
DAUX22	483	110	0.87
FSMSOL	1072	1407	11.13
OUTPUT	86	1148	9.08
UPDATE	85	0	0.00
HPTURB	85	1628	12.88
DZP	482	148	1.17
POSTPR	1	643	5.09
TOTAL		12639	100.00



#### APPENDIX C4

Example 1, ATB Basic Sled Test Simulation  
Perkin-Elmer Output File



CARD 8.1

CARDS 8.2

SEGMENT		WEIGHT ( LB.)	PRINCIPAL MOMENTS OF INERTIA ( LB.-SEC.**2- IN.)			SEGMENT CONTACT ELLIPSOID SEMIAXES ( IN.)			CENTER ( IN.)			PRINCIPAL AXES (DEG)		
I	SYM PLOT		X	Y	Z	X	Y	Z	X	Y	Z	YAW	PITCH	ROLL
1	LT 1	34.772	1.6280	1.0101	1.7954	5.168	7.436	3.778	0.000	0.000	-0.072	0.00	0.00	0.00
2	CT 2	13.099	0.4160	0.2301	0.5857	4.809	6.673	4.145	0.000	0.000	-0.011	0.00	0.00	0.00
3	UT 3	53.673	3.4525	2.7832	2.3509	5.220	6.906	7.314	0.000	0.000	-0.872	0.00	0.00	0.00
4	N 4	3.289	0.0278	0.0278	0.0216	2.520	2.520	3.156	0.000	0.000	0.000	0.00	0.00	0.00
5	H 5	11.927	0.2708	0.3085	0.1584	3.984	3.125	5.836	0.000	0.000	0.000	0.00	0.00	0.00
6	RUL 6	22.725	2.0130	2.0130	0.2576	3.308	3.308	12.652	0.000	0.000	0.000	0.00	0.00	0.00
7	RLL 7	9.763	0.4989	0.4989	0.0626	2.487	2.487	9.616	0.000	0.000	0.000	0.00	0.00	0.00
8	RF 8	2.079	0.0426	0.0412	0.0055	2.866	2.016	5.617	0.000	0.000	1.462	0.00	0.00	0.00
9	LUL 9	22.725	2.0130	2.0130	0.2576	3.308	3.308	12.652	0.000	0.000	0.000	0.00	0.00	0.00
10	LLL A	9.763	0.4989	0.4989	0.0626	2.487	2.487	9.616	0.000	0.000	0.000	0.00	0.00	0.00
11	LF B	2.079	0.0426	0.0412	0.0055	2.866	2.016	5.617	0.000	0.000	1.462	0.00	0.00	0.00
12	RUA C	5.542	0.1743	0.1743	0.0259	2.122	2.122	7.497	0.000	0.000	0.000	0.00	0.00	0.00
13	RLA D	5.901	0.3331	0.3331	0.0214	1.871	1.871	10.269	0.000	0.000	0.000	0.00	0.00	0.00
14	LUA E	5.542	0.1743	0.1743	0.0259	2.122	2.122	7.497	0.000	0.000	0.000	0.00	0.00	0.00
15	LLA F	5.901	0.3331	0.3331	0.0214	1.871	1.871	10.269	0.000	0.000	0.000	0.00	0.00	0.00

CARDS 8.3

JOINT				LOCATION( IN.) - SEG(JNT)			LOCATION( IN.) - SEG(J+1)			PRIN. AXIS(DEG) - SEG(JNT)			PRIN. AXIS(DEG) - SEG(J+1)		
J	SYM	PLOT	JNT PIN	X	Y	Z	X	Y	Z	YAW	PITCH	ROLL	YAW	PITCH	ROLL
1	P	M	1 0	0.000	0.000	-3.850	0.000	0.000	1.610	0.00	0.00	0.00	0.00	5.00	0.00
2	W	N	2 0	0.000	0.000	-1.640	0.000	0.000	6.440	0.00	0.00	0.00	0.00	5.00	0.00
3	NP	O	3 0	0.000	0.000	-8.190	0.000	0.000	0.640	0.00	0.00	0.00	0.00	10.00	0.00
4	HP	P	4 0	0.000	0.000	-0.640	0.000	0.000	5.840	0.00	0.00	0.00	0.00	10.00	0.00
5	RH	Q	1 0	0.000	3.420	-0.310	0.000	0.000	-8.640	0.00	0.00	0.00	0.00	-45.00	0.00
6	RK	R	6 1	0.000	0.000	10.000	0.000	0.000	-6.970	0.00	0.00	0.00	0.00	60.00	0.00
7	RA	S	7 0	0.000	0.000	8.120	2.870	0.000	-2.660	0.00	90.00	0.00	0.00	10.00	0.00
8	LH	T	1 0	0.000	-3.420	-0.310	0.000	0.000	-8.640	0.00	0.00	0.00	0.00	-45.00	0.00
9	LK	U	9 1	0.000	0.000	10.000	0.000	0.000	-6.970	0.00	0.00	0.00	0.00	60.00	0.00
10	LA	V	10 0	0.000	0.000	8.120	2.870	0.000	-2.660	0.00	90.00	0.00	0.00	10.00	0.00
11	RS	W	3 0	0.000	6.240	-5.220	0.000	0.000	-5.370	0.00	0.00	0.00	0.00	-4.10	0.00
12	RE	X	12 1	0.000	0.000	5.420	0.000	0.000	-8.200	0.00	0.00	0.00	0.00	-70.00	0.00
13	LS	Y	3 0	0.000	-6.240	-5.220	0.000	0.000	-5.370	0.00	0.00	0.00	0.00	-4.10	9.00
14	LE	Z	14 1	0.000	0.000	5.420	0.000	0.000	-8.200	0.00	0.00	0.00	0.00	-70.00	0.00

## FLEXURAL SPRING CHARACTERISTICS

## TORSIONAL SPRING CHARACTERISTICS

JOINT	SPRING COEF. ( IN. LB./DEG**J)			ENERGY DISSIPATION COEF.	JOINT STOP (DEG)	SPRING COEF. ( IN. LB./DEG**J)			ENERGY DISSIPATION COEF.	JOINT STOP (DEG)
	LINEAR (J=1)	QUADRATIC (J=2)	CUBIC (J=3)			LINEAR (J=1)	QUADRATIC (J=2)	CUBIC (J=3)		
1 P	0.000	10.000	0.000	0.700	20.000	0.000	10.000	0.000	0.700	5.000
2 W	0.000	10.000	0.000	0.700	20.000	0.000	10.000	0.000	0.700	35.000
3 NP	0.000	5.000	0.000	0.700	25.000	0.000	10.000	0.000	0.700	35.000
4 HP	0.000	5.000	0.000	0.700	25.000	0.000	10.000	0.000	0.700	35.000
5 RH	0.000	10.000	0.000	0.700	70.000	0.000	0.800	0.000	0.700	40.000
6 RK	0.000	1.800	0.000	0.700	60.000	0.000	0.000	0.000	0.000	0.000
7 RA	0.000	7.000	0.000	0.700	35.000	0.000	10.000	0.000	0.700	26.000
8 LH	0.000	10.000	0.000	0.700	70.000	0.000	0.800	0.000	0.700	40.000
9 LK	0.000	1.800	0.000	0.700	60.000	0.000	0.000	0.000	0.000	0.000
10 LA	0.000	7.000	0.000	0.700	35.000	0.000	10.000	0.000	0.700	26.000
11 RS	0.000	10.000	0.000	0.700	122.500	0.000	10.000	0.000	0.700	65.000
12 RE	0.000	1.800	0.000	0.700	70.000	0.000	0.000	0.000	0.000	0.000
13 LS	0.000	10.000	0.000	0.700	122.500	0.000	10.000	0.000	0.700	65.000
14 LE	0.000	1.800	0.000	0.700	70.000	0.000	0.000	0.000	0.000	0.000

CARDS B.5

## JOINT VISCOUS CHARACTERISTICS AND LOCK-UNLOCK CONDITIONS

JOINT	VISCOUS COEFFICIENT ( IN. LB.SEC./DEG)	COULOMB FRICTION COEF. ( IN. LB.)	FULL FRICTION ANGULAR VELOCITY (DEG/SEC.)	MAX TORQUE FOR A LOCKED JOINT ( IN. LB.)	MIN TORQUE FOR UNLOCKED JOINT ( IN. LB.)	MIN. ANG. VELOCITY FOR UNLOCKED JOINT (RAD/SEC.)	IMPULSE RESTITUTION COEFFICIENT
1 P	0.100	0.00	30.00	0.00	0.00	0.00	0.000
2 W	0.100	0.00	30.00	0.00	0.00	0.00	0.000
3 NP	0.100	0.00	30.00	0.00	0.00	0.00	0.000
4 HP	0.100	0.00	30.00	0.00	0.00	0.00	0.000
5 RH	0.100	0.00	30.00	0.00	0.00	0.00	0.000
6 RK	0.100	0.00	30.00	0.00	0.00	0.00	0.000
7 RA	0.100	0.00	30.00	0.00	0.00	0.00	0.000
8 LH	0.100	0.00	30.00	0.00	0.00	0.00	0.000
9 LK	0.100	0.00	30.00	0.00	0.00	0.00	0.000
10 LA	0.100	0.00	30.00	0.00	0.00	0.00	0.000
11 RS	0.100	0.00	30.00	0.00	0.00	0.00	0.000
12 RE	0.100	0.00	30.00	0.00	0.00	0.00	0.000
13 LS	0.100	0.00	30.00	0.00	0.00	0.00	0.000
14 LE	0.100	0.00	30.00	0.00	0.00	0.00	0.000

SEGMENT NO. SYM	ANGULAR VELOCITIES (RAD/SEC.)			LINEAR VELOCITIES ( IN./SEC.)			ANGULAR ACCELERATIONS (RAD/SEC.**2)			LINEAR ACCELERATIONS ( IN./SEC.**2)		
	MAG. TEST	ABS. ERROR	REL. ERROR	MAG. TEST	ABS. ERROR	REL. ERROR	MAG. TEST	ABS. ERROR	REL. ERROR	MAG. TEST	ABS. ERROR	REL. ERROR
1 LT	0.010	0.010	0.0100	0.010	0.010	0.0100	0.100	0.100	0.1000	0.100	0.100	0.0100
2 CT	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
3 UT	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
4 N	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
5 H	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
6 RUL	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
7 RLL	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
8 RF	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
9 LUL	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
10 LLL	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
11 LF	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
12 RUA	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
13 RLA	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
14 LUA	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000
15 LLA	0.010	0.010	0.0100	0.000	0.000	0.0000	0.100	0.100	0.1000	0.000	0.000	0.0000

## VEHICLE DECELERATION INPUTS

PAGE 5  
CARDS C

## SLED ACCELERATION - 20G PEAK

YAW	PITCH	ROLL	VIPS	VTIME	X0(X)	X0(Y)	X0(Z)	NATAB	ATO	ADT	MSEG
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	15	0.000000	0.010000	0

## UNIDIRECTIONAL VEHICLE POSITION TABLES

TIME (MSEC)	ACC (G)	VELOCITY ( IN./SEC.)	POSITION ( IN.)	TIME (MSEC)	ACC (G)	VELOCITY ( IN./SEC.)	POSITION ( IN.)
0.00000	0.00	0.0000	0.00000				
10.00000	5.00	-9.6522	-0.03217				
20.00000	10.00	-38.6088	-0.25739				
30.00000	15.00	-86.8698	-0.86870				
40.00000	20.00	-154.4352	-2.05914				
50.00000	15.00	-222.0006	-3.95740				
60.00000	10.00	-270.2616	-6.43480				
70.00000	5.00	-299.2182	-9.29829				
80.00000	0.00	-308.8704	-12.35482				
90.00000	0.00	-308.8704	-15.44352				
100.00000	0.00	-308.8704	-18.53222				
110.00000	0.00	-308.8704	-21.62093				
120.00000	0.00	-308.8704	-24.70963				
130.00000	0.00	-308.8704	-27.79834				
140.00000	0.00	-308.8704	-30.88704				

NPL NBLT NBAG NPLP NQ NSD NHRNSS NWINDF NJNTF NFORCE  
12 0 0 3 0 0 1 0 0 0

PAGE 6  
CARD D.1

PLANE INPUTS

CARDS D.2

PLANE NO. 1 SEAT. 6 DEGREE OFF H

	X	Y	Z
POINT 1	10.0000	8.0000	-10.0000
POINT 2	28.0100	8.0000	-11.8900
POINT 3	10.0000	-8.0000	-10.0000

PLANE NO. 2 BACK PANEL. 13 DEGR

	X	Y	Z
POINT 1	1.0000	9.0000	-48.9700
POINT 2	10.0000	9.0000	-10.0000
POINT 3	1.0000	-9.0000	-48.9700

PLANE NO. 3 FLOOR.

	X	Y	Z
POINT 1	0.0000	12.0000	-1.3000
POINT 2	60.0000	12.0000	-1.3000
POINT 3	0.0000	-12.0000	-1.3000

PLANE NO. 4 HEAD PAD. 13 DEGR

	X	Y	Z
POINT 1	2.4800	7.5000	-47.2600
POINT 2	4.9600	7.5000	-36.5500
POINT 3	2.4800	-7.5000	-47.2600

PLANE NO. 5 SEAT FRONT PANEL.

	X	Y	Z
POINT 1	28.0100	8.0000	-11.8900
POINT 2	26.6600	8.0000	-4.4000
POINT 3	28.0100	-8.0000	-11.8900

PLANE NO. 6 BACK PANEL2. 13 DEGR

	X	Y	Z
POINT 1	1.0000	9.0000	-48.9700
POINT 2	10.0000	9.0000	-10.0000
POINT 3	1.0000	-9.0000	-48.9700

PLANE NO. 7 FIREWALL.

	X	Y	Z
POINT 1	60.0000	12.0000	-25.0000
POINT 2	60.0000	-12.0000	-25.0000
POINT 3	60.0000	12.0000	-0.7500

## PLANE NO. 8 RIGHT SIDE SEAT/IN.

	X	Y	Z
POINT 1	8.4100	8.1000	-6.6600
POINT 2	8.7000	8.1000	-14.7300
POINT 3	30.5800	8.1000	-6.6400

## PLANE NO. 9 LEFT SIDE SEAT/IN.

	X	Y	Z
POINT 1	8.4100	-8.1000	-6.6600
POINT 2	30.5800	-8.1000	-6.6400
POINT 3	8.7000	-8.1000	-14.7300

## PLANE NO. 10 RUDDER PEDALS.

	X	Y	Z
POINT 1	49.9920	9.0000	-2.2392
POINT 2	52.9920	9.0000	-4.7565
POINT 3	49.9920	-9.0000	-2.2392

## PLANE NO. 11 LEFT SIDE PANEL.

	X	Y	Z
POINT 1	1.0000	-9.0000	-48.9700
POINT 2	10.9000	-9.0000	-6.1000
POINT 3	-7.7700	-9.0000	-46.9500

## PLANE NO. 12 RIGHT SIDE PANEL.

	X	Y	Z
POINT 1	1.0000	9.0000	-48.9700
POINT 2	-7.7700	9.0000	-46.9500
POINT 3	10.9000	9.0000	-6.1000



### BODY SEGMENT SYMMETRY INPUT

**CARD D.7**

[illegible]

FUNCTION NO. 3 SEGMENT-SEGMENT FCN. NT1( 3) = 1

D0	D1	D2	D3	D4
0.0000	-5.0000	0.0000	0.0000	1.0000

FIRST PART OF FUNCTION - 6 TABULAR POINTS

D	F(D)
0.000000	0.0000
1.000000	470.0000
2.000000	890.0000
3.000000	1220.0000
4.000000	1470.0000
5.000000	1580.0000

FUNCTION NO. 6 CONSTANT, F=0.0 NT1( 6) = 19

CARDS E

D0	D1	D2	D3	D4
0.0000	0.0000	0.0000	0.0000	0.0000

FUNCTION IS CONSTANT 0.000000

FUNCTION NO. 7 R FACTOR.

NTI( 7) = 24

D0	D1	D2	D3	D4
0.0000	0.0000	0.7000	0.0000	0.0000

FUNCTION IS CONSTANT 0.700000

FUNCTION NO. 13 STIFF SURFACES

NTI(13) = 29

CARDS E

D0	D1	D2	D3	D4
0.0000	-4.0000	0.0000	0.0000	1.0000

FIRST PART OF FUNCTION - 8 TABULAR POINTS

D	F(D)
0.000000	0.0000
0.100000	5.0000
0.200000	20.0000
0.300000	40.0000
0.400000	60.0000
1.000000	860.0000
2.000000	2400.0000
3.000000	4000.0000

FUNCTION NO. 14 FRICTION FUNC.

NTI(14) = 51

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CARDS E

D0	D1	D2	D3	D4
0.0000	0.0000	0.5000	0.0000	1.0000

FUNCTION IS CONSTANT 0.500000

FUNCTION NO. 19 CF=.25,CREST=.25

NTI(19) = 56

CARDS E

D0	D1	D2	D3	D4
0.0000	0.0000	0.2500	0.0000	0.0000

FUNCTION IS CONSTANT 0.250000

FUNCTION NO. 20 DAMPING COEFF. C=900 NTI(20) = 61

D0	D1	D2	D3	D4
0.0000	1.0000	0.0000	0.0000	1.0000

FIRST PART OF FUNCTION - 5TH DEGREE POLYNOMIAL

A0	A1	A2	A3	A4	A5
0.000000	900.000000	0.000000	0.000000	0.000000	0.000000

FUNCTION NO. 21 RATE OF DEFLEC. NTI(21) = 72

CARDS E

D0	D1	D2	D3	D4
-40.0000	-150.0000	0.0000	0.0000	1.0000

FIRST PART OF FUNCTION - 21 TABULAR POINTS

D	F(D)
-40.000000	0.0000
-30.000000	0.0000
-20.000000	0.0000
-10.000000	0.0000
0.000000	0.0000
5.000000	1.0000
10.000000	1.0000
20.000000	0.9900
30.000000	0.9650
40.000000	0.9280
50.000000	0.8600
60.000000	0.6900
70.000000	0.4750
80.000000	0.3400
90.000000	0.2600
100.000000	0.2000
110.000000	0.1800
120.000000	0.0900
130.000000	0.0600
140.000000	0.0250
150.000000	0.0000

FUNCTION NO. 22 DAMPING COEFF. C=35 NTI(22) = 120

D0	D1	D2	D3	D4
0.0000	1.0000	0.0000	0.0000	1.0000

FIRST PART OF FUNCTION - 5TH DEGREE POLYNOMIAL

A0	A1	A2	A3	A4	A5
0.000000	35.000000	0.000000	0.000000	0.000000	0.000000

FUNCTION NO. 24 DAMPING COEFF. C=0.8 NTI(24) = 131

CARDS E

D0	D1	D2	D3	D4
-1000.0000	-1000.0000	0.0000	0.0000	1.0000

FIRST PART OF FUNCTION - 4 TABULAR POINTS

D	F(D)
-1000.000000	0.6000
-1.000000	0.6000
0.000000	1.0000
1000.000000	1.0000

FUNCTION NO. 25 DAMPING COEFF C=1100 NT1(25) = 145

D0	D1	D2	D3	D4
0.0000	1.0000	0.0000	0.0000	1.0000

FIRST PART OF FUNCTION - 5TH DEGREE POLYNOMIAL

A0	A1	A2	A3	A4	A5
0.000000	1100.000000	0.000000	0.000000	0.000000	0.000000

FUNCTION NO. 26 STIFF SURFACES-LL NT1(26) = 156

CARDS E

D0	D1	D2	D3	D4
0.0000	-4.0000	0.0000	0.0000	1.0000

FIRST PART OF FUNCTION - 8 TABULAR POINTS

D	F(D)
0.000000	0.0000
0.100000	5.0000
0.200000	20.0000
0.300000	40.0000
0.400000	60.0000
2.000000	860.0000
3.000000	2400.0000
4.000000	4000.0000

FUNCTION NO. 31 HARNESS FDF

NTI(31) = 178

PAGE 15  
CARDS E

D0	D1	D2	D3	D4
0.0000	-4.0000	0.0000	0.0000	0.0000

FIRST PART OF FUNCTION - 8 TABULAR POINTS

D	F(D)
0.000000	0.0000
0.010000	150.0000
0.020000	300.0000
0.030000	450.0000
0.050000	850.0000
0.100000	3500.0000
1.000000	35000.0000
4.000000	140000.0000

FUNCTION NO. 32 HARNESS FRICTION

NTI(32) = 200

CARDS E

D0	D1	D2	D3	D4
0.0000	0.0000	0.2000	0.0000	0.2000

FUNCTION IS CONSTANT 0.200000



FUNCTION NO. 34

HARNES FRICION

NTI(34) = 205

D0  
0.0000

D1  
0.0000

D2  
0.9000

D3  
0.0000

D4  
0.2000

FUNCTION IS CONSTANT 0.900000

## CARDS F.1

PLANE	SEGMENT	FORCE DEFLECTION	INERTIAL SPIKE	R FACTOR	G FACTOR	FRICTION COEF. OPT
1- 16 SEAT. 6 DEGREE OFF H	1- 1 LT	13 STIFF SURFACES	-20 DAMPING COEFF. C=900	-21 RATE OF DEFLEC.	0	14 FRICTION FUNC. 1
1- 16 SEAT. 6 DEGREE OFF H	6- 6 RUL	13 STIFF SURFACES	-25 DAMPING COEFF C=1100	-21 RATE OF DEFLEC.	0	14 FRICTION FUNC. 1
1- 16 SEAT. 6 DEGREE OFF H	9- 9 LUL	13 STIFF SURFACES	-25 DAMPING COEFF C=1100	-21 RATE OF DEFLEC.	0	14 FRICTION FUNC. 1
2- 16 BACK PANEL. 13 DEGR	1- 1 LT	13 STIFF SURFACES	-20 DAMPING COEFF. C=900	-21 RATE OF DEFLEC.	0	14 FRICTION FUNC. 1
2- 16 BACK PANEL. 13 DEGR	2- 2 CT	13 STIFF SURFACES	-20 DAMPING COEFF. C=900	-21 RATE OF DEFLEC.	0	14 FRICTION FUNC. 1
2- 16 BACK PANEL. 13 DEGR	3- 3 UT	13 STIFF SURFACES	-20 DAMPING COEFF. C=900	-21 RATE OF DEFLEC.	0	14 FRICTION FUNC. 1
3- 16 FLOOR.	8- 8 RF	13 STIFF SURFACES	-22 DAMPING COEFF. C=35	-21 RATE OF DEFLEC.	0	14 FRICTION FUNC. -1
3- 16 FLOOR.	11- 11 LF	13 STIFF SURFACES	-22 DAMPING COEFF. C=35	-21 RATE OF DEFLEC.	0	14 FRICTION FUNC. -1
4- 16 HEAD PAD. 13 DEGR	5- 5 H	13 STIFF SURFACES	-22 DAMPING COEFF. C=35	-21 RATE OF DEFLEC.	0	14 FRICTION FUNC. 1
10- 16 RUDDER PEDALS.	8- 8 RF	13 STIFF SURFACES	-22 DAMPING COEFF. C=35	-21 RATE OF DEFLEC.	0	14 FRICTION FUNC. 1
10- 16 RUDDER PEDALS.	11- 11 LF	13 STIFF SURFACES	-22 DAMPING COEFF. C=35	-21 RATE OF DEFLEC.	0	14 FRICTION FUNC. 1

## CARDS F.3

SEGMENT	SEGMENT	FORCE DEFLECTION	INERTIAL SPIKE	R FACTOR	G FACTOR	FRICTION COEF. OPT
2- 2 CT	13- 13	3 RLA SEGMENT-SEGMENT FCN.	0	7 R FACTOR.	0	19 CF=.25,CREST=.25 0
2- 2 CT	15- 15	3 LLA SEGMENT-SEGMENT FCN.	0	7 R FACTOR.	0	19 CF=.25,CREST=.25 0
6- 6 RUL	13- 13	3 RLA SEGMENT-SEGMENT FCN.	0	7 R FACTOR.	0	19 CF=.25,CREST=.25 0
9- 9 LUL	15- 15	3 LLA SEGMENT-SEGMENT FCN.	0	7 R FACTOR.	0	19 CF=.25,CREST=.25 0
13- 13 RLA	16- 24	13 VEH STIFF SURFACES	-22 DAMPING COEFF. C=35	-21 RATE OF DEFLEC.	0	14 FRICTION FUNC. 0
15- 15 LLA	16- 24	13 VEH STIFF SURFACES	-22 DAMPING COEFF. C=35	-21 RATE OF DEFLEC.	0	14 FRICTION FUNC. 0

NO. OF HARNESSES = 1

NO. OF BELTS PER HARNESSES = 2

FOR HARNESSES NO. 1 NO. OF POINTS PER BELT = 12 15

HARNESSES NO. 1 BELT NO. 1 FUNCTION NOS. 31 0 0 0 0 REFERENCE SLACK = 0.000 IN.

K	KS	KE	NT	NPD	NDR	FUNCTION NOS.				
1	16	0	109	1	1	0	0	0	0	0
2	1	1	115	0	1	0	0	0	0	34
3	1	1	121	0	1	0	0	0	0	34
4	1	1	127	0	1	0	0	0	0	34
5	1	1	133	0	1	0	0	0	0	34
6	1	23	139	0	1	0	0	0	0	0
7	1	1	145	0	1	0	0	0	0	34
8	1	1	151	0	1	0	0	0	0	34
9	1	1	157	0	1	0	0	0	0	34
10	1	1	163	0	1	0	0	0	0	34
11	1	1	169	0	1	0	0	0	0	34
12	16	0	175	1	1	0	0	0	0	0

CARDS F.8.D

K	BASE REFERENCE ( IN. )			ADJUSTED REFERENCE ( IN. )			OFFSET ( IN. )			PREFERRED DIRECTION ( IN. )		
	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z
1	13.000	8.000	-10.300	13.000	8.000	-10.300	0.000	0.000	0.000	2.400	22.000	-0.300
2	-1.178	7.075	-0.781	-1.178	7.075	-0.781	0.000	0.000	-0.072	0.000	0.000	0.000
3	-0.029	6.796	-1.534	-0.029	6.795	-1.534	0.000	0.000	-0.072	0.000	0.000	0.000
4	0.910	5.778	-2.283	0.910	5.778	-2.283	0.000	0.000	-0.072	0.000	0.000	0.000
5	2.228	2.355	-3.192	2.228	2.355	-3.192	0.000	0.000	-0.072	0.000	0.000	0.000
6	2.957	0.000	3.059	2.957	0.000	3.059	0.000	0.000	-7.000	0.000	0.000	0.000
7	3.070	-0.080	-4.410	2.344	-0.061	-3.367	0.000	0.000	-0.072	0.000	0.000	0.000
8	1.785	-2.325	-3.343	1.785	-2.325	-3.343	0.000	0.000	-0.072	0.000	0.000	0.000
9	0.011	-5.145	-2.728	0.011	-5.145	-2.728	0.000	0.000	-0.072	0.000	0.000	0.000
10	-0.880	-5.789	-2.282	-0.880	-5.789	-2.282	0.000	0.000	-0.072	0.000	0.000	0.000
11	-2.460	-6.099	-1.200	-2.460	-6.098	-1.200	0.000	0.000	-0.072	0.000	0.000	0.000
12	13.000	-8.000	-10.300	13.000	-8.000	-10.300	0.000	0.000	0.000	2.400	22.000	-0.300

HARNESSES NO. 1 BELT NO. 2 FUNCTION NOS. 31 0 0 0 0 REFERENCE SLACK = 0.000 IN.

K	KS	KE	NT	NPD	NDR	FUNCTION NOS.				
13	16	0	187	1	1	0	0	0	0	0
14	1	1	193	0	1	0	0	0	0	32
15	1	1	199	0	1	0	0	0	0	32
16	1	23	205	0	1	0	0	0	0	0
17	1	1	211	0	1	0	0	0	0	32
18	2	2	217	0	1	0	0	0	0	32
19	2	2	223	0	1	0	0	0	0	32
20	3	3	229	0	1	0	0	0	0	32
21	3	3	235	0	1	0	0	0	0	32
22	3	3	241	0	1	0	0	0	0	32
23	3	3	247	0	1	0	0	0	0	32
24	3	22	253	0	0	0	0	0	0	32
25	3	3	259	0	1	0	0	0	0	32
26	3	3	265	0	1	0	0	0	0	32
27	16	0	271	1	1	0	0	0	0	0

CARDS F.8.D

K	BASE REFERENCE ( IN. )			ADJUSTED REFERENCE ( IN. )			OFFSET ( IN. )			PREFERRED DIRECTION ( IN. )		
	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z
13	13.000	-8.000	-10.300	13.000	-8.000	-10.300	0.000	0.000	0.000	0.700	17.500	-21.300
14	-2.445	-6.101	-1.213	-2.445	-6.101	-1.213	0.000	0.000	-0.072	0.000	0.000	0.000
15	-0.960	-6.000	-2.500	-0.906	-5.661	-2.359	0.000	0.000	-0.072	0.000	0.000	0.000
16	0.000	-5.700	3.800	0.000	-5.367	3.578	0.000	0.000	-7.000	0.000	0.000	0.000
17	0.010	-4.000	-4.500	0.008	-3.061	-3.443	0.000	0.000	-0.072	0.000	0.000	0.000
18	1.818	-5.439	-1.820	1.818	-5.439	-1.820	0.000	0.000	-0.011	0.000	0.000	0.000
19	2.500	-2.500	-1.500	3.397	-3.397	-2.038	0.000	0.000	-0.011	0.000	0.000	0.000
20	3.000	-1.500	6.500	2.777	-1.388	6.016	0.000	0.000	-0.872	0.000	0.000	0.000
21	4.487	-0.133	3.734	4.487	-0.133	3.734	0.000	0.000	-0.872	0.000	0.000	0.000
22	4.421	3.319	-1.662	4.421	3.319	-1.662	0.000	0.000	-0.872	0.000	0.000	0.000
23	0.879	4.202	-5.672	0.879	4.202	-5.672	0.000	0.000	-0.872	0.000	0.000	0.000
24	0.300	0.200	-2.800	0.320	0.213	-2.985	0.000	4.000	-3.500	0.000	0.000	0.000
25	-1.000	4.300	-6.000	-0.955	4.105	-5.728	0.000	0.000	-0.872	0.000	0.000	0.000

27	0.000	5.000	-35.200	0.000	5.000	-35.200	0.000	0.000	0.000	0.700	17.500	-21.300
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ZPLT(X)	ZPLT(Y)	ZPLT(Z)	I1	J1	I2	J2	I3	SPLT(1)	SPLT(2)	SPLT(3)
0.	0.	0.	0	0	0	0	0	10.00	6.00	1.00

## INITIAL POSITIONS (INERTIAL REFERENCE)

CARDS G.2

SEGMENT NO. SEG	LINEAR POSITION ( IN. )			LINEAR VELOCITY ( IN./SEC. )		
	X	Y	Z	X	Y	Z
1 LT	14.38100	0.00000	-13.75000	0.00000	0.00000	0.00000
2 CT	13.16068	0.00000	-19.07188	0.00000	0.00000	0.00000
3 UT	11.31383	0.00000	-26.93796	0.00000	0.00000	0.00000
4 N	9.28353	0.00000	-35.53137	0.00000	0.00000	0.00000
5 H	7.77521	0.00000	-41.83338	0.00000	0.00000	0.00000
6 RUL	22.94073	3.42000	-14.48930	0.00000	0.00000	0.00000
7 RLL	38.16022	3.42000	-10.39045	0.00000	0.00000	0.00000
8 RF	48.12719	3.42000	-4.45598	0.00000	0.00000	0.00000
9 LUL	22.94073	-3.42000	-14.48930	0.00000	0.00000	0.00000
10 LLL	38.16022	-3.42000	-10.39045	0.00000	0.00000	0.00000
11 LF	48.12719	-3.42000	-4.45598	0.00000	0.00000	0.00000
12 RUA	12.34164	6.24000	-27.13188	0.00000	0.00000	0.00000
13 RLA	22.75808	6.24000	-21.48521	0.00000	0.00000	0.00000
14 LUA	12.34164	-6.24000	-27.13188	0.00000	0.00000	0.00000
15 LLA	22.75808	-6.24000	-21.48521	0.00000	0.00000	0.00000

## INITIAL ANGULAR ROTATION AND VELOCITY

CARDS G.3

SEGMENT NO. SEG	ANGULAR ROTATION (DEG)			ANGULAR VELOCITY (DEG/SEC.)			IYPR
	YAW	PITCH	ROLL	X	Y	Z	
1 LT	0.00000	12.90000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
2 CT	0.00000	12.95000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
3 UT	0.00000	13.28000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
4 N	0.00000	13.46000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
5 H	0.00000	13.46000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
6 RUL	0.00000	92.90000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
7 RLL	0.00000	48.65000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
8 RF	0.00000	128.80000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
9 LUL	0.00000	92.90000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
10 LLL	0.00000	48.65000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
11 LF	0.00000	128.80000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
12 RUA	0.00000	24.50000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
13 RLA	0.00000	85.00000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
14 LUA	0.00000	24.50000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
15 LLA	0.00000	85.00000	0.00000	0.00000	0.00000	0.00000	3 2 1 0

LINEAR AND ANGULAR VELOCITIES HAVE BEEN SET EQUAL TO THE INITIAL VEHICLE VELOCITIES.

HBPLAY TIME = 0.000 MSEC. NH,NB,NPTS NT= 1 1 11 103  
 NL(1)= 1 2 3 4 5 6 8 9 10 11 12  
 BB = 4.124 1.402 1.574 3.779 2.557 2.656 3.388 1.187 1.940 4.738

HBPLAY TIME = 0.000 MSEC. NH,NB,NPTS NT= 1 2 7 181  
 NL(1)= 13 14 18 21 22 23 27  
 BB = 4.748 7.394 6.842 6.406 5.423 10.829

## TABULAR TIME HISTORY CONTROL PARAMETERS

TYPE	KSG	SELECTED SEGMENTS OR JOINTS
H.1	3	3 -5 5
REF		0 1 16
H.2	3	3 5 5
REF		0 0 3
H.3	3	3 5 5
REF		0 0 3
H.4	3	3 5 5
REF		0 0 16
H.5	3	3 5 5
REF		0 0 5
H.6	3	3 5 5
REF		0 0 3
H.7	2	3 4
REF		0 0
H.8	0	
REF		
H.9	1	4
REF		5
H.10	15	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15
REF		16

SEGMENT	(INERTIAL)			(LOCAL)			(LOCAL)		
	ANGULAR ROTATION (DEG)			ANGULAR VELOCITY (RAD/SEC.)			ANGULAR ACCELERATION (RAD/SEC.**2)		
	YAW	PITCH	ROLL	X	Y	Z	X	Y	Z
1 LT	0.0000	12.9000	0.0000	0.00000	0.00000	0.00000	0.000000	-26.834649	0.000000
2 CT	0.0000	12.9500	0.0000	0.00000	0.00000	0.00000	0.000000	40.304245	0.000000
3 UT	0.0000	13.2800	0.0000	0.00000	0.00000	0.00000	0.000000	-0.859459	0.000000
4 N	0.0000	13.4600	0.0000	0.00000	0.00000	0.00000	0.000000	13.637948	0.000000
5 H	0.0000	13.4600	0.0000	0.00000	0.00000	0.00000	0.000000	-1.165343	0.000000
6 RUL	0.0000	92.9000	0.0000	0.00000	0.00000	0.00000	0.000000	-2.405246	0.000000
7 RLL	0.0000	48.6500	0.0000	0.00000	0.00000	0.00000	0.000000	-12.215669	0.000000
8 RF	0.0000	128.8000	0.0000	0.00000	0.00000	0.00000	0.000000	56.318297	0.000000
9 LUL	0.0000	92.9000	0.0000	0.00000	0.00000	0.00000	0.000000	-2.405246	0.000000
10 LLL	0.0000	48.6500	0.0000	0.00000	0.00000	0.00000	0.000000	-12.215669	0.000000
11 LF	0.0000	128.8000	0.0000	0.00000	0.00000	0.00000	0.000000	56.318297	0.000000
12 RUA	0.0000	24.5000	0.0000	0.00000	0.00000	0.00000	0.000000	-6.917594	0.000000
13 RLA	0.0000	85.0000	0.0000	0.00000	0.00000	0.00000	0.000000	-34.722447	0.000000
14 LUA	0.0000	24.5000	0.0000	0.00000	0.00000	0.00000	0.000000	-6.917594	0.000000
15 LLA	0.0000	85.0000	0.0000	0.00000	0.00000	0.00000	0.000000	-34.722447	0.000000
16 VEH	0.0000	0.0000	0.0000	0.00000	0.00000	0.00000	0.000000	0.000000	0.000000

SEGMENT	(INERTIAL)			(INERTIAL)			(INERTIAL)		
	LINEAR POSITION ( IN. )			LINEAR VELOCITY ( IN./SEC. )			LINEAR ACCELERATIONS (G'S)		
	X	Y	Z	X	Y	Z	X	Y	Z
1 LT	14.3210	0.0000	-13.7500	0.00000	0.00000	0.00000	0.017822	0.000000	-0.088444
2 CT	13.1607	0.0000	-19.0719	0.00000	0.00000	0.00000	0.114863	0.000000	-0.110519
3 UT	11.3138	0.0000	-26.9380	0.00000	0.00000	0.00000	-0.038031	0.000000	-0.075446
4 N	9.2835	0.0000	-35.5314	0.00000	0.00000	0.00000	-0.042274	0.000000	-0.074372
5 H	7.7752	0.0000	-41.8334	0.00000	0.00000	0.00000	-0.047117	0.000000	-0.073212
6 RUL	22.9407	3.4200	-14.4893	0.00000	0.00000	0.00000	0.041548	0.000000	-0.039498
7 RLL	38.1602	3.4200	-10.3904	0.00000	0.00000	0.00000	-0.100994	0.000000	0.188268
8 RF	48.1272	3.4200	-4.4560	0.00000	0.00000	0.00000	-0.187590	0.000000	-0.183587
9 LUL	22.9407	-3.4200	-14.4893	0.00000	0.00000	0.00000	0.041548	0.000000	-0.039498
10 LLL	38.1602	-3.4200	-10.3904	0.00000	0.00000	0.00000	-0.100994	0.000000	0.188268
11 LF	48.1272	-3.4200	-4.4560	0.00000	0.00000	0.00000	-0.187590	0.000000	-0.183587
12 RUA	12.3416	6.2400	-27.1319	0.00000	0.00000	0.00000	-0.114274	0.000000	-0.038215
13 RLA	22.7581	6.2400	-21.4852	0.00000	0.00000	0.00000	-0.266915	0.000000	0.736709
14 LUA	12.3416	-6.2400	-27.1319	0.00000	0.00000	0.00000	-0.114274	0.000000	-0.038215
15 LLA	22.7581	-6.2400	-21.4852	0.00000	0.00000	0.00000	-0.266915	0.000000	0.736709
16 VEH	0.0000	0.0000	0.0000	0.00000	0.00000	0.00000	0.000000	0.000000	0.000000

SEGMENT	(INERTIAL)			(LOCAL)			KINETIC ENERGY		
	U1 ARRAY ( IN./SEC.**2)			U2 ARRAY (RAD/SEC.**2)			( LB.- IN.)		TOTAL
	EXTERNAL LINEAR ACCELERATIONS			EXTERNAL ANGULAR ACCELERATIONS			LINEAR	ANGULAR	
	X	Y	Z	X	Y	Z			
1 LT	-0.12890+03	0.00000+00	-0.11350+04	0.000000+00	-0.480150+02	0.000000+00	0.000000+00	0.000000+00	0.000000+00
2 CT	0.00000+00	0.00000+00	0.38610+03	0.000000+00	0.000000+00	0.000000+00	0.000000+00	0.000000+00	0.000000+00
3 UT	0.69400+02	0.00000+00	0.37010+03	0.000000+00	-0.318610+01	0.000000+00	0.000000+00	0.000000+00	0.000000+00
4 N	0.00000+00	0.00000+00	0.38610+03	0.000000+00	0.000000+00	0.000000+00	0.000000+00	0.000000+00	0.000000+00
5 H	0.78220+02	0.00000+00	0.36800+03	-0.133040-18	-0.267210+00	0.308510-16	0.000000+00	0.000000+00	0.000000+00
6 RUL	-0.53090+02	0.00000+00	-0.11980+03	0.854930-17	0.218270+02	0.123730-14	0.000000+00	0.000000+00	0.000000+00
7 RLL	0.00000+00	0.00000+00	0.38610+03	0.000000+00	0.000000+00	0.000000+00	0.000000+00	0.000000+00	0.000000+00
8 RF	-0.95110+01	0.00000+00	-0.52100+03	0.000000+00	-0.176100+03	0.000000+00	0.000000+00	0.000000+00	0.000000+00
9 LUL	-0.53090+02	0.00000+00	-0.11980+03	0.854930-17	0.218270+02	0.123730-14	0.000000+00	0.000000+00	0.000000+00
10 LLL	0.00000+00	0.00000+00	0.38610+03	0.000000+00	0.000000+00	0.000000+00	0.000000+00	0.000000+00	0.000000+00
11 LF	-0.95110+01	0.00000+00	-0.52100+03	0.000000+00	-0.176100+03	0.000000+00	0.000000+00	0.000000+00	0.000000+00
12 RUA	0.00000+00	0.00000+00	0.38610+03	0.000000+00	0.000000+00	0.000000+00	0.000000+00	0.000000+00	0.000000+00
13 RLA	0.00000+00	0.00000+00	0.38610+03	0.000000+00	0.000000+00	0.000000+00	0.000000+00	0.000000+00	0.000000+00
14 LUA	0.00000+00	0.00000+00	0.38610+03	0.000000+00	0.000000+00	0.000000+00	0.000000+00	0.000000+00	0.000000+00
15 LLA	0.00000+00	0.00000+00	0.38610+03	0.000000+00	0.000000+00	0.000000+00	0.000000+00	0.000000+00	0.000000+00
							TOTAL BODY KINETIC ENERGY		
							0.000000+00	0.000000+00	0.000000+00

JOINT	IPIN	(INERTIAL)			(INERTIAL)			RELATIVE ANGULAR VELOCITY (RAD/SEC.)	
		JOINT FORCES ( LB.)			JOINT TORQUES ( IN. LB.)				
		X	Y	Z	X	Y	Z		
1	P	0	-0.1770+02	0.0000+00	-0.1000+03	0.00000+00	0.00000+00	0.00000+00	0.000
2	W	0	-0.1920+02	0.0000+00	-0.8590+02	0.00000+00	0.00000+00	0.00000+00	0.000
3	NP	0	-0.3120+01	0.0000+00	-0.1580+02	0.00000+00	0.00000+00	0.00000+00	0.000
4	HP	0	-0.2980+01	0.0000+00	-0.1220+02	0.00000+00	0.00000+00	0.00000+00	0.000
5	RH	0	0.2740+01	0.0000+00	0.6530+00	0.00000+00	0.00000+00	0.00000+00	0.000
6	RK	1	-0.1320+01	0.0000+00	-0.5500+01	0.00000+00	0.00000+00	0.00000+00	0.000
7	RA	0	-0.3390+00	0.0000+00	0.2420+01	0.00000+00	0.00000+00	0.00000+00	0.000
8	LH	0	0.2740+01	0.0000+00	0.6530+00	0.00000+00	0.00000+00	0.00000+00	0.000
9	LK	1	-0.1320+01	0.0000+00	-0.5500+01	0.00000+00	0.00000+00	0.00000+00	0.000
10	LA	0	-0.3390+00	0.0000+00	0.2420+01	0.00000+00	0.00000+00	0.00000+00	0.000
11	RS	0	-0.2210+01	0.0000+00	-0.7310+01	0.00000+00	0.00000+00	0.00000+00	0.000
12	RE	1	-0.1580+01	0.0000+00	-0.1550+01	0.00000+00	0.00000+00	0.00000+00	0.000
13	LS	0	-0.2210+01	0.0000+00	-0.7310+01	0.00000+00	0.00000+00	0.00000+00	0.000
14	LE	1	-0.1580+01	0.0000+00	-0.1550+01	0.00000+00	0.00000+00	0.00000+00	0.000

POINT NO.	POINT INDEX	SEGMENT NO.	LENGTH ( IN. )	BELT STRAIN	(LOCAL OR ELLIPSOID)			(INERTIAL)			PENETRATION
				ENERGY LOSS	REFERENCE POINT ( IN. )			BELT FORCES ( LB. )			ENERGY LOSS
				( IN. LB. )	X	Y	Z	X	Y	Z	( IN. LB. )
BELT NO.	1 OF HARNESS NO.			1							
1	1	16	0.000	0.000	13.000	8.000	-10.300	0.000	0.000	0.000	0.000
2	2	1	4.124	0.000	-1.178	7.075	-0.781	0.000	0.000	0.000	0.000
3	3	1	1.402	0.000	-0.029	6.795	-1.534	0.000	0.000	0.000	0.000
4	4	1	1.574	0.000	0.910	5.778	-2.283	0.000	0.000	0.000	0.000
5	5	1	3.779	0.000	2.228	2.355	-3.192	0.000	0.000	0.000	0.000
6	6	1	2.557	0.000	2.957	0.000	3.059	0.000	0.000	0.000	0.000
7	8	1	2.656	0.000	1.785	-2.325	-3.343	0.000	0.000	0.000	0.000
8	9	1	3.388	0.000	0.011	-5.145	-2.728	0.000	0.000	0.000	0.000
9	10	1	1.187	0.000	-0.880	-5.789	-2.282	0.000	0.000	0.000	0.000
10	11	1	1.940	0.000	-2.460	-6.098	-1.200	0.000	0.000	0.000	0.000
11	12	16	4.738	0.000	13.000	-8.000	-10.300	0.000	0.000	0.000	0.000

TOTAL BELT ENERGY LOSS 0.000 0.000

BELT NO.	2 OF HARNES NO.			1							
12	13	16	0.000	0.000	13.000	-8.000	-10.300	0.000	0.000	0.000	0.000
13	14	1	4.748	0.000	-2.445	-6.101	-1.213	0.000	0.000	0.000	0.000
14	18	2	7.394	0.000	1.818	-5.439	-1.820	0.000	0.000	0.000	0.000
15	21	3	6.842	0.000	4.487	-0.133	3.734	0.000	0.000	0.000	0.000
16	22	3	6.406	0.000	4.421	3.319	-1.662	0.000	0.000	0.000	0.000
17	23	3	5.423	0.000	0.879	4.202	-5.672	0.000	0.000	0.000	0.000
18	27	16	10.829	0.000	0.000	5.000	-35.200	0.000	0.000	0.000	0.000

TOTAL BELT ENERGY LOSS 0.000 0.000

TOTAL HARNES ENERGY LOSS 0.000 0.000

HPTURB ITER = 10 AT TIME = 16.000 MSEC. DELMAX = 0.010537 SCALE = 1.000000

HPTURB ITER = 10 AT TIME = 18.000 MSEC. DELMAX = 0.009232 SCALE = 1.000000

HPTURB ITER = 10 AT TIME = 19.000 MSEC. DELMAX = 0.009627 SCALE = 1.000000

HPTURB ITER = 10 AT TIME = 20.000 MSEC. DELMAX = 0.010050 SCALE = 1.000000

HPTURB ITER = 10 AT TIME = 21.000 MSEC. DELMAX = 0.010116 SCALE = 1.000000

HBPLAY TIME = 22.000 MSEC. NH,NB,NPTS NT= 1 2 8 181  
 NL(1)= 13 14 18 21 22 23 24 27  
 BB = 4.748 7.394 6.842 6.406 5.423 0.491 10.338

HPTURB ITER = 10 AT TIME = 22.000 MSEC. DELMAX = 0.012349 SCALE = 1.000000

HPTURB ITER = 10 AT TIME = 23.000 MSEC. DELMAX = 0.011517 SCALE = 1.000000

HPTURB ITER = 10 AT TIME = 24.000 MSEC. DELMAX = 0.011234 SCALE = 1.000000

HPTURB ITER = 10 AT TIME = 25.000 MSEC. DELMAX = 0.011569 SCALE = 1.000000

HPTURB ITER = 10 AT TIME = 26.000 MSEC. DELMAX = 0.012320 SCALE = 1.000000

HPTURB ITER = 10 AT TIME = 28.000 MSEC. DELMAX = 0.010639 SCALE = 1.000000

HPTURB ITER = 10 AT TIME = 29.000 MSEC. DELMAX = 0.012461 SCALE = 1.000000

HPTURB ITER = 10 AT TIME = 30.000 MSEC. DELMAX = 0.014987 SCALE = 1.000000

HBPLAY TIME = 31.000 MSEC. NH,NB,NPTS NT= 1 2 7 181  
 NL(1)= 13 14 18 21 22 24 27  
 BB = 4.748 7.394 6.842 6.406 5.572 10.679

HPTURB ITER = 10 AT TIME = 31.000 MSEC. DELMAX = 0.021341 SCALE = 1.000000

HBPLAY TIME = 32.000 MSEC. NH,NB,NPTS NT= 1 2 8 181  
 NL(1)= 13 14 18 21 22 23 24 27  
 BB = 4.748 7.394 6.842 6.406 5.066 0.260 10.926

HPTURB ITER = 10 AT TIME = 32.000 MSEC. DELMAX = 0.016547 SCALE = 1.000000

HBPLAY TIME = 33.000 MSEC. NH,NB,NPTS NT= 1 2 7 181



BB = 4.748 7.394 6.842 6.406 5.066 11.186  
 HPTURB ITER = 10 AT TIME = 33.000 MSEC. DELMAX = 0.036770 SCALE = 1.000000  
 HBPLAY TIME = 34.000 MSEC. NH,NB,NPTS NT= 1 2 8 181  
 NL(1)= 13 14 18 21 22 23 24 27  
 BB = 4.748 7.394 6.842 6.406 5.066 0.289 10.896  
 HPTURB ITER = 10 AT TIME = 34.000 MSEC. DELMAX = 0.041013 SCALE = 1.000000  
 HBPLAY TIME = 35.000 MSEC. NH,NB,NPTS NT= 1 2 7 181  
 NL(1)= 13 14 18 21 22 24 27  
 BB = 4.748 7.394 6.842 6.406 5.216 11.035  
 HPTURB ITER = 10 AT TIME = 35.000 MSEC. DELMAX = 0.021221 SCALE = 1.000000  
 HBPLAY TIME = 36.000 MSEC. NH,NB,NPTS NT= 1 2 8 181  
 NL(1)= 13 14 18 21 22 23 24 27  
 BB = 4.748 7.394 6.842 6.406 4.847 0.195 11.210  
 HPTURB ITER = 10 AT TIME = 36.000 MSEC. DELMAX = 0.012648 SCALE = 1.000000  
 HPTURB ITER = 10 AT TIME = 37.000 MSEC. DELMAX = 0.015643 SCALE = 1.000000  
 HPTURB ITER = 10 AT TIME = 38.000 MSEC. DELMAX = 0.011152 SCALE = 1.000000  
 HPTURB ITER = 10 AT TIME = 39.000 MSEC. DELMAX = 0.014391 SCALE = 1.000000  
 HPTURB ITER = 10 AT TIME = 40.000 MSEC. DELMAX = 0.017690 SCALE = 1.000000  
 HPTURB ITER = 10 AT TIME = 41.000 MSEC. DELMAX = 0.015081 SCALE = 1.000000  
 HPTURB ITER = 10 AT TIME = 42.000 MSEC. DELMAX = 0.017005 SCALE = 1.000000  
 HBPLAY TIME = 43.000 MSEC. NH,NB,NPTS NT= 1 2 7 181  
 NL(1)= 13 14 18 21 22 24 27  
 BB = 4.748 7.394 6.842 6.406 4.910 11.342  
 HPTURB ITER = 10 AT TIME = 43.000 MSEC. DELMAX = 0.053120 SCALE = 1.000000  
 HBPLAY TIME = 44.000 MSEC. NH,NB,NPTS NT= 1 2 8 181  
 NL(1)= 13 14 18 21 22 23 24 27  
 BB = 4.748 7.394 6.842 6.406 4.496 0.075 11.681  
 HPTURB ITER = 10 AT TIME = 44.000 MSEC. DELMAX = 0.013932 SCALE = 1.000000  
 HPTURB ITER = 10 AT TIME = 45.000 MSEC. DELMAX = 0.012674 SCALE = 1.000000  
 HBPLAY TIME = 46.000 MSEC. NH,NB,NPTS NT= 1 2 7 181  
 NL(1)= 13 18 21 22 23 24 27  
 BB = 12.143 6.842 6.406 4.496 0.055 11.701  
 HPTURB ITER = 10 AT TIME = 46.000 MSEC. DELMAX = 0.014891 SCALE = 1.000000  
 HBPLAY TIME = 47.000 MSEC. NH,NB,NPTS NT= 1 1 10 103  
 NL(1)= 1 3 4 5 6 8 9 10 11 12  
 BB = 5.526 1.574 3.779 2.557 2.656 3.388 1.187 1.940 4.738  
 HPTURB ITER = 10 AT TIME = 47.000 MSEC. DELMAX = 0.018982 SCALE = 1.000000  
 HBPLAY TIME = 48.000 MSEC. NH,NB,NPTS NT= 1 2 6 181  
 NL(1)= 13 18 21 22 24 27  
 BB = 12.143 6.842 6.406 4.534 11.718  
 HPTURB ITER = 10 AT TIME = 48.000 MSEC. DELMAX = 0.064777 SCALE = 1.000000  
 HBPLAY TIME = 49.000 MSEC. NH,NB,NPTS NT= 1 2 7 181  
 NL(1)= 13 18 21 22 23 24 27  
 BB = 12.143 6.842 6.406 4.192 0.045 12.015  
 HPTURB ITER = 10 AT TIME = 49.000 MSEC. DELMAX = 0.010077 SCALE = 1.000000  
 HPTURB ITER = 10 AT TIME = 50.000 MSEC. DELMAX = 0.010283 SCALE = 1.000000  
 HPTURB ITER = 10 AT TIME = 51.000 MSEC. DELMAX = 0.012303 SCALE = 1.000000  
 HBPLAY TIME = 52.000 MSEC. NH,NB,NPTS NT= 1 2 6 181  
 NL(1)= 13 18 21 22 24 27  
 BB = 12.143 6.842 6.406 4.222 12.029

HPTURB ITER = 10 AT TIME = 52.000 MSEC. DELMAX = 0.055553 SCALE = 1.000000

HPTURB ITER = 10 AT TIME = 53.000 MSEC. DELMAX = 0.035482 SCALE = 1.000000

HBPLAY TIME = 54.000 MSEC. NH,NB,NPTS NT= 1 1 9 103  
NL(1)= 1 3 4 5 6 8 9 10 12  
BB = 5.526 1.574 3.779 2.557 2.656 3.388 1.187 6.678

HPTURB ITER = 10 AT TIME = 54.000 MSEC. DELMAX = 0.024287 SCALE = 1.000000

HPTURB ITER = 10 AT TIME = 55.000 MSEC. DELMAX = 0.015678 SCALE = 1.000000

HPTURB ITER = 10 AT TIME = 56.000 MSEC. DELMAX = 0.011486 SCALE = 1.000000

HBPLAY TIME = 57.000 MSEC. NH,NB,NPTS NT= 1 2 7 181  
NL(1)= 13 18 19 21 22 24 27  
BB = 12.143 1.887 4.955 6.406 3.880 12.372

HPTURB ITER = 10 AT TIME = 57.000 MSEC. DELMAX = 0.385309 SCALE = 0.259532

HBPLAY TIME = 58.000 MSEC. NH,NB,NPTS NT= 1 2 8 181  
NL(1)= 13 18 19 20 21 22 24 27  
BB = 12.143 1.887 1.817 3.139 6.406 3.880 12.372

HPTURB ITER = 10 AT TIME = 58.000 MSEC. DELMAX = 0.443658 SCALE = 0.225399

HBPLAY TIME = 59.000 MSEC. NH,NB,NPTS NT= 1 2 9 181  
NL(1)= 13 16 18 19 20 21 22 24 27  
BB = 7.889 4.253 1.887 1.817 3.139 6.406 3.974 12.277

HPTURB ITER = 10 AT TIME = 59.000 MSEC. DELMAX = 0.052001 SCALE = 1.000000

HBPLAY TIME = 60.000 MSEC. NH,NB,NPTS NT= 1 2 8 181  
NL(1)= 13 18 19 20 21 22 24 27  
BB = 12.143 1.887 1.817 3.139 6.406 4.086 12.165

HPTURB ITER = 10 AT TIME = 60.000 MSEC. DELMAX = 0.057808 SCALE = 1.000000

HBPLAY TIME = 61.000 MSEC. NH,NB,NPTS NT= 1 2 7 181  
NL(1)= 13 18 20 21 22 24 27  
BB = 12.143 3.703 3.139 6.406 4.156 12.096

HPTURB ITER = 10 AT TIME = 61.000 MSEC. DELMAX = 0.015872 SCALE = 1.000000

HPTURB ITER = 10 AT TIME = 62.000 MSEC. DELMAX = 0.022130 SCALE = 1.000000

HPTURB ITER = 10 AT TIME = 63.000 MSEC. DELMAX = 0.015337 SCALE = 1.000000

HBPLAY TIME = 64.000 MSEC. NH,NB,NPTS NT= 1 2 6 181  
NL(1)= 13 18 20 21 22 27  
BB = 12.143 3.703 3.139 6.406 16.252

HPTURB ITER = 10 AT TIME = 64.000 MSEC. DELMAX = 0.011067 SCALE = 1.000000

HBPLAY TIME = 66.000 MSEC. NH,NB,NPTS NT= 1 1 8 103  
NL(1)= 1 3 4 5 6 8 9 12  
BB = 5.526 1.574 3.779 2.557 2.656 3.388 7.865

HPTURB ITER = 10 AT TIME = 67.000 MSEC. DELMAX = 0.011853 SCALE = 1.000000

HPTURB ITER = 10 AT TIME = 69.000 MSEC. DELMAX = 0.013454 SCALE = 1.000000

DINT CONV. TEST 72.000 N ANG VEL 22.55 0.2652E-02 0.1176E-03 0.1000E-03 0.1000E-03 0.1000E-03

TEST FAILED AT TIME = 0.072000 FOR H = 0.001000

DINT CONV. TEST 73.000 N ANG VEL 23.86 0.3624E-02 0.1518E-03 0.1000E-03 0.1000E-03 0.1000E-03

TEST FAILED AT TIME = 0.073000 FOR H = 0.001000

DINT CONV. TEST 74.000 N ANG VEL 26.11 0.3039E-02 0.1164E-03 0.1000E-03 0.1000E-03 0.1000E-03

TEST FAILED AT TIME = 0.074000 FOR H = 0.001000

SEGMENT	(INERTIAL)			(LOCAL)			(LOCAL)		
	ANGULAR ROTATION (DEG)			ANGULAR VELOCITY (RAD/SEC.)			ANGULAR ACCELERATION (RAD/SEC.**2)		
	YAW	PITCH	ROLL	X	Y	Z	X	Y	Z
1 LT	10.9078	40.4616	-2.5237	-3.50101	6.77176	3.01702	-712.525841	-923.312215	-344.896206
2 CT	5.8648	8.3877	-35.0629	-28.78011	38.13662	26.32712	2669.823703	4863.705052	714.436129
3 UT	22.6603	16.1876	4.2073	-4.55898	-8.33212	11.28470	-833.189019	-740.536145	24.730107
4 N	9.4134	-28.3216	9.0212	3.10468	-11.10456	11.62142	-474.529280	-2359.202265	525.452347
5 H	-14.7037	-62.0894	29.6482	16.06835	-58.33883	6.84809	321.909908	-351.659929	252.225950
6 RUL	11.0166	100.4701	10.5736	-0.26043	-3.94123	-2.59116	-82.766870	-780.201793	66.972957
7 RLL	-2.0078	53.9069	-3.2449	-2.05452	9.15294	-1.60027	12.275725	-89.117047	79.212811
8 RF	-1.2125	146.0433	2.4774	3.41634	1.03537	-1.56581	-92.295830	747.087281	-23.919556
9 LUL	4.3688	101.7927	4.4680	-0.37199	-3.33541	-0.44435	-290.296221	-679.956631	528.292676
10 LLL	-0.9289	45.3497	-1.2981	-0.57596	5.97768	0.06395	278.790377	-4.508498	528.778814
11 LF	-0.5610	155.8698	1.6050	1.79239	0.13205	-0.59660	-177.520464	1209.576339	196.625307
12 RUA	-75.0950	70.5657	-80.2833	-6.23227	-4.14211	-1.63954	244.397026	-3261.631891	-168.345676
13 RLA	-21.0534	51.2884	-31.6271	-6.18955	1.21106	1.79408	113.635226	2487.522774	-303.100899
14 LUA	-17.8558	62.4794	-23.3643	-2.95595	-0.00123	5.46149	322.014086	-2838.181399	888.201217
15 LLA	-16.0460	60.3973	-21.7744	-2.73881	-15.25083	5.57354	441.700349	4146.746559	916.611615
16 VEH	0.0000	0.0000	0.0000	0.00000	0.00000	0.00000	0.000000	0.000000	0.000000

SEGMENT	(INERTIAL)			(INERTIAL)			(INERTIAL)		
	LINEAR POSITION ( IN.)			LINEAR VELOCITY ( IN./SEC.)			LINEAR ACCELERATIONS (G'S)		
	X	Y	Z	X	Y	Z	X	Y	Z
1 LT	6.0377	0.0702	-13.0395	-334.65671	-2.92122	-92.21272	1.118456	-3.419755	-24.241372
2 CT	3.5221	-1.5083	-17.2697	-403.89532	-63.36301	-39.55188	-7.411998	0.308363	-23.341359
3 UT	1.5893	-2.7194	-24.7657	-399.28403	-115.11128	-20.63141	-8.535068	3.408484	-20.077252
4 N	-0.4611	-2.8941	-33.1662	-319.46157	-121.58509	-38.64033	16.009901	-4.901599	-22.093312
5 H	4.8568	-1.0902	-36.0984	-178.47710	-69.83431	287.80272	-29.256214	-10.703850	8.134162
6 RUL	13.6013	3.3950	-14.9332	-345.17072	-4.32318	-59.80904	2.896528	-1.986709	-14.025632
7 RLL	29.0739	3.6383	-12.6201	-300.76311	12.64266	-73.16830	3.883535	0.620604	6.154392
8 RF	39.4986	3.6714	-8.4455	-258.02278	23.08008	-137.61724	0.173190	0.601745	-0.915789
9 LUL	15.0441	-3.3466	-14.9210	-314.88548	2.85212	-60.25035	6.374569	3.680291	-3.334002
10 LLL	29.7934	-3.3024	-12.0614	-278.81100	10.63011	-57.36381	9.156247	6.479980	13.521611
11 LF	39.2761	-3.3229	-7.6097	-244.93381	11.69052	-92.38042	4.608846	0.164379	1.561647
12 RUA	3.1574	3.4023	-29.0240	-426.99852	-109.61718	-32.04897	-2.643843	6.759738	6.506879
13 RLA	15.1710	5.9986	-24.3530	-429.54688	-25.03050	-46.34975	23.116917	3.958924	9.885922
14 LUA	7.1965	-8.0306	-27.9271	-282.38560	-78.35066	-29.72059	-9.173876	2.088389	27.959874
15 LLA	19.2594	-6.2444	-21.8664	-343.80786	-23.50199	71.96752	11.107169	-20.329519	-12.311190
16 VEH	-12.3548	0.0000	0.0000	-308.87040	0.00000	0.00000	0.000000	0.000000	0.000000



POSTPROCESSOR CONTROL PARAMETERS

N.11	HIC & HSI POINT	CSI POINT
	2	1

DATE: 2 SEPT 1988

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 21.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

## POINT TOTAL ACCELERATION (G'S)

TIME (MSEC)	POINT ( 0.00, 0.00, 0.00) ON SEGMENT NO. 3 - UT				POINT ( 0.00, 0.00, 0.00) ON SEGMENT NO. -5 - H				POINT ( 0.00, 0.00, 0.00) ON SEGMENT NO. 5 - H			
	IN UT REFERENCE				ACCELEROMETER (1G)				IN VEH REFERENCE			
	X	Y	Z	RES	X	Y	Z	RES	X	Y	Z	RES
0.000	-0.020	0.000	-0.082	0.084	-0.262	0.000	0.890	0.928	-0.047	0.000	-0.073	0.087
2.000	-0.014	0.000	-0.107	0.108	-0.260	0.000	0.865	0.903	-0.051	0.000	-0.098	0.111
4.000	-0.007	0.000	-0.179	0.179	-0.258	0.000	0.793	0.834	-0.067	0.000	-0.168	0.181
6.000	-0.006	-0.003	-0.247	0.247	-0.269	0.000	0.725	0.774	-0.093	0.000	-0.232	0.250
8.000	-0.019	-0.012	-0.314	0.315	-0.306	-0.002	0.658	0.725	-0.144	-0.002	-0.289	0.323
10.000	-0.061	-0.023	-0.386	0.391	-0.379	-0.005	0.586	0.698	-0.233	-0.005	-0.342	0.413
12.000	-0.091	-0.032	-0.464	0.474	-0.475	-0.008	0.507	0.695	-0.344	-0.008	-0.396	0.525
14.000	-0.099	-0.023	-0.547	0.556	-0.487	-0.006	0.425	0.646	-0.375	-0.006	-0.474	0.604
16.000	-0.132	-0.024	-0.623	0.638	-0.506	-0.007	0.348	0.614	-0.411	-0.007	-0.544	0.682
18.000	-0.111	-0.005	-0.719	0.727	-0.510	-0.003	0.253	0.570	-0.437	-0.003	-0.635	0.771
20.000	-0.133	-0.001	-0.791	0.802	-0.525	-0.002	0.181	0.555	-0.468	-0.002	-0.702	0.844
22.000	-0.197	-0.016	-0.854	0.876	-0.551	-0.005	0.119	0.564	-0.509	-0.006	-0.756	0.911
24.000	-0.382	-0.063	-1.317	1.373	-0.662	-0.179	-0.342	0.767	-0.724	-0.179	-1.179	1.395
26.000	-0.390	-0.112	-1.296	1.358	-0.685	-0.231	-0.314	0.788	-0.739	-0.231	-1.147	1.384
28.000	-0.357	0.556	-1.166	1.340	-0.682	-0.014	-0.181	0.705	-0.705	-0.014	-1.019	1.239
30.000	-0.438	0.816	-1.246	1.553	-0.702	0.035	-0.256	0.748	-0.742	0.035	-1.087	1.317
32.000	-2.733	-0.835	-0.461	2.895	-1.271	-0.218	0.576	1.412	-1.106	-0.220	-0.149	1.137
34.000	-2.186	-0.420	-0.403	2.263	-1.208	-0.216	0.667	1.397	-1.025	-0.219	-0.076	1.051
36.000	-3.145	-0.474	-0.313	3.196	-1.481	-0.353	0.849	1.743	-1.252	-0.357	0.159	1.312
38.000	-4.178	-0.580	-1.221	4.391	-1.843	-0.709	0.133	1.979	-1.769	-0.710	-0.467	1.963
40.000	-5.137	0.364	-1.250	5.299	-2.004	-0.530	0.280	2.092	-1.897	-0.533	-0.297	1.993
42.000	-6.838	1.397	-2.254	7.334	-2.388	-0.543	-0.390	2.479	-2.417	-0.540	-0.885	2.630
44.000	-14.419	-3.743	0.830	14.920	-4.097	-1.242	3.893	5.787	-3.227	-1.300	3.624	5.024
46.000	-16.621	-1.760	-0.518	16.722	-4.375	-1.075	3.474	5.689	-3.633	-1.143	3.226	4.991
48.000	-21.535	0.772	0.632	21.558	-4.411	-0.608	5.515	7.088	-3.372	-0.744	5.190	6.234
50.000	-41.704	-14.755	6.467	44.707	-8.393	-3.295	18.145	20.262	-5.470	-3.858	18.124	19.321
52.000	-46.097	-12.754	8.809	48.633	-8.850	-2.015	24.198	25.844	-5.684	-2.996	24.033	24.877
54.000	-59.506	-18.177	14.142	63.807	-11.972	-2.812	40.775	42.589	-8.224	-4.949	40.493	41.615
56.000	-60.433	-15.422	13.472	63.808	-11.763	-2.643	48.226	49.710	-9.706	-5.876	47.398	48.737
58.000	-73.471	-17.978	-2.410	75.677	-11.839	-4.818	45.094	46.871	-12.593	-8.610	43.319	45.927
60.000	-93.922	-15.685	14.909	96.382	-10.687	1.243	64.829	65.716	-16.338	-5.515	62.414	64.752
62.000	-39.398	-7.543	-3.263	40.247	-8.458	0.385	50.073	50.783	-16.781	-5.749	46.585	49.848
64.000	-13.416	-3.242	-10.799	17.525	-4.985	0.413	34.219	34.583	-13.561	-4.374	30.511	33.674
66.000	2.837	-2.587	-20.041	20.406	-4.396	-0.971	17.138	17.719	-9.978	-3.581	13.198	16.929
68.000	12.171	-3.027	-29.353	31.921	-6.574	-2.288	10.557	12.647	-10.367	-3.898	5.106	12.195
70.000	12.817	-4.431	-27.755	30.891	-6.991	-2.721	11.812	13.993	-11.904	-4.656	4.693	13.617
72.000	8.827	-2.877	-26.335	27.924	-5.142	-2.316	12.679	13.876	-11.519	-4.665	5.172	13.461
74.000	3.362	-1.720	-32.445	32.664	-5.688	-2.458	13.892	15.211	-13.307	-5.198	4.223	14.897
76.000	-2.984	1.218	-32.702	32.861	-6.355	-2.850	21.202	22.317	-19.656	-7.488	6.458	22.003
78.000	-4.104	3.340	-30.967	31.417	-5.758	-2.791	26.452	27.215	-24.295	-9.144	7.173	26.932
80.000	-0.706	4.868	-21.526	22.081	-3.903	-2.154	32.157	32.464	-29.256	-10.704	8.134	32.197

DATE: 2 SEPT 1988

PAGE 27

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPTOID FOR DASH BOARD

PAGE: 22.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

POINT REL. VELOCITY ( IN./SEC.)

TIME (MSEC)	POINT ( 0.00, 0.00, 0.00) ON SEGMENT NO. 3 - UT				POINT ( 0.00, 0.00, 0.00) ON SEGMENT NO. 5 - H				POINT ( 0.00, 0.00, 0.00) ON SEGMENT NO. 5 - H			
	IN VEH REFERENCE				IN VEH REFERENCE				IN UT REFERENCE			
	X	Y	Z	RES	X	Y	Z	RES	X	Y	Z	RES
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2.000	0.357	0.000	-0.064	0.362	0.349	0.000	-0.062	0.355	-0.008	0.000	0.000	0.008
4.000	1.482	0.000	-0.168	1.491	1.463	0.000	-0.163	1.472	-0.020	0.000	0.000	0.020
6.000	3.368	-0.002	-0.329	3.384	3.332	0.000	-0.320	3.347	-0.037	0.002	0.000	0.037
8.000	6.010	-0.010	-0.534	6.034	5.944	-0.002	-0.519	5.967	-0.067	0.008	0.000	0.068
10.000	9.392	-0.024	-0.792	9.425	9.275	-0.005	-0.764	9.307	-0.120	0.019	0.000	0.121
12.000	13.502	-0.048	-1.096	13.546	13.296	-0.010	-1.048	13.338	-0.211	0.038	0.000	0.214
14.000	18.360	-0.073	-1.462	18.418	18.037	-0.016	-1.386	18.090	-0.332	0.057	0.000	0.336
16.000	23.966	-0.096	-1.885	24.040	23.526	-0.022	-1.782	23.593	-0.452	0.074	-0.001	0.458
18.000	30.318	-0.118	-2.369	30.411	29.761	-0.028	-2.239	29.845	-0.572	0.090	-0.001	0.579
20.000	37.426	-0.138	-2.913	37.539	36.747	-0.034	-2.754	36.851	-0.697	0.104	-0.001	0.704
22.000	45.254	-0.173	-3.495	45.389	44.477	-0.043	-3.312	44.601	-0.798	0.130	-0.001	0.808
24.000	53.624	-0.222	-4.417	53.806	52.814	-0.157	-4.225	52.983	-0.832	0.065	-0.001	0.835
26.000	62.779	-0.294	-5.297	63.002	61.919	-0.307	-5.089	62.128	-0.885	-0.012	0.003	0.885
28.000	72.709	-0.176	-6.137	72.968	71.793	-0.419	-5.907	72.037	-0.945	-0.242	0.010	0.975
30.000	83.404	0.352	-6.915	83.690	82.451	-0.398	-6.666	82.721	-0.986	-0.749	0.019	1.238
32.000	94.080	0.535	-7.240	94.360	93.727	-0.423	-7.110	93.997	-0.376	-0.957	0.041	1.029
34.000	104.889	0.071	-7.234	105.138	105.604	-0.633	-7.306	105.859	0.710	-0.706	0.097	1.006
36.000	116.510	-0.408	-7.277	116.737	118.233	-0.984	-7.495	118.474	1.722	-0.585	0.197	1.830
38.000	127.722	-1.024	-7.102	127.923	131.306	-1.474	-7.573	131.533	3.590	-0.474	0.404	3.643
40.000	139.233	-1.201	-6.715	139.400	145.087	-1.867	-7.440	145.290	5.849	-0.719	0.720	5.937
42.000	149.450	-0.660	-6.479	149.592	158.571	-2.237	-7.528	158.765	9.079	-1.685	1.225	9.315
44.000	155.812	-0.836	-4.740	155.887	170.774	-2.712	-6.337	170.913	14.855	-2.106	2.198	15.163
46.000	157.720	-3.088	-1.115	157.754	181.675	-3.707	-3.283	181.743	23.690	-1.112	4.061	24.061
48.000	156.096	-4.584	3.913	156.213	191.901	-4.378	0.957	191.953	35.308	-0.762	6.593	35.927
50.000	141.126	-13.942	16.832	142.808	199.739	-6.638	13.452	200.301	57.525	5.185	12.814	59.163
52.000	122.195	-24.412	32.266	128.719	206.670	-9.011	29.910	209.017	82.311	11.324	21.803	85.900
54.000	94.373	-38.752	54.224	115.535	211.079	-12.280	56.971	218.976	112.157	18.960	37.279	119.701
56.000	63.940	-52.830	78.311	114.069	213.707	-16.371	91.124	232.899	141.171	23.677	58.599	154.673
58.000	27.937	-68.681	99.258	123.894	214.085	-21.715	126.806	249.767	171.680	26.531	86.244	193.948
60.000	-48.785	-89.387	132.584	167.178	209.556	-25.937	169.668	270.875	238.362	28.911	120.368	268.591
62.000	-77.547	-101.219	145.352	193.355	203.606	-30.570	209.855	293.988	252.303	25.298	154.604	296.984
64.000	-88.016	-107.303	145.939	201.393	199.040	-34.244	238.403	312.451	249.362	19.440	183.655	310.304
66.000	-87.056	-109.586	135.436	194.758	196.297	-37.048	254.173	323.279	237.429	13.587	207.586	315.673
68.000	-81.208	-110.824	115.623	179.570	193.532	-39.896	261.153	327.486	220.628	9.256	230.063	318.891
70.000	-73.848	-112.242	90.482	161.984	189.212	-43.176	264.497	328.061	200.518	6.746	252.981	322.881
72.000	-68.106	-113.520	68.202	148.919	183.289	-46.872	268.296	328.290	181.488	4.619	273.349	328.145
74.000	-67.903	-114.780	45.146	140.795	177.090	-50.470	271.958	328.435	167.908	1.761	295.644	340.002
76.000	-74.122	-116.052	20.340	139.197	166.505	-55.141	276.104	327.105	156.313	-2.407	320.292	356.408
78.000	-83.506	-116.413	-2.649	143.291	150.797	-61.731	281.259	325.049	143.815	-8.988	343.115	372.145
80.000	-90.414	-115.111	-20.631	147.820	130.393	-69.834	287.803	323.589	126.450	-16.916	360.086	382.017

DATE: 2 SEPT 1988  
 RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
 TWO BELT HARNESS WITH HYPERELLIPTOID FOR DASH BOARD  
 VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK  
 CRASH VICTIM: 95TH PERCENTILE MALE

PAGE: 23.01

## POINT REL. LINEAR DISPLACEMENT ( IN. )

TIME (MSEC)	POINT ( 0.00, 0.00, 0.00 ) ON SEGMENT NO. 3 - UT IN VEH REFERENCE				POINT ( 0.00, 0.00, 0.00 ) ON SEGMENT NO. 5 - H IN VEH REFERENCE				POINT ( 0.00, 0.00, 0.00 ) ON SEGMENT NO. 5 - H IN UT REFERENCE			
	X	Y	Z	RES	X	Y	Z	RES	X	Y	Z	RES
0.000	11.314	0.000	-26.938	29.217	7.775	0.000	-41.833	42.550	-0.022	0.000	-15.310	15.310
2.000	11.314	0.000	-26.938	29.218	7.775	0.000	-41.833	42.550	-0.022	0.000	-15.310	15.310
4.000	11.316	0.000	-26.938	29.218	7.777	0.000	-41.834	42.550	-0.022	0.000	-15.310	15.310
6.000	11.320	0.000	-26.939	29.221	7.782	0.000	-41.834	42.552	-0.023	0.000	-15.310	15.310
8.000	11.330	0.000	-26.940	29.225	7.791	0.000	-41.835	42.554	-0.023	0.000	-15.310	15.310
10.000	11.345	0.000	-26.941	29.232	7.806	0.000	-41.836	42.558	-0.022	0.000	-15.310	15.310
12.000	11.368	0.000	-26.943	29.243	7.828	0.000	-41.838	42.564	-0.022	0.000	-15.310	15.310
14.000	11.400	0.000	-26.945	29.257	7.860	0.000	-41.840	42.572	-0.021	0.000	-15.310	15.310
16.000	11.442	0.000	-26.949	29.277	7.901	0.000	-41.844	42.583	-0.020	0.001	-15.310	15.310
18.000	11.496	-0.001	-26.953	29.302	7.954	0.000	-41.848	42.597	-0.017	0.001	-15.310	15.310
20.000	11.564	-0.001	-26.958	29.334	8.021	0.000	-41.853	42.614	-0.015	0.001	-15.310	15.310
22.000	11.646	-0.001	-26.965	29.372	8.102	0.000	-41.859	42.636	-0.011	0.002	-15.310	15.310
24.000	11.745	-0.002	-26.972	29.419	8.199	0.000	-41.866	42.661	-0.005	0.004	-15.310	15.310
26.000	11.861	-0.002	-26.982	29.474	8.314	-0.001	-41.876	42.693	0.003	0.008	-15.310	15.310
28.000	11.996	-0.003	-26.994	29.539	8.447	-0.002	-41.887	42.730	0.014	0.016	-15.310	15.310
30.000	12.152	-0.003	-27.007	29.615	8.601	-0.003	-41.899	42.773	0.027	0.024	-15.310	15.310
32.000	12.330	-0.001	-27.021	29.701	8.777	-0.003	-41.913	42.822	0.044	0.032	-15.310	15.310
34.000	12.529	-0.001	-27.036	29.798	8.977	-0.004	-41.928	42.878	0.069	0.042	-15.310	15.310
36.000	12.750	-0.001	-27.050	29.905	9.200	-0.006	-41.943	42.940	0.102	0.058	-15.309	15.309
38.000	12.995	-0.003	-27.065	30.023	9.450	-0.008	-41.958	43.009	0.147	0.081	-15.308	15.309
40.000	13.262	-0.005	-27.079	30.152	9.726	-0.012	-41.973	43.085	0.206	0.112	-15.306	15.308
42.000	13.551	-0.007	-27.092	30.292	10.030	-0.016	-41.988	43.169	0.279	0.149	-15.303	15.306
44.000	13.857	-0.007	-27.104	30.441	10.360	-0.021	-42.002	43.261	0.371	0.191	-15.298	15.303
46.000	14.171	-0.011	-27.110	30.590	10.712	-0.027	-42.012	43.356	0.499	0.245	-15.288	15.298
48.000	14.486	-0.019	-27.107	30.735	11.086	-0.035	-42.014	43.452	0.659	0.307	-15.273	15.290
50.000	14.784	-0.037	-27.087	30.859	11.478	-0.046	-42.001	43.541	0.868	0.380	-15.247	15.276
52.000	15.048	-0.075	-27.039	30.944	11.884	-0.062	-41.958	43.609	1.144	0.470	-15.201	15.252
54.000	15.266	-0.138	-26.953	30.976	12.302	-0.083	-41.873	43.643	1.497	0.561	-15.128	15.212
56.000	15.424	-0.230	-26.821	30.940	12.727	-0.111	-41.726	43.624	1.939	0.645	-15.010	15.148
58.000	15.520	-0.349	-26.641	30.834	13.156	-0.149	-41.507	43.543	2.449	0.714	-14.836	15.054
60.000	15.493	-0.507	-26.412	30.624	13.579	-0.197	-41.214	43.394	2.991	0.751	-14.606	14.928
62.000	15.361	-0.699	-26.130	30.319	13.993	-0.253	-40.832	43.164	3.548	0.697	-14.323	14.772
64.000	15.193	-0.909	-25.837	29.987	14.395	-0.318	-40.382	42.872	4.108	0.585	-13.976	14.579
66.000	15.017	-1.126	-25.554	29.661	14.790	-0.390	-39.887	42.543	4.633	0.439	-13.579	14.354
68.000	14.848	-1.347	-25.302	29.368	15.180	-0.466	-39.371	42.199	5.107	0.285	-13.141	14.101
70.000	14.693	-1.569	-25.096	29.123	15.563	-0.549	-38.845	41.851	5.528	0.131	-12.660	13.815
72.000	14.552	-1.795	-24.938	28.929	15.936	-0.639	-38.313	41.500	5.887	-0.018	-12.144	13.496
74.000	14.417	-2.024	-24.824	28.778	16.297	-0.737	-37.772	41.145	6.179	-0.156	-11.604	13.147
76.000	14.275	-2.255	-24.759	28.668	16.641	-0.842	-37.225	40.784	6.409	-0.281	-11.038	12.767
78.000	14.118	-2.487	-24.742	28.595	16.959	-0.959	-36.667	40.411	6.577	-0.392	-10.451	12.355
80.000	13.944	-2.719	-24.766	28.551	17.242	-1.090	-36.098	40.019	6.684	-0.491	-9.851	11.915



DATE: 2 SEPT 1988  
 RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
 TWO BELT HARNESS WITH HYPERELLIPOID FOR DASH BOARD  
 VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK  
 CRASH VICTIM: 95TH PERCENTILE MALE

PAGE: 24.01

## SEGMENT ANGULAR ACCELERATION (REV/SEC.\*\*2)

TIME (MSEC)	SEGMENT NO. 3 - UT				SEGMENT NO. 5 - H				SEGMENT NO. 5 - H			
	IN	UT	REFERENCE	RES	IN	H	REFERENCE	RES	IN	VEH	REFERENCE	RES
	X	Y	Z		X	Y	Z		X	Y	Z	
0.000	0.000	-0.137	0.000	0.137	0.000	-0.185	0.000	0.185	0.000	-0.185	0.000	0.185
2.000	0.001	-0.042	0.002	0.043	-0.001	-0.052	0.000	0.052	-0.001	-0.052	0.000	0.052
4.000	0.006	0.040	0.015	0.043	-0.006	-0.067	0.000	0.067	-0.006	-0.067	0.002	0.067
6.000	-0.004	0.247	0.049	0.252	0.021	-0.177	-0.001	0.178	0.020	-0.177	-0.005	0.178
8.000	-0.039	0.665	0.129	0.678	0.107	-0.365	-0.002	0.380	0.104	-0.365	-0.027	0.380
10.000	-0.080	1.188	0.277	1.223	0.221	-0.482	0.002	0.530	0.215	-0.482	-0.050	0.530
12.000	-0.118	1.611	0.416	1.669	0.332	-0.264	0.016	0.424	0.326	-0.264	-0.062	0.424
14.000	-0.083	1.943	0.457	1.997	0.283	-0.730	0.029	0.784	0.282	-0.730	-0.038	0.784
16.000	-0.087	2.460	0.635	2.542	0.302	-1.430	0.043	1.462	0.303	-1.430	-0.029	1.462
18.000	0.008	2.589	0.664	2.673	0.141	-1.610	0.060	1.617	0.151	-1.610	0.026	1.617
20.000	0.037	2.973	0.948	3.120	0.102	-2.115	0.080	2.119	0.118	-2.115	0.054	2.119
22.000	-0.010	3.607	1.429	3.879	0.244	-3.094	0.108	3.106	0.262	-3.094	0.048	3.106
24.000	-8.600	7.157	4.770	12.171	7.768	-7.307	0.183	10.666	7.598	-7.307	-1.626	10.666
26.000	-9.914	7.450	4.950	13.353	10.014	-8.144	0.309	12.911	9.812	-8.143	-2.022	12.911
28.000	-1.602	6.837	5.335	8.819	0.731	-7.928	0.450	7.974	0.814	-7.928	0.260	7.974
30.000	-2.418	7.045	5.092	9.022	-1.971	-8.546	0.594	8.791	-1.785	-8.548	1.017	8.791
32.000	-5.518	18.566	11.214	22.381	8.491	-29.792	0.788	30.988	8.434	-29.793	-1.243	30.988
34.000	-5.789	14.342	10.997	18.977	8.985	-28.116	1.107	29.537	8.988	-28.117	-1.045	29.537
36.000	-10.236	20.115	12.679	25.887	15.101	-38.011	1.455	40.927	15.018	-38.013	-2.127	40.927
38.000	-27.100	26.891	17.134	41.846	30.178	-51.830	1.903	60.006	29.806	-51.828	-5.111	60.006
40.000	-22.699	24.663	16.092	37.182	22.068	-57.722	2.414	61.843	21.998	-57.727	-2.878	61.843
42.000	-30.498	28.252	24.219	48.113	21.827	-71.925	2.986	75.223	21.854	-71.937	-2.442	75.223
44.000	-32.187	56.105	49.690	81.565	50.733	-136.186	3.903	145.381	50.213	-136.179	-8.335	145.381
46.000	-28.042	37.572	48.859	67.714	44.955	-148.639	5.635	155.391	44.854	-148.665	-5.761	155.391
48.000	-20.702	-4.036	40.577	45.731	24.155	-149.938	7.474	152.055	24.678	-150.038	-0.423	152.055
50.000	-48.385	37.032	81.432	101.704	139.703	-302.280	11.206	333.190	138.788	-302.255	-19.874	333.190
52.000	20.899	8.412	77.489	80.698	86.870	-320.679	15.481	332.598	87.017	-320.899	-8.573	332.598
54.000	21.075	54.615	169.909	179.711	120.265	-438.481	21.646	455.190	120.241	-438.852	-12.223	455.190
56.000	15.799	22.276	164.884	167.130	113.182	-428.843	29.299	444.494	113.279	-429.795	-4.359	444.494
58.000	-70.850	-73.615	-213.885	237.035	205.076	-427.000	36.749	475.117	204.444	-428.864	3.808	475.117
60.000	213.357	-282.895	320.674	477.894	-54.947	-386.330	39.469	392.208	-56.394	-388.083	-6.237	392.208
62.000	88.426	-23.362	27.240	95.430	-20.082	-300.005	42.593	303.679	-23.448	-302.770	1.119	303.679
64.000	44.445	-34.608	-63.285	84.723	-20.168	-163.484	40.696	169.676	-26.390	-147.272	10.665	169.676
66.000	-14.123	-63.981	-141.182	155.645	35.355	-125.898	37.342	135.996	24.564	-131.014	26.957	135.996
68.000	-37.438	-24.558	-71.335	84.222	82.975	-179.967	36.180	201.450	67.795	-186.059	36.984	201.450
70.000	-38.031	-65.178	-38.947	84.920	90.968	-166.521	37.777	193.473	68.935	-174.339	47.809	193.473
72.000	-58.153	-115.779	-40.978	135.889	65.468	-76.947	39.363	108.427	34.892	-86.935	54.600	108.427
74.000	-73.956	-128.701	-33.634	152.200	71.790	-104.065	35.913	131.427	39.042	-114.114	52.218	131.427
76.000	-108.913	-153.734	-12.238	188.802	85.877	-134.273	35.927	163.386	46.823	-145.589	57.501	163.386
78.000	-133.289	-152.796	3.154	202.787	80.966	-120.334	37.667	149.849	34.375	-133.462	58.829	149.849
80.000	-132.606	-117.860	3.936	177.457	51.234	-55.968	40.143	85.842	-0.345	-70.727	48.645	85.842

DATE: 2 SEPT 1988

PAGE 30

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 25.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

## SEGMENT REL. ANGULAR VELOCITY (REV/SEC.)

TIME (MSEC)	SEGMENT NO. 3 - UT				SEGMENT NO. 5 - H				SEGMENT NO. 5 - H			
	IN VEH REFERENCE				IN VEH REFERENCE				IN H REFERENCE			
	X	Y	Z	RES	X	Y	Z	RES	X	Y	Z	RES
0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
4.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
6.000	0.000	0.000	0.000	0.000	0.000	-0.001	0.000	0.001	0.000	-0.001	0.000	0.001
8.000	0.000	0.001	0.000	0.001	0.000	-0.001	0.000	0.001	0.000	-0.001	0.000	0.001
10.000	0.000	0.003	0.001	0.003	0.001	-0.002	0.000	0.002	0.001	-0.002	0.000	0.002
12.000	0.000	0.006	0.002	0.006	0.001	-0.003	0.000	0.003	0.001	-0.003	0.000	0.003
14.000	0.000	0.009	0.003	0.010	0.002	-0.004	0.000	0.004	0.002	-0.004	0.000	0.004
16.000	0.000	0.014	0.004	0.014	0.002	-0.006	0.000	0.006	0.002	-0.006	0.000	0.006
18.000	0.000	0.019	0.005	0.019	0.003	-0.009	0.000	0.009	0.003	-0.009	0.000	0.009
20.000	0.000	0.024	0.006	0.025	0.004	-0.013	0.000	0.013	0.004	-0.013	0.000	0.013
22.000	0.001	0.031	0.009	0.032	0.005	-0.018	-0.001	0.019	0.005	-0.018	0.001	0.019
24.000	-0.012	0.044	0.021	0.050	0.016	-0.031	-0.003	0.035	0.017	-0.031	0.001	0.035
26.000	-0.026	0.058	0.033	0.072	0.033	-0.046	-0.007	0.057	0.034	-0.046	0.001	0.057
28.000	-0.036	0.072	0.046	0.093	0.046	-0.062	-0.009	0.077	0.047	-0.062	0.002	0.077
30.000	-0.036	0.085	0.055	0.108	0.044	-0.078	-0.007	0.089	0.044	-0.078	0.003	0.089
32.000	-0.037	0.112	0.075	0.139	0.045	-0.114	-0.006	0.123	0.045	-0.114	0.004	0.123
34.000	-0.049	0.146	0.102	0.185	0.067	-0.174	-0.010	0.187	0.067	-0.174	0.006	0.187
36.000	-0.076	0.180	0.132	0.236	0.105	-0.236	-0.016	0.258	0.106	-0.236	0.009	0.258
38.000	-0.114	0.231	0.174	0.311	0.158	-0.331	-0.025	0.367	0.159	-0.331	0.012	0.367
40.000	-0.139	0.277	0.212	0.376	0.200	-0.436	-0.031	0.481	0.202	-0.436	0.017	0.481
42.000	-0.172	0.326	0.260	0.452	0.239	-0.565	-0.035	0.614	0.240	-0.565	0.022	0.614
44.000	-0.196	0.409	0.348	0.571	0.285	-0.766	-0.041	0.818	0.287	-0.766	0.029	0.818
46.000	-0.235	0.504	0.469	0.728	0.385	-1.056	-0.056	1.125	0.388	-1.056	0.038	1.125
48.000	-0.229	0.530	0.567	0.809	0.447	-1.355	-0.060	1.428	0.449	-1.355	0.051	1.428
50.000	-0.241	0.669	0.811	1.079	0.652	-1.933	-0.092	2.042	0.655	-1.933	0.069	2.042
52.000	-0.192	0.728	0.993	1.246	0.850	-2.558	-0.116	2.698	0.854	-2.558	0.096	2.698
54.000	-0.059	0.902	1.343	1.618	1.071	-3.411	-0.144	3.578	1.075	-3.411	0.132	3.578
56.000	0.073	1.021	1.706	1.989	1.296	-4.299	-0.161	4.493	1.300	-4.297	0.183	4.493
58.000	0.050	0.985	1.756	2.014	1.581	-5.149	-0.162	5.389	1.586	-5.144	0.249	5.389
60.000	0.638	0.350	2.155	2.274	1.585	-6.117	-0.179	6.321	1.591	-6.109	0.325	6.321
62.000	0.889	0.383	2.284	2.480	1.553	-6.864	-0.186	7.040	1.563	-6.852	0.408	7.040
64.000	0.999	0.342	2.217	2.456	1.491	-7.290	-0.171	7.443	1.512	-7.271	0.492	7.443
66.000	0.984	0.240	2.039	2.276	1.477	-7.552	-0.134	7.696	1.514	-7.524	0.570	7.696
68.000	0.901	0.147	1.885	2.095	1.563	-7.860	-0.072	8.014	1.626	-7.821	0.642	8.014
70.000	0.823	0.060	1.817	1.996	1.708	-8.236	0.012	8.412	1.807	-8.184	0.716	8.412
72.000	0.766	-0.148	1.772	1.936	1.824	-8.529	0.116	8.722	1.975	-8.458	0.794	8.722
74.000	0.692	-0.414	1.729	1.908	1.879	-8.677	0.222	8.881	2.095	-8.586	0.868	8.881
76.000	0.606	-0.733	1.717	1.963	1.971	-8.960	0.328	9.180	2.256	-8.849	0.939	9.180
78.000	0.491	-1.104	1.763	2.138	2.058	-9.256	0.445	9.492	2.428	-9.120	1.013	9.492
80.000	0.353	-1.429	1.829	2.347	2.089	-9.448	0.553	9.692	2.557	-9.285	1.090	9.692

DATE: 2 SEPT 1988  
 RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
 TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD  
 VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK  
 CRASH VICTIM: 95TH PERCENTILE MALE

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SEGMENT REL. ANGULAR DISPLACEMENT (DEG)

TIME (MSEC)	SEGMENT NO. 3 - UT IN VEH REFERENCE				SEGMENT NO. 5 - H IN VEH REFERENCE				SEGMENT NO. 5 - H IN UT REFERENCE			
	YAW	PITCH	ROLL	RES	YAW	PITCH	ROLL	RES	YAW	PITCH	ROLL	RES
0.000	0.000	13.280	0.000	13.280	0.000	13.460	0.000	13.460	0.000	0.180	0.000	0.180
2.000	0.000	13.280	0.000	13.280	0.000	13.460	0.000	13.460	0.000	0.180	0.000	0.180
4.000	0.000	13.280	0.000	13.280	0.000	13.460	0.000	13.460	0.000	0.180	0.000	0.180
6.000	0.000	13.280	0.000	13.280	0.000	13.459	0.000	13.459	0.000	0.180	0.000	0.180
8.000	0.000	13.280	0.000	13.280	0.000	13.459	0.000	13.459	0.000	0.179	0.000	0.179
10.000	0.001	13.281	0.000	13.281	0.000	13.458	0.000	13.458	-0.001	0.176	0.000	0.176
12.000	0.001	13.284	0.000	13.284	0.000	13.456	0.001	13.456	-0.001	0.171	0.001	0.172
14.000	0.003	13.290	0.000	13.290	0.000	13.454	0.002	13.454	-0.003	0.164	0.003	0.164
16.000	0.005	13.298	0.000	13.298	0.000	13.450	0.003	13.450	-0.005	0.152	0.005	0.152
18.000	0.008	13.310	0.000	13.310	0.000	13.445	0.005	13.445	-0.008	0.135	0.007	0.136
20.000	0.012	13.325	0.000	13.325	0.000	13.437	0.008	13.437	-0.011	0.112	0.010	0.113
22.000	0.018	13.345	0.001	13.345	0.001	13.426	0.011	13.426	-0.016	0.081	0.014	0.084
24.000	0.027	13.372	-0.003	13.372	0.001	13.409	0.018	13.409	-0.025	0.037	0.027	0.052
26.000	0.043	13.409	-0.017	13.409	0.002	13.381	0.036	13.382	-0.040	-0.027	0.063	0.079
28.000	0.067	13.456	-0.042	13.456	0.003	13.343	0.067	13.343	-0.062	-0.113	0.124	0.179
30.000	0.097	13.513	-0.069	13.513	0.005	13.293	0.101	13.293	-0.089	-0.220	0.191	0.305
32.000	0.136	13.582	-0.095	13.583	0.008	13.227	0.132	13.228	-0.126	-0.354	0.257	0.455
34.000	0.193	13.675	-0.127	13.677	0.011	13.123	0.173	13.124	-0.178	-0.552	0.343	0.673
36.000	0.265	13.791	-0.175	13.795	0.017	12.978	0.237	12.980	-0.245	-0.813	0.471	0.970
38.000	0.359	13.939	-0.243	13.946	0.023	12.775	0.333	12.779	-0.332	-1.162	0.657	1.374
40.000	0.476	14.123	-0.336	14.136	0.032	12.500	0.466	12.508	-0.443	-1.620	0.910	1.907
42.000	0.617	14.341	-0.449	14.364	0.042	12.140	0.628	12.156	-0.579	-2.196	1.220	2.572
44.000	0.797	14.601	-0.582	14.638	0.055	11.672	0.813	11.700	-0.757	-2.920	1.583	3.398
46.000	1.052	14.935	-0.739	14.997	0.068	11.017	1.061	11.067	-1.018	-3.903	2.055	4.511
48.000	1.383	15.315	-0.905	15.414	0.082	10.149	1.367	10.240	-1.367	-5.141	2.620	5.902
50.000	1.837	15.754	-1.063	15.912	0.093	8.975	1.755	9.144	-1.860	-6.738	3.301	7.683
52.000	2.445	16.263	-1.213	16.515	0.095	7.361	2.304	7.712	-2.540	-8.837	4.197	10.024
54.000	3.262	16.853	-1.279	17.247	0.077	5.221	2.994	6.017	-3.499	-11.531	5.240	12.994
56.000	4.376	17.548	-1.225	18.167	0.024	2.443	3.846	4.556	-4.830	-14.954	6.468	16.740
58.000	5.730	18.282	-1.076	19.232	-0.080	-0.956	4.867	4.960	-6.520	-19.021	7.925	21.188
60.000	7.198	18.725	-0.796	20.112	-0.263	-5.032	6.043	7.858	-8.457	-23.473	9.510	26.030
62.000	9.010	18.894	-0.167	20.927	-0.545	-9.713	7.216	12.079	-10.799	-28.287	10.903	31.183
64.000	10.887	19.035	0.596	21.863	-0.927	-14.811	8.405	16.984	-13.329	-33.526	12.297	36.700
66.000	12.684	19.097	1.389	22.806	-1.407	-20.134	9.632	22.235	-15.925	-38.944	13.770	42.339
68.000	14.326	19.070	2.120	23.692	-2.012	-25.641	10.994	27.755	-18.620	-44.470	15.523	48.056
70.000	15.868	18.985	2.772	24.554	-2.808	-31.383	12.610	33.588	-21.668	-50.163	17.827	53.960
72.000	17.346	18.800	3.344	25.369	-3.876	-37.343	14.579	39.712	-25.358	-55.941	20.942	60.003
74.000	18.753	18.447	3.806	26.080	-5.305	-43.404	16.970	46.004	-30.054	-61.584	25.198	66.009
76.000	20.091	17.906	4.127	26.679	-7.292	-49.559	19.979	52.473	-36.534	-66.989	31.360	71.966
78.000	21.384	17.148	4.271	27.175	-10.213	-55.825	23.994	59.178	-46.425	-71.980	41.030	77.911
80.000	22.660	16.188	4.207	27.614	-14.704	-62.089	29.648	66.073	-62.537	-76.081	56.973	83.815

DATE: 2 SEPT 1988  
 RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
 TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD  
 VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK  
 CRASH VICTIM: 95TH PERCENTILE MALE

PAGE: 27.01

## JOINT PARAMETERS

JOINT NO. 3 - NP								JOINT NO. 4 - HP							
TIME (MSEC)	STATE IPIN	JOINT ANGLES (DEG)			TOTAL TORQUE ( IN. LB.)			STATE IPIN	FLEXURE	JOINT ANGLES (DEG)			TOTAL TORQUE ( IN. LB.)		
		FLEXURE	AZIMUTH	TORSION	SPRING	VISCOUS	RES.			FLEXURE	AZIMUTH	TORSION	SPRING	VISCOUS	RES.
0.000	0.	10.180	0.000	0.000	0.000	0.000	0.000	0.	10.000	0.000	0.000	0.000	0.000	0.000	0.000
2.000	0.	10.181	0.000	0.000	0.000	0.118	0.118	0.	9.999	0.000	0.000	0.000	0.000	0.118	0.118
4.000	0.	10.184	0.000	0.000	0.000	0.190	0.190	0.	9.996	0.000	0.000	0.000	0.000	0.194	0.194
6.000	0.	10.189	0.000	0.000	0.000	0.241	0.241	0.	9.991	0.000	0.000	0.000	0.000	0.263	0.263
8.000	0.	10.194	-0.001	0.000	0.000	0.224	0.224	0.	9.985	0.001	0.000	0.000	0.000	0.303	0.303
10.000	0.	10.197	-0.005	0.000	0.000	0.115	0.115	0.	9.979	0.002	0.000	0.000	0.000	0.284	0.284
12.000	0.	10.197	-0.013	-0.001	0.000	0.166	0.166	0.	9.974	0.005	0.000	0.000	0.000	0.187	0.187
14.000	0.	10.192	-0.026	-0.002	0.000	0.401	0.401	0.	9.971	0.009	-0.001	0.000	0.000	0.112	0.112
16.000	0.	10.182	-0.042	-0.003	0.000	0.680	0.680	0.	9.970	0.012	-0.002	0.000	0.000	0.069	0.069
18.000	0.	10.166	-0.061	-0.004	0.000	0.977	0.977	0.	9.969	0.013	-0.003	0.000	0.000	0.072	0.072
20.000	0.	10.144	-0.081	-0.006	0.000	1.281	1.281	0.	9.968	0.012	-0.004	0.000	0.000	0.104	0.104
22.000	0.	10.115	-0.104	-0.009	0.000	1.728	1.728	0.	9.967	0.009	-0.006	0.000	0.000	0.122	0.122
24.000	0.	10.068	-0.222	-0.013	0.000	3.586	3.586	0.	9.970	0.046	-0.009	0.000	0.000	0.771	0.771
26.000	0.	9.997	-0.530	-0.019	0.000	5.256	5.256	0.	9.977	0.134	-0.016	0.000	0.000	0.981	0.981
28.000	0.	9.907	-0.984	-0.026	0.000	6.009	6.009	0.	9.981	0.211	-0.024	0.000	0.000	0.458	0.458
30.000	0.	9.805	-1.332	-0.039	0.000	6.012	6.012	0.	9.978	0.136	-0.034	0.000	0.000	1.331	1.331
32.000	0.	9.671	-1.592	-0.058	0.000	9.657	9.657	0.	9.978	-0.039	-0.045	0.000	0.000	1.704	1.704
34.000	0.	9.440	-2.129	-0.084	0.000	14.463	14.463	0.	10.014	-0.105	-0.062	0.000	0.000	2.267	2.267
36.000	0.	9.152	-3.083	-0.113	0.000	18.782	18.782	0.	10.066	-0.075	-0.088	0.000	0.000	2.371	2.371
38.000	0.	8.767	-4.576	-0.147	0.000	26.352	26.352	0.	10.095	-0.005	-0.122	0.000	0.000	3.606	3.606
40.000	0.	8.280	-6.692	-0.188	0.000	31.362	31.362	0.	10.149	0.007	-0.163	0.000	0.000	3.348	3.348
42.000	0.	7.699	-9.366	-0.240	0.000	37.757	37.757	0.	10.197	-0.171	-0.212	0.000	0.000	4.202	4.202
44.000	0.	6.972	-12.870	-0.317	0.000	52.652	52.652	0.	10.265	-0.573	-0.269	0.000	0.000	7.887	7.887
46.000	0.	5.966	-19.595	-0.430	0.000	71.325	71.325	0.	10.445	-0.726	-0.352	0.000	0.000	11.132	11.132
48.000	0.	4.869	-30.859	-0.581	0.000	80.360	80.360	0.	10.627	-1.060	-0.464	0.000	0.000	10.999	10.999
50.000	0.	3.822	-54.577	-0.804	0.000	125.388	125.388	0.	10.957	-1.213	-0.617	0.000	0.000	25.143	25.143
52.000	0.	4.001	-95.947	-1.088	0.000	150.487	150.487	0.	11.421	-0.891	-0.839	0.000	0.000	25.934	25.934
54.000	0.	6.124	-127.683	-1.502	0.000	193.882	193.882	0.	11.949	-0.784	-1.122	0.000	0.000	32.618	32.618
56.000	0.	9.668	-143.883	-2.084	0.000	220.529	220.529	0.	12.423	-0.721	-1.497	0.000	0.000	27.056	27.056
58.000	0.	13.878	-152.083	-2.748	0.000	235.094	235.094	0.	12.563	-0.690	-1.964	0.000	0.000	26.095	26.095
60.000	0.	18.379	-157.625	-3.482	0.000	234.042	234.042	0.	12.544	-1.090	-2.446	0.000	0.000	28.518	28.518
62.000	0.	22.709	-162.883	-4.505	0.000	238.449	238.449	0.	12.127	-2.354	-2.954	0.000	0.000	43.769	43.769
64.000	0.	26.899	-167.023	-5.484	18.036	216.552	233.247	0.	11.096	-3.358	-3.457	0.000	0.000	73.428	73.428
66.000	0.	30.558	-170.082	-6.297	154.456	176.484	324.673	0.	9.293	-4.188	-3.894	0.000	0.000	115.796	115.796
68.000	0.	33.331	-172.228	-6.882	347.062	123.565	462.542	0.	6.439	-6.114	-4.250	0.000	0.000	175.281	175.281
70.000	0.	35.027	-173.783	-7.296	502.714	67.615	559.233	0.	2.361	-19.607	-4.534	0.000	0.000	244.357	244.357
72.000	0.	35.552	-174.978	-7.592	493.636	30.690	494.729	0.	3.448	-162.475	-4.760	0.000	0.000	303.225	303.225
74.000	0.	35.540	-175.910	-7.807	466.062	24.286	466.652	0.	9.415	-172.198	-4.909	0.000	0.000	300.392	300.392
76.000	0.	35.544	-176.681	-7.960	539.760	20.915	540.627	0.	15.394	-174.585	-4.988	0.000	0.000	299.780	299.780
78.000	0.	35.568	-177.364	-8.079	558.450	19.211	561.920	0.	21.358	-175.662	-5.027	0.000	0.000	295.975	295.975
80.000	0.	35.764	-178.027	-8.198	579.271	26.658	596.493	0.	27.109	-176.275	-5.046	22.243	278.693	300.921	

DATE: 2 SEPT 1988  
 RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
 TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD  
 VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK  
 CRASH VICTIM: 95TH PERCENTILE MALE

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## HP JOINT FORCES &amp; TORQUES ON H IN H REFERENCE

TIME (MSEC)	JOINT FORCE ( LB. 10**2)			JOINT TORQUE ( IN.- LB. 10**2)		
	X	Y	Z	X	Y	Z
0.000	0.000	0.000	-0.126	0.0000+00	0.0000+00	0.0000+00
2.000	0.000	0.000	-0.129	-0.1190-06	0.1180-02	0.2320-07
4.000	0.001	0.000	-0.136	-0.9390-07	0.1940-02	0.7650-06
6.000	0.002	0.000	-0.142	0.2730-04	0.2630-02	0.5870-05
8.000	0.002	0.000	-0.148	0.1160-03	0.3030-02	0.2580-04
10.000	0.001	-0.001	-0.158	0.2380-03	0.2830-02	0.7250-04
12.000	-0.001	-0.001	-0.171	0.3850-03	0.1830-02	0.1600-03
14.000	-0.003	-0.001	-0.181	0.3830-03	0.1010-02	0.2840-03
16.000	-0.005	-0.001	-0.190	0.2970-03	0.4580-03	0.4270-03
18.000	-0.005	0.000	-0.202	0.1480-03	0.3700-03	0.6010-03
20.000	-0.007	0.000	-0.210	0.5030-05	0.6650-03	0.8000-03
22.000	-0.010	-0.001	-0.218	0.6700-04	0.5740-03	0.1070-02
24.000	-0.024	-0.021	-0.273	0.6750-02	-0.3250-02	0.1810-02
26.000	-0.027	-0.028	-0.270	0.8830-02	-0.3010-02	0.3050-02
28.000	-0.026	-0.002	-0.254	0.1060-02	-0.4440-03	0.4440-02
30.000	-0.029	0.004	-0.263	-0.1150-01	0.3300-02	0.5860-02
32.000	-0.097	-0.027	-0.164	-0.1050-01	-0.1090-01	0.7760-02
34.000	-0.090	-0.026	-0.153	-0.1800-02	-0.1980-01	0.1080-01
36.000	-0.123	-0.043	-0.131	0.5600-02	-0.1820-01	0.1410-01
38.000	-0.167	-0.086	-0.217	0.1210-01	-0.2870-01	0.1820-01
40.000	-0.187	-0.065	-0.200	-0.4350-02	-0.2420-01	0.2270-01
42.000	-0.235	-0.067	-0.280	-0.2070-01	-0.2390-01	0.2770-01
44.000	0.440	-0.151	0.231	-0.2000-01	-0.6750-01	0.3560-01
46.000	-0.476	-0.133	0.180	-0.6660-02	-0.9920-01	0.5000-01
48.000	-0.484	-0.078	0.423	-0.4090-01	-0.7850-01	0.6530-01
50.000	-0.964	-0.400	1.929	0.4750-01	-0.2290+00	0.9270-01
52.000	-1.025	-0.250	2.650	0.3330-01	-0.2270+00	0.1220+00
54.000	-1.406	-0.348	4.626	0.4170-01	-0.2810+00	0.1610+00
56.000	-1.393	-0.331	5.514	0.3790-01	-0.1680+00	0.2080+00
58.000	-1.416	-0.595	5.141	0.9100-01	0.1060-01	0.2440+00
60.000	-1.296	0.123	7.496	-0.9790-01	0.1010+00	0.2480+00
62.000	-1.049	0.016	5.739	-0.8070-01	0.3390+00	0.2640+00
64.000	-0.656	0.016	3.853	-0.4060-01	0.6920+00	0.2410+00
66.000	-0.606	-0.153	1.823	-0.4000-01	0.1140+01	0.2020+00
68.000	-0.887	-0.314	1.048	-0.1230+00	0.1740+01	0.1710+00
70.000	-0.958	-0.369	1.210	-0.2590+00	0.2420+01	0.1560+00
72.000	-0.758	-0.324	1.329	-0.3800+00	0.3000+01	0.1430+00
74.000	-0.842	-0.344	1.491	-0.3440+00	0.2980+01	0.8970-01
76.000	-0.939	-0.393	2.383	-0.3400+00	0.2980+01	0.6050-01
78.000	-0.884	-0.387	3.033	-0.3370+00	0.2940+01	0.4530-01
80.000	-0.676	-0.312	3.738	-0.3520+00	0.2990+01	0.4610-01

DATE: 2 SEPT 1988  
 RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
 TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD  
 VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK  
 CRASH VICTIM: 95TH PERCENTILE MALE

PAGE: 29.01

BODY PROPERTIES - REFERENCE SEGMENT NO. 16 (VEH)

INCLUDED SEGMENT NOS: 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15

TIME (MSEC)	CENTER OF GRAVITY ( IN. )			LINEAR MOMENTUM ( LB.-SEC. )			ANGULAR MOMENTUM ( IN.- LB.-SEC. )			KINETIC ENERGY ( LB.- IN. )		
	X	Y	Z	X	Y	Z	X	Y	Z	LINEAR	ANGULAR	TOTAL
0.000	18.183	0.000	-20.231	0.0000+00	0.0000+00	0.0000+00	0.0000+00	0.0000+00	0.0000+00	0.0000+00	0.0000+00	0.0000+00
2.000	18.183	0.000	-20.231	-0.2520-01	0.2870-06	0.7230-04	-0.6990-04	0.1970-01	0.3040-03	0.3820-01	0.4950-02	0.4310-01
4.000	18.185	0.000	-20.231	-0.1210+00	-0.2200-04	-0.6650-02	-0.6410-03	0.9970+00	0.1580-02	0.5050+00	0.3440-01	0.5390+00
6.000	18.189	0.000	-20.231	-0.2990+00	-0.4420-03	-0.3260-01	-0.1210-01	0.3410+01	0.1540-02	0.2420+01	0.1370+00	0.2560+01
8.000	18.197	0.000	-20.231	-0.5430+00	-0.2010-02	-0.8420-01	-0.5540-01	0.7300+01	-0.4720-02	0.7540+01	0.3910+00	0.7930+01
10.000	18.210	0.000	-20.232	-0.8410+00	-0.4970-02	-0.1670+00	-0.1380+00	0.1270+02	-0.1810-01	0.1840+02	0.8620+00	0.1920+02
12.000	18.230	0.000	-20.233	-0.1180+01	-0.9910-02	-0.2830+00	-0.2750+00	0.1940+02	-0.4480-01	0.3840+02	0.1550+01	0.3990+02
14.000	18.257	0.000	-20.234	-0.1550+01	-0.1500-01	-0.4350+00	-0.4160+00	0.2740+02	-0.7490-01	0.7170+02	0.2470+01	0.7420+02
16.000	18.294	0.000	-20.236	-0.1950+01	-0.1970-01	-0.6220+00	-0.5460+00	0.3660+02	-0.9950-01	0.1230+03	0.3650+01	0.1270+03
18.000	18.342	0.000	-20.239	-0.2390+01	-0.2430-01	-0.8440+00	-0.6710+00	0.4690+02	-0.1210+00	0.2000+03	0.5150+01	0.2050+03
20.000	18.402	0.000	-20.242	-0.2870+01	-0.2860-01	-0.1100+01	-0.7890+00	0.5840+02	-0.1340+00	0.3070+03	0.6980+01	0.3140+03
22.000	18.476	0.000	-20.247	-0.3400+01	-0.3560-01	-0.1400+01	-0.9820+00	0.7130+02	-0.1570+00	0.4510+03	0.9230+01	0.4610+03
24.000	18.564	-0.001	-20.253	-0.4010+01	-0.3500-01	-0.1830+01	-0.1640+01	0.8800+02	0.2040+00	0.6410+03	0.1180+02	0.6530+03
26.000	18.669	-0.001	-20.260	-0.4630+01	-0.3650-01	-0.2270+01	-0.2520+01	0.1050+03	0.6070+00	0.8860+03	0.1460+02	0.9010+03
28.000	18.792	-0.001	-20.270	-0.5280+01	-0.2040-02	-0.2700+01	-0.2260+01	0.1220+03	0.1410+01	0.1200+04	0.1790+02	0.1220+04
30.000	18.933	-0.001	-20.280	-0.5980+01	0.9730-01	-0.3110+01	0.4630+00	0.1390+03	0.2860+01	0.1580+04	0.2160+02	0.1600+04
32.000	19.095	0.000	-20.292	-0.6910+01	0.1320+00	-0.3410+01	0.1680+01	0.1600+03	0.4010+01	0.2040+04	0.2640+02	0.2060+04
34.000	19.278	0.000	-20.306	-0.8200+01	0.5830-01	-0.3690+01	-0.2400+00	0.1890+03	0.4550+01	0.2560+04	0.3430+02	0.2590+04
36.000	19.481	0.000	-20.320	-0.9880+01	0.2650-01	-0.4100+01	-0.1550+01	0.2260+03	0.6280+01	0.3150+04	0.4830+02	0.3200+04
38.000	19.704	0.001	-20.336	-0.1220+02	0.8010-01	-0.4540+01	-0.1660+01	0.2770+03	0.1010+02	0.3790+04	0.7210+02	0.3860+04
40.000	19.948	0.001	-20.354	-0.1490+02	0.3240+00	-0.4940+01	0.2720+01	0.3330+03	0.1710+02	0.4490+04	0.1040+03	0.4600+04
42.000	20.212	0.003	-20.373	-0.1800+02	0.7670+00	-0.5410+01	0.1080+02	0.4000+03	0.2780+02	0.5200+04	0.1360+03	0.5330+04
44.000	20.492	0.007	-20.393	-0.2200+02	0.1030+01	-0.5370+01	0.1380+02	0.4830+03	0.3770+02	0.5760+04	0.1660+03	0.5930+04
46.000	20.782	0.010	-20.412	-0.2720+02	0.8250+00	-0.4620+01	0.2800+01	0.5830+03	0.4270+02	0.6110+04	0.1920+03	0.6310+04
48.000	21.078	0.014	-20.426	-0.3360+02	0.1030+01	-0.3130+01	-0.1180+01	0.6990+03	0.5100+02	0.6230+04	0.2060+03	0.6440+04
50.000	21.369	0.015	-20.431	-0.4310+02	-0.4770+00	0.1200+01	-0.5580+02	0.8600+03	0.4090+02	0.5880+04	0.2510+03	0.6140+04
52.000	21.644	0.010	-20.416	-0.5450+02	-0.2460+01	0.6870+01	-0.1220+03	0.1040+04	0.1980+02	0.5390+04	0.3630+03	0.5750+04
54.000	21.894	-0.005	-20.377	-0.6850+02	-0.5450+01	0.1450+02	-0.2110+03	0.1260+04	-0.9270+01	0.4910+04	0.6730+03	0.5580+04
56.000	22.111	-0.030	-20.309	-0.8340+02	-0.8520+01	0.2200+02	-0.2950+03	0.1510+04	-0.3460+02	0.4710+04	0.1040+04	0.5740+04
58.000	22.290	-0.069	-20.216	-0.9910+02	-0.1350+02	0.2790+02	-0.4110+03	0.1790+04	-0.7970+02	0.4760+04	0.1280+04	0.6040+04
60.000	22.406	-0.126	-20.096	-0.1250+03	-0.1820+02	0.3750+02	-0.5240+03	0.2270+04	-0.1200+03	0.5810+04	0.2010+04	0.7820+04
62.000	22.463	-0.202	-19.952	-0.1400+03	-0.2210+02	0.3920+02	-0.6080+03	0.2590+04	-0.1460+03	0.6550+04	0.2260+04	0.8810+04
64.000	22.487	-0.287	-19.810	-0.1500+03	-0.2370+02	0.3700+02	-0.6470+03	0.2840+04	-0.1480+03	0.6730+04	0.2230+04	0.8960+04
66.000	22.490	-0.376	-19.683	-0.1580+03	-0.2410+02	0.3110+02	-0.6590+03	0.3060+04	-0.1450+03	0.6400+04	0.2060+04	0.8460+04
68.000	22.476	-0.465	-19.584	-0.1660+03	-0.2390+02	0.2200+02	-0.6580+03	0.3290+04	-0.1440+03	0.5790+04	0.1890+04	0.7680+04
70.000	22.446	-0.552	-19.523	-0.1710+03	-0.2350+02	0.1140+02	-0.6510+03	0.3480+04	-0.1410+03	0.5240+04	0.1770+04	0.7000+04
72.000	22.406	-0.640	-19.495	-0.1750+03	-0.2370+02	0.4160+01	-0.6480+03	0.3600+04	-0.1420+03	0.4840+04	0.1640+04	0.6480+04
74.000	22.358	-0.728	-19.490	-0.1800+03	-0.2380+02	-0.1300+01	-0.6460+03	0.3690+04	-0.1470+03	0.4530+04	0.1500+04	0.6040+04
76.000	22.298	-0.816	-19.505	-0.1830+03	-0.2400+02	-0.6350+01	-0.6480+03	0.3770+04	-0.1560+03	0.4430+04	0.1430+04	0.5870+04
78.000	22.233	-0.905	-19.537	-0.1850+03	-0.2420+02	-0.1140+02	-0.6550+03	0.3830+04	-0.1660+03	0.4560+04	0.1460+04	0.6020+04
80.000	22.165	-0.995	-19.588	-0.1860+03	-0.2440+02	-0.1610+02	-0.6590+03	0.3860+04	-0.1700+03	0.4770+04	0.1550+04	0.6320+04

DATE: 2 SEPT 1988

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RIN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 30.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK  
CRASH VEHICLE: 95TH PERCENTILE MALE  
CONTACT FORCES - SEGMENT PANELS VS. SEGMENTS

TIME (MSEC)	PANEL 1 (SEAT. 6 DEGREE OFF H) VS. SEGMENT 1 ( LT )							PANEL 1 (SEAT. 6 DEGREE OFF H) VS. SEGMENT 6 ( RUL )						
	DEFL- ECTION ( IN. )	NORMAL FORCE ( LB. )	FRICTION FORCE ( LB. )	RESULTANT FORCE ( LB. )	CONTACT LOCATION ( IN. ) (VEH REFERENCE)			DEFL- ECTION ( IN. )	NORMAL FORCE ( LB. )	FRICTION FORCE ( LB. )	RESULTANT FORCE ( LB. )	CONTACT LOCATION ( IN. ) (VEH REFERENCE)		
					X	Y	Z					X	Y	Z
0.000	0.458	137.10	0.00	137.10	14.372	0.000	-10.459	0.250	29.94	0.00	29.94	24.725	3.420	-11.545
2.000	0.458	137.02	8.94	137.31	14.373	0.000	-10.459	0.250	31.22	4.99	31.62	24.725	3.420	-11.545
4.000	0.458	136.86	27.51	139.60	14.375	0.000	-10.459	0.250	36.69	15.37	39.79	24.726	3.420	-11.545
6.000	0.458	136.72	46.60	144.44	14.380	0.000	-10.460	0.250	44.22	22.11	49.44	24.727	3.420	-11.545
8.000	0.457	138.78	64.83	153.18	14.390	0.000	-10.461	0.251	51.70	25.85	57.80	24.729	3.420	-11.546
10.000	0.458	144.58	72.29	161.65	14.407	0.000	-10.462	0.251	58.35	29.18	65.24	24.732	3.420	-11.546
12.000	0.458	152.48	76.24	170.48	14.431	0.000	-10.465	0.252	63.83	31.91	71.36	24.737	3.420	-11.546
14.000	0.458	161.71	80.85	180.80	14.464	0.000	-10.468	0.253	68.37	34.18	76.44	24.744	3.420	-11.547
16.000	0.459	172.39	86.19	192.73	14.508	0.000	-10.473	0.254	72.13	36.06	80.64	24.755	3.420	-11.548
18.000	0.459	184.02	92.01	205.74	14.565	-0.001	-10.479	0.255	75.12	37.56	83.99	24.770	3.420	-11.550
20.000	0.460	196.74	98.37	219.96	14.635	-0.001	-10.486	0.256	76.24	38.12	85.24	24.790	3.420	-11.552
22.000	0.461	211.45	105.72	236.41	14.720	-0.001	-10.495	0.257	74.47	37.23	83.26	24.816	3.420	-11.555
24.000	0.463	200.50	100.25	224.17	14.822	-0.001	-10.506	0.257	66.45	33.22	74.29	24.849	3.420	-11.558
26.000	0.464	199.45	99.72	222.99	14.942	-0.001	-10.519	0.257	58.64	29.32	65.56	24.891	3.420	-11.563
28.000	0.465	207.89	103.94	232.42	15.081	0.000	-10.533	0.256	49.90	24.95	55.79	24.942	3.420	-11.568
30.000	0.466	228.27	114.13	255.21	15.242	0.001	-10.550	0.255	45.48	22.74	50.85	25.002	3.420	-11.574
32.000	0.468	279.53	139.76	312.52	15.424	0.006	-10.569	0.253	53.74	26.87	60.08	25.069	3.421	-11.581
34.000	0.472	356.68	178.34	398.78	15.630	0.016	-10.591	0.251	53.97	26.99	60.35	25.138	3.421	-11.589
36.000	0.478	448.62	224.31	501.57	15.859	0.038	-10.615	0.248	38.40	19.20	42.93	25.207	3.421	-11.596
38.000	0.485	560.72	280.36	626.90	16.111	0.079	-10.641	0.244	37.83	18.91	42.29	25.272	3.422	-11.603
40.000	0.496	634.27	317.14	709.14	16.385	0.146	-10.670	0.239	65.17	32.59	72.87	25.324	3.424	-11.608
42.000	0.510	664.96	332.48	743.44	16.679	0.237	-10.701	0.234	89.40	44.70	99.96	25.364	3.428	-11.612
44.000	0.527	703.41	351.70	786.43	16.985	0.346	-10.733	0.230	119.38	59.69	133.47	25.391	3.434	-11.615
46.000	0.551	756.42	378.21	845.71	17.293	0.460	-10.765	0.227	157.62	78.81	176.23	25.402	3.441	-11.616
48.000	0.585	828.62	414.31	926.43	17.592	0.567	-10.797	0.225	201.14	100.57	224.88	25.394	3.451	-11.615
50.000	0.634	922.91	461.45	1031.84	17.867	0.638	-10.826	0.225	230.71	115.35	257.94	25.366	3.464	-11.613
52.000	0.705	1043.08	521.54	1166.20	18.102	0.630	-10.850	0.225	229.76	114.88	256.88	25.326	3.480	-11.608
54.000	0.806	1090.42	545.21	1219.13	18.285	0.526	-10.869	0.227	275.31	137.65	307.80	25.267	3.497	-11.602
56.000	0.942	1085.51	542.75	1213.64	18.410	0.360	-10.883	0.237	287.36	143.68	321.28	25.149	3.514	-11.590
58.000	1.113	1255.01	627.50	1403.14	18.483	0.194	-10.890	0.263	319.10	159.55	356.77	24.927	3.526	-11.567
60.000	1.323	1450.74	725.37	1621.98	18.497	0.037	-10.892	0.312	369.55	184.78	413.17	24.589	3.526	-11.531
62.000	1.576	1827.33	913.67	2043.02	18.468	-0.132	-10.889	0.373	440.16	220.08	492.11	24.222	3.511	-11.493
64.000	1.825	2293.38	1146.69	2564.07	18.450	-0.237	-10.887	0.443	571.58	285.79	639.04	23.850	3.487	-11.453
66.000	2.046	2723.02	1361.51	3044.43	18.439	-0.287	-10.886	0.512	745.66	372.83	833.68	23.509	3.460	-11.418
68.000	2.217	3434.09	1717.05	3839.43	18.418	-0.298	-10.883	0.565	895.39	447.69	1001.07	23.230	3.435	-11.388
70.000	2.318	3801.87	1900.93	4250.62	18.370	-0.288	-10.878	0.584	304.97	152.49	340.97	23.046	3.419	-11.369
72.000	2.356	2969.04	1484.52	3319.48	18.300	-0.277	-10.871	0.565	279.61	139.80	312.61	22.958	3.408	-11.360
74.000	2.342	2947.61	1473.80	3295.52	18.218	-0.271	-10.862	0.515	213.84	106.92	239.08	22.945	3.400	-11.359
76.000	2.282	2851.26	210.71	2859.04	18.125	-0.274	-10.853	0.436	108.38	54.19	121.18	23.013	3.395	-11.366
78.000	2.180	2688.19	119.57	2690.85	18.036	-0.292	-10.843	0.328	45.56	22.78	50.93	23.161	3.390	-11.381
80.000	2.039	2461.74	235.32	2472.96	17.954	-0.332	-10.835	0.191	18.66	9.33	20.86	23.244	3.381	-11.390

DATE: 2 SEPT 1988  
 RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
 TWO BELT HARNESS WITH HYPERELLIPTOID FOR DASH BOARD  
 VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK  
 CRASH VICTIM: 95TH PERCENTILE MALE  
 CONTACT FORCES - SEGMENT PANELS VS. SEGMENTS

PAGE: 31.01

TIME (MSEC)	PANEL 1 (SEAT. 6 DEGREE OFF H) VS. SEGMENT 9 ( LUL )							PANEL 2 (BACK PANEL. 13 DEGR) VS. SEGMENT 1 ( LT )						
	DEFL- ECTION	NORMAL FORCE	FRICTION FORCE	RESULTANT FORCE	CONTACT (VEH REFERENCE)	LOCATION ( IN. )		DEFL- ECTION	NORMAL FORCE	FRICTION FORCE	RESULTANT FORCE	CONTACT (VEH REFERENCE)	LOCATION ( IN. )	
	( IN. )	( LB. )	( LB. )	( LB. )	X	Y	Z	( IN. )	( LB. )	( LB. )	( LB. )	X	Y	Z
0.000	0.250	29.94	0.00	29.94	24.725	-3.420	-11.545	0.055	2.77	0.00	2.77	9.382	0.000	-12.674
2.000	0.250	31.23	5.00	31.62	24.725	-3.420	-11.545	0.055	2.76	0.40	2.79	9.382	0.000	-12.674
4.000	0.250	36.71	15.41	39.81	24.726	-3.420	-11.545	0.054	2.68	0.97	2.85	9.382	0.000	-12.675
6.000	0.250	44.24	22.12	49.46	24.727	-3.420	-11.545	0.050	2.51	1.25	2.80	9.382	0.000	-12.676
8.000	0.251	51.74	25.87	57.84	24.729	-3.420	-11.546	0.044	2.18	1.09	2.44	9.382	0.000	-12.677
10.000	0.251	58.41	29.21	65.30	24.732	-3.420	-11.546	0.033	1.65	0.83	1.85	9.381	0.000	-12.680
12.000	0.252	63.91	31.95	71.45	24.737	-3.420	-11.546	0.017	0.86	0.43	0.96	9.380	0.000	-12.684
14.000	0.253	68.45	34.23	76.53	24.744	-3.420	-11.547	-0.006	0.00	0.00	0.00	0.000	0.000	0.000
16.000	0.254	72.21	36.10	80.73	24.755	-3.420	-11.548	-0.036	0.00	0.00	0.00	0.000	0.000	0.000
18.000	0.255	75.19	37.60	84.07	24.770	-3.420	-11.550	-0.077	0.00	0.00	0.00	0.000	0.000	0.000
20.000	0.256	76.31	38.16	85.32	24.790	-3.420	-11.552	-0.128	0.00	0.00	0.00	0.000	0.000	0.000
22.000	0.257	74.63	37.31	83.43	24.815	-3.420	-11.555	-0.192	0.00	0.00	0.00	0.000	0.000	0.000
24.000	0.257	65.18	32.59	72.87	24.849	-3.420	-11.558	-0.269	0.00	0.00	0.00	0.000	0.000	0.000
26.000	0.257	56.40	28.20	63.06	24.891	-3.420	-11.563	-0.362	0.00	0.00	0.00	0.000	0.000	0.000
28.000	0.256	47.59	23.79	53.20	24.943	-3.420	-11.568	-0.472	0.00	0.00	0.00	0.000	0.000	0.000
30.000	0.254	34.68	17.34	38.78	25.005	-3.420	-11.575	-0.601	0.00	0.00	0.00	0.000	0.000	0.000
32.000	0.252	30.42	15.21	34.01	25.079	-3.419	-11.582	-0.749	0.00	0.00	0.00	0.000	0.000	0.000
34.000	0.248	29.66	14.83	33.16	25.168	-3.419	-11.592	-0.918	0.00	0.00	0.00	0.000	0.000	0.000
36.000	0.241	28.14	14.07	31.46	25.280	-3.419	-11.604	-1.108	0.00	0.00	0.00	0.000	0.000	0.000
38.000	0.227	25.44	12.72	28.44	25.426	-3.418	-11.619	-1.317	0.00	0.00	0.00	0.000	0.000	0.000
40.000	0.206	21.30	10.65	23.81	25.615	-3.415	-11.639	-1.546	0.00	0.00	0.00	0.000	0.000	0.000
42.000	0.179	16.89	8.45	18.89	25.850	-3.411	-11.663	-1.794	0.00	0.00	0.00	0.000	0.000	0.000
44.000	0.147	12.03	6.01	13.45	26.130	-3.405	-11.693	-2.056	0.00	0.00	0.00	0.000	0.000	0.000
46.000	0.112	6.87	3.43	7.68	26.435	-3.396	-11.725	-2.328	0.00	0.00	0.00	0.000	0.000	0.000
48.000	0.080	3.99	1.99	4.46	26.760	-3.386	-11.759	-2.601	0.00	0.00	0.00	0.000	0.000	0.000
50.000	0.056	2.78	1.39	3.11	27.008	-3.372	-11.785	-2.864	0.00	0.00	0.00	0.000	0.000	0.000
52.000	0.051	58.93	29.46	65.88	27.020	-3.355	-11.786	-3.104	0.00	0.00	0.00	0.000	0.000	0.000
54.000	0.076	84.08	42.04	94.01	26.648	-3.335	-11.747	-3.311	0.00	0.00	0.00	0.000	0.000	0.000
56.000	0.137	138.11	69.06	154.41	26.015	-3.313	-11.681	-3.479	0.00	0.00	0.00	0.000	0.000	0.000
58.000	0.228	165.60	82.80	185.14	25.312	-3.292	-11.607	-3.609	0.00	0.00	0.00	0.000	0.000	0.000
60.000	0.353	148.11	74.06	165.60	24.605	-3.280	-11.533	-3.695	0.00	0.00	0.00	0.000	0.000	0.000
62.000	0.522	357.14	178.57	399.30	23.920	-3.280	-11.461	-3.747	0.00	0.00	0.00	0.000	0.000	0.000
64.000	0.684	686.47	343.24	767.50	23.448	-3.290	-11.411	-3.784	0.00	0.00	0.00	0.000	0.000	0.000
66.000	0.819	1246.33	623.16	1393.44	23.155	-3.301	-11.380	-3.811	0.00	0.00	0.00	0.000	0.000	0.000
68.000	0.905	1699.87	849.94	1900.52	22.994	-3.313	-11.364	-3.828	0.00	0.00	0.00	0.000	0.000	0.000
70.000	0.924	758.55	379.27	848.08	22.932	-3.322	-11.357	-3.837	0.00	0.00	0.00	0.000	0.000	0.000
72.000	0.888	710.46	355.23	794.31	22.936	-3.329	-11.358	-3.838	0.00	0.00	0.00	0.000	0.000	0.000
74.000	0.814	611.98	305.99	684.21	22.992	-3.333	-11.363	-3.831	0.00	0.00	0.00	0.000	0.000	0.000
76.000	0.713	477.86	238.93	534.26	23.096	-3.334	-11.374	-3.811	0.00	0.00	0.00	0.000	0.000	0.000
78.000	0.591	314.21	157.11	351.30	23.266	-3.333	-11.392	-3.793	0.00	0.00	0.00	0.000	0.000	0.000
80.000	0.450	126.56	63.28	141.50	23.529	-3.333	-11.420	-3.782	0.00	0.00	0.00	0.000	0.000	0.000



DATE: 2 SEPT 1988  
 RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
 TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD  
 VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK  
 CRASH VICTIM: 95TH PERCENTILE MALE  
 CONTACT FORCES - SEGMENT PANELS VS. SEGMENTS

PAGE: 32.01

TIME (MSEC)	PANEL 2 (BACK PANEL. 13 DEGR) VS. SEGMENT 2 ( CT )							PANEL 2 (BACK PANEL. 13 DEGR) VS. SEGMENT 3 ( UT )						
	DEFL- ECTION ( IN. )	NORMAL FORCE ( LB. )	FRICTION FORCE ( LB. )	RESULTANT FORCE ( LB. )	CONTACT LOCATION ( IN. ) (VEH REFERENCE)			DEFL- ECTION ( IN. )	NORMAL FORCE ( LB. )	FRICTION FORCE ( LB. )	RESULTANT FORCE ( LB. )	CONTACT LOCATION ( IN. ) (VEH REFERENCE)		
					X	Y	Z					X	Y	Z
0.000	-0.312	0.00	0.00	0.00	0.000	0.000	0.000	0.133	9.90	0.00	9.90	6.151	0.000	-26.665
2.000	-0.312	0.00	0.00	0.00	0.000	0.000	0.000	0.132	9.87	0.06	9.87	6.151	0.000	-26.665
4.000	-0.314	0.00	0.00	0.00	0.000	0.000	0.000	0.131	9.61	0.75	9.64	6.151	0.000	-26.665
6.000	-0.320	0.00	0.00	0.00	0.000	0.000	0.000	0.126	8.90	1.74	9.07	6.151	0.000	-26.664
8.000	-0.330	0.00	0.00	0.00	0.000	0.000	0.000	0.117	7.52	2.55	7.94	6.152	0.000	-26.663
10.000	-0.347	0.00	0.00	0.00	0.000	0.000	0.000	0.102	5.25	2.42	5.77	6.152	0.000	-26.661
12.000	-0.372	0.00	0.00	0.00	0.000	0.000	0.000	0.079	3.95	1.98	4.42	6.153	0.000	-26.658
14.000	-0.406	0.00	0.00	0.00	0.000	0.000	0.000	0.048	2.38	1.19	2.66	6.154	0.000	-26.654
16.000	-0.452	0.00	0.00	0.00	0.000	0.000	0.000	0.006	0.30	0.15	0.33	6.155	0.000	-26.649
18.000	-0.510	0.00	0.00	0.00	0.000	0.000	0.000	-0.048	0.00	0.00	0.00	0.000	0.000	0.000
20.000	-0.583	0.00	0.00	0.00	0.000	0.000	0.000	-0.114	0.00	0.00	0.00	0.000	0.000	0.000
22.000	-0.671	0.00	0.00	0.00	0.000	0.000	0.000	-0.196	0.00	0.00	0.00	0.000	0.000	0.000
24.000	-0.776	0.00	0.00	0.00	0.000	0.000	0.000	-0.294	0.00	0.00	0.00	0.000	0.000	0.000
26.000	-0.901	0.00	0.00	0.00	0.000	0.000	0.000	-0.409	0.00	0.00	0.00	0.000	0.000	0.000
28.000	-1.045	0.00	0.00	0.00	0.000	0.000	0.000	-0.542	0.00	0.00	0.00	0.000	0.000	0.000
30.000	-1.211	0.00	0.00	0.00	0.000	0.000	0.000	-0.696	0.00	0.00	0.00	0.000	0.000	0.000
32.000	-1.400	0.00	0.00	0.00	0.000	0.000	0.000	-0.872	0.00	0.00	0.00	0.000	0.000	0.000
34.000	-1.612	0.00	0.00	0.00	0.000	0.000	0.000	-1.067	0.00	0.00	0.00	0.000	0.000	0.000
36.000	-1.849	0.00	0.00	0.00	0.000	0.000	0.000	-1.284	0.00	0.00	0.00	0.000	0.000	0.000
38.000	-2.110	0.00	0.00	0.00	0.000	0.000	0.000	-1.523	0.00	0.00	0.00	0.000	0.000	0.000
40.000	-2.397	0.00	0.00	0.00	0.000	0.000	0.000	-1.783	0.00	0.00	0.00	0.000	0.000	0.000
42.000	-2.707	0.00	0.00	0.00	0.000	0.000	0.000	-2.064	0.00	0.00	0.00	0.000	0.000	0.000
44.000	-3.034	0.00	0.00	0.00	0.000	0.000	0.000	-2.361	0.00	0.00	0.00	0.000	0.000	0.000
46.000	-3.370	0.00	0.00	0.00	0.000	0.000	0.000	-2.662	0.00	0.00	0.00	0.000	0.000	0.000
48.000	-3.702	0.00	0.00	0.00	0.000	0.000	0.000	-2.960	0.00	0.00	0.00	0.000	0.000	0.000
50.000	-4.012	0.00	0.00	0.00	0.000	0.000	0.000	-3.238	0.00	0.00	0.00	0.000	0.000	0.000
52.000	-4.276	0.00	0.00	0.00	0.000	0.000	0.000	-3.473	0.00	0.00	0.00	0.000	0.000	0.000
54.000	-4.477	0.00	0.00	0.00	0.000	0.000	0.000	-3.652	0.00	0.00	0.00	0.000	0.000	0.000
56.000	-4.606	0.00	0.00	0.00	0.000	0.000	0.000	-3.757	0.00	0.00	0.00	0.000	0.000	0.000
58.000	-4.661	0.00	0.00	0.00	0.000	0.000	0.000	-3.787	0.00	0.00	0.00	0.000	0.000	0.000
60.000	-4.582	0.00	0.00	0.00	0.000	0.000	0.000	-3.689	0.00	0.00	0.00	0.000	0.000	0.000
62.000	-4.378	0.00	0.00	0.00	0.000	0.000	0.000	-3.478	0.00	0.00	0.00	0.000	0.000	0.000
64.000	-4.149	0.00	0.00	0.00	0.000	0.000	0.000	-3.225	0.00	0.00	0.00	0.000	0.000	0.000
66.000	-3.915	0.00	0.00	0.00	0.000	0.000	0.000	-2.965	0.00	0.00	0.00	0.000	0.000	0.000
68.000	-3.689	0.00	0.00	0.00	0.000	0.000	0.000	-2.720	0.00	0.00	0.00	0.000	0.000	0.000
70.000	-3.476	0.00	0.00	0.00	0.000	0.000	0.000	-2.499	0.00	0.00	0.00	0.000	0.000	0.000
72.000	-3.281	0.00	0.00	0.00	0.000	0.000	0.000	-2.303	0.00	0.00	0.00	0.000	0.000	0.000
74.000	-3.098	0.00	0.00	0.00	0.000	0.000	0.000	-2.127	0.00	0.00	0.00	0.000	0.000	0.000
76.000	-2.921	0.00	0.00	0.00	0.000	0.000	0.000	-1.960	0.00	0.00	0.00	0.000	0.000	0.000
78.000	-2.744	0.00	0.00	0.00	0.000	0.000	0.000	-1.791	0.00	0.00	0.00	0.000	0.000	0.000
80.000	-2.561	0.00	0.00	0.00	0.000	0.000	0.000	-1.618	0.00	0.00	0.00	0.000	0.000	0.000

DATE: 2 SEPT 1988

PAGE 38

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPOID FOR DASH BOARD

PAGE: 33.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

CONTACT FORCES - SEGMENT PANELS VS. SEGMENTS

TIME (MSEC)	PANEL 3 (FLOOR.)				) VS. SEGMENT 8 ( RF )			PANEL 3 (FLOOR.)				) VS. SEGMENT 11 ( LF )		
	DEFL- ECTION	NORMAL FORCE	FRICTION FORCE	RESULTANT FORCE	CONTACT FORCE	LOCATION ( IN.)	REFERENCE	DEFL- ECTION	NORMAL FORCE	FRICTION FORCE	RESULTANT FORCE	CONTACT FORCE	LOCATION ( IN.)	REFERENCE
	( IN.)	( LB.)	( LB.)	( LB.)	X	Y	Z	( IN.)	( LB.)	( LB.)	( LB.)	X	Y	Z
0.000	0.096	4.82	0.00	4.82	46.596	3.420	-1.300	0.096	4.82	0.00	4.82	46.596	-3.420	-1.300
2.000	0.097	4.88	0.97	4.98	46.596	3.420	-1.300	0.097	4.88	0.97	4.98	46.596	-3.420	-1.300
4.000	0.097	4.97	2.11	5.40	46.597	3.420	-1.300	0.097	4.98	2.11	5.40	46.597	-3.420	-1.300
6.000	0.097	5.05	2.52	5.64	46.601	3.420	-1.300	0.097	5.05	2.52	5.64	46.601	-3.420	-1.300
8.000	0.098	5.02	2.51	5.62	46.609	3.420	-1.300	0.098	5.03	2.52	5.62	46.609	-3.420	-1.300
10.000	0.098	4.90	2.45	5.48	46.620	3.420	-1.300	0.098	4.91	2.46	5.49	46.620	-3.420	-1.300
12.000	0.098	4.88	2.44	5.46	46.638	3.420	-1.300	0.098	4.89	2.44	5.46	46.638	-3.420	-1.300
14.000	0.097	4.83	2.42	5.41	46.662	3.420	-1.300	0.097	4.84	2.42	5.41	46.662	-3.420	-1.300
16.000	0.095	4.75	2.37	5.31	46.693	3.420	-1.300	0.095	4.76	2.38	5.32	46.694	-3.420	-1.300
18.000	0.092	4.61	2.31	5.16	46.734	3.420	-1.300	0.093	4.63	2.31	5.17	46.734	-3.420	-1.300
20.000	0.088	4.42	2.21	4.94	46.784	3.420	-1.300	0.089	4.44	2.22	4.97	46.784	-3.420	-1.300
22.000	0.083	4.17	2.08	4.66	46.844	3.420	-1.300	0.084	4.19	2.10	4.69	46.845	-3.420	-1.300
24.000	0.077	3.85	1.92	4.30	46.915	3.420	-1.300	0.078	3.88	1.94	4.34	46.916	-3.420	-1.300
26.000	0.069	3.46	1.73	3.86	46.998	3.420	-1.300	0.070	3.50	1.75	3.91	46.999	-3.420	-1.300
28.000	0.060	2.99	1.50	3.35	47.092	3.420	-1.300	0.061	3.05	1.52	3.41	47.093	-3.420	-1.300
30.000	0.049	2.46	1.23	2.75	47.199	3.420	-1.300	0.051	2.54	1.27	2.83	47.201	-3.420	-1.300
32.000	0.037	1.85	0.93	2.07	47.318	3.420	-1.300	0.040	1.98	0.99	2.21	47.322	-3.420	-1.300
34.000	0.022	1.12	0.56	1.26	47.448	3.420	-1.300	0.027	1.36	0.68	1.52	47.456	-3.420	-1.300
36.000	0.004	0.19	0.10	0.21	47.583	3.420	-1.300	0.013	0.65	0.32	0.73	47.597	-3.420	-1.300
38.000	-0.021	0.00	0.00	0.00	0.000	0.000	0.000	-0.004	0.00	0.00	0.00	0.000	0.000	0.000
40.000	-0.052	0.00	0.00	0.00	0.000	0.000	0.000	-0.024	0.00	0.00	0.00	0.000	0.000	0.000
42.000	-0.092	0.00	0.00	0.00	0.000	0.000	0.000	-0.047	0.00	0.00	0.00	0.000	0.000	0.000
44.000	-0.140	0.00	0.00	0.00	0.000	0.000	0.000	-0.072	0.00	0.00	0.00	0.000	0.000	0.000
46.000	-0.199	0.00	0.00	0.00	0.000	0.000	0.000	-0.101	0.00	0.00	0.00	0.000	0.000	0.000
48.000	-0.268	0.00	0.00	0.00	0.000	0.000	0.000	-0.137	0.00	0.00	0.00	0.000	0.000	0.000
50.000	-0.348	0.00	0.00	0.00	0.000	0.000	0.000	-0.183	0.00	0.00	0.00	0.000	0.000	0.000
52.000	-0.440	0.00	0.00	0.00	0.000	0.000	0.000	-0.245	0.00	0.00	0.00	0.000	0.000	0.000
54.000	-0.543	0.00	0.00	0.00	0.000	0.000	0.000	-0.330	0.00	0.00	0.00	0.000	0.000	0.000
56.000	-0.661	0.00	0.00	0.00	0.000	0.000	0.000	-0.434	0.00	0.00	0.00	0.000	0.000	0.000
58.000	-0.798	0.00	0.00	0.00	0.000	0.000	0.000	-0.554	0.00	0.00	0.00	0.000	0.000	0.000
60.000	-0.960	0.00	0.00	0.00	0.000	0.000	0.000	-0.686	0.00	0.00	0.00	0.000	0.000	0.000
62.000	-1.145	0.00	0.00	0.00	0.000	0.000	0.000	-0.830	0.00	0.00	0.00	0.000	0.000	0.000
64.000	-1.351	0.00	0.00	0.00	0.000	0.000	0.000	-0.974	0.00	0.00	0.00	0.000	0.000	0.000
66.000	-1.576	0.00	0.00	0.00	0.000	0.000	0.000	-1.122	0.00	0.00	0.00	0.000	0.000	0.000
68.000	-1.817	0.00	0.00	0.00	0.000	0.000	0.000	-1.277	0.00	0.00	0.00	0.000	0.000	0.000
70.000	-2.071	0.00	0.00	0.00	0.000	0.000	0.000	-1.446	0.00	0.00	0.00	0.000	0.000	0.000
72.000	-2.335	0.00	0.00	0.00	0.000	0.000	0.000	-1.625	0.00	0.00	0.00	0.000	0.000	0.000
74.000	-2.606	0.00	0.00	0.00	0.000	0.000	0.000	-1.812	0.00	0.00	0.00	0.000	0.000	0.000
76.000	-2.883	0.00	0.00	0.00	0.000	0.000	0.000	-2.005	0.00	0.00	0.00	0.000	0.000	0.000
78.000	-3.160	0.00	0.00	0.00	0.000	0.000	0.000	-2.199	0.00	0.00	0.00	0.000	0.000	0.000
80.000	-3.434	0.00	0.00	0.00	0.000	0.000	0.000	-2.387	0.00	0.00	0.00	0.000	0.000	0.000

DATE: 2 SEPT 1988

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION

TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

PAGE: 34.01

VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

CONTACT FORCES - SEGMENT PANELS VS. SEGMENTS

TIME (MSEC)	PANEL 4 (HEAD PAD. 13 DEGR ) VS. SEGMENT 5 ( H )								PANEL 10 (RUDDER PEDALS. ) VS. SEGMENT 8 ( RF )							
	DEFL- ECTION ( IN. )	NORMAL FORCE ( LB. )	FRICTION FORCE ( LB. )	RESULTANT FORCE ( LB. )	CONTACT (VEH REFERENCE)	LOCATION ( IN. )			DEFL- ECTION ( IN. )	NORMAL FORCE ( LB. )	FRICTION FORCE ( LB. )	RESULTANT FORCE ( LB. )	CONTACT (VEH REFERENCE)	LOCATION ( IN. )		
						X	Y	Z						X	Y	Z
0.000	0.050	2.48	0.00	2.48	3.935	0.000	-40.978		0.002	0.08	0.00	0.08	51.239	3.420	-3.286	
2.000	0.049	2.47	0.02	2.47	3.935	0.000	-40.978		0.001	0.07	0.01	0.07	51.239	3.420	-3.286	
4.000	0.048	2.38	0.19	2.39	3.935	0.000	-40.978		0.002	0.11	0.04	0.12	51.239	3.420	-3.285	
6.000	0.043	2.15	0.41	2.19	3.935	0.000	-40.977		0.005	0.29	0.14	0.32	51.240	3.420	-3.287	
8.000	0.034	1.70	0.55	1.78	3.935	0.000	-40.976		0.010	0.75	0.37	0.83	51.245	3.420	-3.291	
10.000	0.019	0.95	0.41	1.03	3.936	0.000	-40.974		0.019	1.59	0.80	1.78	51.254	3.420	-3.298	
12.000	-0.003	0.00	0.00	0.00	0.000	0.000	0.000		0.031	2.66	1.33	2.98	51.266	3.420	-3.309	
14.000	-0.034	0.00	0.00	0.00	0.000	0.000	0.000		0.048	4.09	2.05	4.58	51.284	3.420	-3.323	
16.000	-0.075	0.00	0.00	0.00	0.000	0.000	0.000		0.070	5.92	2.96	6.62	51.306	3.420	-3.342	
18.000	-0.128	0.00	0.00	0.00	0.000	0.000	0.000		0.096	8.17	4.08	9.13	51.334	3.420	-3.365	
20.000	-0.194	0.00	0.00	0.00	0.000	0.000	0.000		0.128	13.66	6.83	15.28	51.367	3.420	-3.393	
22.000	-0.274	0.00	0.00	0.00	0.000	0.000	0.000		0.165	20.41	10.21	22.82	51.406	3.420	-3.426	
24.000	-0.371	0.00	0.00	0.00	0.000	0.000	0.000		0.205	28.17	14.09	31.50	51.464	3.420	-3.474	
26.000	-0.484	0.00	0.00	0.00	0.000	0.000	0.000		0.249	38.47	19.24	43.01	51.490	3.420	-3.496	
28.000	-0.617	0.00	0.00	0.00	0.000	0.000	0.000		0.296	49.29	24.64	55.10	51.503	3.420	-3.507	
30.000	-0.770	0.00	0.00	0.00	0.000	0.000	0.000		0.343	60.44	30.22	67.58	51.511	3.420	-3.514	
32.000	-0.945	0.00	0.00	0.00	0.000	0.000	0.000		0.392	71.83	35.92	80.31	51.516	3.420	-3.518	
34.000	-1.142	0.00	0.00	0.00	0.000	0.000	0.000		0.440	128.19	64.09	143.32	51.520	3.420	-3.521	
36.000	-1.363	0.00	0.00	0.00	0.000	0.000	0.000		0.477	178.75	89.37	199.85	51.521	3.420	-3.522	
38.000	-1.610	0.00	0.00	0.00	0.000	0.000	0.000		0.496	204.92	102.46	229.11	51.519	3.420	-3.521	
40.000	-1.882	0.00	0.00	0.00	0.000	0.000	0.000		0.498	191.03	95.51	213.58	51.515	3.420	-3.517	
42.000	-2.181	0.00	0.00	0.00	0.000	0.000	0.000		0.492	182.60	91.30	204.15	51.508	3.419	-3.511	
44.000	-2.505	0.00	0.00	0.00	0.000	0.000	0.000		0.482	168.82	84.41	188.75	51.501	3.418	-3.505	
46.000	-2.849	0.00	0.00	0.00	0.000	0.000	0.000		0.470	153.91	76.96	172.08	51.494	3.417	-3.499	
48.000	-3.211	0.00	0.00	0.00	0.000	0.000	0.000		0.460	139.82	69.91	156.32	51.489	3.415	-3.495	
50.000	-3.584	0.00	0.00	0.00	0.000	0.000	0.000		0.450	126.65	63.33	141.60	51.488	3.413	-3.495	
52.000	-3.960	0.00	0.00	0.00	0.000	0.000	0.000		0.441	114.28	57.14	127.77	51.494	3.410	-3.499	
54.000	-4.328	0.00	0.00	0.00	0.000	0.000	0.000		0.430	100.59	50.30	112.47	51.507	3.406	-3.510	
56.000	-4.675	0.00	0.00	0.00	0.000	0.000	0.000		0.415	79.36	39.68	88.73	51.531	3.402	-3.531	
58.000	-4.989	0.00	0.00	0.00	0.000	0.000	0.000		0.388	57.60	28.80	64.40	51.577	3.398	-3.569	
60.000	-5.254	0.00	0.00	0.00	0.000	0.000	0.000		0.346	49.17	24.59	54.98	51.679	3.394	-3.654	
62.000	-5.458	0.00	0.00	0.00	0.000	0.000	0.000		0.289	37.73	18.86	42.18	51.812	3.392	-3.767	
64.000	-5.609	0.00	0.00	0.00	0.000	0.000	0.000		0.215	23.04	11.52	25.75	51.976	3.393	-3.904	
66.000	-5.724	0.00	0.00	0.00	0.000	0.000	0.000		0.125	8.82	4.41	9.86	52.183	3.400	-4.077	
68.000	-5.817	0.00	0.00	0.00	0.000	0.000	0.000		0.020	0.99	0.49	1.10	52.440	3.417	-4.294	
70.000	-5.894	0.00	0.00	0.00	0.000	0.000	0.000		-0.101	0.00	0.00	0.00	0.000	0.000	0.000	
72.000	-5.963	0.00	0.00	0.00	0.000	0.000	0.000		-0.231	0.00	0.00	0.00	0.000	0.000	0.000	
74.000	-6.032	0.00	0.00	0.00	0.000	0.000	0.000		-0.367	0.00	0.00	0.00	0.000	0.000	0.000	
76.000	-6.105	0.00	0.00	0.00	0.000	0.000	0.000		-0.510	0.00	0.00	0.00	0.000	0.000	0.000	
78.000	-6.178	0.00	0.00	0.00	0.000	0.000	0.000		-0.655	0.00	0.00	0.00	0.000	0.000	0.000	
80.000	-6.252	0.00	0.00	0.00	0.000	0.000	0.000		-0.800	0.00	0.00	0.00	0.000	0.000	0.000	

DATE: 2 SEPT 1988

RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
 TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD

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VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK

CRASH VICTIM: 95TH PERCENTILE MALE

CONTACT FORCES - SEGMENT PANELS VS. SEGMENTS

TIME (MSEC)	PANEL 10 (RUDDER PEDALS. ) VS. SEGMENT 11 ( LF )				CONTACT LOCATION ( IN. )		
	DEFL- ECTION ( IN. )	NORMAL FORCE ( LB. )	FRICTION FORCE ( LB. )	RESULTANT FORCE ( LB. )	(VEH REFERENCE) X	Y	Z
0.000	0.002	0.08	0.00	0.08	51.239	-3.420	-3.286
2.000	0.001	0.07	0.01	0.07	51.239	-3.420	-3.286
4.000	0.002	0.11	0.04	0.12	51.239	-3.420	-3.285
6.000	0.005	0.29	0.14	0.32	51.240	-3.420	-3.287
8.000	0.010	0.75	0.37	0.83	51.245	-3.420	-3.291
10.000	0.019	1.60	0.80	1.78	51.254	-3.420	-3.298
12.000	0.031	2.67	1.33	2.98	51.266	-3.420	-3.308
14.000	0.048	4.10	2.05	4.58	51.284	-3.420	-3.323
16.000	0.070	5.93	2.96	6.63	51.306	-3.420	-3.342
18.000	0.096	8.18	4.09	9.15	51.334	-3.420	-3.365
20.000	0.128	13.70	6.85	15.32	51.366	-3.420	-3.393
22.000	0.165	20.47	10.23	22.88	51.406	-3.420	-3.425
24.000	0.206	28.26	14.13	31.59	51.464	-3.420	-3.474
26.000	0.250	38.58	19.29	43.14	51.489	-3.420	-3.496
28.000	0.296	49.45	24.73	55.29	51.503	-3.420	-3.507
30.000	0.344	60.69	30.34	67.85	51.511	-3.420	-3.513
32.000	0.394	72.29	36.14	80.82	51.516	-3.420	-3.518
34.000	0.444	133.60	66.80	149.37	51.519	-3.420	-3.520
36.000	0.483	188.09	94.05	210.29	51.519	-3.420	-3.520
38.000	0.507	219.74	109.87	245.68	51.515	-3.420	-3.518
40.000	0.514	216.05	108.03	241.55	51.508	-3.420	-3.511
42.000	0.515	213.02	106.51	238.16	51.497	-3.421	-3.502
44.000	0.514	212.01	106.00	237.03	51.482	-3.422	-3.490
46.000	0.514	211.89	105.95	236.90	51.465	-3.423	-3.475
48.000	0.514	212.07	106.04	237.10	51.446	-3.425	-3.459
50.000	0.511	207.70	103.85	232.22	51.425	-3.427	-3.441
52.000	0.498	190.37	95.18	212.83	51.399	-3.430	-3.420
54.000	0.472	155.61	77.80	173.97	51.361	-3.432	-3.388
56.000	0.436	107.92	53.96	120.66	51.306	-3.435	-3.342
58.000	0.395	59.01	29.50	65.97	51.268	-3.437	-3.310
60.000	0.353	50.53	25.27	56.50	51.259	-3.438	-3.302
62.000	0.307	41.43	20.72	46.32	51.288	-3.438	-3.327
64.000	0.268	33.64	16.82	37.61	51.387	-3.436	-3.409
66.000	0.234	26.90	13.45	30.07	51.514	-3.432	-3.516
68.000	0.200	20.05	10.02	22.41	51.657	-3.425	-3.637
70.000	0.159	13.90	6.95	15.54	51.813	-3.413	-3.767
72.000	0.112	6.75	3.37	7.55	51.972	-3.393	-3.901
74.000	0.056	2.80	1.40	3.13	52.128	-3.366	-4.032
76.000	-0.008	0.00	0.00	0.00	0.000	0.000	0.000
78.000	-0.077	0.00	0.00	0.00	0.000	0.000	0.000
80.000	-0.141	0.00	0.00	0.00	0.000	0.000	0.000

DATE: 2 SEPT 1988  
 RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
 TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD  
 VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK  
 CRASH VICTIM: 95TH PERCENTILE MALE

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HARNESS SYSTEM BELT ENDPOINT FORCES

TIME (MSEC)	BELT NO. 1 OF HARNESS NO. 1				BELT NO. 2 OF HARNESS NO. 1			
	POINT NO. 1		POINT NO. 12		POINT NO. 13		POINT NO. 27	
	STRAIN ( IN./ IN.)	FORCE ( LB.)	STRAIN ( IN./ IN.)	FORCE ( LB.)	STRAIN ( IN./ IN.)	FORCE ( LB.)	STRAIN ( IN./ IN.)	FORCE ( LB.)
0.000	0.000000	0.00	0.000000	0.00	0.000000	0.00	0.000000	0.00
2.000	0.000025	0.37	0.000017	0.25	0.000014	0.21	0.000018	0.27
4.000	0.000119	1.79	0.000065	0.98	0.000057	0.85	0.000152	2.27
6.000	0.000281	4.22	0.000150	2.25	0.000124	1.86	0.000470	7.04
8.000	0.000523	7.85	0.000276	4.15	0.000219	3.29	0.001018	15.27
10.000	0.000854	12.81	0.000438	6.57	0.000336	5.04	0.001803	27.04
12.000	0.001023	15.34	0.000481	7.21	0.000344	5.16	0.002454	36.81
14.000	0.001320	19.80	0.000515	7.72	0.000433	6.50	0.003168	47.52
16.000	0.001672	25.08	0.000551	8.27	0.000496	7.44	0.003856	57.84
18.000	0.001420	21.30	0.000400	6.00	0.000404	6.06	0.003427	51.41
20.000	0.001831	27.46	0.000484	7.26	0.000498	7.46	0.004276	64.13
22.000	0.002363	35.45	0.000617	9.26	0.000643	9.65	0.005479	82.19
24.000	0.003085	46.27	0.000877	13.15	0.000921	13.81	0.019008	285.12
26.000	0.004040	60.61	0.001215	18.22	0.001284	19.26	0.021036	315.53
28.000	0.006003	90.05	0.001724	25.85	0.001768	26.52	0.027340	410.10
30.000	0.009472	142.08	0.002256	33.83	0.002429	36.44	0.035707	564.14
32.000	0.013979	209.69	0.003249	48.73	0.004372	65.58	0.023671	355.06
34.000	0.019790	296.85	0.004754	71.30	0.008401	126.02	0.020865	312.97
36.000	0.026146	392.20	0.007124	106.86	0.018334	275.01	0.025025	375.38
38.000	0.032200	494.00	0.010831	162.46	0.030199	453.97	0.039302	636.04
40.000	0.037809	606.17	0.021023	315.35	0.040241	654.82	0.056200	1170.59
42.000	0.043063	711.27	0.036025	570.49	0.050245	863.00	0.075150	2182.56
44.000	0.048343	816.85	0.053858	1054.46	0.060539	1408.57	0.064897	1639.53
46.000	0.053827	1052.84	0.071518	1990.44	0.072248	2029.17	0.084525	2679.84
48.000	0.055271	1129.35	0.087363	2830.23	0.056456	1192.15	0.103767	3631.84
50.000	0.058800	1316.42	0.098307	3410.27	0.065766	1685.60	0.093883	3175.81
52.000	0.064710	1629.61	0.098688	3430.48	0.068526	1831.86	0.107224	3752.85
54.000	0.072120	2022.35	0.087992	2863.56	0.074577	2152.58	0.092638	3109.84
56.000	0.076068	2231.59	0.071069	1966.67	0.075155	2183.20	0.089018	2917.94
58.000	0.074497	2148.32	0.049516	840.31	0.069789	1898.82	0.084438	2675.23
60.000	0.061993	1485.61	0.026359	395.38	0.082583	2576.88	0.093363	3148.22
62.000	0.047024	790.48	0.005156	77.34	0.032040	490.80	0.086107	2763.69
64.000	0.028177	422.66	0.000000	0.00	0.024499	367.48	0.065353	1663.72
66.000	0.007038	105.57	0.000000	0.00	0.006231	93.46	0.051787	944.69
68.000	0.000000	0.00	0.000000	0.00	0.000000	0.00	0.037962	609.25
70.000	0.000000	0.00	0.000000	0.00	0.000000	0.00	0.022501	337.51
72.000	0.000000	0.00	0.000000	0.00	0.000000	0.00	0.012711	190.67
74.000	0.000000	0.00	0.000000	0.00	0.000000	0.00	0.006159	92.39
76.000	0.000000	0.00	0.000000	0.00	0.000000	0.00	0.000000	0.00
78.000	0.000000	0.00	0.000000	0.00	0.000000	0.00	0.000000	0.00
80.000	0.000000	0.00	0.000000	0.00	0.000000	0.00	0.000000	0.00

DATE: 2 SEPT 1988  
 RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
 TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD  
 VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK  
 CRASH VICTIM: 95TH PERCENTILE MALE

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CONTACT FORCES - SEGMENT NO. 2 ( CT ) VS. SEGMENT NO. 13 ( RLA )

TIME (MSEC)	DEFL- ECTION ( IN.)	NORMAL FORCE ( LB.)	FRICTION FORCE ( LB.)	RESULTANT FORCE ( LB.)	CONTACT LOCATION ( IN.)							
					SEG. 2 X	LOCAL REFERENCE			SEG. 13 X	LOCAL REFERENCE		
						Y	Z			Y	Z	
0.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
2.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
4.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
6.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
8.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
10.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
12.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
14.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
16.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
18.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
20.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
22.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
24.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
26.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
28.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
30.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
32.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
34.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
36.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
38.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
40.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
42.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
44.000	0.009	4.39	1.10	4.57	.018	5.365	-1.749	-0.875	-0.809	-7.906		
46.000	0.010	3.62	0.90	3.73	2.036	5.360	-1.739	-0.881	-0.803	-7.903		
48.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
50.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
52.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
54.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
56.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
58.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
60.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
62.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
64.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
66.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
68.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
70.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
72.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
74.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
76.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
78.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
80.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		

DATE: 2 SEPT 1988  
 RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
 TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD  
 VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK  
 CRASH VICTIM: 95TH PERCENTILE MALE

PAGE: 38.01

## CONTACT FORCES - SEGMENT NO. 2 ( CT ) VS. SEGMENT NO. 15 ( LLA)

TIME (MSEC)	DEFL- ECTION ( IN.)	NORMAL FORCE ( LB.)	FRICTION FORCE ( LB.)	RESULTANT FORCE ( LB.)	CONTACT LOCATION ( IN.)					
					SEG. 2 LOCAL REFERENCE			SEG. 15 LOCAL REFERENCE		
					X	Y	Z	X	Y	Z
0.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
2.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
4.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
6.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
8.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
10.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
12.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
14.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
16.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
18.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
20.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
22.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
24.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
26.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
28.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
30.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
32.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
34.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
36.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
38.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
40.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
42.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
44.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
46.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
48.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
50.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
52.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
54.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
56.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
58.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
60.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
62.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
64.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
66.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
68.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
70.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
72.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
74.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
76.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
78.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
80.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000

DATE: 2 SEPT 1988  
 RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
 TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD  
 VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK  
 CRASH VICTIM: 95TH PERCENTILE MALE

PAGE: 39.01

## CONTACT FORCES - SEGMENT NO. 6 ( RUL) VS. SEGMENT NO. 13 ( RLA)

TIME (MSEC)	DEFL- ECTION ( IN.)	NORMAL FORCE ( LB.)	FRICTION FORCE ( LB.)	RESULTANT FORCE ( LB.)	CONTACT LOCATION ( IN.)					
					SEG. 6	LOCAL REFERENCE		SEG. 13	LOCAL REFERENCE	
					X	Y	Z	X	Y	Z
0.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
2.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
4.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
6.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
8.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
10.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
12.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
14.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
16.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
18.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
20.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
22.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
24.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
26.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
28.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
30.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
32.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
34.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
36.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
38.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
40.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
42.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
44.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
46.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
48.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
50.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
52.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
54.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
56.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
58.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
60.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
62.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
64.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
66.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
68.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
70.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
72.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
74.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
76.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
78.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
80.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000



DATE: 2 SEPT 1988  
 RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
 TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD  
 VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK  
 CRASH VICTIM: 95TH PERCENTILE MALE

PAGE: 40.01

## CONTACT FORCES - SEGMENT NO. 9 ( LUL) VS. SEGMENT NO. 15 ( LLA)

TIME (MSEC)	DEFL- ECTION ( IN.)	NORMAL FORCE ( LB.)	FRICTION FORCE ( LB.)	RESULTANT FORCE ( LB.)	CONTACT LOCATION ( IN.)							
					SEG. 9 X	LOCAL REFERENCE			SEG. 15 X	LOCAL REFERENCE		
						Y	Z			Y	Z	
0.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
2.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
4.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
6.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
8.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
10.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
12.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
14.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
16.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
18.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
20.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
22.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
24.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
26.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
28.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
30.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
32.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
34.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
36.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
38.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
40.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
42.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
44.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
46.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
48.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
50.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
52.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
54.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
56.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
58.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
60.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
62.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
64.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
66.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
68.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
70.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
72.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
74.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
76.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000		
78.000	0.282	132.75	33.19	136.84	1.229	-1.146	10.441	-1.121	0.658	6.935		
80.000	0.685	321.84	80.46	331.75	1.096	-1.142	10.037	-1.019	0.683	6.725		

DATE: 2 SEPT 1988  
 RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
 TWO BELT HARNESS WITH HYPERELLIPTOID FOR DASH BOARD  
 VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK  
 CRASH VICTIM: 95TH PERCENTILE MALE

PAGE: 41.01

## CONTACT FORCES - SEGMENT NO. 13 ( RLA) VS. SEGMENT NO. 16 (VEH )

TIME (MSEC)	DEFL- ECTION ( IN.)	NORMAL FORCE ( LB.)	FRICTION FORCE ( LB.)	RESULTANT FORCE ( LB.)	CONTACT LOCATION ( IN.)					
					SEG. 13 LOCAL REFERENCE	SEG. 16 LOCAL REFERENCE				
					X	Y	Z	X	Y	Z
0.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
2.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
4.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
6.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
8.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
10.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
12.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
14.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
16.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
18.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
20.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
22.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
24.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
26.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
28.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
30.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
32.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
34.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
36.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
38.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
40.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
42.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
44.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
46.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
48.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
50.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
52.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
54.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
56.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
58.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
60.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
62.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
64.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
66.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
68.000	0.217	24.79	12.39	27.71	1.714	0.433	2.758	32.371	6.599	-23.212
70.000	0.496	193.03	96.51	215.81	1.651	0.426	3.110	32.482	6.706	-23.329
72.000	0.671	444.83	222.41	497.33	1.602	0.408	3.504	32.546	6.820	-23.401
74.000	0.627	362.71	181.36	405.53	1.587	0.388	3.859	32.512	6.921	-23.391
76.000	0.420	87.00	43.50	97.27	1.600	0.370	4.164	32.409	7.003	-23.320
78.000	0.219	23.90	11.95	26.72	1.612	0.354	4.449	32.311	7.076	-23.249
80.000	0.103	5.46	2.73	6.10	1.608	0.342	4.722	32.256	7.143	-23.206

DATE: 2 SEPT 1988  
 RUN DESCRIPTION: EXAMPLE 1: BASIC SLED TEST SIMULATION  
 TWO BELT HARNESS WITH HYPERELLIPSOID FOR DASH BOARD  
 VEHICLE DECELERATION: SLED ACCELERATION - 20G PEAK  
 CRASH VICTIM: 95TH PERCENTILE MALE

PAGE: 42.01

## CONTACT FORCES - SEGMENT NO. 15 ( LLA ) VS. SEGMENT NO. 16 ( VEH )

TIME (MSEC)	DEFL- ECTION ( IN. )	NORMAL FORCE ( LB. )	FRICTION FORCE ( LB. )	RESULTANT FORCE ( LB. )	CONTACT LOCATION ( IN. )					
					SEG. 15	LOCAL REFERENCE		SEG. 16	LOCAL REFERENCE	
					X	Y	Z	X	Y	Z
0.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
2.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
4.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
6.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
8.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
10.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
12.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
14.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
16.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
18.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
20.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
22.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
24.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
26.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
28.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
30.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
32.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
34.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
36.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
38.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
40.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
42.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
44.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
46.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
48.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
50.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
52.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
54.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
56.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
58.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
60.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
62.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
64.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
66.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
68.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
70.000	0.000	0.00	0.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000
72.000	0.524	226.73	113.37	253.49	1.755	0.307	0.651	32.615	-6.119	-23.311
74.000	0.804	610.21	305.10	682.23	1.712	0.298	0.537	32.732	-6.130	-23.436
76.000	0.907	736.13	368.06	823.02	1.699	0.281	0.427	32.764	-6.147	-23.486
78.000	0.798	590.20	295.10	659.86	1.720	0.263	0.294	32.694	-6.176	-23.450
80.000	0.583	303.74	151.87	339.60	1.758	0.244	0.157	32.574	-6.224	-23.368

## HEAD INJURY CRITERION

HIC = 192.44      TIME DURATION = 52.000 TO 65.000 MSEC  
WITH HEAD RESULTANTS = 25.844 AND 23.464 G'S

AVERAGE HEAD RESULTANT FOR TIME DURATION = 46.574 G'S

## HEAD SEVERITY INDEX

HSI = 245.20

MAX HEAD RESULTANT = 65.716 G'S AT 60.000 MSEC

## CHEST SEVERITY INDEX

CSI = 733.64

MAX CHEST RESULTANT = 146.473 G'S AT 59.000 MSEC

SUB	CALLS	TIME	%
MAIN3D	1	155	0.53
INPUT	1	305	1.05
CHAIN	484	832	2.85
EJOINT	484	29	0.10
DINT	41	885	3.04
PDAUX	568	1112	3.82
DAUX	483	1056	3.62
SETUP1	483	766	2.63
CONTCY	483	444	1.52
PLELP	5313	2244	7.70
SEGSEG	2898	2029	6.96
HBELT	1072	4385	15.05
VISPR	483	1922	6.59
SETUP2	483	157	0.54
DAUX11	483	1562	5.36
DAUX12	483	678	2.33
DAUX22	483	370	1.27
FSMSOL	1072	3988	13.68
OUTPUT	86	707	2.43
UPDATE	85	53	0.18
HPTURB	85	3862	13.25
DZP	482	455	1.56
POSTPR	1	1149	3.94
TOTAL		29145	100.00

APPENDIX D1

Example 2, ATB Dynamic Joint Test  
Input File (EX2.AIN)

CARD A1A

IN.	LB.	SEC.	7	000	KNOT	WIND	0.0	0.0	386.088	0.0	CARD	A3		
4	20	0.002	0.0005	0.001	.000063						CARD	A4		
1	020	2	0	0	0	0	0	0	0	0	0	0		
2	1	95TH PERCENTILE MALE										CARD	B1	
LARM	L	5.901	.3331	.3331	.0214	1.871	1.871	110.269	0.000	0.000	0.000	CARD	B2A	
UARM	U	5.542	.1743	.1743	.0259	2.122	2.122	7.497	0.000	0.000	0.000	CARD	B2A	
ELBW	E	1	5	0.00	0.00	8.20	0.00	0.00	-5.42	1	0.00	0.00		
				0.00	0.00	0.00	0.00	-67.19	0.00					
		.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	CARD	B4	
		0.0	0.0	30.	0.0	0.0			0.0	0.0		CARD	B5	
		.00	.00	.00	.00	.00	.00	.01	.01	.001	.001	.001		
		.00	.00	.00	.00	.00	.00	.01	.01	.001	.00	.00		
CONSTANT WIND VELOCITY OF 600 KNOTS												CARD	B6	
0.0	0.0	0.01	2161.	0.00	0.00	0.00	0.00	-3	0.0	2.30		0		
2	1	3												
		0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000		CARD	C5	
		0.000	0.000	0.000	12161.000	0.000	0.000	0.000	0.000	0.000		CARD	C5	
		2.300	0.000	0.000	12161.000	0.000	0.000	0.000	0.000	0.000		CARD	C5	
		4.600	0.000	0.000	12161.000	0.000	0.000	0.000	0.000	0.000		CARD	C5	
1	0	0	0	0	0	0	0	1	0	0		CARD	D1	
1	WIND PLANE											CARD	D2A	
		10.0	10.0	5.0								CARD	D2B	
		-10.0	10.0	5.0								CARD	D2C	
		10.0	-10.0	5.0								CARD	D2D	
0	0	0	0	0	0	0	0	0	0	0	0	CARD	D7	
999												CARD	E1	
1	WIND FORCE											CARD	E6A	
		1.4000	13404.0000	14.6960		1		3				CARD	E6B	
0												CARD	F1A	
0	0												CARD	F3A
0												CARD	F4A	
1	1												CARD	F7A
-1	1	3	1	1	0	1	2	2				CARD	F7B	
-2	2	3	1	1	0	1	1	1				CARD	F7B	
		0.0	0.0	0.0	0	0	0	0	1			CARD	G1A	
		0.66000	0.00000	-18.98000	0.0	0.0	0.0	0.0				CARD	G2A	
		0.00	-2.00	0.00	0.00	0.00	0.00	0.00	3	2	1	0		
		0.00	-2.00	0.00	0.00	0.00	0.00	0.00	3	2	1	0		
0												CARD	H1A	
												CARD	H1B	
0												CARD	H2A	
												CARD	H2B	
3	2	1	0.0	0.0	8.20							CARD	H3A	
		1	2	0.0	0.0	-5.42						CARD	H3B	
		4	2	0.0	0.0	0.0								

## APPENDIX D2

Example 2, ATB Dynamic Joint Test  
386 Directory File (ATBIV2.DIR)



EXP2.TP1	UNIT 1	ATB OUTPUT, VIEW BODY ELEMENT AND CONTACT PLANE INPUT
EXP2.PRP	UNIT 2	ATB PRINTER PLOTS
ATB.ROU	UNIT 3	ATB RESTART RUN OUTPUT FILE
ATB.RIN	UNIT 4	ATB RESTART RUN INPUT FILE
EX2.AIN	UNIT 5	ATB INPUT, GEBOO BODY DESCRIPTION OUTPUT
EXP2.AOU	UNIT 6	ATB PRIMARY OUTPUT FILE
EXP2.TP8	UNIT 8	ATB SUBROUTINE POSTPR OUTPUT FILE
0 IDEF	UNIT 10	DRAWING OPTION SEE PLOTWORKS, PLOT88, 3.1
91 IOPORT	UNIT 10	HARDWARE INTERFACE 91/ 1 SEE PLOTWORKS, PLOT88, 3.1
91 MODEL	UNIT 10	OUTPUT DEVICE 91/64 SEE PLOTWORKS, PLOT88, 3.1
EXP2.T24	21 - 85	LAST ATB TABULAR TIME HISTORY OUTPUT FILE (21-85)

### APPENDIX D3

Example 2, ATB Dynamic Joint Test  
386 Output File (EXP2.AOU)

DEVELOPED BY CALSPAN CORP., P.O. BOX 400, BUFFALO NY 14225  
AND BY J&J TECHNOLOGIES INC., ORCHARD PARK, NY 14127

FOR THE AIR FORCE ARMSTRONG AEROSPACE MEDICAL RESEARCH  
LABORATORY, WRIGHT PATTERSON AIR FORCE BASE  
UNDER CONTRACTS F33615-75C-5002, -78C-0516 AND -80C-05117

AND FOR THE NATIONAL HIGHWAY TRAFFIC SAFETY ADMINISTRATION,  
U.S. DEPARTMENT OF TRANSPORTATION, UNDER CONTRACTS  
FH-11-7592, HS-053-2-485, HS-6-01300 AND HS-6-01410.

PROGRAM DOCUMENTATION: NHTSA REPORT NOS. DOT-HS-801-507  
THROUGH 510 (FORMERLY CALSPAN REPORT NO. 2Q-5180-L-1),  
AVAILABLE FROM NTIS (ACCESSION NOS. PB-241692, 3, 4 AND 5),  
APPENDIXES A-J TO THE ABOVE (AVAILABLE FROM CALSPAN),  
AND REPORT NOS. AMRL-TR-75-14 (NTIS NO. AD-A014 816),  
AFAMRL-TR-80-14 (NTIS NO. AD-A088 029), AND  
AFAMRL-TR-83-073 (NTIS NO. AD-B079 184).

PROGRAM ATB-IV 80386 IMPLEMENTATION COMPLETED BY KETRON,  
OCTOBER 31, 1989, UNDER CONTRACT F33615-88-C-0543

FEB. 4, 1988 IRSIN= 0 IRSOUT= 0 RSTIME = 0.0000

CARDS A

EXAMPLE 2: DYNAMIC JOINT TEST  
SLIP JOINT / 600 KNOT WIND

UNITL = IN. UNITH = LB. UNITT = SEC. GRAVITY VECTOR = ( 0.0000, 0.0000, 386.0880) G = 386.0880

NDINT = 4 NSTEPS = 20 DT = 0.002000 HO = 0.000500 HMAX = 0.001000 HMIN = 0.000063

NPRT ARRAY

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36
1	0	20	2	0	0	0	0	0	0	0	0	0	0	0	0	0	16	0	0	0	0	0	0	0	1	0	0	0	1	0	0	0	0	0	1

CRASH VICTIM 95TH PERCENTILE MALE 2 SEGMENTS 1 JOINTS

PAGE 2

SEGMENT		WEIGHT ( LB.)	PRINCIPAL MOMENTS OF INERTIA ( LB.-SEC.**2- IN.)			SEGMENT CONTACT ELLIPSOID SEMIAXES ( IN.)			CENTER ( IN.)			PRINCIPAL AXES (DEG)		
1	SYM PLOT		X	Y	Z	X	Y	Z	X	Y	Z	YAW	PITCH	ROLL
1	LARM L	5.901	0.3331	0.3331	0.0214	1.871	1.871	10.269	0.000	0.000	0.000	0.00	0.00	0.00
2	UARM U	5.542	0.1743	0.1743	0.0259	2.122	2.122	7.497	0.000	0.000	0.000	0.00	0.00	0.00

CARDS 8.3

JOINT		LOCATION( IN.) - SEG(JNT)			LOCATION( IN.) - SEG(J+1)			PRIN. AXIS(DEG) - SEG(JNT)			PRIN. AXIS(DEG) - SEG(J+1)		
J	SYM PLOT JNT PIN	X	Y	Z	X	Y	Z	YAW	PITCH	ROLL	YAW	PITCH	ROLL
1	ELBW E 1 5	0.000	0.000	8.200	0.000	0.000	-5.420	0.00	0.00	0.00	0.00	-67.19	0.00

UNLOCK CONDITIONS FOR SLIP JOINTS

JOINT	TENSION ( LB.)	COMPRESSION ( LB.)
1	0.000	0.000

## FLEXURAL SPRING CHARACTERISTICS

## TORSIONAL SPRING CHARACTERISTICS

JOINT	SPRING COEF. ( IN. LB./DEG**J)				JOINT STOP (DEG)	SPRING COEF. ( IN. LB./DEG**J)				JOINT STOP (DEG)
	LINEAR (J=1)	QUADRATIC (J=2)	CUBIC (J=3)	ENERGY DISSIPATION COEF.		LINEAR (J=1)	QUADRATIC (J=2)	CUBIC (J=3)	ENERGY DISSIPATION COEF.	
1 ELBW	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

CARDS 8.5

## JOINT VISCOUS CHARACTERISTICS AND LOCK-UNLOCK CONDITIONS

JOINT	VISCOUS COEFFICIENT ( IN. LB.SEC./DEG)	COULOMB FRICTION COEF. ( IN. LB.)	FULL FRICTION ANGULAR VELOCITY (DEG/SEC.)	MAX TORQUE FOR A LOCKED JOINT ( IN. LB.)	MIN TORQUE FOR UNLOCKED JOINT ( IN. LB.)	MIN. ANG. VELOCITY FOR UNLOCKED JOINT (RAD/SEC.)	IMPULSE RESTITUTION COEFFICIENT
1 ELBW	0.000	0.00	30.00	0.00	0.00	0.00	0.000

## SEGMENT INTEGRATION CONVERGENCE TEST INPUT

PAGE 4  
CARDS 8.6

SEGMENT NO. SYM	ANGULAR VELOCITIES (RAD/SEC.)			LINEAR VELOCITIES ( IN./SEC.)			ANGULAR ACCELERATIONS (RAD/SEC.**2)			LINEAR ACCELERATIONS ( IN./SEC.**2)		
	MAG. TEST	ABS. ERROR	REL. ERROR	MAG. TEST	ABS. ERROR	REL. ERROR	MAG. TEST	ABS. ERROR	REL. ERROR	MAG. TEST	ABS. ERROR	REL. ERROR
1 LARM	0.000	0.000	0.0000	0.000	0.000	0.0000	0.010	0.010	0.0010	0.001	0.001	0.0010
2 UARM	0.000	0.000	0.0000	0.000	0.000	0.0000	0.010	0.010	0.0010	0.000	0.000	0.0000

## VEHICLE DECELERATION INPUTS

PAGE 5  
CARDS C

## CONSTANT WIND VELOCITY OF 600 KNOTS

YAW	PITCH	ROLL	VIPS	VTIME	XO(X)	XO(Y)	XO(Z)	NATAB	ATO	ADT	MSEG
0.000	0.000	0.000	12161.000	0.000	0.000	0.000	0.000	-3	0.000000	2.300000	0

SPLINE FIT TABULAR INPUT

LTYPE = 2 LFIT = 1 NPTS = 3

INITIAL LINEAR POSITION ( IN.)				INITIAL ANGULAR POSITION (DEG)			
TIME(SEC.)=	0.0000	X=	0.000	Y=	0.000	Z=	0.000

TIME(SEC.)	LINEAR VELOCITY ( IN./SEC.)			ANGULAR VELOCITY (DEG/SEC.)		
	X	Y	Z	X	Y	Z
0.00000	0.000	0.000	12161.000	0.000	0.000	0.000
2.30000	0.000	0.000	12161.000	0.000	0.000	0.000
4.60000	0.000	0.000	12161.000	0.000	0.000	0.000

VEHICLE LINEAR TIME HISTORY CONSTANT WIND VELOCITY OF 600 KNOTS

TIME (MSEC)	LINEAR DECELERATIONS (G'S)			LINEAR VELOCITIES ( IN./SEC.)			LINEAR DISPLACEMENTS ( IN.)		
	X	Y	Z	X	Y	Z	X	Y	Z
0.000	0.000	0.000	0.000	0.000	0.000	12161.000	0.000	0.000	0.000
2300.000	0.000	0.000	0.000	0.000	0.000	12161.000	0.000	0.000	27970.300
4600.000	0.000	0.000	0.000	0.000	0.000	12161.000	0.000	0.000	55940.600





NPL NBLT NBAG NBLP NQ NSD NHRNSS NWINDF NJNTF NFORCE  
1 0 0 0 0 0 0 1 0 0

PAGE 8  
CARD D.1  
CARDS D.2

PLANE INPUTS

PLANE NO. 1 WIND PLANE

	X	Y	Z
POINT 1	10.0000	10.0000	5.0000
POINT 2	-10.0000	10.0000	5.0000
POINT 3	10.0000	-10.0000	5.0000

BODY SEGMENT SYMMETRY INPUT

CARD D.7

SEG NO. 1 2  
NSYM(J) 0 0

WIND FORCE FUNCTION NO. 1 WIND FORCE

NTI( 1) = 1

PAGE 9  
CARDS E.6

SPEC. HEAT RATIO	SONIC VEL.	ABS. PRESS.	SEGMENT	REF. SEGMENT
1.4000	13404.0000	14.6960	1LARM	3VEH



SEGMENT-ELLIPSOID	SEGMENT-PLANE	WIND FORCE FUNCTION	DRAG COEFFICIENT FUNCTION	BLOCKING SEGMENTS-ELLIPSOID
-1 - 1	3 - 1	1	0	
LARM	VEH -WIND PLANE	WIND FORCE		2- 2
-2 - 2	3 - 1	1	0	
UARM	VEH -WIND PLANE	WIND FORCE		1- 1

ZPLT(X)	ZPLT(Y)	ZPLT(Z)	I1	J1	I2	J2	I3	SPLT(1)	SPLT(2)	SPLT(3)
0.	0.	0.	0	0	0	0	1	10.00	6.00	1.00

INITIAL POSITIONS (INERTIAL REFERENCE)

CARDS G.2

SEGMENT NO. SEG	LINEAR POSITION ( IN.)			LINEAR VELOCITY ( IN./SEC.)		
	X	Y	Z	X	Y	Z
1 LARM	0.66000	0.00000	-18.98000	0.00000	0.00000	0.00000
2 UARM	0.18467	0.00000	-5.36830	0.00000	0.00000	0.00000

INITIAL ANGULAR ROTATION AND VELOCITY

CARDS G.3

SEGMENT NO. SEG	ANGULAR ROTATION (DEG)			ANGULAR VELOCITY (DEG/SEC.)			IYPR			
	YAW	PITCH	ROLL	X	Y	Z				
1 LARM	0.00000	-2.00000	0.00000	0.00000	0.00000	0.00000	3	2	1	0
2 UARM	0.00000	-2.00000	0.00000	0.00000	0.00000	0.00000	3	2	1	0

## TABULAR TIME HISTORY CONTROL PARAMETERS

TYPE KSG SELECTED SEGMENTS OR JOINTS

H.1	0		
REF			
H.2	0		
REF			
H.3	3	1 2 2	
REF		2 1 4	
H.4	0		
REF			
H.5	0		
REF			
H.6	0		
REF			
H.7	1	1	
REF		0	
H.8	2	1 2	
REF		0 0	
H.9	1	1	
REF		1	

SEGMENT	(INERTIAL) ANGULAR ROTATION (DEG)			(LOCAL) ANGULAR VELOCITY (RAD/SEC.)			(LOCAL) ANGULAR ACCELERATION (RAD/SEC.**2)		
	YAW	PITCH	ROLL	X	Y	Z	X	Y	Z
1 LARM	0.0000	-2.0000	0.0000	0.00000	0.00000	0.00000	0.000516	7.241005	-0.000467
2 UARM	0.0000	-2.0000	0.0000	0.00000	0.00000	0.00000	-0.000433	22.756386	0.000000
3 VEH	0.0000	0.0000	0.0000	0.00000	0.00000	0.00000	0.000000	0.000000	0.000000

SEGMENT	(INERTIAL) LINEAR POSITION ( IN.)			(INERTIAL) LINEAR VELOCITY ( IN./SEC.)			(INERTIAL) LINEAR ACCELERATIONS (G'S)		
	X	Y	Z	X	Y	Z	X	Y	Z
1 LARM	0.6600	0.0000	-18.9800	0.00000	0.00000	0.00000	0.123940	0.000002	1.323803
2 UARM	0.1847	0.0000	-5.3683	0.00000	0.00000	0.00000	-0.131968	-0.000003	22.212406
3 VEH	0.0000	0.0000	0.0000	0.00000	0.00000	12161.00000	0.000000	0.000000	0.000000

SEGMENT	(INERTIAL) U1 ARRAY ( IN./SEC.**2) EXTERNAL LINEAR ACCELERATIONS			(LOCAL) U2 ARRAY (RAD/SEC.**2) EXTERNAL ANGULAR ACCELERATIONS			KINETIC ENERGY ( LB.- IN.)		
	X	Y	Z	X	Y	Z	LINEAR	ANGULAR	TOTAL
1 LARM	0.0000E+00	0.0000E+00	0.5094E+03	0.85920E-03	-0.10774E+02	-0.46703E-03	0.00000E+00	0.00000E+00	0.00000E+00
2 UARM	0.0000E+00	0.0000E+00	0.8578E+04	-0.30574E-13	-0.46180E-14	-0.21433E-14	0.00000E+00	0.00000E+00	0.00000E+00
TOTAL BODY KINETIC ENERGY									
	0.00000E+00	0.00000E+00	0.00000E+00						

JOINT	IPIN	(INERTIAL) JOINT FORCES ( LB.)			(INERTIAL) JOINT TORQUES ( IN. LB.)			RELATIVE ANGULAR VELOCITY (RAD/SEC.)
		X	Y	Z	X	Y	Z	
1 ELBW	5	-0.731E+00	-0.139E-04	-0.255E-01	0.0000E+00	0.0000E+00	0.0000E+00	0.000

SEGMENT	(INERTIAL)			(LOCAL)			(LOCAL)		
	ANGULAR ROTATION (DEG)			ANGULAR VELOCITY (RAD/SEC.)			ANGULAR ACCELERATION (RAD/SEC.**2)		
	YAW	PITCH	ROLL	X	Y	Z	X	Y	Z
1 LARM	0.0000	-4.6324	0.0000	0.00002	-2.40848	0.00000	0.000697	-69.675443	0.000000
2 UARM	0.0000	1.9906	0.0000	-0.00004	2.43012	0.00000	-0.000080	-49.821585	-0.000001
3 VEH	0.0000	0.0000	0.0000	0.00000	0.00000	0.00000	0.000000	0.000000	0.000000

SEGMENT	(INERTIAL)			(INERTIAL)			(INERTIAL)		
	LINEAR POSITION ( IN.)			LINEAR VELOCITY ( IN./SEC.)			LINEAR ACCELERATIONS (G'S)		
	X	Y	Z	X	Y	Z	X	Y	Z
1 LARM	0.5275	0.0000	-13.8865	-7.63751	-0.00008	255.94533	-0.811909	-0.000008	17.016782
2 UARM	0.3258	0.0000	-3.6572	8.13242	0.00008	79.32710	0.864511	0.000009	3.974612
3 VEH	0.0000	0.0000	486.4400	0.00000	0.00000	12161.00000	0.000000	0.000000	0.000000

SEGMENT	(INERTIAL)			(LOCAL)			KINETIC ENERGY		
	U1 ARRAY ( IN./SEC.**2)			U2 ARRAY (RAD/SEC.**2)			( LB.- IN.)		
	EXTERNAL LINEAR ACCELERATIONS			EXTERNAL ANGULAR ACCELERATIONS			LINEAR	ANGULAR	TOTAL
1 LARM	0.2556E-02	0.2735E-12	0.6595E+04	0.87740E-07	0.83063E-12	-0.18158E-13	0.50106E+03	0.96612E+00	0.50203E+03
2 UARM	0.4615E-03	0.4939E-13	0.1508E+04	-0.15599E-02	0.98653E+02	-0.90086E-06	0.45639E+02	0.51466E+00	0.46153E+02
TOTAL BODY KINETIC ENERGY							0.54670E+03	0.14808E+01	0.54818E+03

		(INERTIAL)			(INERTIAL)			
		JOINT FORCES ( LB.)			JOINT TORQUES ( IN. LB.)			RELATIVE ANGULAR
JOINT	IPIN	X	Y	Z	X	Y	Z	VELOCITY (RAD/SEC.)
1 ELBW	5	0.479E+01	0.481E-04	0.388E+00	0.0000E+00	0.0000E+00	0.0000E+00	4.839



	HIC & HSI POINT	CSI POINT
N.11	0	0

DATE: FEB. 4, 1988

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RUN DESCRIPTION: EXAMPLE 2: DYNAMIC JOINT TEST

SLIP JOINT / 600 KNOT WIND

PAGE: 21.01

VEHICLE DECELERATION: CONSTANT WIND VELOCITY OF 600 KNOTS

CRASH VICTIM: 95TH PERCENTILE MALE

POINT REL. LINEAR DISPLACEMENT ( IN. )

TIME (MSEC)	POINT ( 0.00, 0.00, 8.20) ON SEGMENT NO. 1 - LARM IN UARM REFERENCE				POINT ( 0.00, 0.00, -5.42) ON SEGMENT NO. 2 - UARM IN LARM REFERENCE				POINT ( 0.00, 0.00, 0.00) ON SEGMENT NO. 2 - UARM IN GRND REFERENCE			
	X	Y	Z	RES	X	Y	Z	RES	X	Y	Z	RES
0.000	0.000	0.000	-5.420	5.420	0.000	0.000	8.200	8.200	0.185	0.000	-5.368	5.371
0.500	0.000	0.000	-5.420	5.420	0.000	0.000	8.200	8.200	0.185	0.000	-5.368	5.371
1.000	0.000	0.000	-5.419	5.419	0.000	0.000	8.199	8.199	0.185	0.000	-5.366	5.370
1.500	0.000	0.000	-5.417	5.417	0.000	0.000	8.197	8.197	0.185	0.000	-5.365	5.368
2.000	0.000	0.000	-5.414	5.414	0.000	0.000	8.194	8.194	0.185	0.000	-5.362	5.365
3.000	0.000	0.000	-5.405	5.405	0.000	0.000	8.185	8.185	0.185	0.000	-5.356	5.359
4.000	0.000	0.000	-5.392	5.392	0.000	0.000	8.172	8.172	0.186	0.000	-5.347	5.350
5.000	0.000	0.000	-5.375	5.375	0.000	0.000	8.155	8.155	0.187	0.000	-5.336	5.339
6.000	0.000	0.000	-5.354	5.354	0.000	0.000	8.134	8.134	0.187	0.000	-5.322	5.325
7.000	0.000	0.000	-5.329	5.329	0.000	0.000	8.109	8.109	0.188	0.000	-5.306	5.309
8.000	-0.001	0.000	-5.299	5.299	0.000	0.000	8.079	8.079	0.190	0.000	-5.288	5.291
9.000	-0.001	0.000	-5.266	5.266	0.000	0.000	8.046	8.046	0.191	0.000	-5.267	5.271
10.000	-0.002	0.000	-5.228	5.228	0.000	0.000	8.008	8.008	0.192	0.000	-5.245	5.249
11.000	-0.002	0.000	-5.185	5.185	0.000	0.000	7.965	7.965	0.194	0.000	-5.221	5.224
12.000	-0.003	0.000	-5.139	5.139	0.000	0.000	7.919	7.919	0.196	0.000	-5.194	5.198
13.000	-0.005	0.000	-5.088	5.088	0.000	0.000	7.868	7.868	0.198	0.000	-5.166	5.170
14.000	-0.006	0.000	-5.032	5.032	0.000	0.000	7.812	7.812	0.200	0.000	-5.135	5.139
15.000	-0.008	0.000	-4.973	4.973	0.000	0.000	7.753	7.753	0.202	0.000	-5.103	5.107
16.000	-0.011	0.000	-4.909	4.909	0.000	0.000	7.689	7.689	0.204	0.000	-5.068	5.073
17.000	-0.013	0.000	-4.840	4.841	0.000	0.000	7.620	7.620	0.207	0.000	-5.032	5.036
18.000	-0.017	0.000	-4.768	4.768	0.000	0.000	7.548	7.548	0.210	0.000	-4.993	4.998
19.000	-0.021	0.000	-4.691	4.691	0.000	0.000	7.471	7.471	0.213	0.000	-4.953	4.957
20.000	-0.026	0.000	-4.610	4.610	0.000	0.000	7.390	7.390	0.216	0.000	-4.910	4.915
21.000	-0.031	0.000	-4.525	4.525	0.000	0.000	7.304	7.304	0.219	0.000	-4.865	4.870
22.000	-0.038	0.000	-4.435	4.435	0.000	0.000	7.214	7.214	0.223	0.000	-4.819	4.824
23.000	-0.045	0.000	-4.341	4.341	0.000	0.000	7.120	7.120	0.227	0.000	-4.770	4.775
24.000	-0.053	0.000	-4.243	4.243	0.000	0.000	7.021	7.021	0.231	0.000	-4.719	4.725
25.000	-0.063	0.000	-4.140	4.141	0.000	0.000	6.919	6.919	0.235	0.000	-4.667	4.672
26.000	-0.073	0.000	-4.033	4.034	0.000	0.000	6.811	6.811	0.239	0.000	-4.612	4.618
27.000	-0.085	0.000	-3.922	3.923	0.000	0.000	6.700	6.700	0.244	0.000	-4.555	4.562
28.000	-0.098	0.000	-3.807	3.808	0.000	0.000	6.584	6.584	0.248	0.000	-4.496	4.503
29.000	-0.113	0.000	-3.687	3.689	0.000	0.000	6.464	6.464	0.254	0.000	-4.436	4.443
30.000	-0.129	0.000	-3.563	3.566	0.000	0.000	6.339	6.339	0.259	0.000	-4.373	4.381
31.000	-0.146	0.000	-3.435	3.438	0.000	0.000	6.209	6.209	0.264	0.000	-4.309	4.317
32.000	-0.165	0.000	-3.302	3.306	0.000	0.000	6.075	6.075	0.270	0.000	-4.243	4.252
33.000	-0.187	0.000	-3.164	3.170	0.000	0.000	5.937	5.937	0.276	0.000	-4.175	4.184
34.000	-0.209	0.000	-3.022	3.030	0.000	0.000	5.793	5.793	0.282	0.000	-4.106	4.115
35.000	-0.234	0.000	-2.876	2.885	0.000	0.000	5.645	5.645	0.289	0.000	-4.035	4.045
36.000	-0.261	0.000	-2.724	2.737	0.000	0.000	5.491	5.491	0.296	0.000	-3.962	3.973
37.000	-0.290	0.000	-2.568	2.584	0.000	0.000	5.333	5.333	0.303	0.000	-3.888	3.900
38.000	-0.320	0.000	-2.407	2.428	0.000	0.000	5.170	5.170	0.310	0.000	-3.813	3.825
39.000	-0.354	0.000	-2.241	2.269	0.000	0.000	5.002	5.002	0.318	0.000	-3.736	3.749
40.000	-0.389	0.000	-2.071	2.107	0.000	0.000	4.828	4.828	0.326	0.000	-3.657	3.672

DATE: FEB. 4, 1988

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RUN DESCRIPTION: EXAMPLE 2: DYNAMIC JOINT TEST

SLIP JOINT / 600 KNOT WIND

PAGE: 22.01

VEHICLE DECELERATION: CONSTANT WIND VELOCITY OF 600 KNOTS

CRASH VICTIM: 95TH PERCENTILE MALE

## JOINT PARAMETERS

## JOINT NO. 1 - ELBW

TIME (MSEC)	STATE IPIN	JOINT ANGLES (DEG)			TOTAL TORQUE ( IN. LB.)		
		FLEXURE	AZIMUTH	TORSION	SPRING	VISCOUS	RES.
0.000	5.	67.190	180.000	0.000	0.000	0.000	0.000
0.500	5.	67.189	180.000	0.000	0.000	0.000	0.000
1.000	5.	67.186	180.000	0.000	0.000	0.000	0.000
1.500	5.	67.181	180.000	0.000	0.000	0.000	0.000
2.000	5.	67.172	180.000	0.000	0.000	0.000	0.000
3.000	5.	67.149	180.000	0.000	0.000	0.000	0.000
4.000	5.	67.116	180.000	0.000	0.000	0.000	0.000
5.000	5.	67.073	180.000	0.000	0.000	0.000	0.000
6.000	5.	67.021	180.000	0.000	0.000	0.000	0.000
7.000	5.	66.959	180.000	0.000	0.000	0.000	0.000
8.000	5.	66.888	180.000	0.000	0.000	0.000	0.000
9.000	5.	66.808	180.000	0.000	0.000	0.000	0.000
10.000	5.	66.720	180.000	0.000	0.000	0.000	0.000
11.000	5.	66.623	180.000	0.000	0.000	0.000	0.000
12.000	5.	66.517	180.000	0.000	0.000	0.000	0.000
13.000	5.	66.403	180.000	0.000	0.000	0.000	0.000
14.000	5.	66.280	180.000	0.000	0.000	0.000	0.000
15.000	5.	66.149	180.000	0.000	0.000	0.000	0.000
16.000	5.	66.010	180.000	0.000	0.000	0.000	0.000
17.000	5.	65.862	180.000	0.000	0.000	0.000	0.000
18.000	5.	65.706	180.000	0.000	0.000	0.000	0.000
19.000	5.	65.542	180.000	0.000	0.000	0.000	0.000
20.000	5.	65.369	180.000	0.000	0.000	0.000	0.000
21.000	5.	65.189	180.000	0.000	0.000	0.000	0.000
22.000	5.	65.001	180.000	0.000	0.000	0.000	0.000
23.000	5.	64.805	180.000	0.000	0.000	0.000	0.000
24.000	5.	64.601	180.000	0.000	0.000	0.000	0.000
25.000	5.	64.390	-180.000	0.000	0.000	0.000	0.000
26.000	5.	64.171	-180.000	0.000	0.000	0.000	0.000
27.000	5.	63.945	-180.000	0.000	0.000	0.000	0.000
28.000	5.	63.712	180.000	0.000	0.000	0.000	0.000
29.000	5.	63.473	180.000	0.000	0.000	0.000	0.000
30.000	5.	63.229	180.000	0.000	0.000	0.000	0.000
31.000	5.	62.978	180.000	0.000	0.000	0.000	0.000
32.000	5.	62.723	180.000	0.000	0.000	0.000	0.000
33.000	5.	62.462	180.000	0.000	0.000	0.000	0.000
34.000	5.	62.199	180.000	0.000	0.000	0.000	0.000
35.000	5.	61.932	180.000	0.000	0.000	0.000	0.000
36.000	5.	61.663	180.000	0.000	0.000	0.000	0.000
37.000	5.	61.392	180.000	0.000	0.000	0.000	0.000
38.000	5.	61.119	180.000	0.000	0.000	0.000	0.000
39.000	5.	60.844	180.000	0.000	0.000	0.000	0.000
40.000	5.	60.567	180.000	0.000	0.000	0.000	0.000

DATE: FEB. 4, 1988  
 RUN DESCRIPTION: EXAMPLE 2: DYNAMIC JOINT TEST  
 SLIP JOINT / 600 KNOT WIND  
 VEHICLE DECELERATION: CONSTANT WIND VELOCITY OF 600 KNOTS  
 CRASH VICTIM: 95TH PERCENTILE MALE

PAGE: 23.01

## SEGMENT WIND FORCE ( LB. )

TIME (MSEC)	SEGMENT NO. 1 - LARM IN GRND REFERENCE				SEGMENT NO. 2 - UARM IN GRND REFERENCE			
	X	Y	Z	RES	X	Y	Z	RES
0.000	0.000	0.000	1.885	1.885	0.000	0.000	117.585	117.585
0.500	0.000	0.000	92.335	92.335	0.000	0.000	28.783	28.783
1.000	0.000	0.000	92.288	92.288	0.000	0.000	28.768	28.768
1.500	0.000	0.000	92.242	92.242	0.000	0.000	28.752	28.752
2.000	0.000	0.000	92.198	92.198	0.000	0.000	28.735	28.735
3.000	0.000	0.000	92.112	92.112	0.000	0.000	28.702	28.702
4.000	0.000	0.000	92.032	92.032	0.000	0.000	28.667	28.667
5.000	0.000	0.000	91.958	91.958	0.000	0.000	28.632	28.632
6.000	0.000	0.000	91.888	91.888	0.000	0.000	28.595	28.595
7.000	0.000	0.000	91.824	91.824	0.000	0.000	23.798	23.798
8.000	0.000	0.000	91.766	91.766	0.000	0.000	23.765	23.765
9.000	0.000	0.000	91.713	91.713	0.000	0.000	23.733	23.733
10.000	0.000	0.000	91.666	91.666	0.000	0.000	23.699	23.699
11.000	0.000	0.000	91.624	91.624	0.000	0.000	23.666	23.666
12.000	0.000	0.000	91.589	91.589	0.000	0.000	23.632	23.632
13.000	0.000	0.000	91.560	91.560	0.000	0.000	23.597	23.597
14.000	0.000	0.000	91.538	91.538	0.000	0.000	23.563	23.563
15.000	0.000	0.000	91.523	91.523	0.000	0.000	23.529	23.529
16.000	0.000	0.000	91.515	91.515	0.000	0.000	23.494	23.494
17.000	0.000	0.000	91.515	91.515	0.000	0.000	23.460	23.460
18.000	0.000	0.000	91.524	91.524	0.000	0.000	23.427	23.427
19.000	0.000	0.000	91.541	91.541	0.000	0.000	23.394	23.394
20.000	0.000	0.000	91.567	91.567	0.000	0.000	23.361	23.361
21.000	0.000	0.000	91.602	91.602	0.000	0.000	23.330	23.330
22.000	0.000	0.000	91.648	91.648	0.000	0.000	23.299	23.299
23.000	0.000	0.000	91.704	91.704	0.000	0.000	23.269	23.269
24.000	0.000	0.000	91.772	91.772	0.000	0.000	23.240	23.240
25.000	0.000	0.000	91.852	91.852	0.000	0.000	23.213	23.213
26.000	0.000	0.000	91.944	91.944	0.000	0.000	23.187	23.187
27.000	0.000	0.000	92.050	92.050	0.000	0.000	23.162	23.162
28.000	0.000	0.000	92.169	92.169	0.000	0.000	20.825	20.825
29.000	0.000	0.000	92.303	92.303	0.000	0.000	20.806	20.806
30.000	0.000	0.000	92.452	92.452	0.000	0.000	20.789	20.789
31.000	0.000	0.000	92.616	92.616	0.000	0.000	20.773	20.773
32.000	0.000	0.000	92.798	92.798	0.000	0.000	20.759	20.759
33.000	0.000	0.000	92.996	92.996	0.000	0.000	16.136	16.136
34.000	0.000	0.000	93.211	93.211	0.000	0.000	16.127	16.127
35.000	0.000	0.000	93.444	93.444	0.000	0.000	16.120	16.120
36.000	0.000	0.000	93.695	93.695	0.000	0.000	16.113	16.113
37.000	0.000	0.000	93.966	93.966	0.000	0.000	16.108	16.108
38.000	0.000	0.000	94.257	94.257	0.000	0.000	16.103	16.103
39.000	0.000	0.000	94.569	94.569	0.000	0.000	16.100	16.100
40.000	0.000	0.000	94.903	94.903	0.000	0.000	16.097	16.097

DATE: FEB. 4, 1988

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RUN DESCRIPTION: EXAMPLE 2: DYNAMIC JOINT TEST

SLIP JOINT / 600 KNOT WIND

PAGE: 24.01

VEHICLE DECELERATION: CONSTANT WIND VELOCITY OF 600 KNOTS

CRASH VICTIM: 95TH PERCENTILE MALE

## ELBW JOINT FORCES &amp; TORQUES ON UARM IN LARM REFERENCE

TIME (MSEC)	JOINT FORCE ( LB. 10**2)			JOINT TORQUE ( IN.- LB. 10**2)		
	X	Y	Z	X	Y	Z
0.000	-0.007	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
0.500	0.022	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
1.000	0.022	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
1.500	0.022	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
2.000	0.023	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
3.000	0.023	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
4.000	0.023	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
5.000	0.023	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
6.000	0.023	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
7.000	0.022	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
8.000	0.022	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
9.000	0.022	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
10.000	0.022	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
11.000	0.023	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
12.000	0.023	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
13.000	0.023	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
14.000	0.024	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
15.000	0.024	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
16.000	0.025	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
17.000	0.025	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
18.000	0.026	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
19.000	0.027	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
20.000	0.027	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
21.000	0.028	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
22.000	0.029	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
23.000	0.030	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
24.000	0.030	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
25.000	0.031	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
26.000	0.033	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
27.000	0.034	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
28.000	0.032	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
29.000	0.034	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
30.000	0.035	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
31.000	0.036	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
32.000	0.038	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
33.000	0.034	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
34.000	0.036	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
35.000	0.038	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
36.000	0.040	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
37.000	0.042	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
38.000	0.044	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
39.000	0.046	0.000	0.000	0.000E+00	0.000E+00	0.000E+00
40.000	0.048	0.000	0.000	0.000E+00	0.000E+00	0.000E+00

ELAPSED CPU TIME = 13.51 SECONDS

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SUB	CALLS	TIME	%
MAIN3D	1	97	7.18
INPUT	1	49	3.63
CHAIN	170	18	1.33
EJOINT	170	0	0.00
DINT	21	77	5.70
PDAUX	211	71	5.26
DAUX	169	47	3.48
SETUP1	169	17	1.26
CONTC	169	17	1.26
WINDY	338	684	50.63
VISPR	169	22	1.63
SETUP2	169	0	0.00
DAUX11	169	12	0.89
DAUX12	169	6	0.44
DAUX22	169	0	0.00
FSMSOL	169	11	0.81
OUTPUT	43	90	6.66
UPDATE	42	0	0.00
DZP	168	28	2.07
POSTPR	1	105	7.77
TOTAL		1351	100.00

APPENDIX D4

Example 2, ATB Dynamic Joint Test  
Perkin-Elmer Output File

DEVELOPED BY CALSPAN CORP., P.O. BOX 400, BUFFALO NY 14225  
AND BY J&J TECHNOLOGIES INC., ORCHARD PARK, NY 14127

FOR THE AIR FORCE ARMSTRONG AEROSPACE MEDICAL RESEARCH  
LABORATORY, WRIGHT PATTERSON AIR FORCE BASE  
UNDER CONTRACTS F33615-75C-5002, -78C-0516 AND -80C-05117

AND FOR THE NATIONAL HIGHWAY TRAFFIC SAFETY ADMINISTRATION,  
U.S. DEPARTMENT OF TRANSPORTATION, UNDER CONTRACTS  
FH-11-7592, HS-053-2-485, HS-6-01300 AND HS-6-01410.

PROGRAM DOCUMENTATION: NHTSA REPORT NOS. DOT-HS-801-507  
THROUGH 510 (FORMERLY CALSPAN REPORT NO. 20-5730-L-1),  
AVAILABLE FROM NTIS (ACCESSION NOS. PB-241692, 3, 4 AND 5),  
APPENDIXES A-J TO THE ABOVE (AVAILABLE FROM CALSPAN),  
AND REPORT NOS. AMRL-TR-75-14 (NTIS NO. AD-A014 816),  
AFAMRL-TR-80-14 (NTIS NO. AD-A088 029), AND  
AFAMRL-TR-83-073 (NTIS NO. AD-B079 184).

PROGRAM ATB-IV, EXECUTED ON THE AAMRL/BB CONCURRENT  
3250 COMPUTER, WRIGHT-PATTERSON AFB, OHIO

FEB. 4, 1988 IRSIN= 0 IRSOUT= 0 RSTIME = 0.0000

CARDS A

EXAMPLE 2: DYNAMIC JOINT TEST  
SLIP JOINT / 600 KNOT WIND

UNITL = IN. UNITM = LB. UNITT = SEC. GRAVITY VECTOR = ( 0.0000, 0.0000, 386.0880) G = 386.0880  
NDINT = 4 NSTEPS = 20 DT = 0.002000 HO = 0.000500 HMAX = 0.001000 HMIN = 0.000063

NPRT ARRAY

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36
1	0	20	2	0	0	0	0	0	0	0	0	0	0	0	0	0	16	0	0	0	0	0	0	0	1	0	0	0	1	0	0	0	0	0	1



SEGMENT I SYM PLOT	WEIGHT ( LB.)	PRINCIPAL MOMENTS OF INERTIA ( LB.-SEC.**2- IN.)			SEGMENT CONTACT ELLIPSOID						PRINCIPAL AXES (DEG)		
					SEMIAXES ( IN.)			CENTER ( IN.)					
		X	Y	Z	X	Y	Z	X	Y	Z	YAW	PITCH	ROLL
1 LARM L	5.901	0.3331	0.3331	0.0214	1.871	1.871	10.269	0.000	0.000	0.000	0.00	0.00	0.00
2 UARM U	5.542	0.1743	0.1743	0.0259	2.122	2.122	7.497	0.000	0.000	0.000	0.00	0.00	0.00

## CARDS B.3

JOINT J SYM PLOT JNT PIN	LOCATION( IN.) - SEG(JNT)			LOCATION( IN.) - SEG(J+1)			PRIN. AXIS(DEG) - SEG(JNT)			PRIN. AXIS(DEG) - SEG(J+1)		
	X	Y	Z	X	Y	Z	YAW	PITCH	ROLL	YAW	PITCH	ROLL
1 ELBW E 1 5	0.000	0.000	8.200	0.000	0.000	-5.420	0.00	0.00	0.00	0.00	-67.19	0.00

## UNLOCK CONDITIONS FOR SLIP JOINTS

JOINT	TENSION ( LB.)	COMPRESSION ( LB.)
-------	-------------------	-----------------------

1	0.000	0.000
---	-------	-------

## FLEXURAL SPRING CHARACTERISTICS

## TORSIONAL SPRING CHARACTERISTICS

JOINT	SPRING COEF. ( IN. LB./DEG**J)				JOINT STOP (DEG)	SPRING COEF. ( IN. LB./DEG**J)				JOINT STOP (DEG)
	LINEAR (J=1)	QUADRATIC (J=2)	CUBIC (J=3)	ENERGY DISSIPATION COEF.		LINEAR (J=1)	QUADRATIC (J=2)	CUBIC (J=3)	ENERGY DISSIPATION COEF.	
1 ELBW	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

CARDS 8.5

## JOINT VISCOUS CHARACTERISTICS AND LOCK-UNLOCK CONDITIONS

JOINT	VISCOUS		COULOMB		FULL FRICTION		MAX TORQUE FOR A LOCKED JOINT ( IN. LB.)	MIN TORQUE FOR UNLOCKED JOINT ( IN. LB.)	MIN. ANG. VELOCITY FOR UNLOCKED JOINT (RAD/SEC.)	IMPULSE RESTITUTION COEFFICIENT
	COEFFICIENT ( IN. LB.SEC./DEG)		FRICTION COEF. ( IN. LB.)		ANGULAR VELOCITY (DEG/SEC.)					
1 ELBW	0.000		0.00		30.00		0.00	0.00	0.00	0.000

SEGMENT INTEGRATION CONVERGENCE TEST INPUT

PAGE 4  
CARDS B.6

SEGMENT NO. SYM	ANGULAR VELOCITIES (RAD/SEC.)			LINEAR VELOCITIES ( IN./SEC.)			ANGULAR ACCELERATIONS (RAD/SEC.**2)			LINEAR ACCELERATIONS ( IN./SEC.**2)		
	MAG. TEST	ABS. ERROR	REL. ERROR	MAG. TEST	ABS. ERROR	REL. ERROR	MAG. TEST	ABS. ERROR	REL. ERROR	MAG. TEST	ABS. ERROR	REL. ERROR
1 LARM	0.000	0.000	0.0000	0.000	0.000	0.0000	0.010	0.010	0.0010	0.001	0.001	0.0010
2 UARM	0.000	0.000	0.0000	0.000	0.000	0.0000	0.010	0.010	0.0010	0.000	0.000	0.0000

## VEHICLE DECELERATION INPUTS

PAGE 5  
CARDS C

CONSTANT WIND VELOCITY OF 600 KNOTS

YAW	PITCH	ROLL	VIPS	VTIME	XO(X)	XO(Y)	XO(Z)	NATAB	ATO	ADT	MSEG
0.000	0.000	0.000	12161.000	0.000	0.000	0.000	0.000	-3	0.000000	2.300000	0

## SPLINE FIT TABULAR INPUT

LTYPE = 2 LFIT = 1 NPTS = 3

INITIAL LINEAR POSITION ( IN.)					INITIAL ANGULAR POSITION (DEG)								
TIME(SEC.)=	0.0000	X=	0.000	Y=	0.000	Z=	0.000	X=	0.000	Y=	0.000	Z=	0.000

TIME(SEC.)	LINEAR VELOCITY ( IN./SEC.)			ANGULAR VELOCITY (DEG/SEC.)		
	X	Y	Z	X	Y	Z
0.00000	0.000	0.000	12161.000	0.000	0.000	0.000
2.30000	0.000	0.000	12161.000	0.000	0.000	0.000
4.60000	0.000	0.000	12161.000	0.000	0.000	0.000

## VEHICLE LINEAR TIME HISTORY CONSTANT WIND VELOCITY OF 600 KNOTS

PAGE NO. 1

TIME (MSEC)	LINEAR DECELERATIONS (G'S)			LINEAR VELOCITIES ( IN./SEC.)			LINEAR DISPLACEMENTS ( IN.)		
	X	Y	Z	X	Y	Z	X	Y	Z
0.000	0.000	0.000	0.000	0.000	0.000	12161.000	0.000	0.000	0.000
2300.000	0.000	0.000	0.000	0.000	0.000	12161.000	0.000	0.000	27970.300
4600.000	0.000	0.000	0.000	0.000	0.000	12161.000	0.000	0.000	55940.600

[illegible]

NPL NBLT NBAG NPLP NQ NSD NHRNSS NWINDF NJNTF NFORCE  
1 0 0 0 0 0 0 1 0 0

PAGE 8  
CARD D.1

PLANE INPUTS

CARDS D.2

PLANE NO. 1 WIND PLANE

	X	Y	Z
POINT 1	10.0000	10.0000	5.0000
POINT 2	-10.0000	10.0000	5.0000
POINT 3	10.0000	-10.0000	5.0000

BODY SEGMENT SYMMETRY INPUT

CARD D.7

SEG NO. 1 2

NSYM(J) 0 0

WIND FORCE FUNCTION NO. 1 WIND FORCE

NTI( 1) = 1

PAGE 9  
CARDS E.6

SPEC. HEAT RATIO  
1.4000

SONIC VEL.  
13404.0000

ABS. PRESS.  
14.6960

SECMENT  
1LARM

REF. SEGMENT  
3VEH





# SEGMENT WIND FORCES

PAGE 11  
CARDS F.7

SEGMENT-ELLIPSOID	SEGMENT-PLANE	WIND FORCE FUNCTION	DRAG COEFFICIENT FUNCTION	BLOCKING SEGMENTS-ELLIPSOID
-1 - 1 LARM	3 - 1 VEH -WIND PLANE	1 WIND FORCE	0	2- 2
-2 - 2 UARM	3 - 1 VEH -WIND PLANE	1 WIND FORCE	0	1- 1

ZPLT(X)	ZPLT(Y)	ZPLT(Z)	I1	J1	I2	J2	I3	SPLT(1)	SPLT(2)	SPLT(3)
0.	0.	0.	0	0	0	0	1	10.00	6.00	1.00

## INITIAL POSITIONS (INERTIAL REFERENCE)

CARDS G.2

SEGMENT NO. SEG	LINEAR POSITION ( IN.)			LINEAR VELOCITY ( IN./SEC.)		
	X	Y	Z	X	Y	Z
1 LARM	0.66000	0.00000	-18.98000	0.00000	0.00000	0.00000
2 UARM	0.18467	0.00000	-5.36830	0.00000	0.00000	0.00000

## INITIAL ANGULAR ROTATION AND VELOCITY

CARDS G.3

SEGMENT NO. SEG	ANGULAR ROTATION (DEG)			ANGULAR VELOCITY (DEG/SEC.)			IYPR
	YAW	PITCH	ROLL	X	Y	Z	
1 LARM	0.00000	-2.00000	0.00000	0.00000	0.00000	0.00000	3 2 1 0
2 UARM	0.00000	-2.00000	0.00000	0.00000	0.00000	0.00000	3 2 1 0

## TABULAR TIME HISTORY CONTROL PARAMETERS

TYPE	KSG	SELECTED SEGMENTS OR JOINTS
------	-----	-----------------------------

H.1 0

REF

H.2 0

REF

H.3 3 1 2 2

REF 2 1 4

H.4 0

REF

H.5 0

REF

H.6 0

REF

H.7 1 1

REF 0

H.8 2 1 2

REF 0 0

H.9 1 1

REF 1

SEGMENT	(INERTIAL) ANGULAR ROTATION (DEG)			(LOCAL) ANGULAR VELOCITY (RAD/SEC.)			(LOCAL) ANGULAR ACCELERATION (RAD/SEC.**2)		
	YAW	PITCH	ROLL	X	Y	Z	X	Y	Z
1 LARM	0.0000	-2.0000	0.0000	0.00000	0.00000	0.00000	0.000348	7.240952	-0.000315
2 UARM	0.0000	-2.0000	0.0000	0.00000	0.00000	0.00000	-0.000292	22.756331	0.000000
3 VEH	0.0000	0.0000	0.0000	0.00000	0.00000	0.00000	0.000000	0.000000	0.000000

SEGMENT	(INERTIAL) LINEAR POSITION ( IN.)			(INERTIAL) LINEAR VELOCITY ( IN./SEC.)			(INERTIAL) LINEAR ACCELERATIONS (G'S)		
	X	Y	Z	X	Y	Z	X	Y	Z
1 LARM	0.6600	0.0000	-18.9800	0.00000	0.00000	0.00000	0.123940	0.000002	1.323803
2 UARM	0.1847	0.0000	-5.3683	0.00000	0.00000	0.00000	-0.131968	-0.000002	22.212334
3 VEH	0.0000	0.0000	0.0000	0.00000	0.00000	12161.00000	0.000000	0.000000	0.000000

SEGMENT	(INERTIAL) U1 ARRAY ( IN./SEC.**2) EXTERNAL LINEAR ACCELERATIONS			(LOCAL) U2 ARRAY (RAD/SEC.**2) EXTERNAL ANGULAR ACCELERATIONS			KINETIC ENERGY ( LB.- IN.)		
	X	Y	Z	X	Y	Z	LINEAR	ANGULAR	TOTAL
1 LARM	0.00000+00	0.00000+00	0.50940+03	0.57981D-03	-0.10774D+02	-0.31516D-03	0.000000+00	0.000000+00	0.000000+00
2 UARM	0.00000+00	0.00000+00	0.85780+04	-0.11465D-13	-0.38367D-14	-0.32149D-14	0.000000+00	0.000000+00	0.000000+00
TOTAL BODY KINETIC ENERGY							0.000000+00	0.000000+00	0.000000+00

JOINT	IPIN	(INERTIAL) JOINT FORCES ( LB.)			(INERTIAL) JOINT TORQUES ( IN. LB.)			RELATIVE ANGULAR VELOCITY (RAD/SEC.)		
		X	Y	Z	X	Y	Z			
1 ELBW	5	-0.731D+00	-0.941D-05	-0.255D-01	0.00000+00	0.00000+00	0.00000+00	0.000		
DINT CONV. TEST		1.000	LARM	ANG ACC	3064.	0.4514E-02	0.1473E-05	0.1000E-03	0.1000E-03	0.1000E-05

TEST FAILED AT TIME = 0.001000 FOR H = 0.000500

SEGMENT	(INERTIAL)			(LOCAL)			(LOCAL)		
	ANGULAR ROTATION (DEG)			ANGULAR VELOCITY (RAD/SEC.)			ANGULAR ACCELERATION (RAD/SEC.**2)		
	YAW	PITCH	ROLL	X	Y	Z	X	Y	Z
1 LARM	0.0000	-4.6312	-0.0023	-0.00364	-2.40686	0.00000	-0.105497	-69.644370	0.000000
2 UARM	0.0000	1.9884	0.0050	0.05666	2.42783	-0.00004	0.012320	-49.752471	-0.000001
3 VEH	0.0000	0.0000	0.0000	0.00000	0.00000	0.00000	0.000000	0.000000	0.000000

SEGMENT	(INERTIAL)			(INERTIAL)			(INERTIAL)		
	LINEAR POSITION ( IN.)			LINEAR VELOCITY ( IN./SEC.)			LINEAR ACCELERATIONS (G'S)		
	X	Y	Z	X	Y	Z	X	Y	Z
1 LARM	0.5275	0.0001	-13.8864	-7.63222	0.01244	255.94443	-0.811510	0.001280	17.016222
2 UARM	0.3257	-0.0001	-3.6569	8.12663	-0.01319	79.35888	0.864086	-0.001363	3.974519
3 VEH	0.0000	0.0000	486.4400	0.00000	0.00000	12161.00000	0.000000	0.000000	0.000000

SEGMENT	(INERTIAL)			(LOCAL)			KINETIC ENERGY		
	U1 ARRAY ( IN./SEC.**2)			U2 ARRAY (RAD/SEC.**2)			( LB.- IN.)		
	EXTERNAL LINEAR ACCELERATIONS			EXTERNAL ANGULAR ACCELERATIONS			LINEAR	ANGULAR	TOTAL
1 LARM	0.25520-02	-0.67750-08	0.65950+04	0.591660-07	-0.894470-10	0.110240-13	0.501060+03	0.964830+00	0.502020+03
2 UARM	0.46090-03	-0.12240-08	0.15070+04	0.245770+00	0.986500+02	-0.883560-06	0.456740+02	0.513700+00	0.461880+02
							TOTAL BODY KINETIC ENERGY		
							0.546730+03	0.147850+01	0.548210+03

		(INERTIAL)			(INERTIAL)			
		JOINT FORCES ( LB.)			JOINT TORQUES ( IN. LB.)			RELATIVE ANGULAR
JOINT	IPIN	X	Y	Z	X	Y	Z	VELOCITY (RAD/SEC.)
1 ELBW	5	0.4790+01	-0.7550-02	0.3880+00	0.00000+00	0.00000+00	0.00000+00	4.835

## POSTPROCESSOR CONTROL PARAMETERS

	NIC & NSI POINT	CSI POINT
N.11	0	0

DATE: FEB. 4, 1988  
 RUN DESCRIPTION: EXAMPLE 2: DYNAMIC JOINT TEST  
 SLIP JOINT / 600 KNOT WIND  
 VEHICLE DECELERATION: CONSTANT WIND VELOCITY OF 600 KNOTS  
 CRASH VICTIM: 95TH PERCENTILE MALE

PAGE: 21.01

## POINT REL. LINEAR DISPLACEMENT ( IN. )

TIME (MSEC)	POINT ( 0.00, 0.00, 8.20) ON SEGMENT NO. 1 - LARM IN UARM REFERENCE				POINT ( 0.00, 0.00, -5.42) ON SEGMENT NO. 2 - UARM IN LARM REFERENCE				POINT ( 0.00, 0.00, 0.00) ON SEGMENT NO. 2 - UARM IN GRND REFERENCE			
	X	Y	Z	RES	X	Y	Z	RES	X	Y	Z	RES
0.000	0.000	0.000	-5.420	5.420	0.000	0.000	8.200	8.200	0.185	0.000	-5.368	5.371
0.500	0.000	0.000	-5.420	5.420	0.000	0.000	8.200	8.200	0.185	0.000	-5.368	5.371
0.750	0.000	0.000	-5.420	5.420	0.000	0.000	8.200	8.200	0.185	0.000	-5.367	5.370
1.000	0.000	0.000	-5.419	5.419	0.000	0.000	8.199	8.199	0.185	0.000	-5.366	5.370
1.500	0.000	0.000	-5.417	5.417	0.000	0.000	8.197	8.197	0.185	0.000	-5.365	5.368
2.000	0.000	0.000	-5.414	5.414	0.000	0.000	8.194	8.194	0.185	0.000	-5.362	5.366
3.000	0.000	0.000	-5.405	5.405	0.000	0.000	8.185	8.185	0.185	0.000	-5.356	5.359
4.000	0.000	0.000	-5.392	5.392	0.000	0.000	8.172	8.172	0.186	0.000	-5.347	5.350
5.000	0.000	0.000	-5.375	5.375	0.000	0.000	8.155	8.155	0.187	0.000	-5.336	5.339
6.000	0.000	0.000	-5.354	5.354	0.000	0.000	8.134	8.134	0.187	0.000	-5.322	5.325
7.000	0.000	0.000	-5.329	5.329	0.000	0.200	8.109	8.109	0.188	0.000	-5.306	5.309
8.000	-0.001	0.000	-5.299	5.299	0.000	0.000	8.079	8.079	0.190	0.000	-5.288	5.291
9.000	-0.001	0.000	-5.266	5.266	0.000	0.000	8.046	8.046	0.191	0.000	-5.268	5.271
10.000	-0.002	0.000	-5.228	5.228	0.000	0.000	8.008	8.008	0.192	0.000	-5.245	5.249
11.000	-0.002	0.000	-5.185	5.185	0.000	0.000	7.965	7.965	0.194	0.000	-5.221	5.224
12.000	-0.003	0.000	-5.138	5.138	0.000	0.000	7.918	7.918	0.196	0.000	-5.194	5.198
13.000	-0.005	0.000	-5.087	5.087	0.000	0.000	7.867	7.867	0.198	0.000	-5.166	5.170
14.000	-0.006	0.000	-5.032	5.032	0.000	0.000	7.812	7.812	0.200	0.000	-5.136	5.139
15.000	-0.008	0.000	-4.973	4.973	0.000	0.000	7.752	7.752	0.202	0.000	-5.103	5.107
16.000	-0.011	0.000	-4.909	4.909	0.000	0.000	7.688	7.688	0.204	0.000	-5.069	5.073
17.000	-0.013	0.000	-4.840	4.840	0.000	0.000	7.620	7.620	0.207	0.000	-5.032	5.036
18.000	-0.017	0.000	-4.768	4.768	0.000	0.000	7.548	7.548	0.210	0.000	-4.993	4.998
19.000	-0.021	0.000	-4.691	4.691	0.000	0.000	7.471	7.471	0.213	0.000	-4.953	4.957
20.000	-0.026	0.000	-4.610	4.610	0.000	0.000	7.389	7.389	0.216	0.000	-4.910	4.915
21.000	-0.031	0.000	-4.524	4.524	0.000	0.000	7.304	7.304	0.219	0.000	-4.865	4.870
22.000	-0.038	0.000	-4.435	4.435	0.000	0.000	7.214	7.214	0.223	0.000	-4.819	4.824
23.000	-0.045	0.000	-4.341	4.341	0.000	0.000	7.120	7.120	0.227	0.000	-4.770	4.775
24.000	-0.053	0.000	-4.242	4.243	0.000	0.000	7.021	7.021	0.231	0.000	-4.719	4.725
25.000	-0.063	0.000	-4.140	4.140	0.000	0.000	6.918	6.918	0.235	0.000	-4.667	4.673
26.000	-0.073	0.000	-4.033	4.034	0.000	0.000	6.811	6.811	0.239	0.000	-4.612	4.618
27.000	-0.085	0.000	-3.922	3.923	0.000	0.000	6.700	6.700	0.244	0.000	-4.555	4.562
28.000	-0.098	0.000	-3.807	3.808	0.000	0.000	6.584	6.584	0.248	0.000	-4.496	4.503
29.000	-0.113	0.000	-3.687	3.689	0.000	0.000	6.464	6.464	0.254	0.000	-4.436	4.443
30.000	-0.129	0.000	-3.563	3.565	0.000	0.000	6.339	6.339	0.259	0.000	-4.373	4.381
31.000	-0.146	0.000	-3.435	3.438	0.000	0.000	6.209	6.209	0.264	0.000	-4.309	4.317
32.000	-0.165	0.000	-3.302	3.306	0.000	0.000	6.075	6.075	0.270	0.000	-4.243	4.251
33.000	-0.186	0.000	-3.164	3.170	0.000	0.000	5.937	5.937	0.276	0.000	-4.175	4.184
34.000	-0.209	0.000	-3.022	3.030	0.000	0.000	5.793	5.793	0.282	0.000	-4.105	4.115
35.000	-0.234	0.000	-2.876	2.885	0.000	0.000	5.645	5.645	0.289	0.000	-4.035	4.045
36.000	-0.261	0.000	-2.724	2.737	0.000	0.000	5.492	5.492	0.296	0.000	-3.962	3.973
37.000	-0.289	0.000	-2.568	2.584	0.000	0.000	5.333	5.333	0.303	0.000	-3.888	3.900
38.000	-0.320	0.000	-2.407	2.428	0.000	0.000	5.170	5.170	0.310	0.000	-3.813	3.825
39.000	-0.353	0.000	-2.241	2.269	0.000	0.000	5.002	5.002	0.318	0.000	-3.735	3.749
40.000	-0.389	0.000	-2.071	2.107	0.000	0.000	4.829	4.829	0.326	0.000	-3.657	3.671

DATE: FEB. 4, 1988  
 RUN DESCRIPTION: EXAMPLE 2: DYNAMIC JOINT TEST  
 SLIP JOINT / 600 KNOT WIND  
 VEHICLE DECELERATION: CONSTANT WIND VELOCITY OF 600 KNOTS  
 CRASH VICTIM: 95TH PERCENTILE MALE

PAGE: 22.01

## JOINT PARAMETERS

JOINT NO. 1 - EL6V

TIME (MSEC)	STATE IPIN	JOINT ANGLES (DEG)			TOTAL TORQUE ( IN. LB.)		
		FLEXURE	AZIMUTH	TORSION	SPRING	VISCOUS	RES.
0.000	5.	67.190	180.000	0.000	0.000	0.000	0.000
0.500	5.	67.189	180.000	0.000	0.000	0.000	0.000
0.750	5.	67.188	-180.000	0.000	0.000	0.000	0.000
1.000	5.	67.186	-180.000	0.000	0.000	0.000	0.000
1.500	5.	67.180	-180.000	0.000	0.000	0.000	0.000
2.000	5.	67.172	-180.000	0.000	0.000	0.000	0.000
3.000	5.	67.149	-180.000	0.000	0.000	0.000	0.000
4.000	5.	67.116	-180.000	0.000	0.000	0.000	0.000
5.000	5.	67.073	-180.000	0.000	0.000	0.000	0.000
6.000	5.	67.021	-180.000	0.000	0.000	0.000	0.000
7.000	5.	66.959	-180.000	0.000	0.000	0.000	0.000
8.000	5.	66.888	-180.000	0.000	0.000	0.000	0.000
9.000	5.	66.808	-180.000	0.000	0.000	0.000	0.000
10.000	5.	66.720	-180.000	0.000	0.000	0.000	0.000
11.000	5.	66.623	-180.000	0.000	0.000	0.000	0.000
12.000	5.	66.517	-180.000	0.000	0.000	0.000	0.000
13.000	5.	66.403	-180.000	0.000	0.000	0.000	0.000
14.000	5.	66.280	-180.000	0.000	0.000	0.000	0.000
15.000	5.	66.149	-180.000	0.000	0.000	0.000	0.000
16.000	5.	66.010	-180.000	0.000	0.000	0.000	0.000
17.000	5.	65.862	-180.000	0.000	0.000	0.000	0.000
18.000	5.	65.706	-180.000	0.000	0.000	0.000	0.000
19.000	5.	65.542	-180.000	0.000	0.000	0.000	0.000
20.000	5.	65.369	-180.000	0.000	0.000	0.000	0.000
21.000	5.	65.189	-180.000	0.000	0.000	0.000	0.000
22.000	5.	65.001	-180.000	0.000	0.000	0.000	0.000
23.000	5.	64.805	-180.000	0.000	0.000	0.000	0.000
24.000	5.	64.601	-180.000	0.000	0.000	0.000	0.000
25.000	5.	64.390	-180.000	0.000	0.000	0.000	0.000
26.000	5.	64.171	-180.000	0.000	0.000	0.000	0.000
27.000	5.	63.945	-180.000	0.000	0.000	0.000	0.000
28.000	5.	63.713	-180.000	-0.001	0.000	0.000	0.000
29.000	5.	63.474	-179.999	-0.001	0.000	0.000	0.000
30.000	5.	63.230	-179.999	-0.001	0.000	0.000	0.000
31.000	5.	62.980	-179.999	-0.002	0.000	0.000	0.000
32.000	5.	62.724	-179.999	-0.002	0.000	0.000	0.000
33.000	5.	62.464	-179.998	-0.002	0.000	0.000	0.000
34.000	5.	62.200	-179.998	-0.003	0.000	0.000	0.000
35.000	5.	61.934	-179.998	-0.003	0.000	0.000	0.000
36.000	5.	61.666	-179.998	-0.003	0.000	0.000	0.000
37.000	5.	61.395	-179.997	-0.004	0.000	0.000	0.000
38.000	5.	61.122	-179.997	-0.004	0.000	0.000	0.000
39.000	5.	60.847	-179.997	-0.004	0.000	0.000	0.000
40.000	5.	60.570	-179.996	-0.005	0.000	0.000	0.000



DATE: FEB. 4, 1988  
 RUN DESCRIPTION: EXAMPLE 2: DYNAMIC JOINT TEST  
 SLIP JOINT / 600 KNOT WIND  
 VEHICLE DECELERATION: CONSTANT WIND VELOCITY OF 600 KNOTS  
 CRASH VICTIM: 95TH PERCENTILE MALE

PAGE: 23.01

## SEGMENT WIND FORCE ( LB. )

TIME (MSEC)	SEGMENT NO. 1 - LARM				SEGMENT NO. 2 - UARM			
	IN GRND REFERENCE				IN GRND REFERENCE			
	X	Y	Z	RES	X	Y	Z	RES
0.000	0.000	0.000	1.885	1.885	0.000	0.000	117.584	117.584
0.500	0.000	0.000	92.336	92.336	0.000	0.000	28.783	28.783
0.750	0.000	0.000	92.311	92.311	0.000	0.000	28.775	28.775
1.000	0.000	0.000	92.288	92.288	0.000	0.000	28.768	28.768
1.500	0.000	0.000	92.242	92.242	0.000	0.000	28.752	28.752
2.000	0.000	0.000	92.198	92.198	0.000	0.000	28.735	28.735
3.000	0.000	0.000	92.112	92.112	0.000	0.000	28.702	28.702
4.000	0.000	0.000	92.032	92.032	0.000	0.000	28.667	28.667
5.000	0.000	0.000	91.958	91.958	0.000	0.000	28.632	28.632
6.000	0.000	0.000	91.888	91.888	0.000	0.000	28.595	28.595
7.000	0.000	0.000	91.825	91.825	0.000	0.000	23.798	23.798
8.000	0.000	0.000	91.766	91.766	0.000	0.000	23.765	23.765
9.000	0.000	0.000	91.713	91.713	0.000	0.000	23.733	23.733
10.000	0.000	0.000	91.666	91.666	0.000	0.000	23.699	23.699
11.000	0.000	0.000	91.624	91.624	0.000	0.000	23.666	23.666
12.000	0.000	0.000	91.589	91.589	0.000	0.000	23.632	23.632
13.000	0.000	0.000	91.560	91.560	0.000	0.000	23.597	23.597
14.000	0.000	0.000	91.538	91.538	0.000	0.000	23.563	23.563
15.000	0.000	0.000	91.523	91.523	0.000	0.000	23.529	23.529
16.000	0.000	0.000	91.516	91.516	0.000	0.000	23.494	23.494
17.000	0.000	0.000	91.516	91.516	0.000	0.000	23.460	23.460
18.000	0.000	0.000	91.524	91.524	0.000	0.000	23.427	23.427
19.000	0.000	0.000	91.541	91.541	0.000	0.000	23.394	23.394
20.000	0.000	0.000	91.567	91.567	0.000	0.000	23.361	23.361
21.000	0.000	0.000	91.602	91.602	0.000	0.000	23.330	23.330
22.000	0.000	0.000	91.648	91.648	0.000	0.000	23.299	23.299
23.000	0.000	0.000	91.704	91.704	0.000	0.000	23.269	23.269
24.000	0.000	0.000	91.772	91.772	0.000	0.000	23.240	23.240
25.000	0.000	0.000	91.852	91.852	0.000	0.000	23.213	23.213
26.000	0.000	0.000	91.944	91.944	0.000	0.000	23.187	23.187
27.000	0.000	0.000	92.050	92.050	0.000	0.000	23.162	23.162
28.000	0.000	0.000	92.169	92.169	0.000	0.000	20.825	20.825
29.000	0.000	0.000	92.303	92.303	0.000	0.000	20.806	20.806
30.000	0.000	0.000	92.451	92.451	0.000	0.000	20.789	20.789
31.000	0.000	0.000	92.615	92.615	0.000	0.000	20.773	20.773
32.000	0.000	0.000	92.796	92.796	0.000	0.000	20.758	20.758
33.000	0.000	0.000	92.994	92.994	0.000	0.000	16.136	16.136
34.000	0.000	0.000	93.209	93.209	0.000	0.000	16.127	16.127
35.000	0.000	0.000	93.442	93.442	0.000	0.000	16.119	16.119
36.000	0.000	0.000	93.693	93.693	0.000	0.000	16.113	16.113
37.000	0.000	0.000	93.963	93.963	0.000	0.000	16.108	16.108
38.000	0.000	0.000	94.254	94.254	0.000	0.000	16.103	16.103
39.000	0.000	0.000	94.566	94.566	0.000	0.000	16.100	16.100
40.000	0.000	0.000	94.900	94.900	0.000	0.000	16.097	16.097

DATE: FEB. 4, 1988  
 RUN DESCRIPTION: EXAMPLE 2: DYNAMIC JOINT TEST  
 SLIP JOINT ' 600 KNOT WIND  
 VEHICLE DECELERATION: CONSTANT WIND VELOCITY OF 600 KNOTS  
 CRASH VICTIM: 95TH PERCENTILE MALE

PAGE: 24.01

## ELBW JOINT FORCES &amp; TORQUES ON UARM IN LARM REFERENCE

TIME (MSEC)	JOINT FORCE ( LB. 10**2)			JOINT TORQUE ( IN.- LB. 10**2)		
	X	Y	Z	X	Y	Z
0.000	-0.007	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
0.500	0.022	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
0.750	0.022	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
1.000	0.022	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
1.500	0.022	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
2.000	0.023	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
3.000	0.023	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
4.000	0.023	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
5.000	0.023	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
6.000	0.023	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
7.000	0.022	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
8.000	0.022	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
9.000	0.022	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
10.000	0.022	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
11.000	0.023	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
12.000	0.023	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
13.000	0.023	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
14.000	0.024	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
15.000	0.024	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
16.000	0.025	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
17.000	0.025	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
18.000	0.026	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
19.000	0.027	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
20.000	0.027	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
21.000	0.028	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
22.000	0.029	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
23.000	0.030	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
24.000	0.030	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
25.000	0.031	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
26.000	0.032	-0.002	0.000	0.0000+00	0.0000+00	0.0000+00
27.000	0.034	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
28.000	0.032	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
29.000	0.034	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
30.000	0.035	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
31.000	0.036	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
32.000	0.038	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
33.000	0.034	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
34.000	0.036	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
35.000	0.038	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
36.000	0.040	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
37.000	0.041	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
38.000	0.044	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
39.000	0.046	0.000	0.000	0.0000+00	0.0000+00	0.0000+00
40.000	0.048	0.000	0.000	0.0000+00	0.0000+00	0.0000+00

SUB	CALLS	TIME	%
MAIN30	1	47	1.52
INPUT	1	44	1.42
CHAIN	192	37	1.20
EJOINT	192	3	0.10
DINT	21	143	4.63
PDAUX	234	123	3.98
DAUX	191	86	2.78
SETUP1	191	46	1.49
CONTC	191	22	0.71
WINDY	382	2109	68.23
VISPR	191	72	2.33
SETUP2	191	6	0.19
DAUX11	191	31	1.00
DAUX12	191	1	0.03
DAUX22	191	9	0.29
FSMSOL	191	22	0.71
OUTPUT	44	79	2.56
UPDATE	43	3	0.10
D2P	190	42	1.36
POSTPR	1	166	5.37
TOTAL		3091	100.00

## APPENDIX E1

Example 2, ATB Dynamic Joint Test  
Input File with Plotting Options (EX2PLOT.AIN)

**CARD A1A**

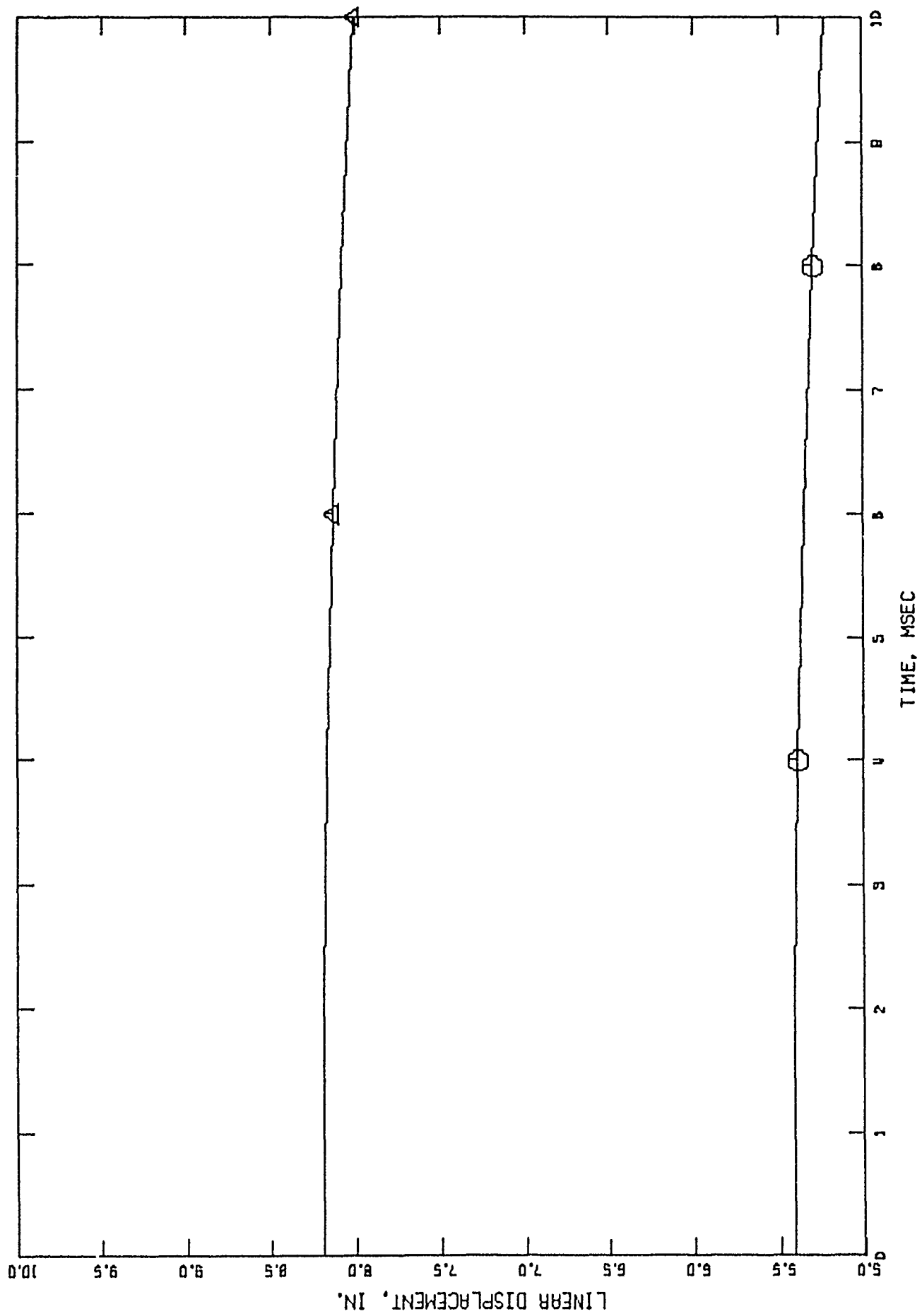
**CARD A1A**

**CARD A1A**

**CARD A1A**

## APPENDIX E2

Example 2, ATB Dynamic Joint Test X-Y Plot



UPPER ARM AND LOWER ARM  
SEGMENTS 1 AND 2

### APPENDIX E3

Example 2, ATB Dynamic Joint Test Printer Plot



T= 0.000 Y0= 0.00000 Z0= 0.00000 Y-Z PLANE

T= 0.000 X0= 0.00000 Z0= 0.00000 X-Z PLANE

T= 0.000 X0= 0.00000 Y0= 0.00000 X-Y PLANE

.....

T= 2.000 X0= 0.00000 Z0= 24.32200 X-Z PLANE

L

T= 2.000 X0= 0.00000 Y0= 0.00000 X-Y PLANE

## APPENDIX F1

Example 1, VIEW -- Input File (EXP1.VIN)

2.0	3.0						
0.0	1000.0	-20.0	0.0	0.0	-20.0	16	2
0.00	9.00						



## APPENDIX F2

Example 1, VIEW -- 386 Output Listing (EXPl.VOU)

[illegible]

4	110.00
---	--------

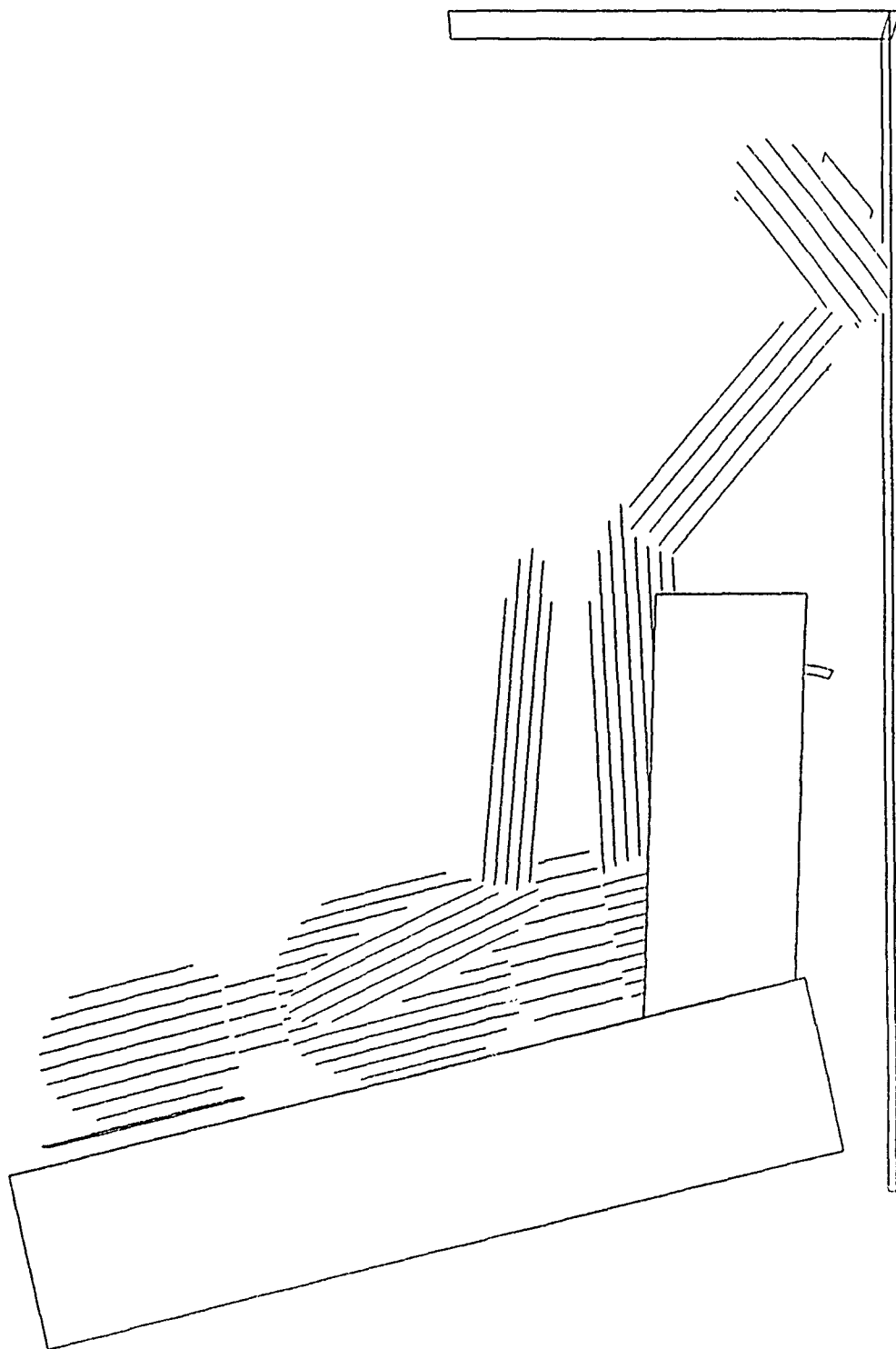
MAIN - PROCESSING FRAME #	1
XMIN,XMAX=	0.000 9.000
MAIN - PROCESSING FRAME #	2
MAIN - PROCESSING FRAME #	3
MAIN - PROCESSING FRAME #	4
MAIN - PROCESSING FRAME #	5
MAIN - PROCESSING FRAME #	6
MAIN - PROCESSING FRAME #	7
MAIN - PROCESSING FRAME #	8
MAIN - PROCESSING FRAME #	9

## APPENDIX F3

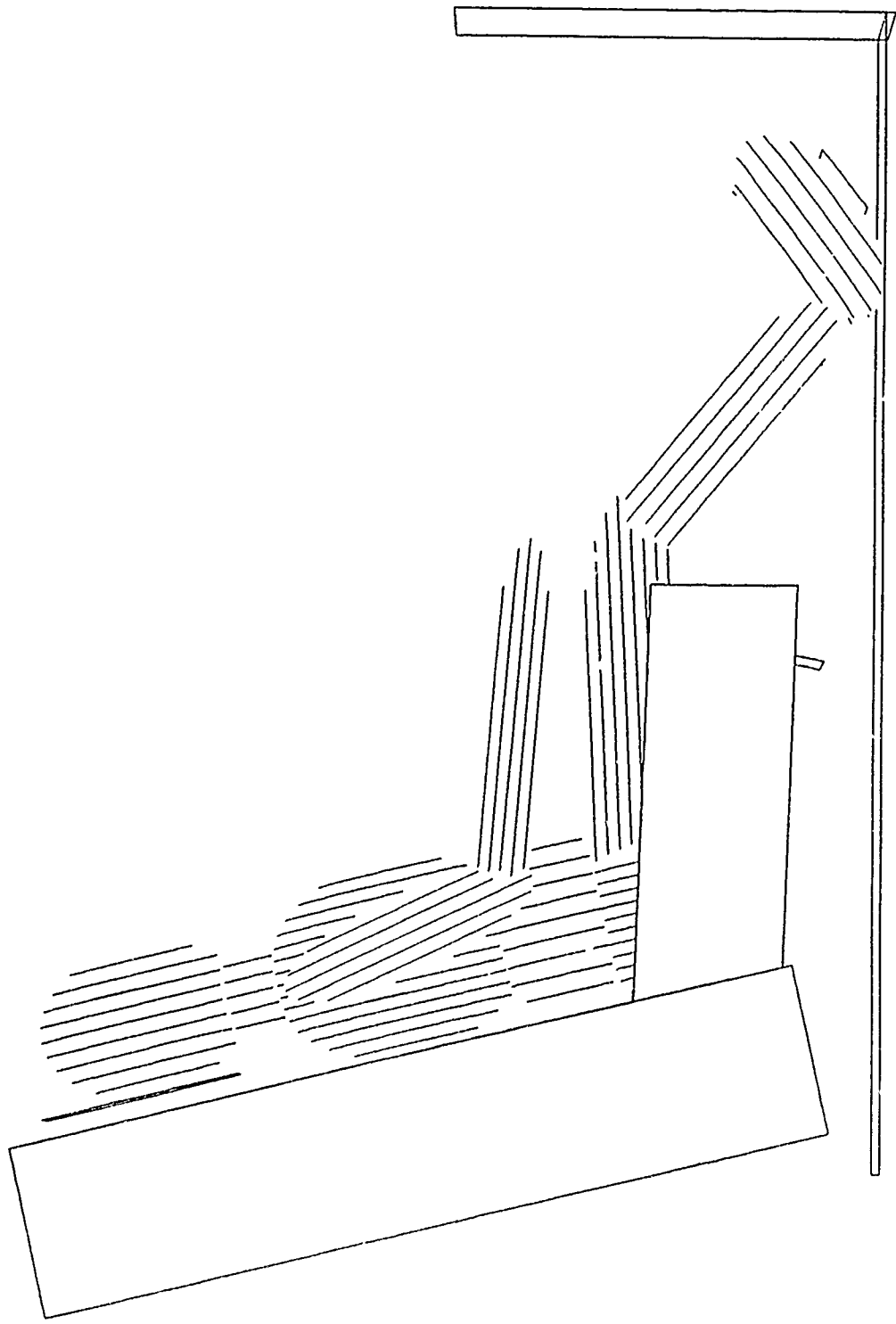
Example 1, VIEW -- 386 Output Graphics

# ATB COURSE EXAMPLE 1

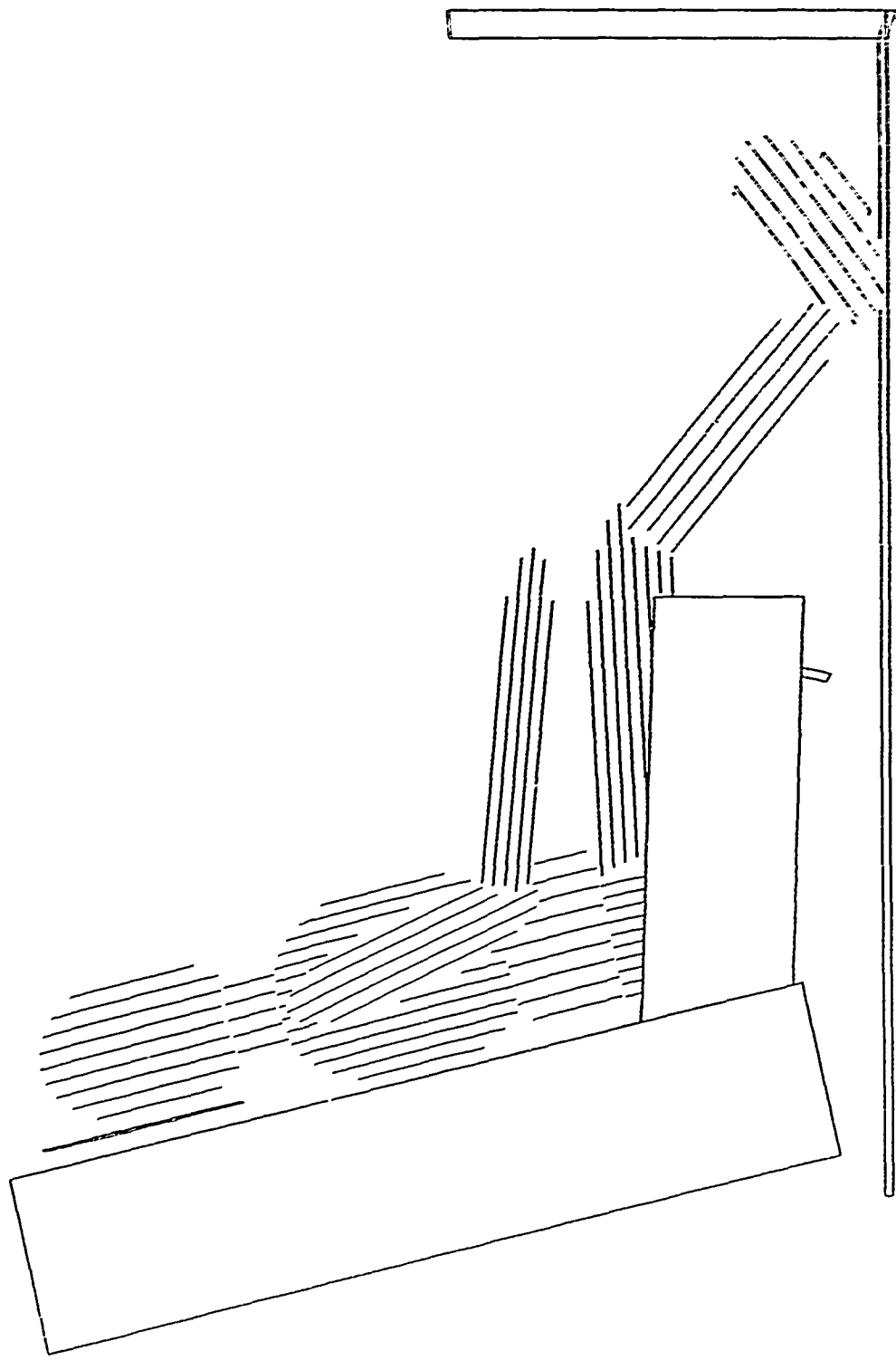
TIME (MSEC) 0



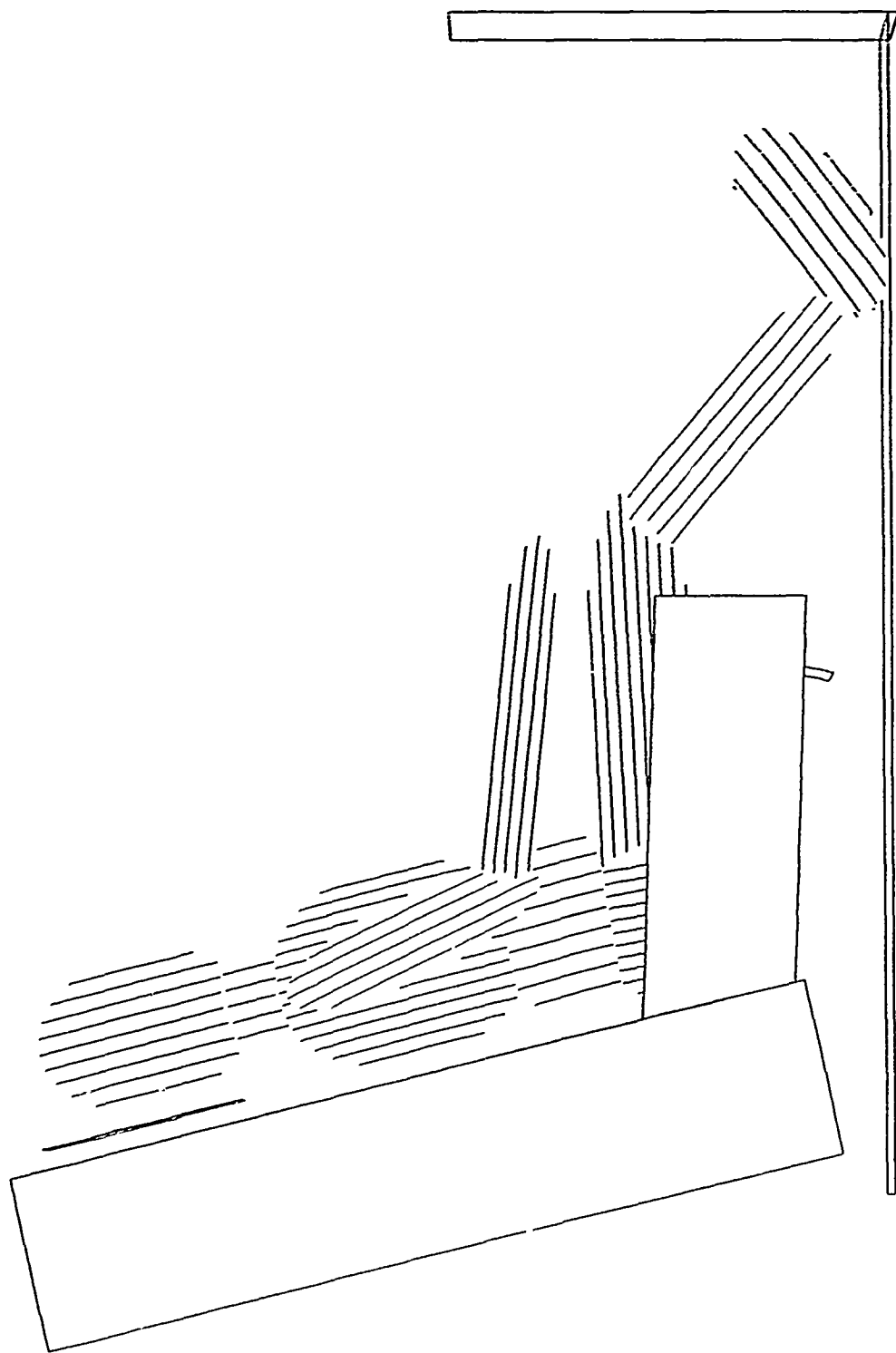
TIME (MSEC) 10



TIME (MSEC) 20

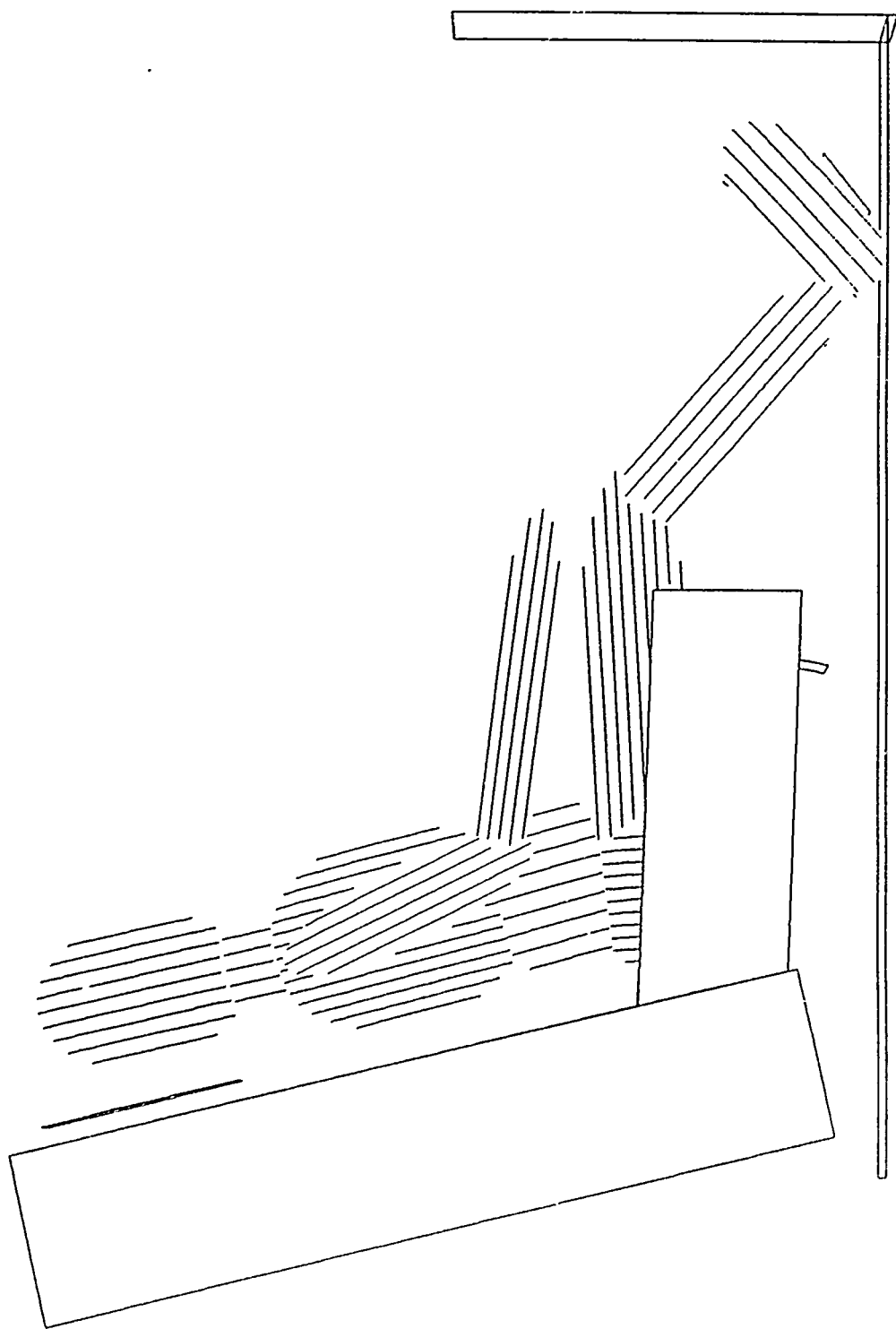


TIME (MSEC) 30

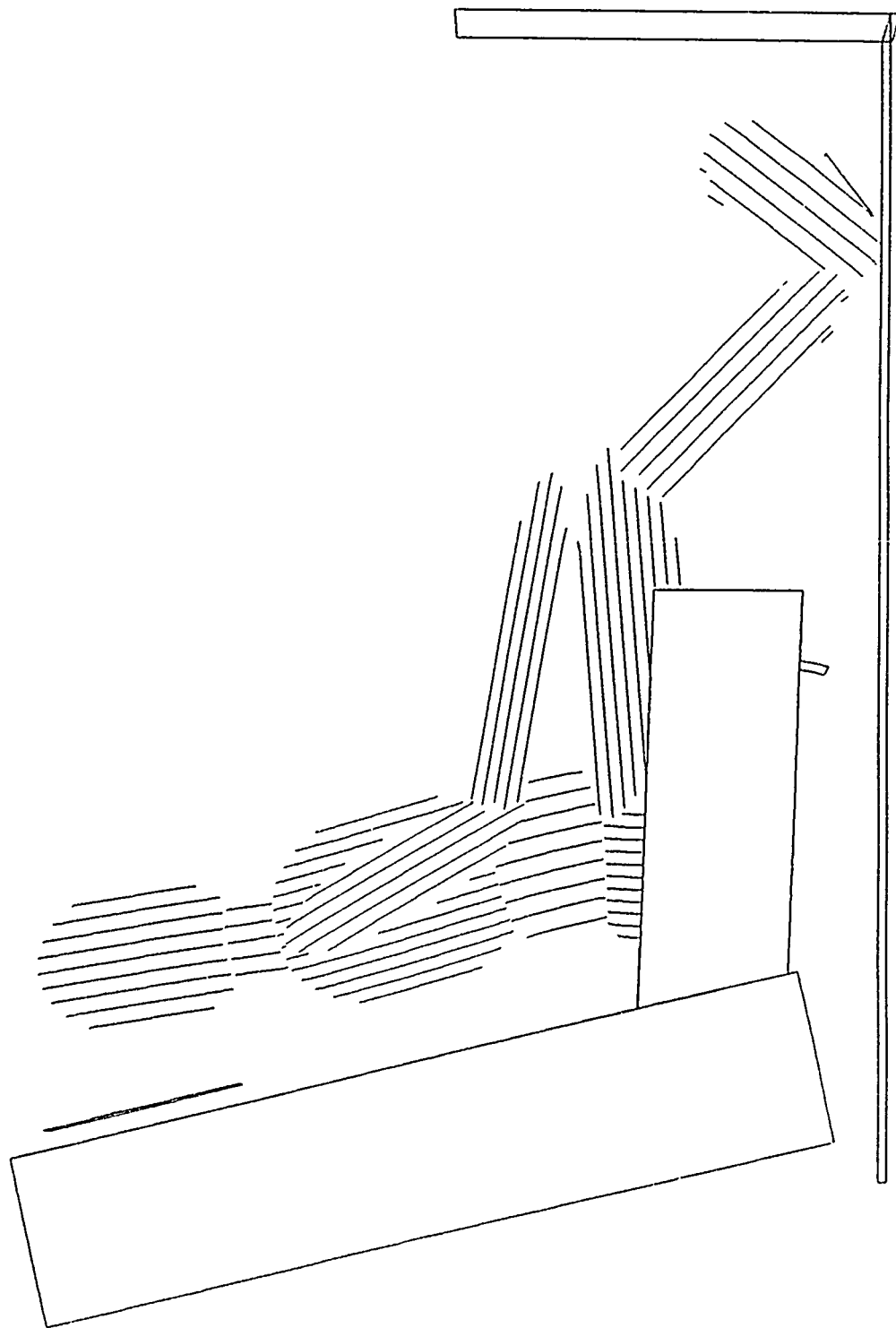




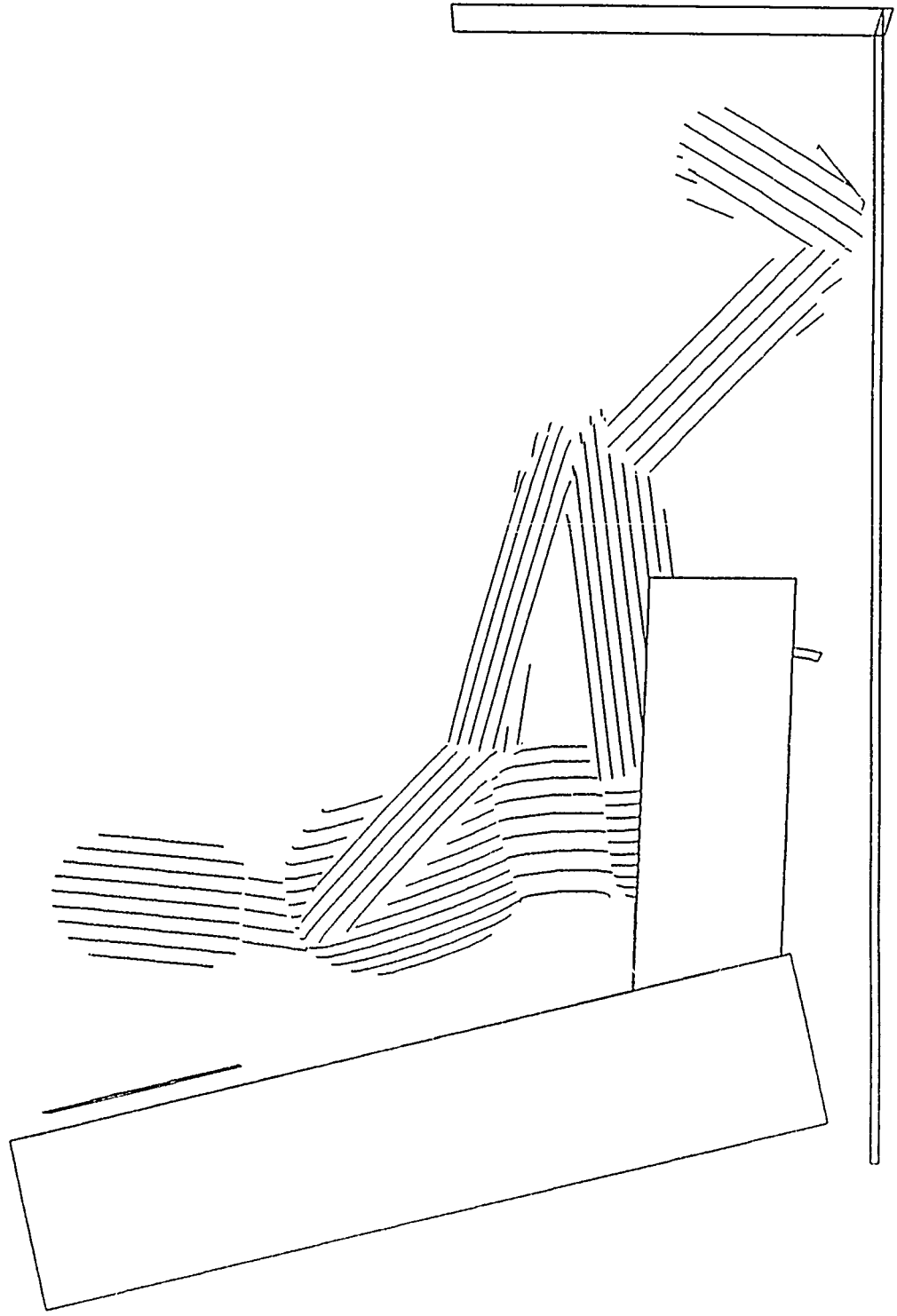
TIME (MSEC) 40



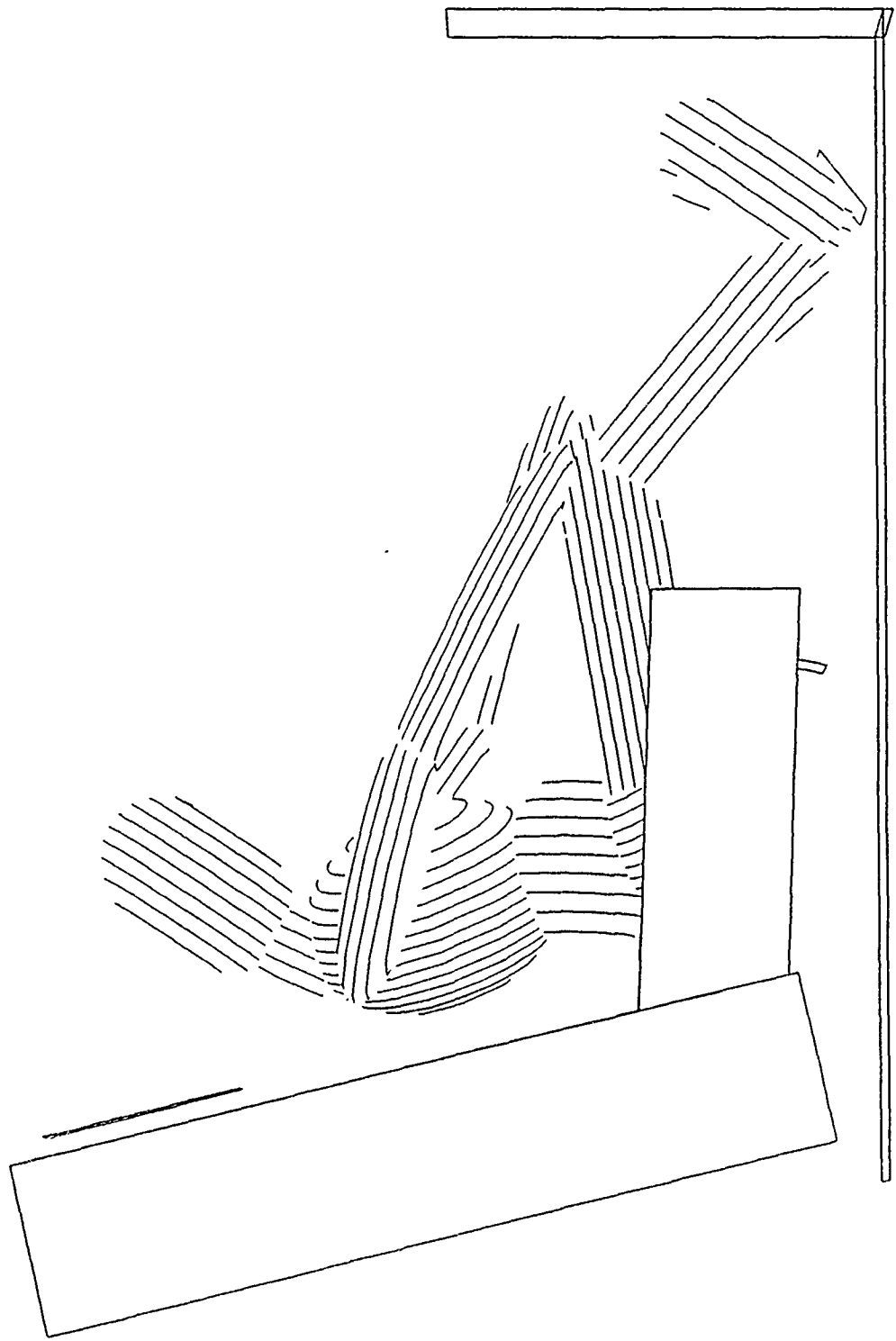
TIME (MSEC) 50



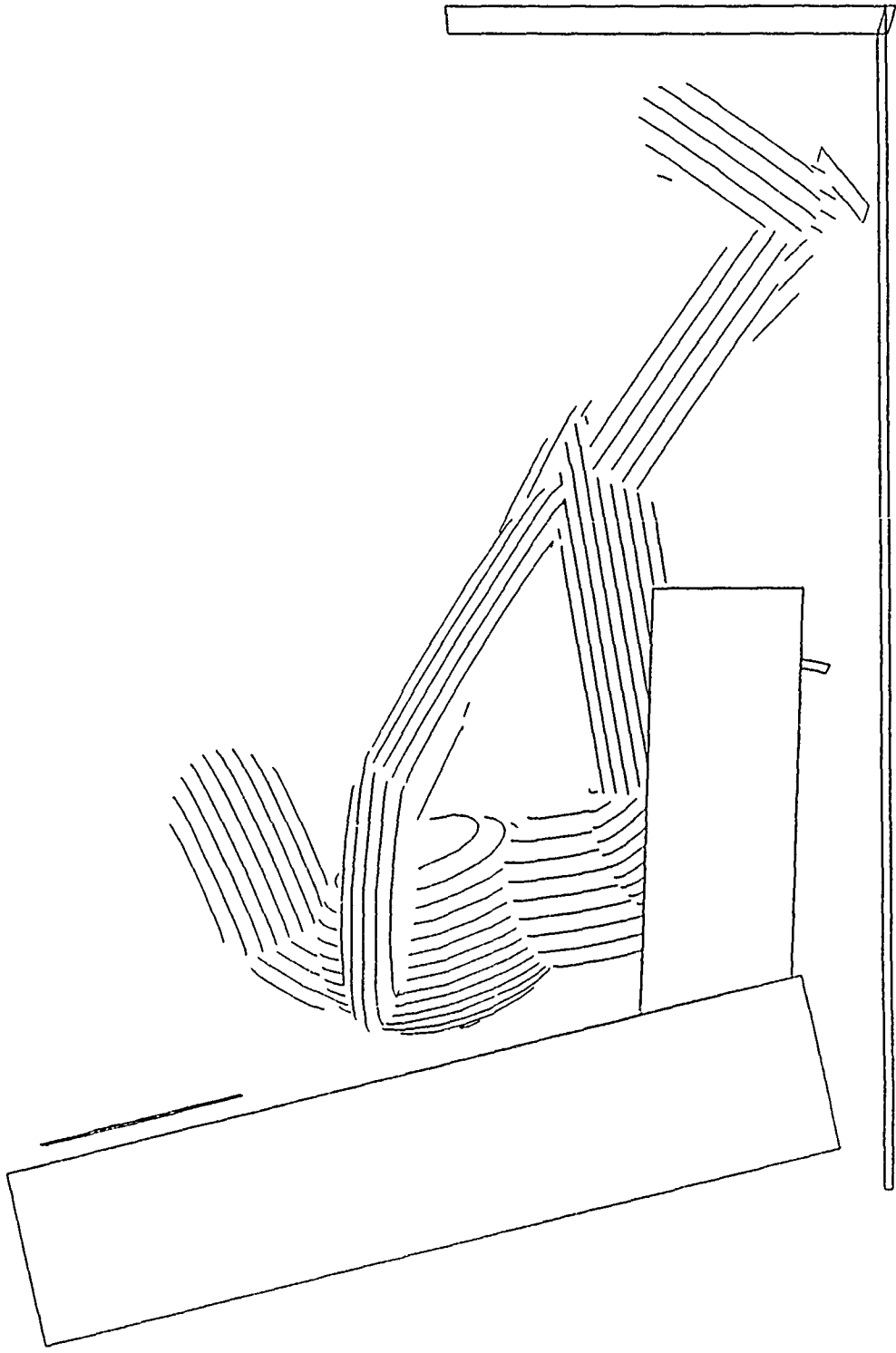
TIME (MSEC) 60



TIME (MSEC) 70



TIME (MSEC) 80



## APPENDIX G1

Example 2, VIEW -- Input File (EXP2.VIW)



APPENDIX G2

Example 2, VIEW -- 386 Output Listing (EXP2.VOU)



[illegible]

4	110.00
4.	4.

```

MAIN - PROCESSING FRAME # 1
XMIN,XMAX=      0.000      9.000
MAIN - PROCESSING FRAME # 2
MAIN - PROCESSING FRAME # 3
MAIN - PROCESSING FRAME # 4
MAIN - PROCESSING FRAME # 5

```

## APPENDIX G3

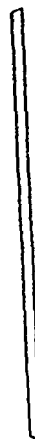
Example 2, VIEW -- 386 Output Graphics

ATB COURSE EXAMPLE 2

TIME (MSEC) 0



TIME (MSEC) 10



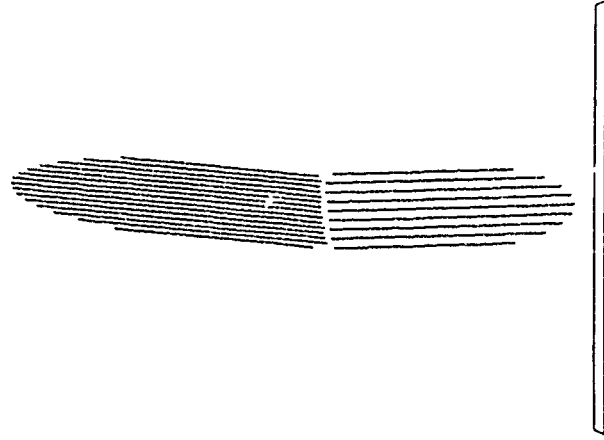
TIME (MSEC) 20



TIME (MSEC) 30



TIME (MSEC) 40





APPENDIX H

386-GEBOB Program Listing

```

C--PROGRAM GEBOD------(PERKIN-ELMER  FTN VII)-----C
C   GEBOD GENERATES BODY DESCRIPTION DATA SETS FOR USE IN THE ARTICULATED C
C   TOTAL BODY (ATB) MODEL.  USER HAS CHOICE OF PRODUCING A DATA SET C
C   CORRESPONDING TO ADULT MALE, ADULT FEMALE, CHILD SUBJECT, OR SOME C
C   DUMMY SUBJECTS.  THE BASIC GEOMETRY OF THE MODEL USED TO CALCULATE THE C
C   BODY DESCRIPTION DATA FOR THE HUMAN DATASETS IS AN EXTENSIVELY C
C   MODIFIED VERSION OF THE MODEL USED BY CALSPAN CORP.  THE MODIFICATIONS C
C   TO THE MODEL AND THE RESULTING PROGRAM, WERE WRITTEN BY THE C
C   UNIVERSITY OF DAYTON RESEARCH INSTITUTE UNDER CONTRACT F33615-81-C-0513. C
C   THE MODIFICATIONS TO INCLUDE DUMMY DATASETS WERE WRITTEN BY BEECHER C
C   RESEARCH COMPANY UNDER CONTRACT F33615-87-C-0530. C
C   80386 IMPLEMENTATION BY KETRON, INC., OCTOBER 31, 1989, UNDER CONTRACT C
C   F33615-88-C-0543. C
C C
C   FILES: C
C   UNIT1--USER SUPPLIED DIMENSIONAL DATA. C
C   UNIT2--GEBOD.DAT DATA FILE FOR I/O. C
C   UNIT3--RESULTS READY FOR INSERTION INTO AN ATB MODEL INPUT DECK. C
C   UNIT5 (CRT OUTPUT)--INPUT PROMPTS ARE WRITTEN TO THIS UNIT. C
C   UNIT7 (CRT INPUT)--SUBJECT DESCRIPTION IS ENTERED TO THIS UNIT. C
C   UNIT9 (PRINTER)--TABLE FORM OF RESULTS. C
C C
C   THE GEBOD.DAT FILE WHICH ACCOMPANIES THIS PROGRAM CONTAINS THE C
C   FOLLOWING DATA: C
C   1. THE NUMBER OF SUBJECT TYPES IN LIST-DIRECTED FORMAT C
C   AVAILABLE TO THE USER. C
C   2. THE TITLES FOR THE SUBJECT TYPES IN LIST-DIRECTED FORMAT. C
C   3. THE AAMRL/BBM ATB INPUT DATASETS THAT ARE AVAILABLE TO SPECIFIC C
C   USERS AND USED AS INPUT TO THIS PROGRAM.  EACH ATB INPUT DATASET C
C   IS PRECEDED BY A HEADER IN LIST-DIRECTED FORMAT STATING THE C
C   NUMBER OF RECORDS IN THE DATASET AND THE SUBJECT TYPE IT IS C
C   ASSOCIATED WITH.  FOR EACH SUBJECT TYPE THERE ARE TWO DATASETS, C
C   ONE IN ENGLISH UNITS AND THE OTHER IN METRIC UNITS.  NOTE C
C   THAT NOT ALL SUBJECT TYPES HAVE DATA STORED IN THIS FILE AND C
C   FOR SOME USERS THERE MAY NOT BE ANY ATB INPUT DATASETS STORED. C
C C
C   ROUTINES (IN ORDER OF APPEARANCE): C
C   PROGRAM GEBOD C
C   BLOCK DATA C
C   SUBROUTINE DIALOG C
C   SUBROUTINE ASKUN C
C   SUBROUTINE PFILE C
C   SUBROUTINE CONTAC C
C   SUBROUTINE SEGMA C
C   SUBROUTINE SGINER C
C   SUBROUTINE ELLIP C
C   ENTRY ELLPMI C
C   SUBROUTINE TORSO C
C   SUBROUTINE FEET C
C   SUBROUTINE RESULTS C
C   SUBROUTINE CNVRT C
C   SUBROUTINE RESULTZ C

```

C	SUBROUTINE ATBOUT	C
C	SUBROUTINE NOATBOUT	C
C	-----	C

```

PROGRAM GEBOD
COMMON /DIMS/ DD(-1:31), REGEQ(24, -1:31), PRED(0:2)
&                                , RANGE(2, -1:1, 3), CONV(-1:1)      80386
COMMON /FLOAT/ PI, PI2, PI4, DENS, GRAV      80386
CHARACTER*12 FILE2, FILE3, FILE9      80386

PI = ACOS(-1.)
PI2 = PI + PI
PI4 = PI2 + PI2

OPEN (UNIT=5, FILE='CON', CARRIAGE CONTROL='LIST')      80386
OPEN (UNIT=7, FILE='CON')      80386
OPEN (UNIT=4, FILE='GEBODII.DIR', STATUS='OLD')      80386
READ (4, '(A12/A12/A12)') FILE2, FILE3, FILE9      80386
OPEN (UNIT=2, FILE=FILE2, STATUS='OLD')      80386
OPEN (UNIT=3, FILE=FILE3, STATUS='NEW')      80386
OPEN (UNIT=9, FILE=FILE9, STATUS='NEW', CARRIAGE CONTROL='FORTRAN') 80386
10 CALL DIALOG (IPTR, ICNT, ISTRT, ISUB)
   IF (ISUB.LE.4) THEN
     IF (IPTR.LT.25) THEN
       DO 100 I = ISTRT, 31
         DD(I) = REGEQ(IPTR+ICNT, I)
         DO 100 J = 0, ICNT - 1
           DD(I) = DD(I) + PRED(J)*REGEQ(IPTR+J, I)
100        ENDIF

       CALL CONTAC
       CALL SEGMAS
       CALL SGINER
       CALL RESULTS (ISTRT)
     ELSE
       CALL RESULTZ (ISUB)
     ENDIF
   REWIND (2)
   GOTO 10
END

```

```

C--BLOCK DATA-----C
C   DATA IN COMMON AREAS                                C
C   /SGMNTS/--SEGMENT DATA                              C
C       ABCN--X,Y, AND Z CONTACT ELLIPSOID SEMIAXES FOR EACH SEGMENT C
C       RMN--MASS OF EACH SEGMENT                        C
C       PHI--SEGMENT MOMENTS OF INERTIA                  C
C       XYZCG--LOCAL REFERENCE COORDINATES OF CENTER OF SEGMENT C
C               CONTACT ELLIPSOIDS                      C
C
C   /JNTS/--JOINT DATA                                  C
C       RNJ--LOCAL REFERENCE SYSTEM COORDINATES OF EACH JOINT.  THIRD C
C           SUBSCRIPT EQUAL TO 2 SPECIFIES LOCAL REFERENCE SYSTEM OF SEGMENT C
C           J+1. A VALUE OF 1 IN THIS POSITION SPECIFIES LOCAL REFERENCE C
C           SYSTEM OF SEGMENT JNT(J), WHERE IN BOTH CASES J IS THE VALUE OF C
C           THE FIRST SUBSCRIPT.                          C
C       JNT--POINTER ARRAY FOR ASSOCIATING JOINTS WITH SEGMENTS C
C       YPRLL--YAW, PITCH, AND ROLL ANGLES OF JOINT AXES RELATIVE TO LOCAL C
C           REFERENCE AXES                               C
C       IPIN--SPECIFIES JOINT TYPE                       C
C
C   /DIMS/--BODY DIMENSION DATA                         C
C       DD--BODY DIMENSIONS                              C
C       REGEQ--REGRESSION EQUATIONS USED TO COMPUTE BODY DIMENSIONS C
C       PRED--VALUES OF PREDICTING VARIABLES TO BE USED WITH REGEQ C
C       RANGE--ACCEPTIBLE RANGE FOR PREDICTING VARIABLES C
C       CONV--CONSTANTS FOR CONVERTING BODY DIMENSIONS FROM METRIC TO C
C           ENGLISH UNITS                                C
C
C   /NAMES/--CHARACTER STRINGS FOR VARIOUS LABLES        C
C       SUBTYP--DESCRIPTION TO USER OF 4 SOURCES OF BODY DIMENSION DATA C
C       SEGLAB--SEGMENT LABLES                           C
C       JNTLAB--JOINT LABLES                             C
C       PLTSYM--PLOTING SYMBOL FOR SEGMENTS AND JOINTS C
C       DIMLAB--NAMES OF THE BODY DIMENSIONS              C
C       TITLE--RUN TITLE SUPPLIED BY THE USER           C
C       UNITS--UNITS FOR USER TO CHOOSE BETWEEN         C
C
C   /FLOAT/--VARIOUS CONSTANTS                          C
C       PI--THE CONSTANT PI                              C
C       PI2--PI**2                                       C
C       PI4--PI**4                                       C
C       DENS--DENSITY USED FOR COMPUTATION OF SEGMENT INERTIAL PROPERTIES C
C       GRAV--ACCELERATION OF GRAVITY                   C
C
C   /CYL/--DATA USED IN RIGHT ELLIPTICAL CYLINDER MODELLING OF SEGMENTS C
C       FOR COMPUTATION OF INERTIAL PROPERTIES           C
C       ZEES--CONTAINS Z CORDINATE GIVING VERTICAL EXTENT OF CYLINDERS C
C       ZH--HEIGHT OF EACH CYLINDER IN THE NUMERICAL INTEGRATION C
C       NSEG--NUMBER OF CYLINDERS IN THE NUMERICAL INTEGRATION C
C       CGZ--Z COORDINATE OF CENTER OF GRAVITY OF MODEL C
C       WTCOR--EIGHT COORECTION FACTOR USED TO ADJUST DENS C
C

```

```

C      ALL DATA WILL BE CALCULATED AND STORED IN ENGLISH UNITS      C
C      DD(-1)--MONTHS      C
C      DD(0)--POUNDS      C
C      DD(1)-DD(31)--INCHES      C
C      DENS--SLUG/IN**3      C
C      GRAV--FT/SEC**2      C
C      RMN--SLUGS      C
C      PHI--SLUG*IN**2      C
C      ALL REMAINING LINEAR MEASUREMENTS ARE IN INCHES      C
C      THESE UNITS ARE UTILIZED UNTIL JUST PRIOR TO WRITTING OUT OF RE-      C
C      SULTS.  VALUES ARE THEN CONVERTED, IN PLACE, TO APPROPRIATE UNITS.      C
C      THE VALUE STORED IN GRAV IS USED FOR CONVERSION FROM SLUGS TO      C
C      POUNDS.      C
C-----C

```

# BLOCK DATA

```

COMMON /SGMNTS/ ABCN(15,3),RMN(15),PHI(3,15),XYZCG(15,3)
COMMON /JNTS/ RNJ(3,28),JNT(14),YPRLL(14,6),IPIN(14)
COMMON /DIMS/ DD(-1:31),REGEQ(24,-1:31),PRED(3),
&      RANGE(2,-1:1,3),CONV(-1:1)
COMMON /NAMES/ SUBTYP(10),SEGLAB(15),JNTLAB(14),PLTSYM(29),
&      DIMLAB(-1:31),TITLE,UNITS(3,-1:2)
COMMON /FLOAT/ PI,PI2,PI4,DENS,GRAV
COMMON /CYL/ ZEES(0:15),ZH(15),NSEG(15),CGZ(15),WTCOR
CHARACTER SUBTYP*35,SEGLAB*3,JNTLAB*2,PLTSYM*1,DIMLAB*24,TITLE*60 80386
CHARACTER UNITS*6

```

```

DATA SEGLAB/'LT ','CT ','UT ','N ','H ','RUL','RLL',
&'RF ','LUL','LLL','LF ','RUA','RLA','LUA','LLA'/
DATA JNTLAB/'P ','W ','NP','HP','RH','RK','RA',
&'LH','LK','LA','RS','RE','LS','LE '/
DATA PLTSYM/'1 ','2 ','3 ','4 ','5 ','6 ','7 ','8 ','9 ','A ','B ','C ','D',
&'E ','F ','M ','N ','O ','P ','Q ','R ','S ','T ','U ','V ','W ','X ','Y ','Z'/
DATA JNT/1,2,3,4,1,6,7,1,9,10,3,12,3,14/
DATA UNITS /'MONTHS','YEARS',' ','LB.','N.','%-TILE',
&      'IN.','M.','%-TILE','ENGLISH','METRIC',' '/
DATA CONV /12.,.2248,39.370/,DENS,GRAV/1.12287E-3,32.17405/

```

## C DIMENSIONAL DATA LABELS

```

DATA DIMLAB /
&      'AGE      ','WEIGHT      ',
&      'STANDING HEIGHT      ','SHOULDER HEIGHT      ',
&      'ARMPIT HEIGHT      ','WAIST HEIGHT      ',
&      'SEATED HEIGHT      ','HEAD LENGTH      ',
&      'HEAD BREADTH      ','HEAD TO CHIN HEIGHT      ',
&      'NECK CIRCUMFERENCE      ','SHOULDER BREADTH      ',
&      'CHEST DEPTH      ','CHEST BREADTH      ',
&      'WAIST DEPTH      ','WAIST BREADTH      ',
&      'BUTTOCK DEPTH      ','HIP BREADTH,STANDING      ',
&      'SHOULDER TO ELBOW LENGTH','FOREARM-HAND LENGTH      ',
&      'BICEPS CIRCUMFERENCE      ','ELBOW CIRCUMFERENCE      ',
&      'FOREARM CIRCUMFERENCE      ','WRIST CIRCUMFERENCE      ',

```

```

&      'KNEE HEIGHT, SEATED      ', 'THIGH CIRCUMFERENCE      ',
&      'UPPER LEG CIRCUMFERENCE', 'KNEE CIRCUMFERENCE      ',
&      'CALF CIRCUMFERENCE      ', 'ANKLE CIRCUMFERENCE      ',
&      'ANKLE HEIGHT, OUTSIDE    ', 'FOOT BREADTH            ',
&      'FOOT LENGTH              '/

DATA RANGE /
& 24.00      , 240.0      , 22.27      , 247.6      , 32.01      , 76.54      ,
& 18.50      , 56.50      , 85.00      , 200.0      , 56.93      , 72.05      ,
& 21.50      , 50.50      , 118.0      , 264.0      , 62.17      , 77.64      /

DATA (REGEQ(J, -1), J=1, 24) /
& 1.000      , .4547E-12, 1.213      , 25.43      , 5.202      , -158.9      ,
& 1.000      , 0.      , 0.      , .4547E-12, 0.      , 0.      ,
& 0.      , 0.      , 0.      , 0.      , 0.      , 0.      ,
& 0.      , 0.      , 0.      , 0.      , 0.      , 0.      /

DATA (REGEQ(J, 0), J=1, 24) /
& .6625      , -.7660      , 1.000      , .4547E-12, 3.743      , -122.2      ,
& 0.      , 1.000      , 0.      , .4547E-12, 1.000      , .4547E-12,
& 3.737      , -111.2      , 1.000      , 0.      , .4547E-12, 1.000      ,
& .9095E-12, 4.530      , -142.7      , 1.000      , 0.      , .9095E-12/

DATA (REGEQ(J, 1), J=1, 24) /
& .1756      , 32.62      , .2314      , 35.58      , 1.000      , .2274E-12,
& 0.      , 0.      , 1.000      , .2274E-12, .7589E-01, 54.16      ,
& 1.000      , .2274E-12, 0.      , 1.000      , .2274E-12, .5850E-01,
& 59.66      , 1.000      , .4547      , 2.0.      , 1.000      , .4547E-12/

DATA (REGEQ(J, 2), J=1, 24) /
& .1518      , 24.79      , .1994      , 27.37      , .8721      , -3.898      ,
& 0.      , 0.      , .8721      , -3.898      , .7182E-01, 42.77      ,
& .8751      , -3.936      , .7555E-02, .8469      , -3.096      , .5844E-01,
& 47.02      , .8911      , -5.049      , .8583E-02, .8522      , -3.824      /

DATA (REGEQ(J, 3), J=1, 24) /
& .1467      , 22.53      , .1916      , 25.19      , .8315      , -4.469      ,
& 0.      , -.1217E-01, .8770      , -5.954      , .5840E-01, 39.83      ,
& .8309      , -5.762      , -.6495E-02, .8551      , -6.484      , .4637E-01,
& 43.06      , .8398      , -7.529      , -.3761E-02, .8569      , -8.066      /

DATA (REGEQ(J, 4), J=1, 24) /
& .1186      , 17.74      , .1530      , 19.97      , .6822      , -4.726      ,
& 0.      , -.1855E-01, .7519      , -7.012      , .5302E-01, 32.73      ,
& .6845      , -4.206      , 0.      , .6845      , -4.206      , .3642E-01,
& 35.59      , .7043      , -7.256      , -.6506E-02, .7338      , -8.185      /

DATA (REGEQ(J, 5), J=1, 24) /
& .7804E-01, 19.17      , .1047      , 20.34      , .4412      , 4.849      ,
& .5848E-02, .1910E-01, .3393      , 8.114      , .3620E-01, 29.09      ,
& .4225      , 6.734      , .5773E-02, .4010      , 7.376      , .2664E-01,
& 32.06      , .4043      , 8.460      , .4060E-02, .3859      , 9.039      /

DATA (REGEQ(J, 6), J=1, 24) /
& .3642E-02, 6.881      , .5571E-02, 6.881      , .2249E-01, 6.110      ,
& -.3975E-02, .2793E-02, .3264E-01, 5.825      , .4897E-02, 6.625      ,
& .3600E-01, 4.950      , .3021E-02, .2471E-01, 5.286      , .3209E-02,
& 7.266      , .2680E-01, 5.952      , .2233E-02, .1668E-01, 6.271      /

DATA (REGEQ(J, 7), J=1, 24) /
& .3642E-02, 5.220      , .5337E-02, 5.237      , .2096E-01, 4.532      ,
& -.6471E-03, .3641E-02, .1071E-01, 4.873      , .4089E-02, 5.194      ,

```

```

& .1347E-01, 4.855      , .4089E-02,0.      , 5.194      , .3060E-02,
& 5.611      , .1174E-01, 5.322      , .3060E-02,0.      , 5.611      /
DATA (REGEQ(J, 8), J=1,24) /
& .8988E-02, 6.582      , .1266E-01, 6.666      , .5203E-01, 4.867      ,
& -.2157E-02, .4550E-02, .4621E-01, 5.080      , .7362E-02, 7.688      ,
& .6816E-01, 4.275      , .3057E-02, .5674E-01, 4.615      , .3143E-02,
& 8.420      , .4659E-01, 5.712      ,0.      , .4659E-01, 5.712      /
DATA (REGEQ(J, 9), J=1,24) /
& .2281E-01, 8.421      , .3449E-01, 8.448      , .1301      , 4.177      ,
& -.2812E-02, .3292E-01, .2141E-01, 7.760      , .2316E-01, 10.34      ,
& .8900E-01, 7.607      , .2316E-01,0.      , 10.34      , .2444E-01,
& 10.85      , .6527E-01, 10.54      , .2806E-01, -.6185E-01, 14.54      /
DATA (REGEQ(J,10), J=1,24) /
& .3595E-01, 7.530      , .4866E-01, 8.020      , .2040      , .8749      ,
& .4037E-02, .1483E-01, .1271      , 3.354      , .1927E-01, 11.66      ,
& .1246      , 6.160      , .1369E-01, .7344E-01, 7.682      , .1612E-01,
& 13.24      , .1181      , 7.790      , .1253E-01, .6133E-01, 9.578      /
DATA (REGEQ(J,11), J=1,24) /
& .2870E-01, 5.225      , .4249E-01, 5.333      , .1620      , -.2418E-01,
&0.      , .3764E-01, .2091E-01, 4.589      , .3412E-01, 4.965      ,
& .7300E-01, 4.650      , .3989E-01, -.7607E-01, 9.086      , .2690E-01,
& 4.984      , .6114E-01, 5.386      , .3174E-01, -.8265E-01, 9.915      /
DATA (REGEQ(J,12), J=1,24) /
& .2699E-01, 5.195      , .3856E-01, 5.411      , .1504      , .3666      ,
& .4513E-02, .2798E-01, .2213E-01, 4.506      , .3185E-01, 6.968      ,
& .8875E-01, 5.357      , .3505E-01, -.4222E-01, 9.255      , .2911E-01,
& 7.854      , .8877E-01, 6.709      , .3254E-01, -.5866E-01, 11.35      /
DATA (REGEQ(J,13), J=1,24) /
& .1284E-01, 5.024      , .2279E-01, 4.763      , .7598E-01, 2.485      ,
& -.8176E-02, .3995E-01, -.3147E-01, 6.097      , .2922E-01, 2.979      ,
& .5358E-01, 3.279      , .3511E-01, -.7761E-01, 7.183      , .3026E-01,
& 3.528      , .5167E-01, 5.174      , .3706E-01, -.1162      , 10.46      /
DATA (REGEQ(J,14), J=1,24) /
& .2718E-01, 5.367      , .3977E-01, 5.508      , .1522      , .4650      ,
& .3925E-02, .3503E-01,0.      , 5.406      , .3527E-01, 5.010      ,
& .1060      , 2.734      , .3800E-01, -.3598E-01, 6.959      , .3741E-01,
& 5.694      , .1105      , 4.473      , .4211E-01, -.8025E-01, 10.48      /
DATA (REGEQ(J,15), J=1,24) /
& .2730E-01, 4.812      , .4032E-01, 4.910      , .1528      , -.1220      ,
& .4893E-02, .3874E-01, -.1900E-01, 5.466      , .3419E-01, 3.976      ,
& .7090E-01, 3.803      , .4021E-01, -.7937E-01, 8.275      , .3077E-01,
& 4.095      , .6978E-01, 4.566      , .3632E-01, -.9475E-01, 9.749      /
DATA (REGEQ(J,16), J=1,24) /
& .3552E-01, 5.542      , .4957E-01, 5.905      , .1968      , -.7718      ,
& .1151E-01, .3192E-01, .1642E-01, 5.020      , .4052E-01, 8.610      ,
& .1285      , 5.563      , .4294E-01, -.3192E-01, 10.34      , .2803E-01,
& 9.019      , .1258      , 5.100      , .2803E-01,0.      , 9.019      /
DATA (REGEQ(J,17), J=1,24) /
& .3933E-01, 6.369      , .5175E-01, 7.038      , .2237      , -.9239      ,
& .8433E-03,0.      , .2193      , -.7898      , .1702E-01, 10.04      ,
& .1962      , -.3163      , .2976E-02, .1851      , .1459E-01, .1256E-01,
& 11.97      , .2087      , -.4158      ,0.      , .2087      , -.4158      /

```

```

DATA (RECEQ(J,18), J=1,24) /
& .4900E-01, 8.421 , .6536E-01, 9.182 , .2804 , -.7587 ,
& -.2689E-02, .4490E-02, .2776 , -.6374 , .2092E-01, 13.78 ,
& .2478 , .6324 , .2960E-02, .2367 , .9615 , .1671E-01,
& 16.54 , .2646 , .9735 , .1677E-02, .2570 , 1.213 /
DATA (REGEQ(J,19), J=1,24) /
& .2664E-01, 4.976 , .4173E-01, 4.878 , .1501 , .1143 ,
& 0. , .5211E-01, -.4492E-01, 6.478 , .4369E-01, 4.522 ,
& .5386E-01, 6.646 , .5528E-01, -.1527 , 12.79 , .3340E-01,
& 6.608 , .5996E-01, 8.219 , .4067E-01, -.1243 , 14.02 /
DATA (REGEQ(J,20), J=1,24) /
& .2267E-01, 5.152 , .3434E-01, 5.166 , .1290 , .9440 ,
& -.1938E-02, .3358E-01, .1344E-01, 4.738 , .2421E-01, 7.539 ,
& .1221 , 2.826 , .2086E-01, .4420E-01, 5.145 , .1919E-01,
& 8.967 , .1061 , 4.894 , .1767E-01, .2601E-01, 7.416 /
DATA (REGEQ(J,21), J=1,24) /
& .2267E-01, 5.152 , .3434E-01, 5.166 , .1290 , .9440 ,
& -.1938E-02, .3358E-01, .1344E-01, 4.738 , .2643E-01, 5.879 ,
& .7088E-01, 4.719 , .2938E-01, -.3890E-01, 7.986 , .2116E-01,
& 7.411 , .6768E-01, 6.359 , .2341E-01, -.3835E-01, 9.700 /
DATA (REGEQ(J,22), J=1,24) /
& .1145E-01, 3.971 , .1771E-01, 3.951 , .6620E-01, 1.791 ,
& -.3478E-02, .1804E-01, .1674E-01, 3.447 , .1090E-01, 4.503 ,
& .5371E-01, 2.463 , .9530E-02, .1810E-01, 3.523 , .9921E-02,
& 5.202 , .5166E-01, 3.317 , .9386E-02, .9137E-02, 4.657 /
DATA (REGEQ(J,23), J=1,24) /
& .5917E-01, 9.584 , .7857E-01, 10.55 , .3433 , -1.746 ,
& -.8480E-02, -.4527E-02, .4045 , -3.654 , .3002E-01, 14.98 ,
& .3345 , -2.547 , .6469E-02, .3104 , -1.828 , .2467E-01,
& 17.67 , .3558 , -2.889 , .5244E-02, .3321 , -2.141 /
DATA (REGEQ(J,24), J=1,24) /
& .6066E-01, 9.311 , .8944E-01, 9.551 , .3382 , -1.560 ,
& .1018E-01, .8338E-01, -.2709E-01, 10.25 , .8417E-01, 11.13 ,
& .1869 , 9.912 , .9769E-01, -.1781 , 20.77 , .6998E-01,
& 11.01 , .1614 , 11.89 , .8237E-01, -.2117 , 23.64 /
DATA (REGEQ(J,25), J=1,24) /
& .4805E-01, 7.998 , .7076E-01, 8.195 , .2691 , -.6787 ,
& .5930E-02, .6358E-01, 0. , 8.043 , .6412E-01, 9.905 ,
& .1664 , 7.448 , .7187E-01, -.1022 , 15.44 , .3229E-01,
& 9.621 , .1412 , 5.370 , .3229E-01, 0. , 9.621 /
DATA (REGEQ(J,26), J=1,24) /
& .4805E-01, 7.998 , .7076E-01, 8.195 , .2691 , -.6787 ,
& .5930E-02, .6358E-01, 0. , 8.043 , .4406E-01, 8.684 ,
& .1458 , 4.985 , .4605E-01, -.2626E-01, 10.11 , .3334E-01,
& 9.686 , .1512 , 4.918 , .3334E-01, 0. , 9.686 /
DATA (REGEQ(J,27), J=1,24) /
& .3544E-01, 6.685 , .5209E-01, 6.839 , .1998 , .2129 ,
& .1539E-02, .4370E-01, .2825E-01, 5.794 , .4012E-01, 8.335 ,
& .1106 , 6.386 , .4429E-01, -.5493E-01, 11.31 , .3250E-01,
& 9.002 , .8842E-01, 8.469 , .3718E-01, -.3000E-01, 13.77 /
DATA (REGEQ(J,28), J=1,24) /
& .1770E-01, 5.116 , .2659E-01, 5.152 , .1016 , 1.786 ,

```



```

&-.3664E-02, .2284E-01, .3523E-01, 3.995      , .1809E-01, 5.999      ,
& .7603E-01, 3.449      , .1720E-01, .1177E-01, 5.361      , .1610E-01,
& 6.028      , .6599E-01, 4.216      , .1665E-01, -.9456E-02, 6.593      /
DATA (REGEQ(J,29), J=1,24) /
& .6837E-02, 1.319      , .9232E-02, 1.417      , .4015E-01, -.2052E-01,
&-.1302E-02,0.      , .4697E-01, -.2305      , .3434E-02, 2.230      ,
& .4163E-01, .9788E-02,0.      , .4163E-01, .9788E-02, .4310E-02,
& 4.652      , .8736E-01, -.6990      , -.1090E-02, .9230E-01, -.8545      /
DATA (REGEQ(J,30), J=1,24) /
& .8742E-02, 2.193      , .1221E-01, 2.283      , .5052E-01, .5281      ,
&-.1722E-02, .4119E-02, .4407E-01, .7576      , .4638E-02, 2.901      ,
& .2947E-01, 1.611      , .3353E-02, .1694E-01, 1.984      , .4136E-02,
& 3.12      , .3418E-01, 1.459      , .2907E-02, .2101E-01, 1.873      /
DATA (REGEQ(J,31), J=1,24) /
& .2436E-01, 5.384      , .3275E-01, 5.742      , .1416      , .7017      ,
&-.5757E-02,0.      , .1715      , -.2125      , .1365E-01, 7.738      ,
& .1299      , 1.186      , .5296E-02, .1101      , 1.775      , .1028E-01,
& 8.858      , .1309      , 1.502      , .3570E-02, .1148      , 2.012      /

```

C

C YAW,PITCH AND ROLL

DATA YPRLL/

```

& 46*0.,8.1,0.,-8.1,-8.1,0.,8.1,28.8,80.,-28.8,-80.,0.,0.,20., REV1/87

```

```

& 0.,-44.4,65.6,-80.,-44.4,65.6,-80.,-39.6,-70.,-39.6,-70., REV1/87

```

```

& 4*0.,14.5,-3.3,0.,-14.5,3.3,0.,63.3,0.,-63.3,0./ REV1/87

```

DATA IPIN/0,0,0,0,0,1,0,0,1,0,0,1,0,1/

END

```

C--SUBROUTINE DIALOG-----C
C   DIALOG WRITES PROMPTS TO THE CRT AND ACCEPTS INPUT FROM THE CRT   C
C   DESCRIBING THE SUBJECT FOR WHICH BODY DESCRIPTION DATA IS TO BE   C
C   PRODUCED.  THE PARAMETERS, IPTR, ICNT, AND ISTRT, ARE RETURNED TO THE C
C   MAIN ROUTINE SPECIFYING THE CHOICES MADE BY THE USER               C
C   IPTR--SPECIFIES ROW OF REGEQ CONTAINING FIRST REGRESSION EQUATION   C
C   COEFFICIENT TO BE USED.  IPTR IS SET TO 25 FOR USER SUPPLIED      C
C   DIMENSIONAL DATA.                                                 C
C   ICNT--NUMBER OF COEFFICIENTS IN THE REGRESSION EQUATION TO BE USED. C
C   ISTRT--FIRST BODY DIMENSION TO BE GENERATED:                      C
C   ISTRT =-1 (AGE) FOR CHILD SUBJECTS                                  C
C   ISTRT =0 (WEIGHT) FOR ADULT SUBJECTS OR USER SUPPLIED DATA        C
C   VALUES ARE ALSO READ INTO PRED FOR THE PREDICTING VARIABLES       C
C-----C

```

```

SUBROUTINE DIALOG (IPTR,ICNT,ISTRT,ISUB)
COMMON /DIMS/ DD(-1:31),REGEQ(24,-1:31),PRED(-1:1),
&      RANGE(2,-1:1,3),CONV(-1:1)
COMMON /NAMES/ SUBTYP(10),SEGLAB(15),JNTLAB(14),PLTSYM(29),
&      DIMNM(-1:31),TITLE,UNITS(3,-1:2)
CHARACTER SUBTYP*35,SEGLAB*3,JNTLAB*2,PLTSYM*1,ANS*1,DIMNM*24
CHARACTER TITLE*60,UNITS*6
CHARACTER*12 FILE1
INTEGER IPTMAT(-1:2,3),IPT2(13)
EQUIVALENCE (IPTMAT,IPT2)
DATA IPT2 /1,3,5,7,11,11,13,15,18,18,20,22,25/

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```

WRITE (5,22)
READ (7,333) TITLE
WRITE (5,333) ' '//TITLE
WRITE (9,333) '1'//TITLE

```

```

10 READ (2,*) NUMTYP
   READ (2,*) (SUBTYP(I),I=1,NUMTYP)
   WRITE (5,33) (I,SUBTYP(I),I=1,NUMTYP)
   WRITE (5,44)
   READ (7,222) ISUB
   IF (ISUB.GT.NUMTYP .OR. ISUB.LT.1) GOTO 10
   WRITE (9,333) '0'//SUBTYP(ISUB)
   ISTRT = -1
   IF (ISUB.GT.1) ISTRT = 0
   IF (ISUB.EQ.4) GOTO 100
   IF (ISUB.GT.4) THEN
     IPTR = 0
     ICNT = 0
     ISTRT = 0
     RETURN
   ENDIF

20  WRITE (5,33) (I+1,DIMNM(I),I=ISTRT,1).3,'ALL OF THE ABOVE'
   WRITE (5,55)
   READ (7,222) IDIM

```

```

IDIM = IDIM - 1
IF (IDIM.LT.1STRT .OR. IDIM.GT.2) GOTO 20
IF (IDIM.GE.2) THEN
    LPSTRT = 1STRT
    LPEND = 1
ELSE
    LPSTRT = IDIM
    LPEND = LPSTRT
ENDIF

WRITE (9,555)
DO 50 I = LPSTRT,LPEND
    CALL ASKUN (DIMNM(1),UNITS(1,I),ICHOS,1STRT+3)
    IF (ICHOS.GE.3) THEN
        CALL PTILE (ISUB,I,PRED(I))
    ELSE
        TCONV = 1.
        IF (ICHOS.GE.2) TCONV = CONV(I)
40      WRITE (5,77) DIMNM(1),(RANGE(J,I,ISUB)/TCONV,J=1,2)
        READ (5,444) PRED(I)
        WRITE (9,666) DIMNM(1),PRED(I),UNITS(ICHOS,I)
        PRED(I) = PRED(I)*TCONV
        IF ((PRED(I)-RANGE(1,I,ISUB))*(PRED(I)-RANGE(2,I,ISUB))
&          .GT. 0.) GOTO 40
    ENDIF
50      CONTINUE

    IF (IDIM.LT.2) THEN
        PRED(-1) = PRED(IDIM)
    ELSE
        IF (ISUB.GT.1) THEN
            DO 60 I=-1,0
60          PRED(I) = PRED(I+1)
        ENDIF
    ENDIF

    IPTR = IPTMAT(IDIM,ISUB)
    ICNT = IPTMAT(IDIM+1,ISUB) - IPTR - 1
    RETURN

100  WRITE (5,88)
    READ (7,333) ANS
    IF (ANS.EQ.'N'.OR.ANS.EQ.'n') STOP 'FROM DIALOG'
    IF (ANS.NE.'Y'.AND.ANS.NE.'y') GOTO 100
    CLOSE (UNIT=4)
    OPEN (UNIT=4,FILE='GEBOD11.DIR',STATUS='OLD')
    READ (4,'(///A12)') FILE1
    OPEN (UNIT=1,FILE=FILE1,STATUS='OLD')
    READ (1,99) (DD(I),I=0,31)
    CLOSE (UNIT=1)
    IPTR = 25
    CALL ASKUN(SUBTYP(4),UNITS(1,2),ICHOS,2)
    IF (ICHOS.GE.2) THEN

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```

        DD(0) = DD(0)*CONV(0)
        DO 120 I=1,31
120      DD(I) = DD(I)*CONV(I)
        ENDIF
        RETURN

22      FORMAT (// ' PROGRAM GEBOD'/' GEBOD GENERATES BODY DESCRIPTION',
&          ' DATA'/' SUITABLE FOR INPUT TO THE ATB MODEL'/
&          ' PLEASE ENTER A DESCRIPTION OF THE SUBJECT' ,
&          ' (<60 CHARS.)')
33      FORMAT (//(I12,')',3X,A/))
44      FORMAT (' ENTER NUMBER CORRESPONDING TO DESIRED SUBJECT TYPE')
55      FORMAT (' ENTER NUMBER CORRESPONDING TO '/' PREDICTING',
&          ' DIMENSION(S) TO BE SUPPLIED')
77      FORMAT (' ENTER VALUE FOR ',A24/' IN THE RANGE ',G10.4,',',G10.4)
88      FORMAT (// ' TO UTILIZE EXTERNAL DIMENSIONAL DATA, THE DATA MUST',
&          ' BE'/' IN THE PROPER FORMAT AND IN A FILE ASSIGNED TO UNIT 1'/
&          ' HAS THE ABOVE BEEN SATISFIED (Y/N) ?')
99      FORMAT (8F10.0)
222     FORMAT (BN,I60)
333     FORMAT (A)
444     FORMAT (G60.0)
555     FORMAT ('OSELECTED BODY DIMENSIONS'/)
666     FORMAT (A40,G15.4,A6)
        END

```

```

C--SUBROUTINE ASKUN-----C
C   ASKUN ASKS USER CHOICE OF UNITS TO BE USED WITH SOME INPUT VARIABLE C
C   OR THE OUTPUT OF RESULTS.  THE PARAMETERS ARE THE FOLLOWING: C
C   VARB--CHARACTER STRING DESCRIBING WHAT UNITS ARE TO BE SELECTED FOR C
C   UNITS--UNITS AVAILABLE TO CHOOSE FROM C
C   ICHOS--RETURNS WHICH OF THE UNITS WAS CHOSEN C
C   ICNT--NUMBER OF DIFFERENT UNITS AVAILABLE TO CHOOSE FROM C
C-----C

```

```

SUBROUTINE ASKUN (VARB,UNITS,ICHOS,ICNT)
CHARACTER VARB*(*),UNITS(ICNT)*6,UNITIN*6

```

```

30  WRITE (5,66) VARB
    WRITE (5,55) (I,UNITS(I),I=1,ICNT)
    READ (7,44) ICHOS
    IF ( (ICHOS-1)*(ICHOS-ICNT) .GT. 0)   GOTO 30

```

```

    RETURN
44  FORMAT (BN,I60)
55  FORMAT (I10,')',5X,A)
66  FORMAT (// ' SELECT UNITS FOR ',A)
    END

```

```

C--SUBROUTINE PTILE-----C
C   PTILE COMPUTES A PERCENTILE POINT, SPECIFIED BY THE USER, OF A BODY   C
C   DIMENSION USED AS A PREDICTOR, BY ASSUMING THE DIMENSION IS          C
C   NORMALLY DISTRIBUTED.  THE PARAMETERS ARE THE FOLLOWING:              C
C   ISUB--SPECIFIES SUBJECT TYPE, AND THUS WHICH POSITION OF THE          C
C   MEAN AND STANDARD ARRAYS TO USE.                                     C
C   IDIM--THE DIMENSION A PERCENTILE POINT IS TO BE COMPUTED FOR          C
C   PRED--RETURNS THE COMPUTED PERCENTILE POINT                          C
C   NOTE:  THIS ROUTINE REQUIRES USE OF IMSL ROUTINE MDNRIS              C
C-----C

```

```

      SUBROUTINE PTILE (ISUB,IDIM,PRED)
      COMMON /NAMES/ SUBTYP(10),SEGLAB(15),JNTLAB(14),PLTSYM(29),
&          DIMNM(-1:31),TITLE,UNITS(3,-1:2)      80386
      REAL MEAN(0:1,2:3), STDEV(0:1,2:3)
      CHARACTER SUBTYP*35,SEGLAB*3,JNTLAB*2,PLTSYM*1,DIMNM*24      80386
      CHARACTER TITLE*60,UNITS*6
      DATA MEAN,STDEV/127.24,63.82,173.54,69.82,16.57,2.36,21.42,2.44/

10    WRITE (5,111) DIMNM(IDIM)
      READ (7,99) PCENT
      IF ( (PCENT-1.)*(PCENT-100.) .GE. 0.) GOTO 10
      WRITE (9,222) DIMNM(IDIM),PCENT
      PCENT = PCENT/100.

      CALL NDTRI (PCENT,X,D,IER)
      PRED = MEAN(IDIM,ISUB) + X*STDEV(IDIM,ISUB)

      RETURN
99    FORMAT (F40.0)
111   FORMAT (' ENTER DESIRED PERCENTILE FOR ',A/
&          ' (A REAL VALUE BETWEEN 0. AND 100.)')
222   FORMAT (A40,G15.4,'%-TILE')
      END

```

```

C--SUBROUTINE NDTRI-----C
C  NDTRI COMPUTES X (THE OUTPUT ARGUMENT SUCH THAT P=Y=THE      C
C  PROBABILITY THAT U, THE RANDOM VARIABLE, IS LESS THAN OR EQUAL  C
C  TO X.), D (THE OUTPUT DENSITY, F(X).), AND IER (THE OUTPUT      C
C  ERROR CODE.) USING P (THE INPUT PROBABILITY.).                C
C-----C

```

```

      SUBROUTINE NDTRI(P,X,D,IE)
C
      IE=0
      X=.999999E+38                      80386
      D=X
      IF(P)1,4,2
1     IE=-1
      GO TO 12
2     IF (P-1.0)7,5,1
4     X=-.999999E+38                      80386
5     D=0.0
      GO TO 12
C
7     D=P
      IF(D-0.5)9,9,8
8     D=1.0-D
9     T2=ALOG(1.0/(D*D))
      T=SQRT(T2)
      X=T-(2.515517+0.802853*T+0.010328*T2)/(1.0+1.432788*T+0.189269*T2
&  +0.001308*T*T2)
      IF(P-0.5)10,10,11
10    X=-X
11    D=0.3989423*EXP(-X*X/2.0)
12    RETURN
      END

```

C--SUBROUTINE CONTAC-----C  
 C     CONTAC COMPUTES JOINT LOCATIONS AND CONTACT ELLIPSOID SEMIAXES.     C  
 C-----C

```

SUBROUTINE CONTAC
COMMON /FLOAT/ PI,PI2,PI4,DENS,GRAV
COMMON /SGMNTS/ AN(15),BN(15),CN(15),RMN(15),PHI(3,15),XYZCG(15,3)
COMMON /JNTS/ RNJ(3,28),JNT(14),YPRLL(14,6),IPIN(14)
COMMON /DIMS/ DD(-1:31),REGEQ(24,-1:31),PRED(3),
&                RANGE(2,-1:1,3),CONV(-1:1)

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C     THE CENTERS OF GRAVITY AND JOINT X,Y COORDINATES ARE ALL SET TO ZERO.

```

DO 10 J=1,3
DO 10 I=1,15
10 XYZCG(I,J)=0.0
DO 20 J=1,2
DO 20 I=1,28
20 RNJ(J,I)=0.0

```

C     NON-ZERO X,Y JOINT COORDINATES ARE COMPUTED.

```

RNJ(1,21)=DD(29)*0.5
RNJ(1,24)=RNJ(1,21)
RNJ(2,5)=0.5*(DD(16)-DD(24)/PI)
RNJ(2,8)=-RNJ(2,5)
RNJ(2,11)=0.5*(DD(10)-DD(19)/PI)
RNJ(2,13)=-RNJ(2,11)

```

C     SMW IS ONE HALF THE HEIGHT OF THE ABDOMEN SEGMENT.

C     OLAP IS USED AS AN OVERLAP AMOUNT BETWEEN CERTAIN CONTACT ELLIPSOIDS.  
 SMW = (DD(2) - DD(4))/10.  
 OLAP = DD(9)/PI

C     Z COORDINATES OF JOINTS ARE COMPUTED RELATIVE TO SEGMENT JNT(J),

C     WHERE J IS THE SECOND SUBSCRIPT OF RNJ

```

RNJ(3,1) = (DD(1) - DD(5) - DD(4) + SMW)/2.
RNJ(3,2) = -SMW
RNJ(3,3) = -9.*SMW/2.
RNJ(3,4) = (DD(8) + DD(2) - DD(1) + OLAP/2.)/2.
RNJ(3,5) = (DD(4) - SMW - DD(1) + DD(5) - DD(24)/PI)/2.
RNJ(3,6)=0.5*(DD(1)-DD(5)-DD(23)+DD(24)/PI)
RNJ(3,7)=0.5*(DD(23)-DD(29)-DD(28)/PI2)
RNJ(3,8) = RNJ(3,5)
RNJ(3,9)=RNJ(3,6)
RNJ(3,10)=RNJ(3,7)
RNJ(3,11)=-DD(2)+DD(3)+DD(19)/PI2
RNJ(3,12)=0.5*(DD(17)-DD(20)/PI)
RNJ(3,13)=RNJ(3,11)
RNJ(3,14)=RNJ(3,12)

```

C     Z COORDINATES OF JOINTS ARE COMPUTED RELATIVE TO SEGMENT J-13,

C     WHERE J IS THE SECOND SUBSCRIPT OF RNJ  
 RNJ(3,15) = SMW



$RNJ(3,16) = -RNJ(3,3)$   
 $RNJ(3,17) = (DD(1) - DD(8) - DD(2) - OLAP/2.)/2.$   
 $RNJ(3,18) = DD(8)/2. + OLAP/4.$   
 $RNJ(3,19) = 0.5*(-DD(1)+DD(5)+DD(23)-DD(26)/PI)$   
 $RNJ(3,20) = (DD(29) - DD(23) - DD(28)/PI2 + DD(26)/PI)/2.$   
 $RNJ(3,21) = DD(28)/PI2 - DD(31)/2.$   
 $RNJ(3,22) = RNJ(3,19)$   
 $RNJ(3,23) = RNJ(3,20)$   
 $RNJ(3,24) = RNJ(3,21)$   
 $RNJ(3,25) = 0.5*(DD(19)/PI-DD(17))$   
 $RNJ(3,26) = 0.5*(DD(20)/PI-DD(18))$   
 $RNJ(3,27) = RNJ(3,25)$   
 $RNJ(3,28) = RNJ(3,26)$

C SEGMENT CONTACT ELLIPSOID X SEMIAXES ARE COMPUTED.

$AN(5) = DD(6)*0.5$   
 $AN(4) = DD(9)/PI2$   
 $AN(3) = DD(11)*0.5$   
 $AN(2) = DD(13)*0.5$   
 $AN(1) = DD(15)*0.5$   
 $AN(6) = (DD(24)+DD(25))/PI4$   
 $AN(7) = DD(27)/PI2$   
 $AN(8) = DD(29)*0.5$   
 $AN(9) = AN(6)$   
 $AN(10) = AN(7)$   
 $AN(11) = AN(8)$   
 $AN(12) = DD(19)/PI2$   
 $AN(13) = DD(21)/PI2$   
 $AN(14) = AN(12)$   
 $AN(15) = AN(13)$

C SEGMENT CONTACT ELLIPSOID Y SEMIAXES ARE COMPUTED.

$BN(5) = DD(7)*0.5$   
 $BN(4) = AN(4)$   
 $BN(3) = DD(12)*0.5$   
 $BN(2) = DD(14)*0.5$   
 $BN(1) = DD(16)*0.5$   
 $BN(6) = AN(6)$   
 $BN(7) = AN(7)$   
 $BN(8) = DD(30)*0.5$   
 $BN(9) = AN(9)$   
 $BN(10) = AN(10)$   
 $BN(11) = BN(8)$   
 $BN(12) = AN(12)$   
 $BN(13) = AN(13)$   
 $BN(14) = AN(14)$   
 $BN(15) = AN(15)$

C SEGMENT CONTACT ELLIPSOID Z SEMIAXES ARE COMPUTED.

$CN(5) = (DD(8) + OLAP/2.)/2.$   
 $CN(4) = (DD(1) - DD(8) - DD(2) + OLAP/2.)/2.$   
 $CN(3) = 9.*SMW/2.$

```

CN(2) = SMW + OLAP/2.
CN(1) = (DD(4)+DD(5)-DD(1) - SMW)*0.5
CN(6)=(DD(1)-DD(5)-DD(23)+DD(24)/PI+DD(26)/PI)*0.5
CN(7)=(DD(23)-DD(29)+DD(28)/PI2)*0.5
CN(8)=DD(31)*0.5
CN(9)=CN(6)
CN(10)=CN(7)
CN(11)=CN(8)
CN(12)=DD(17)*0.5
CN(13)=DD(18)*0.5
CN(14)=CN(12)
CN(15)=CN(13)

```

```

C   THE GLOBAL LOCATION OF SEGMENT CENTERS IS PLACED IN XYZCG FOR
C   SEGMENTS THAT WILL USE ELLIP IN COMPUTATION OF MASS AND
C   MOMENTS OF INERTIA.

```

```

XYZCG(1,3) = (DD(4) - SMW + D(1) - DD(5))/2.
XYZCG(2,3) = DD(4)
XYZCG(3,3) = DD(2) - 9.*SMW/2.
XYZCG(8,3) = DD(29) - DD(31)/2. + DD(28)/PI2
XYZCG(11,3) = XYZCG(8,3)

```

```

RETURN
END

```

```

C--SUBROUTINE SEGMA-----C
C  SEGMA COMPUTES APPROXIMATE SEGMENT MASSES.  WTCOR IS THEN COMPUTED  C
C  TO ADJUST BODY DENSITY, DENS, SO THAT TOTAL BODY MASS AGREES      C
C  WITH DD(0).  SEGMENT MASSES ARE THEN RECOMPUTED USING WTCOR.      C
C-----C

```

```

      SUBROUTINE SEGMA
C  EXTERNAL TORSO, FEET 80386
      COMMON /FLOAT/ PI,PI2,PI4,DENS,GRAV
      COMMON /CYL/ ZEES(0:15),ZH(15),NSEG(15),CGZ(15),WTCOR
      COMMON /JNTS/ RNJ(3,28),JNT(14),YPRLL(14,6),IPIN(14) 80386
      COMMON /SGMNTS/ ABCN(15,3),RMN(15),PHI(45),XYCG(30),ZCG(15)
      COMMON /DIMS/ DD(-1:31),REGEQ(24,-1:31),PRED(3),
&      RANGE(2,-1:1,3),CONV(-1:1) 80386
      REAL AN(15),BN(15),CN(15)
      EQUIVALENCE (AN,ABCN),(BN,ABCN(1,2)),(CN,ABCN(1,3))
      SUMM=0.0

C  POSITIONS 0 THRU 3 OF ZEES DEFINE THE VERTICAL LIMITS OF TORSO
C  SEGMENTS. 10 THRU 11 DEFINE THE LIMITS OF THE FEET.
      SMW = (DD(2) - DD(4))/10.
      ZEES(0) = DD(1) - DD(5)
      ZEES(1) = DD(4) - SMW
      ZEES(2) = DD(4) + SMW
      ZEES(3) = DD(2)
      ZEES(11) = DD(29) + DD(28)/PI2
      ZEES(10) = ZEES(11) - DD(31)
      DO 5 I = 1,3
        CALL ELLIP (I,1,RMN(I)) 80386
        ZCG(I) = CGZ(I) - ZCG(I)
5      SUMM = SUMM + RMN(I)
      CALL ELLIP (11,2,RMN(11)) 80386
      SUMM = SUMM + 2.*RMN(11)
      RMN(8) = RMN(11)
      ZCG(11) = CGZ(11) - ZCG(11)
      ZCG(8) = ZCG(11)
      DO 7 I = 1,3
6      RNJ(3,I) = RNJ(3,I) + ZCG(I)
      RNJ(3,15) = ZCG(2) + RNJ(3,15)
      RNJ(3,16) = ZCG(3) + RNJ(3,16)
      RNJ(3,5) = ZCG(1) + RNJ(3,5)
      RNJ(3,8) = ZCG(1) + RNJ(3,8)
      RNJ(3,11) = RNJ(3,11) + ZCG(3)
      RNJ(3,13) = RNJ(3,13) + ZCG(3)
      RNJ(3,21) = RNJ(3,21) + ZCG(8)
      RNJ(3,24) = RNJ(3,24) + ZCG(11)
      DO 10 I = 4,7
      RMN(I) = 4.0/3.0*PI*AN(I)*BN(I)*CN(I)*DENS
      SUMM = SUMM+RMN(I)
      IF (I.GT.5) THEN
        SUMM = SUMM + RMN(I)
        RMN(I+3) = RMN(I)

```

```

        ENDIF
10  CONTINUE
    DO 15 I = 12,13
        RMN(I) = 4.0/3.0*PI*AN(I)*BN(I)*CN(I)*DENS
        SUMM = SUMM+2.*RMN(I)
15  RMN(I+2) = RMN(I)
C
C      THE FOLLOWING ADJUSTS SEGMENT MASSES TO TOTAL BODY WEIGHT
C
        WTCOR = DD(0)/SUMM/GRAV
        DO 20 I=1,15
            RMN(I)=RMN(I)*WTCOR
20  CONTINUE
        RETURN
        END

```

```

C--SUBROUTINE SGINER-----C
C   SGINER COMPUTES SEGMENT MOMENTS OF INERTIA.                      C
C-----C

```

```

      SUBROUTINE SGINER
C   EXTERNAL TORSO, FEET                                           80386
      COMMON /FLOAT/ PI,PI2,PI4,DENS,GRAV                          80386
      COMMON /SGMNTS/ AN(15),BN(15),CN(15),RMN(15),PHI(3,15),XYZCG(15,3)80386

      DO 5 I=1,3
5       CALL ELLPMI (I,1,PHI(1,I))                                80386
      DO 10 I=4,7
      TEMP=RMN(I)/5.0
      A2=AN(I)*AN(I)
      B2=BN(I)*BN(I)
      C2=CN(I)*CN(I)
      PHI(1,I)=TEMP*(B2+C2)
      PHI(2,I)=TEMP*(A2+C2)
      PHI(3,I)=TEMP*(A2+B2)
      IF (I.GT.5) THEN
        DO 7 J = 1,3
7        PHI(J,I+3) = PHI(J,I)
      ENDIF
10      CONTINUE
      DO 20 I=12,13
      TEMP=RMN(I)/5.0
      A2=AN(I)*AN(I)
      B2=BN(I)*BN(I)
      C2=CN(I)*CN(I)
      PHI(1,I)=TEMP*(B2+C2)
      PHI(2,I)=TEMP*(A2+C2)
      PHI(3,I)=TEMP*(A2+B2)
      DO 15 J = 1,3
15      PHI(J,I+2) = PHI(J,I)
20      CONTINUE
      CALL ELLPMI (11,2,PHI(1,11))                                80386
      DO 25 J=1,3
25      PHI(J,8) = PHI(J,11)
      RETURN
      END

```

```

C--SUBROUTINE ELLIP-----C
C   ELLIP COMPUTES MASS AND CENTER OF GRAVITY LOCATION OF A RIGHT   C
C   ELLIPTICAL SOLID.  THE PARAMETERS ARE:                          C
C       ISEG--SPECIFIES SEGMENT BEING MODELLED BY RIGHT ELLIPTICAL SOLID   C
C       IABEVAL--SPECIFIES SUBROUTINE TO BE USED TO COMPUTE SEMIAXES OF THE   C
C           THE SOLID AT SPECIFIC Z HEIGHTS.                             C
C       TMASS--RETURNS THE MASS COMPUTED FOR THE SOLID.                C
C-----C

```

```

SUBROUTINE ELLIP (ISEG,IABEVAL,TMASS)                                80386
COMMON /CYL/ ZEES(0:15),ZH(15),NSEG(15),CGZ(15),WTCOR
COMMON /FLOAT/ PI,PI2,PI4,DENS,GRAV
REAL IXX,IXXP,IYY,IYYP,IZZ,IZZP
REAL MASS
REAL MI(3)
TMASSO=0.0
Z0 = ZEES(ISEG-1)
Z1 = ZEES(ISEG)
NSEG(ISEG)=0.0
10  NSEG(ISEG)=NSEG(ISEG)+10
TCGN=0.0
TMASS=0.0
ZH(ISEG)=(Z1-Z0)/FLOAT(NSEG(ISEG))
DO 100 I=1,NSEG(ISEG)
  Z = Z0 + (FLOAT(I-1)+.5)*ZH(ISEG)
  IF (IABEVAL.EQ.1) THEN                                           80386
    CALL TORSO(Z,A,B)                                             80386
  ELSE IF (IABEVAL.EQ.2) THEN                                     80386
    CALL FEET(Z,A,B)                                              80386
  ELSE                                                            80386
    STOP 'FROM ELLIP (IABEVAL)'                                  80386
  END IF                                                         80386
  MASS=PI*A*B*ZH(ISEG)*DENS
  CG=Z
  CGN=CG*MASS
  TMASS=TMASS+MASS
100 TCGN=TCGN+CGN
TMASSN=TMASS
IF (ABS(TMASSN-TMASSO)/TMASSN.GT.5.E-5) THEN
  TMASSO = TMASSN
  GOTO10
ENDIF
CGZ(ISEG)=TCGN/TMASS
RETURN

```

```

C ENTRY ELLPMI
C   ELLPMI COMPUTES MOMENTS OF INERTIA OF A RIGHT ELLIPTICAL SOLID, BASED
C   ON THE NUMERICAL INTEGRATION DETERMINED BY ELLIP.  THE FIRST TWO
C   PARAMETERS ARE THE SAME AS THOSE USED BY ELLIP.  THE THIRD, MI,
C   RETURNS THE MOMENTS OF INERTIA OF THE SOLID.

```

```

ENTRY ELLPMI (ISEG,IABEVAL,MI)                                80386

```

```

DO 5 I=1,3
5  MI(I)=0.0
   ZO = ZEES(ISEG-1)
   DO 200 I=1,NSEG(ISEG)
   Z = ZO + (FLOAT(I-1)+.5)*ZH(ISEG)
   IF (IABEVAL.EQ.1) THEN
CALL TORSO(Z,A,B)
ELSE IF (IABEVAL.EQ.2) THEN
CALL FEET(Z,A,B)
ELSE
STOP 'FROM ELLPMI (IABEVAL)'
END IF
MASS=PI*A*B*ZH(ISEG)*DENS*WTCOR
IXX=(MASS/12)*(3.0*B**2+ZH(ISEG)**2)
IYY=(MASS/12)*(3.0*A**2+ZH(ISEG)**2)
IZZ=(MASS/4.0)*(A**2+B**2)
DIST=Z-CGZ(ISEG)
IXXP=IXX+MASS*DIST**2
IYYP=IYY+MASS*DIST**2
IZZP=IZZ
MI(1)=MI(1)+IXXP
MI(2)=MI(2)+IYYP
MI(3)=MI(3)+IZZP
200 Z=Z+ZH(ISEG)
RETURN
END

```

80386  
80386  
80386  
80386  
80386  
80386  
80386

```

C--SUBROUTINE TORSO-----C
C   TORSO COMPUTES SEMIAXIS VALUES FOR THE RIGHT ELLIPTICAL MODEL OF THE   C
C   THREE TORSO SEGMENTS.  THE PARAMETERS ARE THE FOLLOWING:               C
C   Z--VERTICAL LOCATION AT WHICH THE SEMIAXES ARE TO BE COMPUTED          C
C   X--RETURNS X SEMIAXIS                                                  C
C   Y--RETURNS Y SEMIAXIS                                                  C
C-----C

```

```

      SUBROUTINE TORSO (Z,X,Y)
      COMMON /DIMS/ D(-1:31),REGEQ(24,-1:31),PRED(3),
&              RANGE(2,-1:1,3),CONV(-1:1)
      COMMON /FLOAT/ PI,PI2,PI4,DENS,GRAV
      REAL H2,H3,H4,H5,H6

```

80386  
80386  
80386

```

C   H2--TOP OF SOLID
C   H3--BREAK BETWEEN TOP SEMI-ELLIPSOID AND TOP FRUSTRUM
C   H4--BREAK BETWEEN TWO FRUSTRUM
C   H5--BREAK BETWEEN BOTTOM FRUSTRUM AND BOTTOM SEMI-ELLIPSOID
C   H6--BOTTOM OF SOLID

      H2=D(2)
      H3=D(3)
      H4=D(4)
      H5=(D(1)-D(5))+D(24)/PI2
      H6=(D(1)-D(5))
      IF (Z.LT.H4)THEN
        IF (Z.LT.H5)THEN
          IF (Z.LT.H6)STOP 'Z IS LESS THAN MIN.'
          Y= SQRT(1. - ((Z - H5)/D(24)/PI2)**2)
          X = D(15)/2.*Y
          Y = D(16)/2.*Y
        ELSE
          Y=(Z-D(4))/(H5-D(4))
          X = (Y*(D(15)-D(13)) +D(13))/2.
          Y = (Y*(D(16)-D(14)) +D(14))/2.
        END IF
      ELSE
        IF(Z.LT.H3)THEN
          Y=(Z-D(3))/(D(4)-D(3))
          X= (Y*(D(13)-D(11))+D(11))/2.
          Y= (Y*(D(14)-D(12))+D(12))/2.
        ELSE
          IF (Z.GT.H2) STOP 'Z IS GREATER THAN MAX.'
          Y=SQRT(1. - ((Z - D(3))/(D(2) - D(3)) )**2)
          X= Y*D(11)/2.
          Y= Y*D(12)/2.
        END IF
      END IF
      END

```



```

C--SUBROUTINE FEET-----C
C   FEET COMPUTES SEMIAXIS VALUES FOR THE RIGHT ELLIPTICAL MODEL OF THE C
C   FEET.  THE PARAMETERS ARE THE FOLLOWING: C
C   Z--Z LOCATION (TOE TO HEEL) AT WHICH SEMIAXES ARE TO BE COMPUTED C
C   X--RETURNS X SEMIAXIS C
C   Y--RETURNS Y SEMIAXIS C
C-----C

```

```

SUBROUTINE FEET (Z,X,Y)
COMMON /CYL/ ZEES(0:15),ZH(15),NSEG(15),CGZ(15),WTCOR
COMMON /DIHS/ DD(-1:31),REGEQ(24,-1:31),FRED(3),      80386
&   RANGE(2,-1:1,3),CONV(-1:1)      80386
COMMON /FLOAT/ PI,PI2,PI4,DENS,GRAY      80386

```

```

C   H2--TOP OF SOLID
C   H1--BREAK BETWEEN ELLIPTICAL CYLINDER AND FRUSTRUM
C   H0--BOTTOM OF SOLID

```

```

ANKR = DD(28)/PI2
H2 = DD(29) + ANKR
H1 = DD(29) - ANKR
H0 = H2 - DD(31)

```

```

IF (Z.GT.H1) THEN
  IF (Z.GT.H2) STOP 'Z VALUE TOO LARGE IN FEET'
  X = ANKR
  Y = ANKR
ELSE
  IF (Z.LT.H0) STOP 'Z VALUE TOO SMALL IN FEET'
  X = ANKR/(DD(31) - 2.*ANKR)*(Z - DD(29) + DD(31) - ANKR)
  Y = (ANKR - DD(30)/2.)/(DD(31) - 2.*ANKR)
  Y = Y*(Z - DD(29) + ANKR) + ANKR
ENDIF

```

```

RETURN
END

```

```

C--SUBROUTINE RESULTS-----C
C   RESULTS WRITES OUT THE COMPUTED BODY DESCRIPTION DATA.      C
C-----C

      SUBROUTINE RESULTS (ISTRT)
      COMMON /SGMNTS/ A(15),B(15),C(15),RMN(15),PHI(3,15),
&                XCG(15),YCG(15),ZCG(15)
      COMMON /JNTS/ RNJ(3,14,2),JNT(14),YPRLL(14,6),IPIN(14)
      COMMON /DIMS/ DD(-1:31),REGEQ(24,-1:31),PRED(3),
&                RANGE(2,-1:1,3),CONV(-1:1)
      COMMON /NAMES/ SUBTYP(10),SEGLAB(15),JNTLAB(14),PLTSYM(29),
&                DIMLAB(-1:31),TITLE,UNITS(3,-1:2)
      COMMON /CYL/ ZEES(0:15),ZH(15),NSEG(15),CGZ(15),WTCOR
      CHARACTER SUBTYP*35,SEGLAB*3,JNTLAB*2,PLTSYM*1,DIMLAB*24,TITLE*60
      CHARACTER ANS*1,UNITS*6,LABL1(2)*6,LABL2(2)*12,LABL3(2)*2,
&                LABL4(2)*4,VARB*6
      INTEGER ID2(14,3)
      DATA LABL1,LABL2,LABL3,LABL4 /'WEIGHT','MASS','LB-SEC**2-IN',
&    'N-SEC**2-M','IN.','M.','LB.','N.'/,VARB/'OUTPUT'/
      DATA ID2/6*0,2,0,0,2,0,2,0,2,6*0.3,0,0,3,0,3,0,3.6*0,
&    1,0,0,1,0,1,0,1/

      WRITE (9,11)
      CALL ASKUN (VARB,UNITS(1,2),IUN,2)
      CALL CNVRT (IUN)
      IF (ISTRT.LT.0) WRITE (9,22) -1,DIMLAB(-1),DD(-1),UNITS(1,-1)
      WRITE (9,22) 0,DIMLAB(0),DD(0),UNITS(IUN,0)
      WRITE (9,22) (I,DIMLAB(I),DD(I),UNITS(IUN,I),I=1,31)
      WRITE (9,66) WTCOR

      WRITE (9,44) '1'//TITLE
      WRITE(9,1170) LABL1(IUN),LABL2(IUN),LABL3(IUN),LABL3(IUN),
&                LABL4(IUN)
      WRITE(9,1180) (I,SEGLAB(I),PLTSYM(I),RMN(I),(PHI(J,I),J=1,3),
&                A(I),B(I),C(I),XCG(I),YCG(I),ZCG(I),I=1,15)
      WRITE(9,1190) LABL3(IUN),LABL3(IUN)
      WRITE(9,1200) (I,JNTLAB(I),PLTSYM(I+15),JNT(I),IPIN(I),
&                ((RNJ(J,I,K),J=1,3),K=1,2),(YPRLL(I,I),I=1,6),I=1,14)
      WRITE (9,201)

10    WR_      ,33)
      READ (9,44) ANS
      IF (ANS.EQ.'Y'.OR.ANS.EQ.'y') THEN
        WRITE (3,77) TITLE(1,52)
        WRITE(3,1300) (SEGLAB(I),PLTSYM(I),RMN(I),(PHI(J,I),J=1,3),
&                A(I),B(I),C(I),XCG(I),YCG(I),ZCG(I),I=1,15)
C      WRITE(3,1320) (JNTLAB(I),PLTSYM(I+15),JNT(I),IPIN(I),
&                ((RNJ(J,I,K),J=1,3),K=1,2),
&                (YPRLL(I,J),J=1,6),(ID2(I,J),J=1,3),I=1,14)
      ELSE
        IF (ANS.NE.'N'.AND.ANS.NE.'n') GOTO 10
      ENDIF

```

```

20  WRITE (5,55)
    READ (7,44) ANS
    IF (ANS.EQ.'N'.OR.ANS.EQ.'n')  STOP 'FROM RESULTS'      80386
    IF (ANS.NE.'Y'.AND.ANS.NE.'y')  GOTO 20                 80386
    RETURN

11  FORMAT ('-COMPUTED BODY DIMENSIONS'/)
22  FORMAT (I10,A30,G15.4,A6)
33  FORMAT (//' IS ATB MODEL FORMATTED OUTPUT DESIRED (Y/N) ?')
44  FORMAT (A)
55  FORMAT (//' IS IT DESIRED TO PRODUCE ANOTHER BODY DESCRIPTION ',
    &      'DATA SET (Y/N) ?')
66  FORMAT ('OWEIGHT CORRECTION FACTOR =',F10.3)
77  FORMAT (4X,'15',4X,'14',8X,A52,'CARD B.1')
1170 FORMAT(      1H0,"CRASH VICTIM PARAMETERS (3-D)"/1H0,33X,
    1 25HSEGMENT MOMENT OF INERTIA,
    2 19X,25HSEGMENT CONTACT ELLIPSOID/5X,7HSEGMENT,7X,A6
    3,15X,(' ',A12,')',17X,10HSEMIAXIS (,A2,')',14X,'CENTER (',
    4 A2,')'/3X,12HNO. SYM PLOT,4X,(' ',A4,')',10X,1HX,10X,1HY,10X,
    51HZ,12X,1HX,6X,1HY,6X,1HZ,12X,1HX,7X,1HY,6X,1HZ/1H )
1180 FORMAT ((3X,I2,2X,A4,A2,6X,F6.2,3X,3(4X,F7.5),5X,3(2X,F5.2),5X,3
    1(3X,F5.2)))
1190 FORMAT(1H0,///3X,5HJOINT,16X,'LOCATION(' ',A2,')' - SEG(JNT)',5X,
    1 'LOCATION(' ',A2,')' - SEG(J+1)',2X,'PRIN. AXIS(DEG) - SEG(JNT)',
    2 ' PRIN. AXIS(DEG) - SEG(J+1)'/2X,'J SYM PLOT JNT PIN',
    3 4X,2(1X,'X',8X,'Y',8X,'Z',8X),2('YAW',5X,'PITCH',5X,'ROLL',6X)/)
1200 FORMAT ((I3,A4,A3,2X,2I3,4(3F9.2,1X)))
1201 FORMAT(77X,'JOINTS RA, LA, RE, & LE ARE ORDERED PITCH, YAW, ROLL')REV1/87
1300 FORMAT(A4,A2,F6.2,3F6.4,6F6.3,6X,'CARD B.2')
1320 FORMAT(A4,1X,A1,2I4,6F6.2,22X,'CARD B.3'/14X,6F6.2,24X,3I2)      REV1/87

END

```

```

C--SUBROUTINE CNVRT-----C
C   CNVRT CONVERTS ALL OUTPUT DATA TO THE UNITS SELECTED BY THE USER   C
C-----C

```

```

      SUBROUTINE CNVRT (IUN)
      COMMON /SGMNTS/ ABC(15,3),RMN(15),PHI(3,15),XYZCG(15,3)
      COMMON /JNTS/  RNJ(3,28),JNT(14),YPRLL(14,6),IPIN(14)      80386
      COMMON /DIMS/  DD(-1:31),REGEQ(24,-1:31),PRED(3),          80386
&      RANGE(2,-1:1,3),CONVT(-1:1)                               80386
      REAL CONV(2,3)
      DATA CONV /1.,.0254,32.17405,143.1072,12.,106.2045/

      DO 100 I = 1,15
        DO 10 J = 1,3
          ABC(I,J) = ABC(I,J)*CONV(IUN,1)
          XYZCG(I,J) = XYZCG(I,J)*CONV(IUN,1)
10          PHI(J,I) = PHI(J,I)/CONV(IUN,3)
100         RMN(I) = RMN(I)*CONV(IUN,2)

      DO 200 I = 1,28
        DO 200 J = 1,3
200         RNJ(J,I) = RNJ(J,I)*CONV(IUN,1)

      IF (IUN.GT.1) THEN
        DD(0) = DD(0)/CONV(1,2)*CONV(2,2)
        DO 300 I=1,31
300         DD(I) = DD(I)*CONV(2,1)
      ENDIF

      RETURN
      END

```

```

C--SUBROUTINE RESULTZ(ISUB)-----C
C   RESULTZ WRITES OUT THE COMPUTED BODY DESCRIPTION DATA FOR ISUB GT 4.   C
C-----C

```

```

SUBROUTINE RESULTZ (ISUB)

COMMON /NAMES/ SUBTYP(10),SEGLAB(15),JNTLAB(14),PLTSYM(29),
&              DIMLAB(-1:31),TITLE,UNITS(3,-1:2)

CHARACTER ANS*1,UNITS*6,VARB*6,SUBTYP*35,SEGLAB*3,          80386
&          JNTLAB*2,PLTSYM*1,DIMLAB*24,TITLE*60,HEADER*30

VARB = 'OUTPUT'
CALL ASKUN (VARB,UNITS(1,2),IUN,2)
10 WRITE (5,33)
   READ (7,44) ANS
50 READ (2,*) NUMREC,HEADER
   IF (HEADER.NE.SUBTYP(ISUB)) THEN
      DO 30 I=1,NUMREC
         READ (2)
30    CONTINUE
      GOTO 50
   ELSE
      IF (IUN.EQ.2) THEN
         DO 40 I=1,NUMREC+1
            READ(2)
40    CONTINUE
      ENDIF
   ENDIF
   IF (ANS.EQ.'Y'.OR.ANS.EQ.'y') THEN          80386
      CALL ATBOUT (IUN)
   ELSE
      IF (ANS.EQ.'N'.OR.ANS.EQ.'n') THEN        80386
         CALL NOATBOUT (IUN)
      ELSE
         GOTO 10
      ENDIF
   ENDIF
20 WRITE (5,55)
   READ (7,44) ANS
   IF (ANS.EQ.'N'.OR.ANS.EQ.'n') STOP 'FROM RESULTZ'      80386
   IF (ANS.NE.'Y'.AND.ANS.NE.'y') GOTO 20                80386
   RETURN

33  FORMAT (// ' IS ATB MODEL FORMATTED OUTPUT DESIRED (Y/N) ? ' )
44  FORMAT (A)
55  FORMAT (// ' IS IT DESIRED TO PRODUCE ANOTHER BODY DESCRIPTION ',
&         ' DATA SET (Y/N) ? ' )

END

```

```

C--SUBROUTINE ATBOUT(IUN)-----C
C   ATBOUT WRITES OUT THE BODY DESCRIPTION DATA FOR ISUB GT 4           C
C   IN READABLE FORMAT AND ATB INPUT FORMAT                             C
C-----C

```

SUBROUTINE ATBOUT (IUN)

```

      CHARACTER SEG*4,JOINT(30)*4,CGS*1,JS*1,LABL2(2)*12,BLANK*4,
&          LABL3(2)*3,LABL4(2)*4,BDYTTL(5)*30,KTITLE(5)*20,
&          KTITLE2(5,50)*20
      INTEGER IDYPR(6),NS(3),JOINTF(30),NF(5),IPIN(30),
&          IGLOB(30),IFLAG(30)
      REAL YPRPMI(3),YPR1(3),YPR2(3),YPR3(3),ANG(3),THETA(50),
&          BD(6),PHI(3),SR(3,60),VISC(7),SPRING(5,90),X(30),
&          Y(30),F(50)

      DATA LABL2,LABL3,LABL4 /'LB-SEC**2-IN',' N-SEC**2-M ',
&          'IN.',' M.','LB.',' N.'/

      BLANK = ' '
      IPAGE = 1
C I/O CARDB.1
      READ (2,200) NSEG,NJNT,(BDYTTL(I),I=1,5)
      WRITE (3,300) NSEG,NJNT,(BDYTTL(I),I=1,5)
      WRITE (9,900) (BDYTTL(I),I=1,5),NSEG,NJNT,IPAGE
      WRITE (9, '(T121, 'CARDS B.1' )')
      IPAGE = IPAGE+1
C I/O B.2 CARDS
      WRITE (9,902)
      WRITE (9,904) LABL2(IUN),LABL3(IUN),LABL3(IUN)
      WRITE (9,906) LABL4(IUN)
      DO 1 I=1,NSEG
        READ (2,202) SEG,CGS,W,(PHI(J),J=1,3),
&          (BD(J),J=1,6),LPMI
        IF (IUN.EQ.1) THEN
          WRITE (3,302) SEG,CGS,W,(PHI(J),J=1,3),
&          (BD(J),J=1,6),LPMI
        ELSE
          IF (IUN.EQ.2) THEN
            WRITE (3,303) SEG,CGS,W,(PHI(J),J=1,3),
&          (BD(J),J=1,6),LPMI
          ENDIF
        ENDIF
      ENDIF
C I/O B.2.2 CARDS IF LPMI NE 0
      DO 14 M=1,3
14      YPRPMI(M) = 0.0
      IF (LPMI.NE.0) THEN
        READ (2,204) (YPRPMI(J),J=1,3)
        WRITE (3,304) (YPRPMI(J),J=1,3)
      ENDIF
      WRITE (9,908) I,SEG,CGS,W,(PHI(J),J=1,3),
&          (BD(J),J=1,6),(YPRPMI(J),J=1,3)

```

```

1 CONTINUE
C I/O B.3 CARDS IF NJNT NE 0
  IF (NJNT.EQ.0) GOTO 5
  WRITE (9,910)
  WRITE (9,912) LABL3(IUN),LABL3(IUN)
  WRITE (9,914)
  DO 2 J=1,NJNT
    READ(2,206) JOINT(J),JS,JNT,IPIN(J),
    & (SR(I,2*J-1),I-1,3),(SR(I,2*J),I-1,3),
    & ISLIP,C1,C2
    WRITE (3,306) JOINT(J),JS,JNT,IPIN(J),
    & (SR(I,2*J-1),I-1,3),(SR(I,2*J),I-1,3),
    & ISLIP,C1,C2
    READ (2,208) (YPR1(I),I-1,3),(YPR2(I),I-1,3),
    & (YPR3(I),I-1,3),(IDYPR(I),I-1,6)
    WRITE (3,308) (YPR1(I),I-1,3),(YPR2(I),I-1,3),
    & (YPR3(I),I-1,3),(IDYPR(I),I-1,6)
    WRITE (9,916) J,JOINT(J),JS,JNT,IPIN(J),
    & (SR(I,2*J-1),I-1,3),(SR(I,2*J),I-1,3),
    & (YPR1(I),I-1,3),(YPR2(I),I-1,3)
2 CONTINUE
C I/O B.4 CARDS
  WRITE (9,918) IPAGE
  IPAGE = IPAGE+1
  WRITE (9,'(T121, ''CARDS B.4'')')
  WRITE (9,920)
  WRITE (9,922) LABL3(IUN),LABL4(IUN),LABL3(IUN),LABL4(IUN)
  WRITE (9,924)
  WRITE (9,926)
  DO 3 J=1,NJNT
    READ (2,210) (SPRING(I,3*J-2),I-1,5),
    & (SPRING(I,3*J-1),I-1,5)
    WRITE (3,310) (SPRING(I,3*J-2),I-1,5),
    & (SPRING(I,3*J-1),I-1,5)
    WRITE (9,928) J,JOINT(J),(SPRING(I,3*J-2),I-1,5),
    & (SPRING(I,3*J-1),I-1,5)
C IF JOINT(J) J IS AN EULER JOINT(J), I/O ANOTHER CARD
  IFLAG(J) = 0
  IF (IABS(IPIN(J)).GE.5.AND.IABS(IPIN(J)).LE.7) THEN
    IF (ISLIP.EQ.0) IFLAG(J) = 1
  ELSE
    IF (IABS(IPIN(J)).EQ.4) THEN
      IFLAG(J) = 1
    ELSE
      IF (IPIN(J).LE.-8.AND.IPIN(J).GE.-10) IFLAG(J) = 1
    ENDIF
  ENDIF
  IF (IFLAG(J).EQ.1) THEN
    READ (2,210) (SPRING(I,3*J),I-1,5),
    & (ANG(I),I-1,3)
    WRITE (3,310) (SPRING(I,3*J),I-1,5),
    & (ANG(I),I-1,3)

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```

        WRITE (9,929) (SPRING(I,3*J),I-1,5)
C    &    (ANG(I),I-1,3)
        ENDIF
    3 CONTINUE
C I/O B.5 CARDS
    WRITE (9,(''-''',119X,' 'CARDS B.5'''))
    WRITE (9,930)
    WRITE (9,932)
    WRITE (9,934)
    WRITE (9,936) LABL3(IUN),LABL4(IUN),LABL3(IUN),
&LABL4(IUN),LABL3(IUN),LABL4(IUN),LABL3(IUN),LABL4(IUN)
    DO 4 J-1,NJNT
        READ (2,212) (VISC(I),I-1,7)
        WRITE (3,312) (VISC(I),I-1,7)
        WRITE (9,938) J,JOINT(J),(VISC(I),I-1,7)
C IF JOINT(J) J IS AN EULER JOINT(J), THEN I/O TWO MORE CARDS
        IF (IFLAG(J).EQ.1) THEN
            READ (2,212) (VISC(I),I-1,7)
            WRITE (3,312) (VISC(I),I-1,7)
            WRITE (9,939) (VISC(I),I-1,7)
            READ (2,212) (VISC(I),I-1,7)
            WRITE (3,312) (VISC(I),I-1,7)
            WRITE (9,939) (VISC(I),I-1,7)
        ENDIF
    4 CONTINUE
C I/O NJNTF FROM THE D.1 CARD
    5 READ (2,214) NJNTF
    WRITE (3,314) NJNTF
    WRITE (9,940) IPAGE
    IPAGE = IPAGE+1
    WRITE (9,942) NJNTF
C I/O E.1 CARDS
    NUM = 1
    6 READ (2,216) IONE,(KTITLE(I),I-1,5)
    WRITE (3,316) IONE,(KTITLE(I),I-1,5)
    IF (IONE.GT.50) GOTO 7
    IF (NUM.EQ.1) THEN
        WRITE (9,944) IPAGE
        IPAGE = IPAGE+1
        NUM = 2
    ELSE
        NUM = 1
        WRITE (9,('////////'))
    ENDIF
    WRITE (9,946) IONE,(KTITLE(I),I-1,5)
C READ E.2 CARD
    READ (2,218) D0,D1,D2,D3,D4
    WRITE (3,318) D0,D1,D2,D3,D4
    WRITE (9,948)
    WRITE (9,950) D0,D1,D2,D3,D4
C I/O E.3 AND E.4 CARDS
    IF (D1.EQ.0) THEN

```



```

C      F1 = 'CONSTANT'
      WRITE (9,960) D2
    ELSE
      IF (D1.LT.0) THEN
C      F1 = 'TABULAR'
      READ (2,220) NPI
      READ (2,218) (X(I),Y(I),I=1,NPI)
      WRITE (3,320) NPI
      WRITE (3,322) (X(I),Y(I),I=1,NPI)
      WRITE (9,952) NPI
      WRITE (9,962)
      WRITE (9,964) (X(I),Y(I),I=1,NPI)
C IF D2 = 0, F2 DOES NOT EXIST
      IF (D2.GT.0) THEN
C      F2 = 'POLYNOMIAL'
      READ (2,218) A0,A1,A2,A3,A4,A5
      IF (IUN.EQ.1) THEN
        WRITE (3,324) A0,A1,A2,A3,A4,A5
      ELSE
        WRITE (3,326) A0,A1,A2,A3,A4,A5
      ENDIF
      WRITE (9,958)
      WRITE (9,966)
      WRITE (9,968) A0,A1,A2,A3,A4,A5
    ENDIF
  ELSE
    IF (D1.GT.0) THEN
C    F1 = 'POLYNOMIAL'
    READ (2,218) A0,A1,A2,A3,A4,A5
    IF (IUN.EQ.1) THEN
      WRITE (3,324) A0,A1,A2,A3,A4,A5
    ELSE
      IF (IUN.EQ.2) THEN
        WRITE (3,326) A0,A1,A2,A3,A4,A5
      ENDIF
    ENDIF
    WRITE (9,954)
    WRITE (9,966)
    WRITE (9,968) A0,A1,A2,A3,A4,A5
    IF (D2.LT.0) THEN
C    F2 = 'TABULAR'
    READ (2,220) NPI
    READ (2,218) (X(I),Y(I),I=1,NPI)
    WRITE (3,320) NPI
    WRITE (3,322) (X(I),Y(I),I=1,NPI)
    WRITE (9,956) NPI
    WRITE (9,962)
    WRITE (9,964) (X(I),Y(I),I=1,NPI)
  ELSE
    IF (D2.GT.0) THEN
C    F2 = 'POLYNOMIAL'
    READ (2,218) A0,A1,A2,A3,A4,A5

```

```

        IF (IUN.EQ.1) THEN
            WRITE (3,324) A0,A1,A2,A3,A4,A5
        ELSE
            WRITE (3,326) A0,A1,A2,A3,A4,A5
        ENDIF
        WRITE (9,958)
        WRITE (9,966)
        WRITE (9,968) A0,A1,A2,A3,A4,A5 .
    ENDIF
ENDIF
ENDIF
ENDIF
ENDIF
GOTO 6
C I/O E.7 CARDS
7 IF (NJNTF.NE.0) THEN
    DO 8 I=1,NJNTF
        READ (2,216) ITWO,(KTITLE2(J,ITWO),J=1,5)
        WRITE (3,328) ITWO,(KTITLE2(J,ITWO),J=1,5)
        WRITE (9,944) IPAGE
        IPAGE = IPAGE+1
        WRITE (9,970) ITWO,(KTITLE2(J,ITWO),J=1,5)
        READ (2)
        WRITE (3)
        READ (2,222) NTHETA,NPHI
        WRITE (3,330) NTHETA,NPHI
        IF (NTHETA.GT.0) THEN
            DO 15 K=2,NTHETA
                THETA(K) = DFLOAT(K-1)*180.0/DFLOAT(NTHETA-1)
15          CONTINUE
                WRITE (9,972) NTHETA,NPHI
                WRITE (9,974)
                WRITE (9,976) (THETA(J),J=2,NTHETA)
                WRITE (9,('(' ' ' '))')
            ELSE
                IF (NTHETA.LT.0) THEN
                    NPOLY = -NTHETA-1
                    WRITE (9,978) NPOLY,NPHI
                    WRITE (9,980)
                    WRITE (9,982) (BLANK,J,J=1,NPOLY)
                    WRITE (9)
                ENDIF
            ENDIF
            NTHETE = IABS(NTHETA)
            PHIDEG = 360.0/DFLOAT(NPHI)
            DO 9 K=1,NPHI
                READ (2,218) THETA0,(F(J),J=2,NTHETE)
                WRITE (3,332) THETA0,(F(J),J=2,NTHETE)
                DEG = PHIDEG*DFLOAT(K-1) - 180.0
                WRITE (9,984) DEG,THETA0,(F(J),J=2,NTHETE)
9          CONTINUE
8          CONTINUE

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```

ENDIF
C I/O F.4 CARDS
C INITIALIZE IGLOB(J),J=1,18 SO 'CARD F.4' WILL PRINT OUT
DO 10 J=1,18
10 IGLOB(J) = 0
IF (NJNT.NE.0) THEN
  READ (2,224) (IGLOB(J),J=1,NJNT)
  WRITE (3,334) (IGLOB(J),J=1,18)
  IF (NJNT.GT.18) THEN
    WRITE (3,334) (IGLOB(J),J=19,NJNT)
  ENDIF
DO 11 J=1,NJNT
  IF (IGLOB(J).EQ.1) THEN
    READ (2,226) NJ,(NS(I),I=1,3),
&      (NF(I),I=1,5)
    WRITE (3,226) NJ,(NS(I),I=1,3),
&      (NF(I),I=1,5)
  ENDIF
11 CONTINUE
ENDIF
C I/O F.5 CARD
C INITIALIZE JOINTF(J),J=1,18 TO ZERO SO 'CARD F.5' WILL PRINT
DO 12 J=1,18
12 JOINTF(J) = 0
IF (NJNT.GT.0.AND.NJNTF.GT.0) THEN
  WRITE (9,986) IPAGE
  IPAGE = IPAGE+1
  READ (2,224) (JOINTF(J),J=1,NJNT)
  WRITE (3,336) (JOINTF(J),J=1,18)
  IF (NJNT.GT.18) THEN
    WRITE (3,336) (JOINTF(J),J=19,NJNT)
  ENDIF
DO 13 K=1,NJNT
  NUMF = JOINTF(K)
  IF (NUMF.NE.0) THEN
    WRITE (9,988) K,JOINT(K),NUMF,
&      (KTITLE2(I,NUMF),I=1,5)
  ENDIF
13 CONTINUE
ENDIF
C FINISHED CARD I/O
RETURN

200 FORMAT (2I6,8X,5A6)
202 FORMAT (A4,1X,A1,10F6.0,I4)
204 FORMAT (12X,3F6.0)
206 FORMAT (A4,1X,A1,2I4,6F6.0,I4,2F6.0)
208 FORMAT (14X,9F6.0,6I2)
210 FORMAT (2(4F6.0,F12.0))
212 FORMAT (F6.0,4F6.0,18X,2F6.0)
214 FORMAT (48X,I6)
216 FORMAT (I4,4X,5A4)

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218  FORMAT (6F12.0)
220  FORMAT (I6)
222  FORMAT (2I6)
224  FORMAT (18I4)
226  FORMAT (9I4)
300  FORMAT (2I6,8X,5A6,T73,'CARD B.1')
302  FORMAT (A4,1X,A1,F6.3,3F6.4,6F6.3,I4,T73,'CARD B.2')
303  FORMAT (A4,1X,A1,F6.2,3F6.4,6F6.3,I4,T73,'CARD B.2')
304  FORMAT (12X,2F6.2,F6.1)
306  FORMAT (A4,1X,A1,2I4,6F6.2,I4,2F6.2,T73,'CARD B.3')
308  FORMAT (14X,9F6.2,6I2)
310  FORMAT (2(4F6.2,F12.2),'CARD B.4')
312  FORMAT (F6.3,4F6.0,18X,2F6.0,T73,'CARD B.5')
314  FORMAT (48('X'),I6,6('X'),T73,'CARD D.1')
316  FORMAT (I4,4X,5A4,T73,'CARD E.1')
318  FORMAT (5F12.2,T73,'CARD E.2')
320  FORMAT (I6,66X,'CARD E.4')
322  FORMAT (6F12.2,'CARD E.4')
324  FORMAT (6F12.2,'CARD E.3')
326  FORMAT (6E12.5,'CARD E.3')
328  FORMAT (I4,4X,5A4,T73,'CARD E.7')
330  FORMAT (2I6,T73,'CARD E.7')
332  FORMAT (6F12.3,'CARD E.7')
334  FORMAT (18I4,'CARD F.4')
336  FORMAT (18I4,'CARD F.5')
900  FORMAT ('1 CRASH VICTIM      ',5A6,3X,I2,' SEGMENTS',3X,
&I2,' JOINTS',T124,'PAGE',I4)
902  FORMAT (T26,'PRINCIPAL MOMENTS OF INERTIA',T68,'SEGMENT',
&' CONTACT ELLIPSIOD',T121,'CARDS B.2')
904  FORMAT (T4,'SEGMENT',T17,'WEIGHT',T32,(' ',A12,')',T60,
&'SEMIAXES (' ',A4,')',T87,'CENTER (' ',A4,')',
&T111,'PRINCIPAL AXES (DEG)')
906  FORMAT (' I SYM PLOT      (' ',A4,')',T30,'X',T39,'Y',T48,
&'Z',T59,'X',T67,'Y',T75,'Z',T85,'X',T93,'Y',T101,'Z',
&T110,'YAW',T118,'PITCH',T128,'ROLL',/)
908  FORMAT (1X,I2,1X,A4,A3,F11.3,2X,3F9.4,2(2X,3F8.3),1X,3F9.2)
910  FORMAT ('-',T121,'CARDS B.3')
912  FORMAT (' JOINT',T24,'LOCATION(' ',A4,') - SEG(JNT)      ',
&'LOCATION(' ',A4,') - SEG(J+1) PRIN. AXIS(DEG) - SEG',
&'(JNT) PRIN. AXIS(DEG) - SEG(J+1)')
914  FORMAT (' J SYM PLOT PIN',T27,'X',T36,'Y',T45,'Z',T55,
&'X',T64,'Y',T73,'Z',T82,'YAW',T90,'PITCH',T100,'ROLL',
&T110,'YAW',T118,'PITCH',T128,'ROLL',/)
916  FORMAT (1X,I2,2A4,I5,I3,2(1X,3F9.3),2(1X,3F9.2))
918  FORMAT ('1 JOINT TORQUE CHARACTERISTICS',T124,'PAGE',
&I4)
920  FORMAT (T24,'FLEXURAL SPRING CHARACTERISTICS',T83,
&'TORSIONAL SPRING CHARACTERISTICS',/)
922  FORMAT (8X,2(7X,'SPRING COEF. (' ',2A4,'/DEG**J)',6X,
&'ENERGY',5X,'JOINT'))
924  FORMAT (' JOINT',2(9X,'LINEAR',4X,'QUADRATIC',5X,'CUBIC'
&,4X,'DISSIPATION STOP'))

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926  FORMAT (8X,2(8X,'(J-1)',7X,'(J-2)',7X,'(J-3)',7X,'COEF.',
&5X,'(DEG)'),/)
928  FORMAT (1X,I2,A4,2(3X,3F12.3,2F10.3))
929  FORMAT (10X,3F12.3,2F10.3)
930  FORMAT (T39,'JOINT VISCOUS CHARACTERISTICS AND LOCK-'
&,'UNLOCK CONDITIONS',/)
932  FORMAT (T15,'VISCOUS',T31,'COULOMB',T45,'FULL FRICTION',
&T63,'MAX TORQUE FOR',T81,'MIN TORQUE FOR',T99,'MIN. ',
&'ANG. VELOCITY',T123,'IMPULSE')
934  FORMAT (' JOINT',T13,'COEFFICIENT',T28,'FRICTION COEF. ',
&'ANGULAR VELOCITY',T63,'A LOCKED JOINT',T81,'UNLOCKED ',
&'JOINT',T121,'RESTITUTION')
936  FORMAT (T9,'(' ,2A4,' SEC/DEG)',T29,'(' ,2A4,')',T45,
&'(DEG/ SEC)',T65,'(' ,2A4,')',T83,'(' ,2A4,')',T103,
&'(RAD/ SEC)',T121,'COEFFICIENT',/)
938  FORMAT (1X,I2,A4,F14.3,2F15.2,4X,2F18.2,F20.2,F17.2)
939  FORMAT (7X,F14.3,2F15.2,4X,2F18.2,F20.2,F17.2)
940  FORMAT ('1',T6,'NPL',T13,'NBLT',T21,'NBAG',T29,'NELP',T39,
&'NQ',T46,'NSD',T51,'NHRNSS',T59,'NWINDF',T68,'NJNTF',
&T75,'NFORCE',T124,'PAGE',I4)
942  FORMAT (8(4X,'XXXX'),4X,I4,4X,'XXXX',T121,'CARD D.1')
944  FORMAT ('1',T124,'PAGE',I4)
946  FORMAT (' FUNCTION NO. ',I4,T22,5A4,T121,'CARDS E.1',/)
948  FORMAT (T11,'D0',T26,'D1',T41,'D2',T56,'D3',T71,'D4')
950  FORMAT (1X,F14.4,4F15.4)
952  FORMAT ('-',T8,'FIRST PART OF FUNCTION - ',I4,' TABULAR ',
&'POINTS',/)
954  FORMAT ('-',T8,'FIRST PART OF FUNCTION - 5TH DEGREE ',
&'POLYNOMIAL',/)
956  FORMAT ('-',T8,'SECOND PART OF FUNCTION - ',I4,' TABULAR ',
&'POINTS',/)
958  FORMAT ('-',T8,'SECOND PART OF FUNTION - 5TH DEGREE ',
&'POLYNOMIAL',/)
960  FORMAT ('-',T8,'FUNCTION IS CONSTANT ',F11.6)
962  FORMAT (T9,'0',T26,'F(0)')
964  FORMAT (1X,F14.6,F15.4)
966  FORMAT (T9,'A0',T24,'A1',T39,'A2',T54,'A3',T69,'A4',T84,
&'A5')
968  FORMAT (6E15.7)
970  FORMAT (5X,'JOINT FORCE FUNCTION NO. ',I4,T38,5A4,T121,
&'CARD E.7'//)
972  FORMAT ('- FUNCTION IS TABULAR FOR ',I2,' X ',I2,' VALUES',
&' OF THETA AND PHI',/)
974  FORMAT (T31,'THETA')
976  FORMAT (T6,'PHI',T14,'THETA0',F16.3,4F20.3/(15X,5F20.3))
978  FORMAT ('- FUNCTION IS COEFFICIENTS OF ',I2,' ORDER ',
&'POLYNOMIALS IN (THETA-THETA0) FOR ',I2,' VALUES OF PHI')
980  FORMAT ('0',T28,'COEFFICIENTS OF (THETA-THETA0)**N')
982  FORMAT (T6,'PHI',T14,'THETA0',7X,5(A4,'N =',I2,11X)/
&(25X,A4,'N =',I2,11X,A4,'N =',I2,11X,A4,'NX =',I2,11X,A4,
&'N =',I2,11X,A4,'N =',I2) )
984  FORMAT (F9.2,F10.3,5G20.7/(19X,5G20.7))

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```
986  FORMAT ('1',122X,'PAGE ',I4/120X,'CARD F.5'/  
&      ' THE FOLLOWING JOINT RESTORING FORCE FUNCTIONS AS DEFINED  
& ON CARDS E.7 WILL BE USED.'//4X,'JOINT',10X,'FUNCTION'//)  
988  FORMAT (I6,'-',A4,I10,'-',5A4)
```

END

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C--SUBROUTINE NOATBOUT(IUN)-----C
C   ATBOUT WRITES OUT THE BODY DESCRIPTION DATA FOR ISUB GT 4           C
C   IN READABLE FORMAT.                                                 C
C-----C

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# SUBROUTINE NOATEBOUT (IUN)

```

      CHARACTER SEG*4,JOINT(30)*4,CGS*1,JS*1,LABL2(2)*12,BLANK*4,
&          LABL3(2)*3,LABL4(2)*4,BDYTTL(5)*30,KTITLE(5)*20,
&          KTITLE2(5,50)*20
      INTEGER IDYPR(6),NS(3),JOINTF(30),NF(5),IPIN(30),
&          IGLOB(30),IFLAG(30)
      REAL YPRPMI(3),YPR1(3),YPR2(3),YPR3(3),ANG(3),THETA(50),
&          BD(6),PHI(3),SR(3,60),VISC(7),SPRING(5,90),X(30),
&          Y(30),F(50)

      DATA LABL2,LABL3,LABL4 /'LB-SEC**2-IN',' N-SEC**2-M ',
&          'IN.',' M.','LB.',' N.'/

      BLANK = ' '
      IPAGE = 1
C I/O CARDB.1
      READ (2,200) NSEG,NJNT,(BDYTTL(I),I=1,5)
      WRITE (9,900) (BDYTTL(I),I=1,5),NSEG,NJNT,IPAGE
      WRITE (9,('T121,','CARDS B.1'))
      IPAGE = IPAGE+1
C I/O B.2 CARDS
      WRITE (9,902)
      WRITE (9,904) LABL2(IUN),LABL3(IUN),LABL3(IUN)
      WRITE (9,906) LABL4(IUN)
      DO 1 I=1,NSEG
        READ (2,202) SEG,CGS,W,(PHI(J),J=1,3),
&          (BD(J),J=1,6),LPMI
C I/O B.2.2 CARDS IF LPMI NE 0
        DO 14 M=1,3
          14 YPRPMI(M) = 0.0
          IF (LPMI.NE.0) THEN
            READ (2,204) (YPRPMI(J),J=1,3)
          ENDIF
          WRITE (9,908) I,SEG,CGS,W,(PHI(J),J=1,3),
&          (BD(J),J=1,6),(YPRPMI(J),J=1,3)
        1 CONTINUE
C I/O B.3 CARDS IF N NT NE 0
      IF (NJNT.EQ.0) GOTO 5
      WRITE (9,910)
      WRITE (9,912) LABL3(IUN),LABL3(IUN)
      WRITE (9,914)
      DO 2 J=1,NJNT
        READ(2,206) JOINT(J),JS,JNT,IPIN(J),
&          (SR(I,2*J-1),I=1,3),(SR(I,2*J),I=1,3),
&          ISLIP,C1,C2
        READ (2,208) (YPR1(I),I=1,3),(YPR2(I),I=1,3),

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& (YPR3(I),I-1,3),(IDYPR(I),I-1,6)
WRITE (9,916) J,JOINT(J),JS,JNT,IPIN(J),
& (SR(I,2*J-1),I-1,3),(SP(I,2*J),I-1,3),
& (YPR1(I),I-1,3),(YPR2(I),I-1,3)
2 CONTINUE
C I/O B.4 CARDS
WRITE (9,918) IPAGE
IPAGE = IPAGE+1
WRITE (9,'(T121,''CARDS B.4'')')
WRITE (9,920)
WRITE (9,922) LABL3(IUN),LABL4(IUN),LABL3(IUN),LABL4(IUN)
WRITE (9,924)
WRITE (9,926)
DO 3 J=1,NJNT
READ (2,210) (SPRING(I,3*J-2),I-1,5),
& (SPRING(I,3*J-1),I-1,5)
WRITE (9,928) J,JOINT(J),(SPRING(I,3*J-2),I-1,5),
& (SPRING(I,3*J-1),I-1,5)
C IF JOINT(J) J IS AN EULER JOINT(J), I/O ANOTHER CARD
IFLAG(J) = 0
IF (IABS(IPIN(J)).GE.5.AND.IABS(IPIN(J)).LE.7) THEN
IF (ISLIP.EQ.0) IFLAG(J) = 1
ELSE
IF (IABS(IPIN(J)).EQ.4) THEN
IFLAG(J) = 1
ELSE
IF (IPIN(J).LE.-8.AND.IPIN(J).GE.-10) IFLAG(J) = 1
ENDIF
ENDIF
IF (IFLAG(J).EQ.1) THEN
READ (2,210) (SPRING(I,3*J),I-1,5),
& (ANG(I),I-1,3)
WRITE (9,929) (SPRING(I,3*J),I-1,5)
C & (ANG(I),I-1,3)
ENDIF
3 CONTINUE
C I/O B.5 CARDS
WRITE (9,'(''-''',119X,''CARDS B.5'')')
WRITE (9,930)
WRITE (9,932)
WRITE (9,934)
WRITE (9,936) LABL3(IUN),LABL4(IUN),LABL3(IUN),
&LABL4(IUN),LABL3(IUN),LABL4(IUN),LABL3(IUN),LABL4(IUN)
DO 4 J=1,NJNT
READ (2,212) (VISC(I),I-1,7)
WRITE (9,938) J,JOINT(J),(VISC(I),I-1,7)
C IF JOINT(J) J IS AN EULER JOINT(J), THEN I/O TWO MORE CARDS
IF (IFLAG(J).EQ.1) THEN
READ (2,212) (VISC(I),I-1,7)
WRITE (9,939) (VISC(I),I-1,7)
READ (2,212) (VISC(I),I-1,7)
WRITE (9,939) (VISC(I),I-1,7)

```



```

        ENDIF
    4 CONTINUE
C I/O NJNTF FROM THE D.1 CARD
    5 READ (2,214) NJNTF
      WRITE (9,940) IPAGE
      IPAGE = IPAGE+1
      WRITE (9,942) NJNTF
C I/O E.1 CARDS
      NUM = 1
    6 READ (2,216) IONE,(KTITLE(I),I=1,5)
      IF (IONE.GT.50) GOTO 7
      IF (NUM.EQ.1) THEN
        WRITE (9,944) IPAGE
        IPAGE = IPAGE+1
        NUM = 2
      ELSE
        NUM = 1
        WRITE (9,'(////////)')
      ENDIF
      WRITE (9,946) IONE,(KTITLE(I),I=1,5)
C READ E.2 CARD
      READ (2,218) D0,D1,D2,D3,D4
      WRITE (9,948)
      WRITE (9,950) D0,D1,D2,D3,D4
C I/O E.3 AND E.4 CARDS
      IF (D1.EQ.0) THEN
C          F1 = 'CONSTANT'
          WRITE (9,960) D2
      ELSE
          IF (D1.LT.0) THEN
C              F1 = 'TABULAR'
              READ (2,220) NPI
              READ (2,218) (X(I),Y(I),I=1,NPI)
              WRITE (9,952) NPI
              WRITE (9,962)
              WRITE (9,964) (X(I),Y(I),I=1,NPI)
C IF D2 = 0, F2 DOES NOT EXIST
              IF (D2.GT.0) THEN
C                  F2 = 'POLYNOMIAL'
                  READ (2,218) A0,A1,A2,A3,A4,A5
                  WRITE (9,958)
                  WRITE (9,966)
                  WRITE (9,968) A0,A1,A2,A3,A4,A5
              ENDIF
          ELSE
              IF (D1.GT.0) THEN
C                  F1 = 'POLYNOMIAL'
                  READ (2,218) A0,A1,A2,A3,A4,A5
                  WRITE (9,954)
                  WRITE (9,966)
                  WRITE (9,968) A0,A1,A2,A3,A4,A5
                  IF (D2.LT.0) THEN

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```

C          F2 = 'TABULAR'
          READ (2,220) NPI
          READ (2,218) (X(I),Y(I),I-1,NPI)
          WRITE (9,956) NPI
          WRITE (9,962)
          WRITE (9,964) (X(I),Y(I),I-1,NPI)
        ELSE
          IF (D2.GT.0) THEN
C          F2 = 'POLYNOMIAL'
          READ (2,218) A0,A1,A2,A3,A4,A5
          WRITE (9,958)
          WRITE (9,966)
          WRITE (9,968) A0,A1,A2,A3,A4,A5
        ENDIF
      ENDIF
    ENDIF
  ENDIF
GOTO 6
C I/O E.7 CARDS
  7 IF (NJNTF.NE.0) THEN
    DO 8 I=1,NJNTF
      READ (2,216) ITWO,(KTITLE2(J,ITWO),J-1,5)
      WRITE (9,944) IPAGE
      IPAGE = IPAGE+1
      WRITE (9,970) ITWO,(KTITLE2(J,ITWO),J-1,5)
      READ (2)
      READ (2,222) NTHETA,NPHI
      IF (NTHETA.GT.0) THEN
        DO 15 K=2,NTHETA
          THETA(K) = DFLOAT(K-1)*180.0/DFLOAT(NTHETA-1)
15      CONTINUE
          WRITE (9,972) NTHETA,NPHI
          WRITE (9,974)
          WRITE (9,976) (THETA(J),J-2,NTHETA)
          WRITE (9,('' '''))
        ELSE
          IF (NTHETA.LT.0) THEN
            NPOLY = -NTHETA-1
            WRITE (9,978) NPOLY,NPHI
            WRITE (9,980)
            WRITE (9,982) (BLANK,J,J-1,NPOLY)
            WRITE (9)
          ENDIF
        ENDIF
      NTHETE = IABS(NTHETA)
      PHIDEG = 360.0/DFLOAT(NPHI)
      DO 9 K=1,NPHI
        READ (2,218) THETA0,(F(J),J-2,NTHETE)
        DEG = PHIDEG*DFLOAT(K-1) - 180.0
        WRITE (9,984) DEG,THETA0,(F(J),J-2,NTHETE)
9      CONTINUE

```

```

      8  CONTINUE
      ENDIF
C I/O F.4 CARDS
C  INITIALIZE IGLOB(J),J-1,18 SO 'CARD F.4' WILL PRINT OUT
      DO 10 J-1,18
10   IGLOB(J) = 0
      IF (NJNT.NE.0) THEN
          READ (2,224) (IGLOB(J),J-1,NJNT)
          DO 11 J-1,NJNT
              IF (IGLOB(J).EQ.1) THEN
                  READ (2,226) NJ,(NS(I),I-1,3),
&                  (NF(I),I-1,5)
              ENDIF
          11  CONTINUE
      ENDIF
C I/O F.5 CARD
C  INITIALIZE JOINTF(J),J-1,18 TO ZERO SO 'CARD F.5' WILL PRINT
      DO 12 J-1,18
12   JOINTF(J) = 0
      IF (NJNT.GT.0.AND.NJNTF.GT.0) THEN
          WRITE (9,986) IPAGE
          IPAGE = IPAGE+1
          READ (2,224) (JOINTF(J),J-1,NJNT)
          DO 13 K-1,NJNT
              NUMF = JOINTF(K)
              IF (NUMF.NE.0) THEN
                  WRITE (9,988) K,JOINT(K),NUMF,
&                  (KTITLE2(I,NUMF),I-1,5)
              ENDIF
          13  CONTINUE
      ENDIF
C FINISHED CARD I/O
      RETURN

```

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200  FORMAT ('16,8X,5A6)
202  FORMAT (A4,1X,A1,10F6.0,I4)
204  FORMAT (12X,3F6.0)
206  FORMAT (A4,1X,A1,2I4,6F6.0,I4,2F6.0)
208  FORMAT (14X,9F6.0,6I2)
210  FORMAT (2(4F6.0,F12.0))
212  FORMAT (F6.0,4F6.0,18X,2F6.0)
214  FORMAT (48X,I5)
216  FORMAT (I4,4X,5A4)
218  FORMAT (6F12.0)
220  FORMAT (I6)
222  FORMAT (2I6)
224  FORMAT (18I4)
226  FORMAT (9I4)
900  FORMAT ('1 CRASH VICTIM      ',5A6,3X,I2,' SEGMENTS',3X,
&I2,' JOINTS',T124,' PAGE',I4)
902  FORMAT (T26,' PRINCIPAL MOMENTS OF INERTIA',T68,' SEGMENT',
&' CONTACT ELLIPSIOD',T121,' CARDS B.2')

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904  FORMAT (T4,'SEGMENT',T17,'WEIGHT',T32,'(' ,A12,')',T60,
&'SEMIAXES (' ,A4,')',T87,'CENTER (' ,A4,')',
&T111,'PRINCIPAL AXES (DEG)')
906  FORMAT (' I SYM PLOT (' ,A4,')',T30,'X',T39,'Y',T48,
&'Z',T59,'X',T67,'Y',T75,'Z',T85,'X',T93,'Y',T101,'Z',
&T110,'YAW',T118,'PITCH',T128,'ROLL',/)
908  FORMAT (1X,I2,1X,A4,A3,F11.3,2X,3F9.4,2(2X,3F8.3),1X,3F9.2)
910  FORMAT ('-',T121,'CARDS B.3')
912  FORMAT (' JOINT',T24,'LOCATION(' ,A4,') - SEG(JNT) ',
&'LOCATION(' ,A4,') - SEG(J+1) PRIN. AXIS(DEG) - SEG',
&'(JNT) PRIN. AXIS(DEG) - SEG(J+1)')
914  FORMAT (' J SYM PLOT PIN',T27,'X',T36,'Y',T45,'Z',T55,
&'X',T64,'Y',T73,'Z',T82,'YAW',T90,'PITCH',T100,'ROLL',
&T110,'YAW',T118,'PITCH',T128,'ROLL',/)
916  FORMAT (1X,I2,2A4,I5,I3,2(1X,3F9.3),2(1X,3F9.2))
918  FORMAT ('1 JOINT TORQUE CHARACTERISTICS',T124,'PAGE',
&I4)
920  FORMAT (T24,'FLEXURAL SPRING CHARACTERISTICS',T83,
&'TORSIONAL SPRING CHARACTERISTICS',/)
922  FORMAT (8X,2(7X,'SPRING COEF. (' ,2A4,')/DEG**J)',6X,
&'ENERGY',5X,'JOINT'))
924  FORMAT (' JOINT',2(9X,'LINEAR',4X,'QUADRATIC',5X,'CUBIC'
&,4X,'DISSIPATION STOP'))
926  FORMAT (8X,2(8X,'(J-1)',7X,'(J-2)',7X,'(J-3)',7X,'COEF.',
&5X,'(DEG)'),/)
928  FORMAT (1X,I2,A4,2(3X,3F12.3,2F10.3))
929  FORMAT (10X,3F12.3,2F10.3)
930  FORMAT (T39,'JOINT VISCOUS CHARACTERISTICS AND LOCK-'
&,'UNLOCK CONDITIONS',/)
932  FORMAT (T15,'VISCOUS',T31,'COULOMB',T45,'FULL FRICTION',
&T63,'MAX TORQUE FOR',T81,'MIN TORQUE FOR',T99,'MIN. ',
&'ANG. VELOCITY',T123,'IMPULSE')
934  FORMAT (' JOINT',T13,'COEFFICIENT',128,'FRICTION COEF. ',
&'ANGULAR VELOCITY',T63,'A LOCKED JOINT',T81,'UNLOCKED ',
&'JOINT',T121,'RESTITUTION')
936  FORMAT (T9,'(' ,2A4,') SEC/DEG)',T29,'(' ,2A4,')',T45,
&'(DEG/ SEC)',T65,'(' ,2A4,')',T83,'(' ,2A4,')',T103,
&'(RAD/ SEC)',T121,'COEFFICIENT',/)
938  FORMAT (1X,I2,A4,F14.3,2F15.2,4X,2F18.2,F20.2,F17.2)
939  FORMAT (7X,F14.3,2F15.2,4X,2F18.2,F20.2,F17.2)
940  FORMAT ('1',T6,'NPL',T13,'NBLT',T21,'NBAG',T29,'NELP',T39,
&'NQ',T46,'NSD',T51,'NHRNSS',T59,'NWINDF',T68,'NJNTF',
&T75,'NFORCE',T124,'PAGE',I4)
942  FORMAT (8(4X,'XXXX'),4X,I4,4X,'XXXX',T121,'CARD D.1')
944  FORMAT ('1',T124,'PAGE',I4)
946  FORMAT (' FUNCTION NO.',I4,T22,5A4,T121,'CARDS E.1',/)
948  FORMAT (T11,'D0',T26,'D1',T41,'D2',T56,'D3',T71,'D4')
950  FORMAT (1X,F14.4,4F15.4)
952  FORMAT ('-',T8,'FIRST PART OF FUNCTION - ',I4,' TABULAR ',
&'POINTS',/)
954  FORMAT ('-',T8,'FIRST PART OF FUNCTION - 5TH DEGREE ',
&'POLYNOMIAL',/)

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956  FORMAT ('-',T8,'SECOND PART OF FUNCTION - ',I4,' TABULAR ',
&'POINTS',/)
958  FORMAT ('-',T8,'SECOND PART OF FUNTION - 5TH DEGREE ',
&'POLYNOMIAL',/)
960  FORMAT ('-',T8,'FUNCTION IS CONSTANT ',F11.6)
962  FORMAT (T9,'0',T26,'F(0)')
964  FORMAT (1X,F14.6,F15.4)
966  FORMAT (T9,'A0',T24,'A1',T39,'A2',T54,'A3',T69,'A4',T84,
&'A5')
968  FORMAT (6E15.7)
970  FORMAT (5X,'JOINT FORCE FUNCTION NO. ',I4,T38,5A4,T121,
&'CARD E.7'//)
972  FORMAT ('- FUNCTION IS TABULAR FOR ',I2,' X ',I2,' VALUES',
&' OF THETA AND PHI',/)
974  FORMAT (T31,'THETA')
976  FORMAT (T6,'PHI',T14,'THETA0',F16.3,4F20.3/(15X,5F20.3))
978  FORMAT ('- FUNCTION IS COEFFICIENTS OF ',I2,' ORDER ',
&'POLYNOMIALS IN (THETA-THETA0) FOR ',I2,' VALUES OF PHI')
980  FORMAT ('0',T28,'COEFFIECIENTS OF (THETA-THETA0)**N')
982  FORMAT (T6,'PHI',T14,'THETA0',7X,5(A4,'N -',I2,11X)/
&(26X,A4,'N -',I2,11X,A4,'N -',I2,11X,A4,'N -',I2,11X,A4,
&'N -',I2,11X,A4,'N -',I2) )
984  FORMAT (F9.2,F10.3,5G20.7/(19X,5G20.7))
986  FORMAT ('1',122X,'PAGE ',I4/120X,'CARD F.5'/
&      ' THE FOLLOWING JOINT RESTORING FORCE FUNCTIONS AS DEFINED
& ON CARDS E.7 WILL BE USED.'//4X,'JOINT',10X,'FUNCTION'//)
988  FORMAT (I6,'-',A4,I10,'-',5A4)

      END

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APPENDIX I

386-ATB Program Listing

BLOCK DATA		REV IV	07/23/86	TWOPI
C	IMPLICIT REAL*8 (A-H,O-Z)			DECKA
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,			DECKA
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG			PAGE
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),			DECKA
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI			TWOPI
	COMMON/JBARTZ/ MNPL( 30),MNBLT( 8),MNSEG( 30),MNBAG( 6),			DECKA
*	MPL(3,5,30),MBLT(3,5,8),MSEG(3,5,30),MBAG(3,10,6),			DECKA
*	NTPL( 5,30),NTBLT( 5,8),NTSEG( 5,30)			DECKA
	COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),			DECKA
*	BLTTTL(5,8),PLTTL(5,30),BAGTTL(5,6),SEG(30),			DECKA
*	JOINT(30),CGS(30),JS(30)			DECKA
	REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTL,BAGTTL,SEG,JOINT			DECKA
	LOGICAL*1 CGS,JS			DECKA
	COMMON/FORCES/PSF(7,70),BSF(4,20),SSF(10,40),BAGSF(3,20),			NCFORC
*	PRJNT(7,30),NPANEL(5),NPSF,NBSF,NSSF,NBGSF			DECKA
	COMMON/RSAGE/ XSG(3,20,3),DPMI(3,3,30),LPMI(30),			ATBIII
*	NSG(9),MSG(20,9),MCG,MCGIN(24,5),KREF(20,9)			TTHKREF
	COMMON/CDINT/ UU(4),GH(3,4),			DECKA
*	E(3,240),FF(5,240),GG(5,240),Y(5,240),U(5,240),			DECKA
*	H,HPRINT,TSAGE,TPRINT,ISTART,ICNT,IDBL,IFLAG,LDMMY			80386
	COMMON/DAMPER/ APSDM(3,20),APSDN(3,20),ASD(5,20),MSDM(20),MSDN(20)			DECKA
	COMMON/HRNESS/ BAR(15,100),BB(100),BBDOT(100),PLOSS(2,100),			DECKA
*	XLONG(20),HTIME(2),IBAR(5,100),NL(2,100),			DECKA
*	NPTSPB(20),NPTPLY(20),NTHRNS(20),NBLTPH(5)			DECKA
C	NOTE: FF REPLACES F.			DECKA
	LOGICAL*1 FREE,LDMMY			80386
	COMMON/TEMPVS/ JTMPVS(24000),FREE(30),LDMMY(2),DDMY(23109)			80386
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),			DECKA
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)			DECKA
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),			SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),			DECKA
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)			DECKA
	COMMON/CNTRSF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)			EDGE
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)			BUTLER2
	COMMON/VPOSTN/ ZPLT(3),SPLT(3),AXV(3,6),VATAB(6,501,6),			VEHICL
*	VTO(6),VDT(6),TIMEV(6),OMEGV(6),NVTAB(6),INDXV(6)			DECKA
	COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),			DECKA
*	F(3,30),TQ(3,30),WJ(30),A11(3,3,30)			SLIP
	COMMON/CEULER/ IEULER(30),HIR(3,3,90),ANG(3,30),ANGD(3,30),			JDRIFT
*	FE(3,30),TQE(3,30),CONST(5,30)			JDRIFT
	COMMON/FLXBLE/ HF(4,12,8),B42(3,3,24),V4(3,8),NFLEX(3,8)			DECKA
	COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24),			DECKA
*	HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12),			DECKA
*	RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12),			DECKA
*	KQ1(12),KQ2(12),KQTYPE(12)			DECKA
	COMMON/TEMPVI/ CREST,TTI(3),R1I(3),R2I(3),JSTOP(4,2,30)			DECKA
	COMMON/INTEST/ SGTEST(3,4,30),XTEST(3,120),SEGT(120),REGT(120)			DECKA
	REAL SEGT			DECKA
	COMMON/COMAIN/ VAR(240),DER(240),DT,H0,HMAX,HMIN,RSTIME,			DECKA
*	ISTEP,NSTEPS,NDINT,NEQ,IRSIN,IRSOUT			DECKA

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COMMON/ABDATA/ ZDEP(3,5),DBR(3,3,5),DPVCTR(3,5),DEPLOY(3,5),      DECKA
*              AB(3,5),B(9,4,5),ZR(3,4,5),BFB(3,4,5),DRR(9,4,5),    DECKA
*              VBAGG(5),VSCS(5),SPRK(5),CK(5),CMASS(5),CYMIN(5),     DECKA
*              CYMOUT(5),BAGPV(5),PD(5),VBAG(5),VOLBP(5),           DECKA
*              PCYV(5),PCYMIN(5),PVBAG(5),TV1(3,4,5),TV2(3,10,5),   DECKA
*              SWITCH(5),PYMOUT(5),SCALE(5),PREVT,IFULL(6)          DECKA
COMMON/CYDATA/ CYTD(5),CYP(5),CYSP(5),CYT0(5),CYV0(5),CYCD(5),      DECKA
*              CYK(5),CYR(5),CYAT(5),CYPV(5),CYCD0(5),CYA0(5),      DECKA
*              CYP0(5),CYSS(5),CYL0(5),CYC(5),CYRHO0(5),CYVMAX(5),  DECKA
*              CYORFC(5),CYRHO(5),CYT(5),CYP(5),CYV(5)             DECKA
COMMON/WINDFR/ WTIME(30),QFU(3,5),QFV(3,5),WF(3,30),IWIND(30),      WINDOP
*              MWSEG(7,30),NFWSEG(6),NFWNT(5),MOWSEG(30,30)         WINDOP
END                                                                    DECKA

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C		MAINA
C	AAMRL ARTICULATED TOTAL BODY (ATBIV) MODEL COMPUTER PROGRAM	ATBIV
C	DEVELOPED BY CALSPAN CORP. AND J&J TECHNOLOGIES INC.	BUTLER1
C		REV IV 07/23/86TWOPI
C	80386 IMPLEMENTATION BY KETRON, INC. - OCTOBER 31, 1989	80386
C	MAIN PROGRAM	MAINA
C		MAINA
C	PERFORMS CARD INPUT, PROGRAM INITIALIZATION,	MAINA
C	CONTROL OF INTEGRATION LOOP AND OPTIONAL OUTPUT.	MAINA
C		MAINA
	IMPLICIT REAL*8(A-H,O-Z)	MAINA
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,	MAINA
	* NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	PAGE
	COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),	MAINA
	* BLTTTL(5,8),PLTTL(5,30),BAGTTL(5,6),SEG(30),	MAINA
	* JOINT(30),CGS(30),JS(30)	MAINA
	REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTL,BAGTTL,SEG,JOINT	MAINA
	LOGICAL*1 CGS,JS	MAINA
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),	MAINA
	* UNITL,UNITM,UNITT,GRAVITY(3),TWOPI	TWOPI
	COMMON/COMAIN/ VAR(240),DER(240),DT,HO,HMAX,HMIN,RSTIME,	MAINA
	* ISTEP,NSTEPS,NDINT,NEQ,IRSIN,IRSOUT	MAINA
	LOGICAL NPRT1,NPRT2,NPRT3	MAINA
	COMMON/DEVICE/ IDEF,IOPORT,MODEL	80386
	CHARACTER*12 FILE1,FILE2,FILE3,FILE4,FILE5,FILE6,FILE8,FILE20	80386
	CHARACTER*1 CHR	80386
	CALL ELTIME(1, 1)	MAINA
C		PECONV
C	MAKE THE OUTPUT FILES PRINTER CONTROL FILES FOR THE P&E	PECONV
C		PECONV
	OPEN (UNIT=14,FILE='ATBIV.DIR',STATUS='OLD')	80386
	READ (14,'(6(A12/),A12)')FILE1,FILE2,FILE3,FILE4,FILE5,FILE6,FILE8	80386
	READ (14,'(2(I4/),I4)')IDEF,IOPORT,MODEL	80386
	OPEN (UNIT=5,FILE=FILE5,STATUS='OLD')	80386
	OPEN (UNIT=6,FILE=FILE6,STATUS='NEW',CARRIAGE CONTROL='FORTRAN')	80386
C	CALL CARCON(6,1)	80386
C	CALL CARCON(2,1)	80386
C		MA*NA
C	WRITE PROLOGUE ON PRIMARY OUTPUT UNIT.	MAINA
C		MAINA
	NPG-2	PAGE
	WRITE(6,11)	MAINA
	11 FORMAT(1H1,30X,'AAMRL ARTICULATED TOTAL BODY (ATB) MODEL',52X,	ATBIV
	* 'PAGE 1'////	PAGE
	* 31X,'DEVELOPED BY CALSPAN CORP., P.O. BOX 400, BUFFALO NY 14225'/	BUTLER1
	* 31X,'AND BY J&J TECHNOLOGIES INC., ORCHARD PARK, NY 14127' //	EDGE
	* 31X,'FOR THE AIR FORCE ARMSTRONG AEROSPACE MEDICAL RESEARCH ' /	VEHICL
	* 31X,'LABORATORY, WRIGHT PATTERSON AIR FORCE BASE ' /	ATBIV
	* 31X,'UNDER CONTRACTS F33615-75C-5002,-78C-0516 AND -80C-05117' //	BUTLER1
	* 31X,'AND FOR THE NATIONAL HIGHWAY TRAFFIC SAFETY ADMINISTRATION,'	BUTLER1
	* /31X,'U.S. DEPARTMENT OF TRANSPORTATION, UNDER CONTRACTS' /	BUTLER1
	* 31X,'FH-11-7592, HS-053-2-485, HS-6-01300 AND HS-6-01410.' ////	BUTLER1

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* 31X,'PROGRAM DOCUMENTATION: NHTSA REPORT NOS. DOT-HS-801-507' / BUTLER1
* 31X,'THROUGH 510 (FORMERLY CALSPAN REPORT NO. ZQ-5180-L-1),' / BUTLER1
* 31X,'AVAILABLE FROM NTIS (ACCESSION NOS. PB-241692,3,4 AND 5),' / BUTLER1
* 31X,'APPENDIXES A-J TO THE ABOVE (AVAILABLE FROM CALSPAN),' / BUTLER1
* 31X,'AND REPORT NOS. AMRL-TR-75-14 (NTIS NO. AD-A014 816),' / ATBIV
* 31X,'AFAMRL-TR-80-14 (NTIS NO. AD-A088 029), AND' / ATBIV
* 31X,'AFAMRL-TR-83-073 (NTIS NO. AD-B079 184).'////
* 31X,'PROGRAM ATB-IV 80386 IMPLEMENTATION COMPLETED BY KETRON,'/ 80386
* 31X,'OCTOBER 31, 1989, UNDER CONTRACT F33615-88-C-0543'////) 80386
C * 31X,'PROGRAM ATB-IV, EXECUTED ON THE AAMRL/BB CONCURRENT' / 80386
C * 31X,'3250 COMPUTER, WRIGHT-PATTERSON AFB, OHIO'////) 80386
C MAINA
C INPUT CARDS A.1 AND A.2, TEST FOR RESTART. MAINA
C MAINA
C CALL BLKDTA MAINA
  READ(5,12) DATE,IRSIN,IRSOUT,RSTIME,COMENT MAINA
12 FORMAT(3A4,2I4,F8.0/20A4/20A4) MAINA
  WRITE(6,13) DATE,IRSIN,IRSOUT,RSTIME,COMENT MAINA
13 FORMAT(////4X,3A4,' IRSIN=',I4,' IRSOUT=',I4,' RSTIME =',F8.4, MAINA
  * 61X,'CARDS A'//1X,20A4/1X,20A4//) MAINA
  IF (IRSIN.NE.0) 80386
  * OPEN (UNIT=4, FILE=FILE4, STATUS='OLD', FORM='UNFORMATTED') 80386
  IF (IRSOUT.NE.0) 80386
  * OPEN (UNIT=3, FILE=FILE3, STATUS='NEW', FORM='UNFORMATTED') 80386
  IF (IRSIN.NE.0) GO TO 18 MAINA
C MAINA
C INPUT CARDS A.3,A.4 AND A.5. MAINA
C MAINA
C READ(5,14) UNITL,UNITM,UNITT,GRAVITY,G MAINA
14 FORMAT(3A4,4F12.0) MAINA
  IF (G.EQ.0.0) G = DSQRT(GRAVITY(1)**2+GRAVITY(2)**2+GRAVITY(3)**2) MAINA
  READ(5,15) NDINT,NSTEPS,DT,HO,HMAX,HMIN,NPRT MAINA
15 FORMAT(2I4,4F8.0/36I2) MAINA
  WRITE(6,16) UNITL,UNITM,UNITT,GRAVITY,G, CHGIII
  * NDINT,NSTEPS,DT,HO,HMAX,HMIN MAINA
16 FORMAT(5X,'UNITL = ',A4,5X,'UNITM = ',A4,5X,'UNITT = ',A4, CHGIII
  * 5X,'GRAVITY VECTOR = (' ,F9.4,' ,',F9.4,' ,',F9.4,' )',5X,'G = ' CHGIII
  * F9.4,/,5X,'NDINT = ',I4,5X,'NSTEPS = ',I5,5X,'DT = ',F8.6, MAINA
  * 5X,'HO = ',F8.6,5X,'HMAX = ',F8.6,5X,'HMIN = ',F8.6) MAINA
  WRITE(6,17) (I,I=1,36),NPRT MAINA
17 FORMAT('O NPRT ARRAY'/3X,36I3/3X,36I3) MAINA
  NPRT4 = NPRT(4) MAINA
  IF(NPRT(25).GT.6) STOP 93 TGMOD1
  IF (NPRT(4).NE.0) 80386
  * OPEN (UNIT=8, FILE=FILE8, STATUS='NEW', FORM='UNFORMATTED') 80386
  IF (NPRT(4).LT.0) GO TO 50 MAINA
  IF (NPRT(4).EQ.0.OR.NPRT(4).EQ.1.OR.NPRT(4).EQ.4) THEN 80386
    READ (14, '(A12)', END=38) FILE20 80386
    IDOT=INDEX(FILE20, '.') 80386
    IF(IDOT.LT.2.OR.IDOT.GT.9)GO TO 38 80386
    CHR=FILE20(IDOT+2:IDOT+2) 80386
    IF(LLT(CHR,'0').OR.LGT(CHR,'9'))GO TO 38 80386

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	CHR=FILE20(IDOT+3:IDOT+3)	80386
	IF(LLT(CHR,'0').OR.LGT(CHR,'9'))GO TO 38	80386
	READ(FILE20(IDOT+2:IDOT+3),'(I2)')IMULT	80386
	IF(IMULT.LT.21.OR.IMULT.GT.85)GO TO 38	80386
	DO 37 II=21,IMULT	80386
	WRITE(FILE20(IDOT+2:IDOT+3),'(I2)')II	80386
	OPEN (UNIT=II,FILE=FILE20,STATUS='NEW',	80386
	* CARRIAGE CONTROL='FORTRAN')	80386
37	CONTINUE	80386
	ENDIF	80386
38	CONTINUE	80386
	IF (NPRT(1).NE.0)	80386
	* OPEN (UNIT=1,FILE=FILE1,STATUS='NEW',FORM='UNFORMATTED')	80386
	IF (NPRT(5).NE.0.OR.NPRT(6).NE.0.OR.NPRT(7).NE.0)	80386
	* OPEN (UNIT=2,FILE=FILE2,STATUS='NEW',CARRIAGE CONTROL='FORTRAN')	80386
C		MAINA
C	CALL INPUT ROUTINES	MAINA
C		MAINA
	CALL BINPUT	MAINA
	CALL VINPUT	MAINA
	CALL SINPUT	MAINA
	CALL CINPUT	MAINA
C		MAINA
C	PROGRAM INITIALIZATION	MAINA
C		MAINA
	TIME = 0.0	MAINA
	CALL INITAL	MAINA
	GO TO 19	MAINA
C		MAINA
C	READ INPUT DATA FROM RESTART TAPE AND WRITE NEW TAPE.	MAINA
C	THE FIVE FUNCTIONS OF SUBROUTINE RSTART ARE:	MAINA
C	1. READ INPUT & INITIALIZATION RECORD FROM OLD RESTART TAPE.	MAINA
C	2. WRITE INPUT & INITIALIZATION RECORD ONTO NEW RESTART TAPE.	MAINA
C	3. READ TIME POINT RECORD FROM OLD RESTART TAPE.	MAINA
C	4. READ NEW INPUT DATA FROM INPUT STREAM FOR RESTART.	MAINA
C	5. WRITE TIME POINT RECORD ONTO NEW RESTART TAPE.	MAINA
C		MAINA
18	CALL RSTART(1,IRSIN)	MAINA
	CALL RSTART(4,5)	MAINA
	NPRT4 = NPRT(4)	MAINA
19	IF (IRSOUT.NE.0) CALL RSTART(2,IRSOUT)	MAINA
C		MAINA
C	INTEGRATION LOOP - ADVANCE TIME BY EITHER INTEGRATING THROUGH	MAINA
C	SUBROUTINE DINT OR BY FETCHING TIME POINT RECORD FROM RESTART TAPE	MAINA
C		MAINA
	TIME = 0.0	MAINA
	ISTEP = 0	MAINA
20	IF (IRSIN.EQ.0) GO TO 23	MAINA
	IF (TIME.GT.RSTIME+0.5*DT) GO TO 23	MAINA
	IF (DABS(TIME-RSTIME).LT.0.5*DT) GO TO 21	MAINA
	CALL RSTART(3,IRSIN)	MAINA
	GO TO 24	MAINA

21	CALL RSTART(4,5)	MAINA
	IF (NPRT(4).LT.0) GO TO 50	MAINA
23	CALL DINT	MAINA
C		MAINA
C	OPTIONAL OUTPUT	MAINA
C	1. PRINTER PLOT ON OUTPUT UNIT 2 CONTROLLED BY NPRT(5) & (6).	MAINA
C		MAINA
24	CALL PRIPLT	MAINA
C		MAINA
C	2. RESTART DATA ON UNIT IRSOUT CONTROLLED BY IRSOUT # 0.	MAINA
C		MAINA
	IF (IRSOUT.NE.0) CALL RSTART(5,IRSOUT)	MAINA
C		MAINA
C	3. SUBROUTINE PRINT ON PRIMARY OUTPUT UNIT CONTROLLED BE NPRT(3).	MAINA
C		MAINA
	NPRT3 = (NPRT(3).EQ.1)	MAINA
	IF (NPRT(3).GT.1) NPRT3 = (MOD(ISTEP,NPRT(3)).EQ.0)	MAINA
	IF (NPRT3) CALL PRINT(6HMAIN3D)	MAINA
C		MAINA
C	4. PROGRAM VIEW PLOT DATA ON UNIT 1 CONTROLLED BY NPRT(1).	MAINA
C		MAINA
	NPRT1 = (NPRT(1).EQ.1)	MAINA
	IF (NPRT(1).GT.1) NPRT1 = (MOD(ISTEP,NPRT(1)).EQ.0)	MAINA
	IF (NPRT1) CALL UNIT1(0)	MAINA
C		MAINA
C	5. SUBROUTINE ELTIME ON PRIMARY OUTPUT UNIT CONTROLLED BY NPRT(2).	MAINA
C		MAINA
	NPRT2 = (NPRT(2).EQ.1)	MAINA
	IF (NPRT(2).GT.1) NPRT2 = (MOD(ISTEP,NPRT(2)).EQ.0)	MAINA
	IF (NPRT2) CALL ELTIME(NPG,1)	PAGE
C		MAINA
C	END OF INTEGRATION LOOP.	MAINA
C		MAINA
	ISTEP = ISTEP+1	MAINA
	IF (ISTEP.LE.NSTEPS) GO TO 20	MAINA
C		MAINA
C	6. SUBROUTINE POSTPR ON PRIMARY OUTPUT UNIT CONTROLLED BY NPRT(4).	MAINA
C		MAINA
50	IF (NPRT4 GT.0) END FILE 8	MAINA
	IF (NPRT(4).EQ.0 .OR. NPRT(4).EQ.4) GO TO 60	MAINA
	PRDT = 1000.0*DT	MAINA
	CALL POSTPR (PRDT)	MAINA
	IF (NPRT2) CALL ELTIME(NPG,1)	PAGE
C		MAINA
C	7. END OF RUN - CALL ELTIME IF NOT CALLED ABOVE.	MAINA
C		MAINA
60	IF (.NOT.NPRT2) CALL ELTIME(NPG,1)	PAGE
	STOP 1	MAINA
	END	MAINA

	SUBROUTINE ADJUST (M,D1)		ADJUST
C		REV IV 07/23/86	TWOPI
	IMPLICIT REAL*8 (A-H,O-Z)		ADJUST
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),		ADJUST
	* UNITL,UNITH,UNITT,GRAVITY(3),TWOPI		TWOPI
	COMMON/CDINT/ UU(4),GH(3,4),		ADJUST
	* E(3,240), F(5,240),GG(5,240),Y(5,240),U(5,240),		ADJUST
	* H,HPRINT,HS,TPRINT,TSTART,ICNT,IDBL,IFLAG,IDMMY		80386
	COMMON/COMAIN/ VAR(240),DER(240),DT,H0,HMAX,HMIN,RSTIME,		ADJUST
	* ISTEP,NSTEPS,NDINT,NEQ,IRSIN,IRSOUT		ADJUST
	IF (M.NE.1) GO TO 12		ADJUST
C			ADJUST
C	M = 1:		ADJUST
C			ADJUST
	DO 11 I=1,NEQ		ADJUST
	W = VAR(I) - GG(1,I)		ADJUST
	Z = DER(I) - GG(2,I)		ADJUST
	ZZ = Z - GG(5,I)*W - GG(3,I)*UU(3) - GG(4,I)*UU(4)		ADJUST
	GG(3,I) = GG(3,I) + ZZ*UU(1)		ADJUST
	GG(4,I) = GG(4,I) + ZZ*UU(2)		ADJUST
	Y(1,I) = VAR(I)		ADJUST
11	Y(2,I) = DER(I)		ADJUST
	GO TO 99		ADJUST
12	IF (M.EQ.3) GO TO 23		ADJUST
C			ADJUST
C	M = 2,4,5:		ADJUST
C			ADJUST
	H1 = EPS(1)/H		ADJUST
	N2 = NEQ/2		ADJUST
	DO 20 I=1,NEQ,3		ADJUST
	ZA = 0.0		ADJUST
	IF (I.LE.N2) GO TO 20		ADJUST
	IF (M.EQ.4) GO TO 16		ADJUST
	VARX = VAR(I) - Y(1,I)		ADJUST
	VARY = VAR(I+1) - Y(1,I+1)		ADJUST
	VARZ = VAR(I+2) - Y(1,I+2)		ADJUST
	DERX = DER(I) - Y(2,I)		ADJUST
	DERY = DER(I+1) - Y(2,I+1)		ADJUST
	DERZ = DER(I+2) - Y(2,I+2)		ADJUST
	GO TO 17		ADJUST
16	VARX = VAR(I) - U(1,I)		ADJUST
	VARY = VAR(I+1) - U(1,I+1)		ADJUST
	VARZ = VAR(I+2) - U(1,I+2)		ADJUST
	DERX = DER(I) - U(2,I)		ADJUST
	DERY = DER(I+1) - U(2,I+1)		ADJUST
	DERZ = DER(I+2) - U(2,I+2)		ADJUST
17	U(3,I) = U(3,I) + VARX*DERX + VARY*DERY + VARZ*DERZ		ADJUST
	U(4,I) = U(4,I) + VARX**2 + VARY**2 + VARZ**2		ADJUST
	IF (U(4,I).EQ.0.0) GO TO 18		FIXADJ
	ZA = H1		FIXADJ
	IF (U(3,I).LT.H1*U(4,I)) ZA = U(3,I)/U(4,I)		FIXADJ
18	GG(5,I+2) = ZA		FIXADJ

	GG(5,I+1) = ZA	ADJUST
20	GG(5,I) = ZA	ADJUST
	GO TO (99,21,99,23,25),M	ADJUST
C		ADJUST
C	M = 2:	ADJUST
C		ADJUST
21	DO 22 I=1,NEQ	ADJUST
	ZA = GG(5,I)	ADJUST
	Y1 = Y(4,I) - ZA*Y(3,I)	ADJUST
	Y2 = GG(2,I) - ZA*GG(1,I)	ADJUST
	Y3 = DER(I) - ZA*VAR(I)	ADJUST
	GG(3,I) = -Y1*GH(1,1) + Y2*GH(2,1) + Y3*GH(3,1)	ADJUST
	GG(4,I) = Y1*GH(1,2) - Y2*GH(2,2) + Y3*GH(3,2)	ADJUST
	Y(1,I) = 0.5*(Y(1,I)+VAR(I))	ADJUST
22	Y(2,I) = 0.5*(Y(2,I)+DER(I))	ADJUST
	GO TO 99	ADJUST
C		ADJUST
C	M = 3,4:	ADJUST
C		ADJUST
23	DO 24 I=1,NEQ	ADJUST
	ZA = GG(5,I)	ADJUST
	Y1 = GG(2,I) - ZA*GG(1,I)	ADJUST
	Y2 = Y(2,I) - ZA*Y(1,I)	ADJUST
	Y3 = DER(I) - ZA*VAR(I)	ADJUST
	GG(3,I) = -Y1*GH(1,3) + Y2*GH(2,3) - Y3*GH(3,3)	ADJUST
	GG(4,I) = Y1*GH(1,4) - Y2*GH(2,4) + Y3*GH(3,4)	ADJUST
	U(1,I) = VAR(I)	ADJUST
24	U(2,I) = DER(I)	ADJUST
	GO TO 99	ADJUST
C		ADJUST
C	M = 5:	ADJUST
C		ADJUST
25	DO 26 I=1,NEQ	ADJUST
	ZA = GG(5,I)	ADJUST
	Y1 = GG(2,I) - ZA*GG(1,I)	ADJUST
	Y2 = DER(I) - ZA*VAR(I)	ADJUST
	Y3 = U(2,I) - ZA*U(1,I)	ADJUST
	GG(3,I) = -Y1*GH(1,3) + Y2*GH(2,3) - Y3*GH(3,3)	ADJUST
	GG(4,I) = Y1*GH(1,4) - Y2*GH(2,4) + Y3*GH(3,4)	ADJUST
	Y(1,I) = VAR(I)	ADJUST
26	Y(2,I) = DER(I)	ADJUST
99	RETURN	ADJUST
	END	ADJUST

	SUBROUTINE AIRBAG	AIRBAG
		REV IV 07/24/86SLIP
C	AIRBAG ROUTINE CALLED BY SUBROUTINE CONTCT TO DETERMINE THE INTER-AIRBAG	AIRBAG
C	ACTION OF THE BAG WITH REACTION PANELS AND BODY SEGMENTS BY USE OFAIRBAG	AIRBAG
C	SUBROUTINE BGG. THE DIFFERENTIAL PRESSURE, FORCE AND TORQUE ON THE AIRBAG	AIRBAG
C	BAG IS EVALUATED AND THE RESULTING FORCE AND TORQUE ON THE BODY	AIRBAG
C	SEGMENTS ARE ADDED TO THE U1 AND U2 ARRAYS.	AIRBAG
C		AIRBAG
	IMPLICIT REAL*8 (A-H,O-Z)	AIRBAG
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,	AIRBAG
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),	AIRBAG
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)	AIRBAG
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),	SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),	AIRBAG
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)	AIRBAG
	COMMON/JBARTZ/ MNPL( 30),MNBLT( 8),MNSEG( 30),MNBAG( 6),	AIRBAG
*	MPL(3,5,30),MBLT(3,5,8),MSEG(3,5,30),MBAG(3,10,6),	AIRBAG
*	NTPL( 5,30),NTBLT( 5,8),NTSEG( 5,30)	AIRBAG
	COMMON/FORCES/PSF(7,70),BSF(4,20),SSF(10,40),BAGSF(3,20),	NCFORC
*	PRJNT(7,30),NPANEL(5),NPSF,NBSF,NSSF,NBGSF	AIRBAG
	COMMON/CNTRSF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)	EDGE
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),	AIRBAG
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI	TWOPI
	COMMON/ABDATA/ ZDEP(3,5),DBR(3,3,5),DPVCTR(3,5),DEPLOY(3,5),	AIRBAG
*	AB(3,5),B(9,4,5),ZR(3,4,5),BFB(3,4,5),DRR(9,4,5),	AIRBAG
*	VBAGG(5),VSCS(5),SPRK(5),CK(5),CMASS(5),CYMIN(5),	AIRBAG
*	CYMOUT(5),BAGPV(5),PD(5),VBAG(5),VOLBP(5),	AIRBAG
*	PCYV(5),PCYMIN(5),PVBAG(5),TV1(3,4,5),TV2(3,10,5),	AIRBAG
*	SWITCH(5),PYMOUT(5),SCALE(5),PREVT,IFULL(6)	AIRBAG
	COMMON/CYDATA/ CYTD(5),CYPA(5),CYSP(5),CYTO(5),CYVO(5),CYCD(5),	AIRBAG
*	CYK(5),CYR(5),CYAT(5),CYPV(5),CYCDO(5),CYA0(5),	AIRBAG
*	CYPO(5),CYSS(5),CYLO(5),CYC(5),CYRH00(5),CYVMAX(5),	AIRBAG
*	CYORFC(5),CYRHO(5),CYT(5),CYP(5),CYV(5)	AIRBAG
	COMMON/TEMPVS/ TMP(9),TMP1(3),TORQ(3),FORCE(3,5),TORA(3,5),	AIRBAG
*	TQB(3,10),FRB(3,10),VOL(10),DELF(3),VOLP(4,5),FRA(4,5)	AIRBAG
*	,DDMY(34955)	80386
C	NOTE: THIS COMMON/TEMPVS/ IS SHARED BY AIRBAG AND AIRBGG.	AIRBAG
	CALL ELTIME(1,24)	AIRBAG
	DELT = TIME-PREVT	AIRBAG
	NBGSF = 0	AIRBAG
	DO 70 J=1,NBAG	AIRBAG
	IF (MNBAG(J).EQ.0) GO TO 70	AIRBAG
	IF (IFULL(J).LE.0) GO TO 69	AIRBAG
	CALL AIRBGG(J)	AIRBAG
C		AIRBAG
C	COMPUTE CMOUT: MASS FLOW OUT OF BAG	AIRBAG
C	BAGPV: UNDISTORTED BAG VOLUME	AIRBAG
C		AIRBAG
	IF (PD(J).GT.CYPV(J)) CYMOUT(J) = PYMOUT(J)	AIRBAG
*	+ DELT*CYORFC(J)*DSQRT(PD(J))	AIRBAG
	BAGPV(J) = CYPA(J)*((CYMIN(J)-CYMOUT(J))*SWITCH(J))*CYK(J)	AIRBAG

C		AIRBAG
C	BAG IS FULLY INFLATED, COMPUTE DIFFERENTIAL PRESSURE	AIRBAG
C		AIRBAG
	PD(J) = BAGPV(J)/(VBAG(J)-VOLBP(J))*CYK(J) - CYP(A(J)	AIRBAG
	JB = NVEH + J	AIRBAG
	KP = NPANEL(J)	AIRBAG
	KBAG = MNBAG(J)	AIRBAG
C		AIRBAG
C	OPTIONAL DIAGNOSTIC OUTPUT	AIRBAG
C		AIRBAG
	IF (NPRT(21).NE.0) WRITE(6,41)	AIRBAG
	* ((FRB(I,K),I-1,3),(TQB(I,K),I-1,3),K-1,KBAG),(FORCE(I,J),I-1,3),	AIRBAG
	* (TORA(I,J),I-1,3),TORQ,((FRA(I,K),I-1,3),VOLP(K,J),K-1,KP),	AIRBAG
	* (VOL(K),K-1,KBAG),VOLBP(J),CYMOUT(J),BAGPV(J),PD(J)	AIRBAG
41	FORMAT ('OAIRBAG CONTCT'/(1X,9G14.6))	AIRBAG
	IF (PD(J).LT.0.0) PD(J) = 0.0	AIRBAG
	IF (PD(J).EQ.0.0) GO TO 46	AIRBAG
C		AIRBAG
C	SET UP BAGSF ARRAY FOR OUTPUT ROUTINE	AIRBAG
C		AIRBAG
	KBGSF = NBGSF+5	AIRBAG
	DO 42 K=1,KP	AIRBAG
	KBGSF = KBGSF+1	AIRBAG
	DO 42 I=1,3	AIRBAG
42	BAGSF(I,KBGSF) = PD(J)*FRA(I,K)	AIRBAG
	DO 45 I=1,KBAG	AIRBAG
	KBGSF = KBGSF+1	AIRBAG
	IF (VOL(I).EQ.0.0) GO TO 45	AIRBAG
	M = MBAG(2,I,J)	AIRBAG
C		AIRBAG
C	FINAL COMPUTATIONS OF FORCE AND TORQUE ON AIRBAG	AIRBAG
C		AIRBAG
	DO 44 K=1,3	AIRBAG
	FRB(K,I) = PD(J)*FRB(K,I)	AIRBAG
	BAGSF(K,KBGSF) = FRB(K,I)	AIRBAG
	U1(K,M) = U1(K,M) - FRB(K,I)	AIRBAG
44	U2(K,M) = U2(K,M) + PD(J)*TQB(K,I)	AIRBAG
45	CONTINUE	AIRBAG
46	DO 47 K=1,3	AIRBAG
	FORCE(K,J) = PD(J)*FORCE(K,J)	AIRBAG
47	TORA (K,J) = PD(J)*TORA (K,J)	AIRBAG
	IF (VOLP(1,J).NE.0.0) GO TO 55	AIRBAG
C		AIRBAG
C	AIRBAG IS NOT INTERSECTING PRIMARY REACTION PANEL.	AIRBAG
C	COMPUTE ARTIFICIAL FORCE AND TORQUE WITH A LINEAR SPRING FUNCTION	AIRBAG
C	IN AN ATTEMPT TO TIE +X SEMIAXIS ENDPOINT OF AIRBAG TO DEPLOYMENT	AIRBAG
C	POINT ON REACTION PANEL.	AIRBAG
C		AIRBAG
	DO 51 K=1,3	AIRBAG
51	TMP(K) = BFB(K,1,J) + ZDEP(K,J)	AIRBAG
	CALL DOT31 (D(1,1,NVEH),TMP,TMP1)	AIRBAG
	DO 52 K=1,3	AIRBAG



	DELF(K) = TMP1(K) + SEGLP(K,NVEH) - SEGLP(K,JB)	AIRBAG
52	TMP(K) = BD(K+3,JB)	AIRBAG
	TMP(1) = TMP(1) + BD(1,JB)	AIRBAG
	CALL DOT31 (D(1,1,JB),TMP,TMP1)	AIRBAG
	DO 53 K=1,3	AIRBAG
	DELF(K) = SPRK(J)*(DELF(K)-TMP1(K))	AIRBAG
	BAGSF(K,NBGSF+5) = DELF(K)	AIRBAG
53	FORCE(K,J) = FORCE(K,J) + DELF(K)	AIRBAG
	CALL MAT31 (D(1,1,JB),DELF,TMP1)	AIRBAG
	CALL CROSS (TMP,TMP1,DELF)	AIRBAG
	DO 54 K=1,3	AIRBAG
54	TORA(K,J) = TORA(K,J) + DELF(K)	AIRBAG
55	XDD = CYMIN(J) - CYMOUT(J) + W(JB)	AIRBAG
	FMASS = CMASS(J)*XDD/G	AIRBAG
	TMASS = CMASS(J)*(XDD+W(JB)*2.0/3.0)/G	AIRBAG
	DO 56 I=1,3	AIRBAG
56	TMP(I) = WMEG(I,JB)*PHI(I,JB)	AIRBAG
	CALL CROSS (WMEG(1,JB),TMP,TMP1)	AIRBAG
	DO 57 I=1,3	AIRBAG
	SEGLA(I,JB) = FORCE(I,J)/FMASS + GRAVITY(I)	AIRBAG
57	WMEGD(I,JB) = (TORA(I,J)/TMASS-TMP1(I))*RPHI(I,JB)	AIRBAG
69	NBGSF = NBGSF + 5 + NPANEL(J) + MNBAG(J)	AIRBAG
70	CONTINUE	AIRBAG
	CALL ELTIME(2,24)	AIRBAG
	RETURN	AIRBAG
	END	AIRBAG

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C      SUBROUTINE AIRBGG(J)
C
C      REV III.5 10/17/85EDGE
C      CALLED BY SUBROUTINES AIRBAG AND AIRBG3 TO COMPUTE VOLUMES OF
C      INTERSECTION BETWEEN AIRBAGS AND PANELS AND SEGMENTS.
C
C      IMPLICIT REAL*8 (A-H,O-Z)
C      COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,
*      NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG
C      COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),
*      SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)
C      COMMON/JBARTZ/ MNPL( 30),MNBLT( 8),MNSEG( 30),MNBAG( 6),
*      MPL(3,5,30),MBLT(3,5,8),MSEG(3,5,30),MBAG(3,10,6),
*      NTPL( 5,30),NTBLT( 5,8),NTSEG( 5,30)
C      COMMON/FORCES/PSF(7,70),BSF(4,20),SSF(10,40),BAGSF(3,20),
*      PRJNT(7,30),NPANEL(5),NPSF,NBSF,NSSF,NBSGF
C      COMMON/CNTRSF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)
C      COMMON/ABDATA/ ZDEP(3,5),DBR(3,3,5),DPVCTR(3,5),DEPLOY(3,5),
*      AB(3,5),B(9,4,5),ZR(3,4,5),BFB(3,4,5),DRR(9,4,5),
*      VBAGG(5),VSCS(5),SPRK(5),CK(5),CMASS(5),CYMIN(5),
*      CYMOUT(5),BAGPV(5),PD(5),VBAG(5),VOLBP(5),
*      PCYV(5),PCYMIN(5),PVBAG(5),TV1(3,4,5),TV2(3,10,5),
*      SWITCH(5),PYMOUT(5),SCALE(5),PREVT,IFULL(6)
C      COMMON/CYDATA/ CYTD(5),CYPA(5),CYSP(5),CYT0(5),CYV0(5),CYCD(5),
*      CYK(5),CYR(5),CYAT(5),CYPV(5),CYCD0(5),CYA0(5),
*      CYP0(5),CYSS(5),CYL0(5),CYC(5),CYRH00(5),CYVMAX(5),
*      CYORFC(5),CYRHO(5),CYT(5),CYP(5),CYV(5)
C      COMMON/TEMPVS/ TMP(9),TMP1(3),TORQ(3),FORCE(3,5),TORA(3,5),
*      TQB(3,10),FRB(3,10),VOL(10),DELF(3),VOLP(4,5),FRA(4,5)
C      ,DMY(34955)
C      NOTE: THIS COMMON/TEMPVS/ IS SHARED BY AIRBAG AND AIRBGG.
C      JB = NVEH + J
C      VOLBP(J) = 0.0
C
C      COMPUTE THERMODYNAMIC PROPERTIES OF AIRBAG
C      CYRHO : DENSITY
C      CYT : TEMPERATURE
C      CYP : PRESSURE
C      CYMIN : MASS FLOW INTO BAG
C      VBCALC : CALCULATED VOLUME
C
C      Q = 1.0
C      Q1 = 1.0
C      Q2 = 1.0
C      IF (TIME.LE.CYTD(J)) GO TO 13
C      Q = 1.0 + CYC(J)*(TIME-CYTD(J))
C      CYK1 = 2.0/(CYK(J)-1.0)
C      Q1 = 1.0/Q**CYK1
C      Q2 = 1.0/Q**((CYK(J)*CYK1)
13  CYRHO(J) = CYRH00(J)*Q1
C      CYT(J) = CYT0(J)/Q**2
C      CYP(J) = CYP0(J)*Q2
C      CYMIN(J) = CYV0(J)*(CYRH00(J)-CYRHO(J))

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	CYV(J) - CYVMAX(J)*(1.0-Q2)	AIRBGG
	IF (TIME.LT.CYTD(J)) GO TO 31	AIRBGG
	IF (BD(1,JB).EQ.0.0) GO TO 31	AIRBGG
	IF (TIME.LE.0.0) GO TO 31	AIRBGG
	VOLB = 0.0	AIRBGG
C		AIRBGG
C	COMPUTE AIRBAG ELLIPSOID MATRIX AND ZERO BAG FORCE AND TORQUE.	AIRBGG
C		AIRBGG
	IF (IFULL(J).NE.0) GO TO 21	AIRBGG
	SAB = SCALE(J)*AB(1,J)	AIRBGG
	DO 19 I=1,3	AIRBGG
19	TMP(I) = DEPLOY(I,J) + SAB*DPVCTR(I,J)	AIRBGG
	CALL DOT31 (D(1,1,NVEH),TMP,SEGLP(1,JB))	AIRBGG
	DO 20 I=1,3	AIRBGG
20	SEGLP(I,JB) = SEGLP(I,JB) + SEGLP(I,NVEH)	AIRBGG
21	DO 23 I=1,3	AIRBGG
	FORCE(I,J) = 0.0	AIRBGG
23	TORA (I,J) = 0.0	AIRBGG
C		AIRBGG
C	COMPUTE FORCE,TORQUE AND VOLUME OF INTERSECTION	AIRBGG
C	OF AIRBAG WITH REACTION PANEL ELLIPSOIDS.	AIRBGG
C		AIRBGG
	KP = NPANEL(J)	AIRBGG
	DO 26 K=1,KP	AIRBGG
	CALL BGG(	AIRBGG
	* BD(7,JB),SEGLP(1,JB),D(1,1,JB),BD(4,JB),SEGLV(1,JB),WMEG(1,JB),	AIRBGG
	* B(1,K,J),SEGLP(1,NVEH),D(1,1,NVEH),BFB(1,K,J),SEGLV(1,NVEH),	AIRBGG
	* WMEG(1,NVEH),VSCS(J),IFULL(J),TV1(1,K,J),	AIRBGG
	* FRA(1,K),TORQ,TQB,VOLP(K,J))	AIRBGG
	VOLBP(J) = VOLBP(J) + VOLP(K,J)	AIRBGG
	DO 26 I=1,3	AIRBGG
	FORCE(I,J) = FORCE(I,J) + FRA(I,K)	AIRBGG
26	TORA (I,J) = TORA (I,J) + TORQ(I)	AIRBGG
C		AIRBGG
C	COMPUTE FORCE,TORQUE AND VOLUME OF INTERSECTION	AIRBGG
C	OF AIRBAG WITH CONTACTING SEGMENT ELLIPSOIDS.	AIRBGG
C		AIRBGG
	KBAG = MNBAG(J)	AIRBGG
	DO 30 I=1,KBAG	AIRBGG
	M = MBAG(2,I,J)	AIRBGG
	MM = MBAG(3,I,J)	AIRBGG
	CALL BGG(	AIRBGG
	* BD(7,JB),SEGLP(1,JB),D(1,1,JB),BD(4,JB),SEGLV(1,JB),WMEG(1,JB),	AIRBGG
	* BD(7,MM),SEGLP(1,M),D(1,1,M),BD(4,MM),SEGLV(1,M),WMEG(1,M),	AIRBGG
	* VSCS(J),IFULL(J),TV2(1,I,J),FRB(1,I),TORQ,TQB(1,I),VOL(I))	AIRBGG
	IF (VOL(I).EQ.0.0) GO TO 30	AIRBGG
	VOLB = VOLB + VOL(I)	AIRBGG
	DO 28 K=1,3	AIRBGG
	FORCE(K,J) = FORCE(K,J) + FRB(K,I)	AIRBGG
28	TORA (K,J) = TORA (K,J) + TORQ(K)	AIRBGG
30	CONTINUE	AIRBGG
	VOLBP(J) = VOLBP(J) + VOLB	AIRBGG

31 RETURN  
END

AIRBGG  
AIRBGG

	SUBROUTINE AIRBG1	REV IV 07/24/86SLIP	AIRBG1
C			
C	READS AND PRINTS THE INPUT CARDS THAT DESCRIBE THE PHYSICAL		AIRBG1
C	DIMENSIONS AND GAS DYNAMICS OF THE AIRBAG RESTRAINTS AND		AIRBG1
C	PERFORMS INITIALIZATION REQUIRED BY THE AIRBAG ROUTINE.		AIRBG1
C			AIRBG1
	IMPLICIT REAL*8 (A-H,O-Z)		AIRBG1
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		AIRBG1
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	PAGE	
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),		AIRBG1
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		AIRBG1
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),	SLIP	
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),		AIRBG1
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)		AIRBG1
	COMMON/FORCES/PSF(7,70),BSF(4,20),SSF(10,40),BAGSF(3,20),	NCFORC	
*	PRJNT(7,30),NPANEL(5),NPSF,NBSF,NSSF,NBGSF		AIRBG1
	COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),		AIRBG1
*	BLTTTL(5,8),PLTTL(5,30),BAGTTL(5,6),SEG(30),		AIRBG1
*	JOINT(30),CGS(30),JS(30)		AIRBG1
	REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTL,BAGTTL,SEG,JOINT		AIRBG1
	LOGICAL*1 CGS,JS		AIRBG1
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),		AIRBG1
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI	TWOPI	
	COMMON/CNTRSF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)	EDGE	
	COMMON/INTEST/ SGTEST(3,4,30),XTEST(3,120),SEGT(120),REGT(120)		AIRBG1
	REAL SEGT		AIRBG1
	COMMON/ABDATA/ ZDEP(3,5),DBR(3,3,5),DPVCTR(3,5),DEPLOY(3,5),		AIRBG1
*	AB(3,5),B(9,4,5),ZR(3,4,5),BFB(3,4,5),DRR(9,4,5),		AIRBG1
*	VBAGG(5),VSCS(5),SPRK(5),CK(5),CMASS(5),CYMIN(5),		AIRBG1
*	CYMOUT(5),BAGPV(5),PD(5),VBAG(5),VOLBP(5),		AIRBG1
*	PCYV(5),PCYMIN(5),PVBAG(5),TV1(3,4,5),TV2(3,10,5),		AIRBG1
*	SWITCH(5),PYMOUT(5),SCALE(5),PREVT,IFULL(6)		AIRBG1
	COMMON/CYDATA/ CYTD(5),CYPA(5),CYSP(5),CYT0(5),CYV0(5),CYCD(5),		AIRBG1
*	CYK(5),CYR(5),CYAT(5),CYPV(5),CYCD0(5),CYA0(5),		AIRBG1
*	CYP0(5),CYSS(5),CYL0(5),CYC(5),CYRHO0(5),CYVMAX(5),		AIRBG1
*	CYORFC(5),CYRHO(5),CYT(5),CYP(5),CYV(5)		AIRBG1
	COMMON/TEMPVS/ TMP(9),TMP1(3),DMMY(35101)	80386	
	DIMENSION YB(3),YP(3),IDYPR(3)		AIRBG1
	REAL BAG(6)		AIRBG1
	DATA BAG/4HBAG1,4HBAG2,4HBAG3,4HBAG4,4HBAG5,4HBAG /		AIRBG1
	DATA IDYPR/3,2,1/		AIRBG1
	DATA MAXNPL/4/,MAXSEG/30/	CHGIII	
C			AIRBG1
C	MAKE ROOM FOR BAG DATA IN SEGMENT ARRAYS BETWEEN VEH AND GRND.		AIRBG1
C			AIRBG1
	MSEG = 0	CHGIII	
	IF (NVEH.GT.NSEG) MSEG = NVEH - NSEG	CHGIII	
	L = NSEG + NBAG + MSEG + 1	CHGIII	
	K = NSEG + MSEG + 1	CHGIII	
	W(L) = W(K)	AIRBG1	
	RW(L) = RW(K)	AIRBG1	
	SEG(L) = SEG(K)	AIRBG1	

	ISING(L) = ISING(K)	AIRBG1
	IF (L-1.GT.NJNT) JNT (L-1) = 0	AIRBG1
	IF (L-1.GT.NJNT) IPIN(L-1) = 0	AIRBG1
	DO 19 I=1,3	AIRBG1
	SEGLP(I,L) = SEGLP(I,K)	AIRBG1
	SEGLV(I,L) = SEGLV(I,K)	AIRBG1
	SEGLA(I,L) = SEGLA(I,K)	AIRBG1
	WMEG (I,L) = WMEG (I,K)	AIRBG1
	WMEGD(I,L) = WMEGD(I,K)	AIRBG1
	PHI (I,L) = PHI (I,K)	AIRBG1
	RPHI (I,L) = RPHI (I,K)	AIRBG1
	DO 18 J=1,3	AIRBG1
	D(I,J,L) = D(I,J,K)	AIRBG1
18	SGTEST(I,J,L) = SGTEST(I,J,K)	AIRBG1
19	SGTEST(I,4,L) = SGTEST(I,4,K)	AIRBG1
	NGRND = NSEG + NBAG + MSEG + 1	CHGIII
	IF (NGRND.GT.MAXSEG) STOP 75	CHGIII
	DO 40 J=1,NBAG	AIRBG1
	JB = NVEH + J	AIRBG1
C		AIRBG1
C	READ AND PRINT CARDS D.4.A -D.4.F FOR THE JTH AIRBAG.	AIRBG1
C		AIRBG1
	READ(5,13) (BAGTTL(I,J),I = 1,5),NPANEL(J),	AIRBG1
	* (AB(I,J),I=1,3) , (BD(I,JB),I=4,6),	AIRBG1
	* YB,(ZDEP(I,J),I=1,3),	AIRBG1
	* W(JB),CYTD(J),CYP A(J),CYSP(J),CYTO(J),CYVO(J),	AIRBG1
	* CYCD(J),CYK(J),CYR(J),CYAT(J),CYPV(J),CYCDO(J),	AIRBG1
	* CYAO(J),SPRK(J),VSCS(J),CK(J),CMASS(J)	AIRBG1
13	FORMAT (5A4,I4/(6F12.0))	AIRBG1
	IF (NPANEL(J).GT.MAXNPL) STOP 76	CHGIII
	IF (MOD(J,2).EQ.1) WRITE(6,15) NPG	PAGE
	IF (MOD(J,2).EQ.1) NPG=NPG+1	PAGE
15	FORMAT('1',122X,'PAGE',15/' AIRBAG INPUTS',105X,'CARDS D.4')	PAGE
	WRITE(6,14) J,(BAGTTL(I,J),I = 1,5 ),	AIRBG1
	* (AB(I,J),I=1,3) , (BD(I,JB),I=4,6),	AIRBG1
	* YB,(ZDEP(I,J),I=1,3),	AIRBG1
	* W(JB),CYTD(J),CYP A(J),CYSP(J),CYTO(J),CYVO(J),	AIRBG1
	* CYCD(J),CYK(J),CYR(J),CYAT(J),CYPV(J),CYCDO(J),	AIRBG1
	* CYAO(J),SPRK(J),VSCS(J),CK(J),CMASS(J)	AIRBG1
14	FORMAT('0 AIRBAG NO.',I4,4X,5A4//	AIRBG1
	* 29X,'AIR BAG SEMIAXES',46X,'C.G. OFFSET'/6X,6G20.9//	AIRBG1
	* 15X,'YAW',16X,'PITCH',15X,'ROLL',30X,'DEPLOYMENT POINT'	AIRBG1
	* /6X,6G20.9//	AIRBG1
	* 15X,'XBM',16X,'CYTD',16X,'CYP A',16X,'CYSP',16X,'CYTO',16X,'CYVO'	AIRBG1
	* /6X,6G20.9//	AIRBG1
	* 14X,'CYCD',17X,'CYK',17X,'CYR',16X,'CYAT',16X,'CYPV',16X,'CYCDO'	AIRBG1
	* /6X,6G20.9//	AIRBG1
	*14X,'CYAO',16X,'SPRK',16X,'VSCS',17X,'CK',17X,'CMASS'/6X,5G20.9)	AIRBG1
	KP = NPANEL(J)	AIRBG1
	DO 25 K=1,KP	AIRBG1
C		AIRBG1
C	READ AND PRINT CARDS D.4.G AND D.4.H FOR THE KTH PANEL TO	AIRBG1

C	CONTACT THE JTH AIRBAG. THESE PANELS ARE APPROXIMATED BY	AIRBG1
C	ELLIPSOIDS. THE FIRST PANEL (K=1) IS THE REACTION PANEL THAT	AIRBG1
C	INCLUDES THE DEPLOYMENT POINT.	AIRBG1
C		AIRBG1
	READ(5,11) (B(I,K,J),I=1,3),(BFB(I,K,J),I=1,3),	AIRBG1
	* (ZR(I,K,J),I=1,3),YP	AIRBG1
11	FORMAT(6F12.0)	AIRBG1
	WRITE(6,12) K,(B(I,K,J),I=1,3),(BFB(I,K,J),I=1,3),	AIRBG1
	* (ZR(I,K,J),I=1,3),YP	AIRBG1
12	FORMAT('0 PANEL NO.',I4//	AIRBG1
	* 24X,'PANEL ELLIPSOID SEMIAXES',43X,'C.G. OFFSET'/6X,6G20.9//	AIRBG1
	* 29X,'PANEL LOCATION',32X,'YAW',16X,'PITCH',15X,'ROLL'/6X,6G20.9)	AIRBG1
C		AIRBG1
C	CONVERT B FROM ELLIPSOID SEMIAXES TO MATRIX	AIRBG1
C		AIRBG1
	DO 21 I=1,3	AIRBG1
21	TMP(I) = B(I,K,J)	AIRBG1
	DO 22 I=1,9	AIRBG1
22	B(I,K,J) = 0.0	AIRBG1
	DO 23 I=1,3	AIRBG1
23	B(4*I-3,K,J) = 1.0/TMP(I)**2	AIRBG1
	CALL DRCYPR (DRR(1,K,J),YP,IDYPR)	AIRBG1
	CALL MAT33 (B(1,K,J),DRR(1,K,J),TMP)	AIRBG1
	CALL DOT33 (DRR(1,K,J),TMP,B(1,K,J))	AIRBG1
	CALL DOT31 (DRR(1,K,J),BFB(1,K,J),TMP)	AIRBG1
	DO 24 I=1,3	AIRBG1
24	BFB(I,K,J) = TMP(I) + ZR(I,K,J)	AIRBG1
25	CONTINUE	AIRBG1
C		AIRBG1
C	COMPUTE GEOMETRY OF DEPLOYMENT POINT ON FIRST PANEL.	AIRBG1
C		AIRBG1
	CALL DRCYPR (DBR(1,1,J),YB,IDYPR)	AIRBG1
	CALL DOT31 (DRR(1,1,J),ZDEP(1,J),DEPLOY(1,J))	AIRBG1
	DO 31 I=1,3	AIRBG1
	DPVCTR(I,J) = -DBR(1,I,J)	AIRBG1
31	DEPLOY(I,J) = DEPLOY(I,J) + BFB(I,1,J)	AIRBG1
	CALL PANEL (DBR(1,1,J),DEPLOY(1,J),JB)	AIRBG1
C		AIRBG1
C	INITIALIZATION OF AIRBAG GEOMETRY.	AIRBG1
C		AIRBG1
	VBAGG(J) = 4.0/3.0*PI*AB(1,J)*AB(2,J)*AB(3,J)	AIRBG1
	PHI(1,JB) = (AB(2,J)**2+AB(3,J)**2)/5.0	AIRBG1
	PHI(2,JB) = (AB(3,J)**2+AB(1,J)**2)/5.0	AIRBG1
	PHI(3,JB) = (AB(1,J)**2+AB(2,J)**2)/5.0	AIRBG1
	JNT(JB-1) = 0	AIRBG1
	IPIN(JB-1) = 0	AIRBG1
	SEG(JB) = BAG(J)	AIRBG1
	IF (NBAG.EQ.1) SEG(JB) = BAG(6)	AIRBG1
	ISING(JB) = -1	AIRBG1
	RW(JB) = G/W(JB)	AIRBG1
	DO 36 I=1,3	AIRBG1
	BD(I,JB) = 0.0	AIRBG1

	RPHI(I,JB) = 1.0/PHI(I,JB)	AIRBG1
	DO 36 K=1,4	AIRBG1
36	SGTEST(I,K,JB) = 0.0	AIRBG1
	DO 35 I=7,24	AIRBG1
35	BD(I,JB) = 0.0	AIRBG1
	IFULL(J) = 0	AIRBG1
	CYMOUT(J) = 0.0	AIRBG1
	PYMOUT(J) = 0.0	AIRBG1
	DO 38 I=1,3	AIRBG1
	DO 37 K=1,4	AIRBG1
37	TV1(I,K,J) = 0.0	AIRBG1
	DO 38 K=1,10	AIRBG1
38	TV2(I,K,J) = 0.0	AIRBG1
C		AIRBG1
C	AIR CYLINDER INITIALIZATION	AIRBG1
C		AIRBG1
	CYPO(J) = CYSP(J)+CYPA(J)	AIRBG1
	CYSS(J) = DSQRT(CYK(J)*CYR(J)*CYTO(J)*G)	AIRBG1
	CYLO(J) = CYVO(J)/CYAT(J)	AIRBG1
	CYK1 = CYK(J)-1.0	AIRBG1
	CYK2 = 0.5*(CYK(J)+1.0)	AIRBG1
	CYK3 = CYK2*(-CYK2/CYK1)	AIRBG1
	CYC(J) = 0.5*CYK1*CYSS(J)*CYCD(J)/CYLO(J)*CYK3	AIRBG1
	CYRHOO(J) = CYP0(J)/(CYR(J)*CYTO(J))	AIRBG1
	CYVMAX(J) = CYVO(J)/CYK(J)*CYP0(J)/CYPA(J)	AIRBG1
	CYORFC(J) = CYCDO(J)*CYAO(J)*G*DSQRT(2.0*CYPA(J)*CYK(J))/CYSS(J)	AIRBG1
	IF (NPRT(22).NE.0) WRITE(6,39)	AIRBG1
	* (SEGLP(I,JB),I=1,3),(SEGLV(I,JB),I=1,3),(WMEG(I,JB),I=1,3),	AIRBG1
	* VBAGG(J),CYP0(J),CYSS(J),CYC(J),CYRHOO(J),CYVMAX(J),CYORFC(J)	AIRBG1
39	FORMAT('0 AIRBAG SINPUT'/(1X,9G14.6))	AIRBG1
40	CONTINUE	AIRBG1
	PREVT = 0.0	AIRBG1
	RETURN	AIRBG1
	END	AIRBG1



	SUBROUTINE AIRBG3(IRESET)	AIRBG3
C		REV IV 07/23/86TWOPI
C		AIRBG3
C	THIS SUBROUTINE IS CALLED BY SUBROUTINE UPDATE AT START (IRESET-1)	AIRBG3
C	AND END (IRESET-2) OF EACH INTEGRATION STEP TO DETERMINE IF EACH	AIRBG3
C	AIRBAG HAS BEEN FULLY INFLATED.	AIRBG3
C		AIRBG3
	IMPLICIT REAL*8 (A-H,O-Z)	AIRBG3
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,	AIRBG3
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),	AIRBG3
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)	AIRBG3
	COMMON/JBARTZ/ MNPL( 30),MNBLT( 8),MNSEG( 30),MNBAG( 6),	AIRBG3
*	MPL(3,5,30),MBLT(3,5,8),MSEG(3,5,30),MBAG(3,10,6),	AIRBG3
*	NTPL( 5,30),NTBLT( 5,8),NTSEG( 5,30)	AIRBG3
	COMMON/FORCES/PSF(7,70),BSF(4,20),SSF(10,40),BAGSF(3,20),	NCFORC
*	PRJNT(7,30),NPANEL(5),NPSF,NBSF,NSSF,NBGSF	AIRBG3
	COMMON/CNTRSF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)	EDGE
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),	AIRBG3
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI	TWOPI
	COMMON/ABDATA/ ZDEP(3,5),DBR(3,3,5),DPVCTR(3,5),DEPLOY(3,5),	AIRBG3
*	AB(3,5),B(9,4,5),ZR(3,4,5),BFB(3,4,5),DRR(9,4,5),	AIRBG3
*	VBAGG(5),VSCS(5),SPRK(5),CK(5),CMASS(5),CYMIN(5),	AIRBG3
*	CYMOUT(5),BAGPV(5),PD(5),VBAG(5),VOLBP(5),	AIRBG3
*	PCYV(5),PCYMIN(5),PVBAG(5),TV1(3,4,5),TV2(3,10,5),	AIRBG3
*	SWITCH(5),PYMOUT(5),SCALE(5),PREVT,IFULL(6)	AIRBG3
	COMMON/CYDATA/ CYTD(5),CYPA(5),CYSP(5),CYTO(5),CYVO(5),CYCD(5),	AIRBG3
*	CYK(5),CYR(5),CYAT(5),CYPV(5),CYCD0(5),CYA0(5),	AIRBG3
*	CYPO(5),CYSS(5),CYLO(5),CYC(5),CYRHO0(5),CYVMAX(5),	AIRBG3
*	CYORFC(5),CYRHO(5),CYT(5),CYP(5),CYV(5)	AIRBG3
	COMMON/TEMPVS/ TMP(9),TMP1(3),DMMY(35101)	80386
	CALL ELTIME(1,29)	AIRBG3
	JRESET = IRESET	AIRBG3
	IF (JRESET.EQ.1) PREVT = TIME	AIRBG3
	NBGSF = 0	AIRBG3
	DO 50 J=1,NBAG	AIRBG3
	IF (MNBAG(J).EQ.0) GO TO 50	AIRBG3
	JB = NVEH + J	AIRBG3
	JFULL = IFULL(J) + 2	AIRBG3
	IF (JFULL.LT.1 .OR. JFULL.GT.3) GO TO 11	AIRBG3
	IF (JRESET-1) 13,13,14	BUTLER1
11	WRITE(6,12) TIME	AIRBG3
12	FORMAT ('O ERROR IN SUBROUTINE AIRBG3 AT TIME -',F10.6)	AIRBG3
	STOP 32	AIRBG3
13	IF (JFULL-2) 41,49,49	BUTLER1
14	IF (JFULL-2) 11,21,31	BUTLER1
C		AIRBG3
C	END OF INTEGRATION STEP WHEN IFULL=0. TEST FOR FULL INFLATION.	AIRBG3
C		AIRBG3
21	PD(J) = 0.0	AIRBG3
	PCYV(J) = CYV(J)	AIRBG3
	PCYMIN(J) = CYMIN(J)	AIRBG3

	PVBAG(J) = VBAG(J)	AIRBG3
22	CALL AIRBGG(J)	AIRBG3
	VBAG(J) = CYV(J) + VOLBP(J)	AIRBG3
	IF (SCALE(J).EQ.1.0) GO TO 23	AIRBG3
	SCALE(J) = (VBAG(J)/VBAGG(J))*THIRD	AIRBG3
	IF (SCALE(J).LT.1.0) GO TO 24	AIRBG3
	SCALE(J) = 1.0	AIRBG3
	GO TO 22	AIRBG3
23	IFULL(J) = -1	AIRBG3
	CYHOUT(J) = 0.0	AIRBG3
	PSW1 = (VBAG(J)-VBAGG(J))*PCYV(J)/PCYMIN(J)	AIRBG3
	PSW2 = (VBAGG(J)-PVBAG(J))*CYV(J)/CYMIN(J)	AIRBG3
	SWITCH(J) = (PSW1+PSW2)/(VBAG(J)-PVBAG(J))	AIRBG3
	BAGPV(J) = CYP(A(J))*(CYMIN(J)*SWITCH(J))*CYK(J)	AIRBG3
	PD(J) = BAGPV(J)/(CYV(J))*CYK(J) - CYP(A(J))	AIRBG3
24	DO 25 K=1,3	AIRBG3
	BD(K,JB) = SCALE(J)*AB(K,J)	AIRBG3
	IF (SCALE(J).EQ.0.0) GO TO 25	AIRBG3
	BD(4*K+12,JB) = BD(K,JB)**2	AIRBG3
	BD(4*K+ 3,JB) = 1.0/BD(4*K+12,JB)	AIRBG3
25	TMP(K) = DEPLOY(K,J) + BD(1,JB)*DPVCTR(K,J)	AIRBG3
	CALL PANEL (DBR(1,1,J),TMP,JB)	AIRBG3
C		AIRBG3
C	SET UP BAGSF ARRAY FOR OUTPUT.	AIRBG3
C		AIRBG3
31	BAGSF(1,NBGSF+1) = CYP(J)	AIRBG3
	BAGSF(2,NBGSF+1) = CYT(J)	AIRBG3
	BAGSF(3,NBGSF+1) = PD(J)	AIRBG3
	CALL DOT31 (D(1,1,JB),BD(4,JB),TMP)	AIRBG3
	DC 32 K=1,3	AIRBG3
	B/GSF(K,NBGSF+3) = BD(K,JB)	AIRBG3
32	TMP(K) = TMP(K) + SEGLP(K,JB) - SEGLP(K,NVEH)	AIRBG3
	CALL MAT31 (D(1,1,NVEH),TMP,BAGSF(1,NBGSF+2))	AIRBG3
	CALL YPRDEG (D(1,1,JB),BAGSF(1,NBGSF+4))	AIRBG3
	NBGSF = NBGSF + 5 + NPANEL(J) + MNBAG(J)	AIRBG3
	GO TO 50	AIRBG3
C		AIRBG3
C	START OF INTEGRATION STEP WITH IFULL = -1, RESET INTEGRATOR.	AIRBG3
C		AIRBG3
41	IFULL(J) = 1	AIRBG3
	IRESET = -1	AIRBG3
49	PYMOUT(J) = CYMOUT(J)	AIRBG3
50	CONTINUE	AIRBG3
	CALL ELTIME(2,29)	AIRBG3
	RETURN	AIRBG3
	END	AIRBG3

	SUBROUTINE BELTG (ZA,ZB,ZC,BD)		BELTG
		REV IV 07/23/86	TWOPI
C	COMPUTE TANGENT POINTS, UNIT VECTORS FROM TANGENT POINTS TO		BELTG
C	ANCHOR POINTS AND LENGTHS OF THE BELT SEGMENTS.		BELTG
C			BELTG
C	ARGUMENTS:		BELTG
C			BELTG
C	ZA,ZB - ANCHOR POINTS RELATIVE TO ELLIPSOID CENTER.		BELTG
C	ZC - FIXED POINT OF BELT ON SEGMENT ELLIPSOID.		BELTG
C	BD - SEGMENT ELLIPSOID SEMIAXES AND CENTER.		BELTG
C			BELTG
C	RESULTS ARE RETURNED TO CALLING ROUTINE VIA COMMON/TEMPVS/.		BELTG
C			BELTG
	IMPLICIT REAL*8 (A-H,O-Z)		BELTG
	DIMENSION ZA(3),ZB(3),ZC(3),BD(24)		BELTG
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		BELTG
	*          NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),		BELTG
	*          UNITL,UNITM,UNITT,GRAVITY(3),TWOPI		TWOPI
C	NOTE: BELTRT AND BELTG SHARE FIRST PART OF TEMPVS		BELTG
	COMMON/TEMPVS/ APA(3),UVA(3),DLGA,UAA,APB(3),UVB(3),DLGB,UBB		BELTG
	*          ,TA(3),TB(3),TC(3),UP(3),B(3)		BELTG
	*          ,UC(3),AX(3),XE(3),BX(3),ACA(3),ACB(3),DMMY(35064)		80386
C			BELTG
C	COMPUTE		BELTG
C	TC: NORMALIZED VECTOR OF BELT PLANE DETERMINED		BELTG
C	BY ANCHOR POINTS AND FIXED POINT.		BELTG
C			BELTG
	DO 10 K=1,3		BELTG
	TA(K) = ZC(K)-ZA(K)		BELTG
10	TB(K) = ZC(K)-ZB(K)		BELTG
	CALL CROSS(TB,TA,TC)		BELTG
	S = DSQRT(TC(1)**2 + TC(2)**2 + TC(3)**2)		BELTG
	TC(1) = TC(1)/S		BELTG
	TC(2) = TC(2)/S		BELTG
	TC(3) = TC(3)/S		BELTG
C			BELTG
C	GET DISTANCE OF BELT PLANE TO CENTER OF ELLIPSIOD.		BELTG
C			BELTG
	BET = TC(1)*ZC(1)+TC(2)*ZC(2)+TC(3)*ZC(3)		BELTG
C			BELTG
C	COMPUTE		BELTG
C	XE: CENTER OF ELLIPSE DETERMINED BY INTERSECTION		BELTG
C	OF BELT PLANE AND SEGMENT ELLIPSOID.		BELTG
C			BELTG
	CALL MAT31 (BD(16),TC,XE)		BELTG
	GG = BET/(TC(1)*XE(1)+TC(2)*XE(2)+TC(3)*XE(3))		BELTG
	DLGA = 0.0		BELTG
	DLGB = 0.0		BELTG
	DO 15 K=1,3		BELTG
	XE(K) = XE(K)*GG		BELTG
	UC(K) = ZC(K)-XE(K)		BELTG

	APA(K) - UC(K)	BELTG
15	APB(K) - UC(K)	BELTG
	YAY - GG*BET	BELTG
	YAY1 = 1.0-YAY	BELTG
	IF (YAY1.LE.EPS(6)) GO TO 70	BELTG
C		BELTG
C	CALCULATE POSSIBLE TANGENT POINTS FROM	BELTG
C	UVA,UVB: VECTORS FROM ELLIPSE CENTER TO MIDPOINT OF	BELTG
C	LINE CONNECTING POSSIBLE TANGENT POINTS.	BELTG
C	ACA,ACB: VECTORS FROM UVA,UVB TO TANGENT POINTS (POSITIVE).	BELTG
C		BELTG
	CALL MAT31 (BD(7),ZA,AX)	BELTG
	CALL MAT31 (BD(7),ZB,BX)	BELTG
	ZZA = AX(1)*ZA(1)+AX(2)*ZA(2)+AX(3)*ZA(3)	BELTG
	IF( ZZA.LE.1.0) STOP 88	CHGIII
	ZZB = BX(1)*ZB(1)+BX(2)*ZB(2)+BX(3)*ZB(3)	BELTG
	IF( ZZB.LE.1.0) STOP 89	CHGIII
	C2A = YAY1/(ZZA-YAY)	BELTG
	C2B = YAY1/(ZZB-YAY)	BELTG
	CALL CROSS(TC,AX,ACA)	BELTG
	CALL CROSS(TC,BX,ACB)	BELTG
	TTA = 0.0	BELTG
	TTB = 0.0	BELTG
	DO 21 I=1,3	BELTG
	DO 21 J=1,3	BELTG
	K = 3*J+I+3	BELTG
	TTA = TTA + ACA(I)*BD(K)*ACA(J)	BELTG
21	TTB = TTB + ACB(I)*BD(K)*ACB(J)	BELTG
	C3A = DSQRT((1.0 - C2A)*YAY1/TTA)	CHGIII
	C3B = DSQRT((1.0 - C2B)*YAY1/TTB)	CHGIII
	TT = DSQRT(UC(1)**2 + UC(2)**2 + UC(3)**2)	BELTG
	DO 24 K=1,3	BELTG
	UVA(K) = C2A*(ZA(K)-XE(K))	BELTG
	UVB(K) = C2B*(ZB(K)-XE(K))	BELTG
	ACA(K) = C3A*ACA(K)	BELTG
	ACB(K) = C3B*ACB(K)	BELTG
	UC(K) = UC(K)/TT	BELTG
24	B(K) = 0.0	BELTG
C		BELTG
C	OBTAIN EQUATION OF ELLIPSE	BELTG
C	B1*X**2 + 2*B2*X*Y + B3*Y**2 = 1	BELTG
C	IN UC,UP COORDINATES WHERE UC POINTS TO FIXED POINT.	BELTG
C		BELTG
	CALL CROSS(TC,UC,UP)	BELTG
	DO 22 I=1,3	BELTG
	DO 22 J=1,3	BELTG
	K = 3*J+I+3	BELTG
	B(1) = B(1) + UC(I)*BD(K)*UC(J)	BELTG
	B(2) = B(2) + UC(I)*BD(K)*UP(J)	BELTG
22	B(3) = B(3) + UP(I)*BD(K)*UP(J)	BELTG
	B(1) = B(1)/YAY1	BELTG
	B(2) = B(2)/YAY1	BELTG

	B(3) - B(3)/YAY1	BELTG
C		BELTG
C	COMPUTE ANGLES FROM FIXED POINT TO POSSIBLE TANGENT POINTS.	BELTG
C		BELTG
	UCUVA = UC(1)*UVA(1) + UC(2)*UVA(2) + UC(3)*UVA(3)	BELTG
	UCUVB = UC(1)*UVB(1) + UC(2)*UVB(2) + UC(3)*UVB(3)	BELTG
	UCACA = UC(1)*ACA(1) + UC(2)*ACA(2) + UC(3)*ACA(3)	BELTG
	UCACB = UC(1)*ACB(1) + UC(2)*ACB(2) + UC(3)*ACB(3)	BELTG
	UPUVA = UP(1)*UVA(1) + UP(2)*UVA(2) + UP(3)*UVA(3)	BELTG
	UPUVB = UP(1)*UVB(1) + UP(2)*UVB(2) + UP(3)*UVB(3)	BELTG
	UPACA = UP(1)*ACA(1) + UP(2)*ACA(2) + UP(3)*ACA(3)	BELTG
	UPACB = UP(1)*ACB(1) + UP(2)*ACB(2) + UP(3)*ACB(3)	BELTG
	TH1 = DATAN2(UPUVA-UPACA,UCUVA-UCACA)	BELTG
	TH2 = DATAN2(UPUVA+UPACA,UCUVA+UCACA)	BELTG
	TH3 = DATAN2(UPUVB-UPACB,UCUVB-UCACB)	BELTG
	TH4 = DATAN2(UPUVB+UPACB,UCUVB+UCACB)	BELTG
	IF (TH1.LT.0.0) TH1 = TWOPI + TH1	BELTG
	IF (TH2.LT.0.0) TH2 = TWOPI + TH2	BELTG
	IF (TH3.LT.0.0) TH3 = TWOPI + TH3	BELTG
	IF (TH4.LT.0.0) TH4 = TWOPI + TH4	BELTG
C		BELTG
C	CHOOSE PROPER TANGENT POINTS AND BELT ARC LENGTHS.	BELTG
C		BELTG
	THMIN = DMIN1(TH1,TH2,TH3,TH4)	BELTG
	IF (THMIN.EQ.TH1.AND.DMIN1(TH2,TH3,TH4).NE.TH4) GO TO 61	BELTG
	IF (THMIN.EQ.TH2.AND.DMAX1(TH1,TH3,TH4).EQ.TH4) GO TO 61	BELTG
	IF (THMIN.EQ.TH3.AND.DMIN1(TH1,TH2,TH4).NE.TH2) GO TO 63	BELTG
	IF (THMIN.EQ.TH4.AND.DMAX1(TH1,TH2,TH3).EQ.TH2) GO TO 63	BELTG
	GO TO 70	BELTG
61	THA = TH1	BELTG
	THB = TWOPI-TH4	BELTG
	DO 62 K=1,3	BELTG
	APA(K) = UVA(K)-ACA(K)	BELTG
62	APB(K) = UVB(K)+ACB(K)	BELTG
	GO TO 65	BELTG
63	THA = TWOPI-TH2	BELTG
	THB = TH3	BELTG
	DO 64 K=1,3	BELTG
	APA(K) = UVA(K)+ACA(K)	BELTG
64	APB(K) = UVB(K)-ACB(K)	BELTG
65	CONTINUE	BELTG
	EPS1 = EPS(1)	BELTG
	DLGA = DABS(ELONG(B(1),B(2),B(3),EPS1,THA))	BELTG
	DLGB = DABS(ELONG(B(1),B(2),B(3),EPS1,THB))	BELTG
C		BELTG
C	CALCULATE BELT LENGTHS AND UNIT VECTORS	BELTG
C	FROM TANGENT POINTS TO ANCHOR POINTS.	BELTG
C		BELTG
70	UAA=0.	BELTG
	UBB=0.	BELTG
	DO 80 K=1,3	BELTG
	APA(K) = APA(K)+XE(K)	BELTG

APB(K) = APB(K)+XE(K)	BELTG
UVA(K)=ZA(K)-APA(K)	BELTG
UVB(K)=ZB(K)-APB(K)	BELTG
APA(K)=APA(K)+BD(K+3)	BELTG
APB(K)=APB(K)+BD(K+3)	BELTG
UAA=UAA+UVA(K)**2	BELTG
UBB=UBB+UVB(K)**2	BELTG
80 CONTINUE	BELTG
UAA=DSQRT(UAA)	BELTG
UBB=DSQRT(UBB)	BELTG
DO 90 K=1,3	BELTG
UVA(K)=UVA(K)/UAA	BELTG
UVB(K)=UVB(K)/UBB	BELTG
90 CONTINUE	BELTG
C	BELTG
C OPTIONAL OUTPUT	BELTG
C	BELTG
IF (NPRT(15).EQ.0) GO TO 99	BELTG
WRITE(6,50)	BELTG
50 FORMAT(1X,'BELT RESTRAINT')	BELTG
WRITE(6,60) APA,UVA,DLGA,UAA	BELTG
WRITE(6,60) APB,UVB,DLGB,UBB	BELTG
60 FORMAT (1X,1P8D15.5)	BELTG
99 CONTINUE	BELTG
RETURN	BELTG
END	BELTG

	SUBROUTINE BELTRT(I,II,MM,M NT)		BELTRT
		REV IV 07/23/86	TWOPI
C	THE ROUTINE CALLS SUBROUTINE BELTG TO COMPUTE THE TANGENT POINTS		BELTRT
C	AND BELT LENGTHS AND APPLIES THE RESTRAINT FORCES TO THE U1 ARRAY		BELTRT
C	AND BELT TORQUES TO THE U2 ARRAY FOR ELLIPSOID(II) ATTACHED TO		BELTRT
C	BODY SEGMENT (I) BY BELT (M) ATTACHED TO SEGMENT (MM).		BELTRT
C			BELTRT
	IMPLICIT REAL*8(A-H,O-Z)		BELTRT
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		BELTRT
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),		BELTRT
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		BELTRT
	COMMON/CNTRSRF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)		EDGE
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)		DIMENB
	COMMON/FORCES/PSF(7,70),BSF(4,20),SSF(10,40),BAGSF(3,20),		NCFORC
*	PRJNT(7,30),NPANEL(5),NPSF,NBSF,NSSF,NBSGF		BELTRT
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),		BELTRT
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI		TWOPI
	COMMON/RSAVE/ XSG(3,20,3),DPMI(3,3,30),LPMI(30),		TGMOD4
*	NSG(9),MSG(20,9),MCG,MCGIN(24,5),KREF(20,9)		TTHKREF
C	NOTE: BELTRT AND BELTG SHARE FIRST PART OF TEMPVS		BELTRT
	COMMON/TEMPVS/ APA(3),UVA(3),DLGA,UAA,APB(3),UVB(3),DLGB,UBB		BELTRT
*	,DDMY(35097)		80386
	DIMENSION TA(3),TB(3),ZA(3),ZB(3),TT(3),TTT(3),TA1(3),TB1(3)		TGMOD4
C			BELTRT
	CALL ELTIME(1,22)		BELTRT
C			BELTRT
C	CONVERT SEGMENT POSITION TO SEGMENT REFERENCE.		BELTRT
C			BELTRT
	MA = MOD(MM,100)		JTF984
	MB = MM/100		JTF984
	IF (MB.EQ.0) MB=MA		JTF984
	CALL DOT31 (D(1,1,MA),BELT(1,M),TA)		BELTRT
	CALL DOT31 (D(1,1,MB),BELT(4,M),TB)		BELTRT
	DO 10 K=1,3		BELTRT
	TA(K) = SEGLP(K,MA) + TA(K) - SEGLP(K,I)		BELTRT
10	TB(K) = SEGLP(K,MB) + TB(K) - SEGLP(K,I)		BELTRT
	CALL MAT31 (D(1,1,I),TA,ZA)		BELTRT
	CALL MAT31 (D(1,1,I),TB,ZB)		BELTRT
	DO 13 K=1,3		BELTRT
	ZA(K) = ZA(K) - BD(K+3,II)		BELTRT
13	ZB(K) = ZB(K) - BD(K+3,II)		BELTRT
C			BELTRT
C	COMPUTE NEW BELT LENGTHS AND EXPANSION.		BELTRT
C			BELTRT
	CALL BELTG (ZA, ZB, BELT(7,M), BD(1,II))		BELTRT
	TLA = DLGA+UAA		BELTRT
	TLB = DLGB+UBB		BELTRT
	TL = TLA+TLB		BELTRT
	IF (TIME.NE.0.0) GO TO 11		BELTRT
C			BELTRT
C	IF TIME=0, COMPUTE INITIAL BELT LENGTHS		BELTRT

C	AND STORE RESULTS IN BELT ARRAY.	BELTRT
C		BELTRT
	IF (BELT(11,M).LT.0.0) BELT(11,M)=-BELT(11,M)-TL	BELTRT
	IF (BELT(11,M).LT.0.0) BELT(11,M)=0.0	BELTRT
	BELT(12,M) = TLA+TLA/TL*BELT(11,M)	BELTRT
	BELT(13,M) = TLB+TLB/TL*BELT(11,M)	BELTRT
	B1213 = BELT(12,M) + BELT(13,M)	BELTRT
	BELT(10,M) = B1213	BELTRT
	DO 305 LL=1,3	TGMOD4
	TA1(LL) = APA(LL)	TGMOD4
305	TB1(LL) = APB(LL)	TGMOD4
	IF(LPMI(I).EQ.0) GO TO 306	TGMOD4
	CALL DOT31(DPMI(1,1,I),APA,TA1)	TGMOD4
	CALL DOT31(DPMI(1,1,I),APB,TB1)	TGMOD4
306	CONTINUE	TGMOD4
	WRITE (6,14) M, B1213, BELT(12,M), BELT(13,M), UNITL,I,TA1, TB1	TGMOD4
14	FORMAT('0 INITIAL LENGTHS OF BELT NO.',I3,' AND ITS SEGMENTS ARE',	BELTRT
	* 3F12.4,1X,A4/'0 INITIAL TANGENT POINTS IN LOCAL REFERENCE	TGMOD4
	*OF SEGMENT ',I2,' ARE:',/,2(3X,3F12.3))	TGMOD4
C		BELTRT
C	CONVERT TANGENT POINTS TO INERTIAL REFERENCE AND STORE.	BELTRT
C		BELTRT
11	CALL DOT31 (D(1,1,I),APA,TPTS(1,M))	BELTRT
	CALL DOT31 (D(1,1,I),APB,TPTS(4,M))	BELTRT
	DO 12 K=1,3	BELTRT
	TPTS(K ,M) = TPTS(K ,M) + SEGLP(K,I)	BELTRT
12	TPTS(K+3,M) = TPTS(K+3,M) + SEGLP(K,I)	BELTRT
	SDOT = 0.0	BELTRT
	NCF = NTAB(NT+5)	BELTRT
	IF (NCF.NE.0) GO TO 15	BELTRT
C		BELTRT
C	ZERO BELT FRICTION, COMPUTE STRAIN AND FORCE OF ENTIRE BELT.	BELTRT
C		BELTRT
	B1213 = BELT(12,M)+BELT(13,M)	BELTRT
	S = (TL-B1213)/B1213	BELTRT
	SA = S	BELTRT
	SB = S	BELTRT
	IF (S.LT.0.0) S = 0.0	BELTRT
	CALL FRCDFL (S,SDOT,NT,1,FA,ELOSS)	BELTRT
	FB = FA	BELTRT
	GO TO 17	BELTRT
C		BELTRT
C	FULL BELT FRICTION, COMPUTE STRAIN AND FORCE OF EACH PART OF BELT.	BELTRT
C		BELTRT
15	IF (TL.GT.BELT(10,M)) GO TO 16	BELTRT
	FA = 0.0	BELTRT
	FB = 0.0	BELTRT
	SA = (TL-BELT(10,M))/BELT(10,M)	BELTRT
	SB = SA	BELTRT
	BELT(12,M) = TLA	BELTRT
	BELT(13,M) = TLB	BELTRT
	GO TO 17	BELTRT



16	S = (TLA-BELT(12,M))/BELT(12,M)	BELTRT
	SA = S	BELTRT
	IF (S.LT.0.0) S = 0.0	BELTRT
	CALL FRCDFL (S,SDOT,NT,1,FA,ELOSS)	BELTRT
	S = (TLB-BELT(13,M))/BELT(13,M)	BELTRT
	SB = S	BELTRT
	IF (S.LT.0.0) S = 0.0	BELTRT
	CALL FRCDFL (S,SDOT,NT+6,1,FB,ELOSS)	BELTRT
	BELT(10,M) = 0.0	BELTRT
17	BSF(1,NBSF) = SA	BELTRT
	BSF(2,NBSF) = FA	BELTRT
	BSF(3,NBSF) = SB	BELTRT
	BSF(4,NBSF) = FB	BELTRT
	IF (FA+FB.LE.0.0) GO TO 31	BELTRT
C		BELTRT
C	COMPUTE FORCE VECTORS.	BELTRT
C		BELTRT
	DO 20 K=1,3	BELTRT
	UVA (K) = FA*UVA(K)	BELTRT
20	UVB(K) = FB*UVB(K)	BELTRT
C		BELTRT
C	CONVERT FORCES TO INERTIAL REFERENCE AND ADD TO U1 ARRAY.	BELTRT
C		BELTRT
	CALL DOT31(D(1,1,I),UVA,TT )	BELTRT
	CALL DOT31(D(1,1,I),UVB,TTT)	BELTRT
	DO 30 K=1,3	BELTRT
	U1(K,MA) = U1(K,MA) - TT(K)	JTF984
	U1(K,MB) = U1(K,MB) - TTT(K)	JTF984
30	U1(K,I) = U1(K,I)+TTT(K) - TT(K)	JTF984
C		BELTRT
C	CONVERT TORQUES TO LOCAL REFERENCE AND ADD TO U2 ARRAY.	BELTRT
C		BELTRT
	CALL MAT31(D(1,1,MA),TT,ZA)	JTF984
	CALL MAT31(D(1,1,MB),TTT,ZB)	JTF984
	CALL CROSS(BELT(1,M),ZA,TA)	JTF984
	CALL CROSS(BELT(4,M),ZB,TB)	JTF984
	CALL CROSS(APA,UVA,TT)	BELTRT
	CALL CROSS(APB,UVB,TTT)	BELTRT
	DO 40 K=1,3	BELTRT
	U2(K,MA) = U2(K,MA) - TA(K)	JTF984
	U2(K,MB) = U2(K,MB) - TB(K)	JTF984
40	U2(K,I) = U2(K,I)+(TT(K)+TTT(K))	BELTRT
31	CONTINUE	BELTRT
	CALL ELTIME(2,22)	BELTRT
	RETURN	BELTRT
	END	BELTRT



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      BA(I,4)=BA(I,4)+DA(I,J)*(ZB(J)-ZA(J))      BGG
      DAB(I,J)=0.                                BGG
      DO 5 K=1,3                                  BGG
5     DAB(I,J)=DAB(I,J)+DA(I,K)*DB(J,K)          BGG
C                                                    BGG
C     COMPUTE DISTANCE BETWEEN ELLIPSOID CENTERS AND BGG
C     CONVERT ELLIPSOID MATRIX OF OBJECT TO AIRBAG REFERENCE. BGG
C                                                    BGG
      DO 10 I=1,3                                  BGG
      DO 10 J=1,3                                  BGG
      TEMP(I,J) = 0.0                              BGG
      BA(I,4)=BA(I,4)+DAB(I,J)*BFB(J)             BGG
      DO 10 K=1,3                                  BGG
10    TEMP(I,J) = TEMP(I,J) + B(I,K)*DAB(J,K)     BGG
      CALL MAT33(DAB,TEMP,BA)                     BGG
C                                                    BGG
C     CHECK FOR INTERSECTION AND DETERMINE POINTS OF MAXIMUM PENETRATION BGG
C                                                    BGG
      TB = 1.0                                     BGG
      CALL INTERS (A,BA,BA(1,4),TB,Y,TV(1),T1)     BGG
      IF (TB.GT.1.0) RETURN                        BGG
      CALL EDEPTH (A,BA,BA(1,4),TB,Y,CPA,CPB,TV(2),TV(3)) BGG
C                                                    BGG
C     SET UP ORTHOGONAL SYSTEM USING VECTOR BETWEEN POINTS BGG
C     OF MAXIMUM PENETRATION AS ONE AXIS.          BGG
C                                                    BGG
      P = 0.                                       BGG
      DO 20 I=1,3                                  BGG
      PLANE(I,3) = CPA(I)-CPB(I)                  BGG
20    P = PLANE(I,3)**2+P                          BGG
      IF (P.LT.EPS(6)) GO TO 99                   BGG
      PP = DSQRT(P)                               BGG
      DO 25 I=1,3                                  BGG
25    TEMP(I,1) = PLANE(I,3)/PP                   BGG
      CALL ORTHO(PLANE,TEMP,4)                    BGG
C                                                    BGG
C     DEFINE PLANES AT MAXIMUM PENETRATION POINTS. BGG
C                                                    BGG
      DO 40 I=1,3                                  BGG
      PLANE(4,I) = 0.0                             BGG
      DO 40 J=1,3                                  BGG
40    PLANE(4,I) = PLANE(4,I)+PLANE(J,I)*CPB(J)   BGG
      DO 45 K=1,3                                  BGG
45    CBB(K)=CPB(K)-BA(K,4)                       BGG
C                                                    BGG
C     ESTIMATES OF VOLUME AND AREA BASED ON RADII OF CURVATURE BGG
C     AND PENETRATION.                             BGG
C                                                    BGG
      IF=2                                         BGG
      AREA=PI                                      BGG
      DO 70 L=1,2                                  BGG
      RA=RCRT(A,PLANE,CPA,L)                      BGG

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	RB=RCRT(BA, PLANE, CBB, L)	BGG
	IF(PP.GT.RA)RA=PP	BGG
	R=(RA-RB)*.5	BGG
	RC=(RA+RB)*.5	BGG
	VP=PP/(RA+RB)	BGG
	VD=VP	BGG
	ALP=RC*DSQRT(VP*(2.-VP))	BGG
	IF(R.GE.0.)GO TO 60	BGG
	AB=RA+RB-PP	BGG
	BET=(RA**2-RB**2+AB**2)*.5/AB	BGG
	ALP=DSQRT(RA**2-BET**2)	BGG
	R=0.	BGG
	VD=1.-BET/RA	BGG
	VP=(PP+BET-RA)/RB	BGG
60	VLM(L)=RB*(RB*VP)**2*(1.-VP/3.)+RA*(RA*VD)**2*(1.-VD/3.)	BGG
	IF(R.GT.0.)VLM(L)=VLM(L)-ALP*R*R*(PI-2.*(DASIN(1.-VP)+	BGG
	* (1.-VP)*ALP/RC))	BGG
	VLM(L)=VLM(L)*PI	BGG
	AREA=AREA*ALP	BGG
70	IP=1	BGG
	VOL=(VLM(1)+VLM(2))*5	BGG
	IF (IFULL.EQ.0) GO TO 99	BGG
C		BGG
C	SET UP FORCE VECTOR ALONG LINE OF MAXIMUM PENETRATION.	BGG
C		BGG
	CALL DOT31(DAB,CBB,ZBB)	BGG
	DO 76 K=1,3	BGG
	YFA(K)=CPB(K)+BFA(K)	BGG
	YFB(K)=ZBB(K)+BFB(K)	BGG
	FORCE(K) = -AREA*PLANE(K,3)	BGG
76	T1(K) = VA(K)-VB(K)	BGG
C		BGG
C	COMPUTE ANGULAR VELOCITY COMPONENTS,RELATIVE VELOCITY, COMPONENTS	BGG
C	OF RELATIVE VELOCITY ALONG MAX PENETRATION LINE AND MAGNITUDE OF	BGG
C	FORCE.	BGG
C		BGG
	CALL MAT31(DA,T1,T2)	BGG
	CALL CROSS(WA,YFA,T1)	BGG
	CALL CROSS(WB,YFB,T3)	BGG
	CALL MAT31(DAB,T3,T4)	BGG
	FM = 0.0	BGG
	SUM = 0.0	BGG
	DO 77 K=1,3	BGG
	T5(K) = T2(K)+T1(K)-T4(K)	BGG
	SUM = SUM+T5(K)*PLANE(K,3)	BGG
77	FM = FM+FORCE(K)**2	BGG
C		BGG
C	COMPUTE COMPONENTS OF RELATIVE VELOCITY IN TANGENT PLANE,	BGG
C	FRICTION FORCE AND TOTAL FORCE VECTOR.	BGG
C		BGG
	S3 = 0.0	BGG
	DO 78 K=1,3	BGG

	T6(K) = T5(K) - SUM*PLANE(K,3)	BGG
78	S3 = S3+T6(K)**2	BGG
	SQ3 = DSQRT(S3)	BGG
	IF (SQ3.LT.S3TEST) SQ3=S3TEST/(2.0-SQ3/S3TEST)	BGG
	FF = VSCS*DSQRT(FM)/SQ3	BGG
	DO 79 K=1,3	BGG
79	FORCE(K) = FORCE(K) - FF*T6(K)	BGG
C		BGG
C	COMPUTE FRB: FORCE ON REACTION SURFACE IN ITS LOCAL REFERENCE.	BGG
C	TORQ: TORQUE ON AIRBAG IN AIRBAG REFERENCE.	BGG
C	TQB: TORQUE ON REACTION SURFACE IN ITS LOCAL REFERENCE.	BGG
C	FRA: FORCE ON AIRBAG IN INERTIAL REFERENCE.	BGG
C		BGG
	CALL DOT31(DAB, FORCE, FRB)	BGG
	CALL CROSS(YFA, FORCE, TORQ)	BGG
	CALL CROSS(FRB, YFB, TQB)	BGG
	CALL DOT31(DA, FORCE, FRA)	BGG
99	RETURN	BGG
	END	BGG

	SUBROUTINE BINPUT		REV IV 07/24/86	BINPUT
C			SLIP	
C	READS THE INPUT CARDS THAT CONTAINS THE PHYSICAL DIMENSIONS AND			BINPUT
C	CHARACTERISTICS OF THE CRASH VICTIM'S BODY SEGMENTS AND JOINTS.			BINPUT
C				BINPUT
	IMPLICIT REAL*8(A-H,O-Z)			BINPUT
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,			BINPUT
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG			PAGE
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),			SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),			BINPUT
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)			BINPUT
	COMMON/CNTRSF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)			EDGE
	COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),			BINPUT
*	BLTTTL(5,8),PLTTL(5,30),BAGTTL(5,6),SEG(30),			BINPUT
*	JOINT(30),CGS(30),JS(30)			BINPUT
	REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTL,BAGTTL,SEG,JOINT			BINPUT
	LOGICAL*1 CGS,JS			BINPUT
	COMMON/INTEST/ SGTEST(3,4,30),XTEST(3,120),SEGT(120),REGT(120)			BINPUT
	REAL SEGT			BINPUT
	COMMON/FLXBLE/ HF(4,12,8),B42(3,3,24),V4(3,8),NFLEX(3,8)			BINPUT
	COMMON/GEULER/ IEULER(30),H1R(3,3,90),ANG(3,30),ANGD(3,30),			JDRIFT
*	FE(3,30),TQE(3,30),CONST(5,30)			JDRIFT
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),			BINPUT
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI			TWOPI
	COMMON/RSAVE/ XSG(3,20,3),DPMI(3,3,30),LPMI(30),			ATBIII
*	NSG(9),MSG(20,9),MCG,MCGIN(24,5),KREF(20,9)			TTHKREF
	LOGICAL*1 EULER,SLIP,LDMY			80386
	COMMON/TEMPVS/ YPR1(3,30),YPR2(3,30),YPR3(3,30),YPRPMI(3,30),			BINPUT
*	T1(6),TMP1(3,3),TMP2(3,3),KNT(30),IDYPR(6,30),			SLIP
*	EULER(30),LDMY(2),DMY(34620)			80386
	DATA MXNSEG/30/,MXNJNT/30/,MNFLX/8/			MISC
	CALL ELTIME(1, 2)			BINPUT
	IDYPRT = 0			TGMOD5
C				BINPUT
C	INPUT CARD B.1			BINPUT
C				BINPUT
	READ (5,11) NSEG,NJNT,BDYTTL			BINPUT
11	FORMAT (2I6,8X,5A4)			BINPUT
	IF (NSEG.GT.MXNSEG) STOP 77			MISC
	IF (NJNT.GT.MXNJNT) STOP 78			MISC
C				BINPUT
C	INPUT CARDS B.2.I FOR EACH SEGMENT			BINPUT
C				BINPUT
	DO 12 I=1,NSEG			BINPUT
	READ (5,13) SEG(I),CGS(I),W(I),(PHI(J,I),J=1,3),			BINPUT
*	(BD(J,I),J=1,6),LPMI(I)			BINPUT
13	FORMAT(A4,1X,A1,10F6.0,14)			BINPUT
	DO 81 J=1,3			BINPUT
	IDYPR(J,I) = 4 J			BINPUT
81	YPRPMI(J,I) = 0.0			BINPUT
	IF (LPMI(I).EQ.0) GO TO 12			BINPUT
	READ (5,82) (YPRPMI(J,I),J=1,3)			BINPUT

82	FORMAT(12X,3F6.0)	BINPUT
12	CALL DRCYPR (DPHI(1,1,I),YPRPHI(1,I),IDYPR(1,I))	BINPUT
C		BINPUT
C	INPUT CARDS B.3.J FOR EACH JOINT.	BINPUT
C		BINPUT
	NFLX = 0	BINPUT
	IF (NJNT.EQ.0) GO TO 27	BINPUT
	SLIP = .FALSE.	SLIP
	DO 14 J=1,NJNT	BINPUT
	READ (5,15) JOINT(J),JS(J),JNT(J),IPIN(J),(SR(I,2*J-1),I-1,3),	BINPUT
	* (SR(I,2*J),I-1,3),IEULER(J),CONST(1,J),CONST(2,J),	SLIP
	* (YPR1(I,J),I-1,3),(YPR2(I,J),I-1,3),	SLIP
	* (YPR3(I,J),I-1,3),(IDYPR(I,J),I-1,6)	BINPUT
	ID1 = IDYPR(1,J)	BINPUT
	ID4 = IDYPR(4,J)	BINPUT
	EULER(J) = .FALSE.	SLIP
	IF (IPIN(J).EQ.4) EULER(J) = .TRUE.	SLIP
	IF (IEULER(J).EQ.0.AND.IPIN(J).LE.-4) EULER(J) = .TRUE.	SLIP
	IF (.NOT.EULER(J).AND.IABS(IPIN(J)).GE.5) SLIP = .TRUE.	SLIP
	IF(ID1.NE.0.OR.ID4.NE.0) IDYPRT = 1	TGMOD5
	DO 479 II=1,6	TGMOD5
479	IF(IABS(IDYPR(II,J)).GT.3) STOP 101	TGMOD5
	DO 14 I=1,3	BINPUT
	IF (ID1.EQ.0) IDYPR(I,J) = 4-I	BINPUT
14	IF (ID4.EQ.0) IDYPR(I+3,J) = 4-I	BINPUT
15	FORMAT(A4,1X,A1,2I4,6F6.0,I4,2F6.0/14X,9F6.0,6I2)	SLIP
C		BINPUT
C	COMPUTE NFLX AND NFLEX ARRAY FROM NEGATIVE VALUES OF JNT(J).	BINPUT
C	NFLX WILL BE NUMBER OF CONSTRAINT TORQUES FOR FLEXIBLE SEGMENTS.	BINPUT
C	NFLEX(1, ) REFERENCE SEGMENT (LOWEST NUMBERED SEGMENT OF CHAIN)	BINPUT
C	NFLEX(2, ) INTERIOR SEGMENT NUMBERS	BINPUT
C	NFLEX(3, ) TERMINATING SEGMENT (HIGHEST NUMBERED SEGMENT IN CHAIN)	BINPUT
C	VALUES OF NFLEX NEED NOT BE SEQUENTIAL BUT MUST BE ORDERED.	BINPUT
C	FLEXIBLE SEGMENT MUST BE SIMPLE CHAIN, I.E., BRANCHING SEGMENTS	BINPUT
C	CANNOT BE ATTACHED TO INTERIOR SEGMENTS BUT MAY BE ATTACHED TO	BINPUT
C	REFERENCE OR TERMINATING SEGMENTS.	BINPUT
C		BINPUT
	DO 16 J=1,NJNT	BINPUT
16	KNT(J) = JNT(J)	BINPUT
	DO 22 J=1,NJNT	BINPUT
	IF (KNT(J).GE.0) GO TO 22	BINPUT
	NFA = NFLX+1	BINPUT
	IT = J+1	BINPUT
	IF (IT.GT.NJNT) GO TO 18	BINPUT
	JPl = J+1	BINPUT
	DO 17 L=JPl,NJNT	BINPUT
	IF (IABS(KNT(L)).NE.IT) GO TO 17	BINPUT
	KL = KNT(L)	BINPUT
	KNT(L) = 0	BINPUT
	IF (KL.GT.0) GO TO 18	BINPUT
	NFLX = NFLX+1	BINPUT
	NFLEX(1,NFLX) = IABS(KNT(J))	BINPUT

NFLEX(2,NFLX) - IT	BINPUT
IT - L+1	BINPUT
17 CONTINUE	BINPUT
18 IF (NFLX.GE.NFA) GO TO 20	BINPUT
WRITE (6,19)	BINPUT
19 FORMAT('OERROR IN DEFINING FLEXIBLE SEGMENTS, ONLY ONE NEGATIVE	JNBINPUT
*T IN STRING. PROGRAM TERMINATED.')	BINPUT
STOP 3	BINPUT
20 DO 21 K=NFA,NFLX	BINPUT
21 NFLEX(3,K) - IT	BINPUT
22 CONTINUE	BINPUT
C	BINPUT
C INPUT CARDS B.4.J FOR EACH JOINT.	BINPUT
C	BINPUT
DO 23 J=1,NJNT	BINPUT
READ (5,24) (SPRING(I,3*J-2),I-1,5),(SPRING(I,3*J-1),I-1,5)	BINPUT
23 IF (EULER(J)) READ(5,24)(SPRING(I,3*J),I-1,5),(ANG(I,J),I-1,3)	SLIP
24 FORMAT(2(4F6.0,F12.0))	BINPUT
C	BINPUT
C INPUT CARDS B.5.J FOR EACH JOINT.	BINPUT
C	BINPUT
DO 25 J=1,NJNT	BINPUT
READ (5,26) (VISC(I,3*J-2),I-1,7)	BINPUT
IF (.NOT.EULER(J)) GO TO 25	SLIP
READ (5,26) (VISC(I,3*J-1),I-1,7)	BINPUT
READ (5,26) (VISC(I,3*J ),I-1,7)	BINPUT
25 CONTINUE	BINPUT
26 FORMAT(5F6.0,18X,2F6.0)	BINPUT
C	BINPUT
C INPUT CARDS B.6.I FOR EACH SEGMENT.	BINPUT
C	BINPUT
27 DO 28 I=1,NSEG	BINPUT
28 READ (5,29) ((SGTEST(J,K,I),J=1,3),K=1,4)	BINPUT
29 FORMAT(12F6.0)	BINPUT
C	BINPUT
C PRINT CARD B.1	BINPUT
C	BINPUT
WRITE (6,30) BDYTTL,NSEG,NJNT,NPG,UNITM,UNITT,UNITL,UNITL,	PAGE
* UNITL,UNITM	PAGE
NPG=NPG+1	PAGE
30 FORMAT('1 CRASH VICTIM',5X,5A4,I5,' SEGMENTS',I5,' JOINTS',58X,	PAGE
* 'PAGE',I5/120X,'CARD B.1'/25X,'PRINCIPAL MOMENTS OF INERTIA',	PAGE
* 14X,'SEGMENT CONTACT ELLIPSOID',28X,'CARDS B.2'/	BINPUT
* 3X,'SEGMENT',6X,'WEIGHT',7X,'(' ,A4,' - ',A4,'**2',A4,')',	BINPUT
* 11X,'SEMIAXES (' ,A4,')',12X,'CENTER (' ,A4,')',	BINPUT
* 11X,'PRINCIPAL AXES (DEG)'/	BINPUT
* ' I SYM PLOT (' ,A4,')',7X,'X',8X,'Y',8X,'Z ',	BINPUT
* 2(9X,'X',7X,'Y',7X,'Z'),8X,'YAW',5X,'PITCH',5X,'ROLL'//)	BINPUT
C	BINPUT
C PRINT CARDS B.2.I FOR EACH SEGMENT.	BINPUT
C	BINPUT
DO 31 I=1,NSEG	BINPUT



31	WRITE (6,32) I,SEG(I),CGS(I),W(I),(PHI(J,I),J-1,3),	BINPUT
*	(BD(J,I),J-1,6),(YPRPMI(J,I),J-1,3)	BINPUT
32	FORMAT(I3,1X,A4,2X,A1,F11.3,2X,3F9.4,2(2X,3F8.3),1X,3F9.2)	BINPUT
	IF (NJNT.EQ.0) GO TO 50	BUTLER1
C		BINPUT
C	PRINT CARDS B.3.J FOR EACH JOINT.	BINPUT
C		BINPUT
	IF(IDYPRT.EQ.0) WRITE(6,33) UNITL,UNITL	TGMOD5
	IF(IDYPRT.EQ.1) WRITE(6,733) UNITL,UNITL	TGMOD5
33	FORMAT(///120X,'CARDS B.3'/	BINPUT
*	3X,'JOINT',15X,'LOCATION(' ,A4,' ) - SEG(JNT)',	BINPUT
*	3X,'LOCATION(' ,A4,' ) - SFJ(J+1)',	BINPUT
*	2X,'PRIN. AXIS(DEG) - SEG(JNT)',	BINPUT
*	2X,'PRIN. AXIS(DEG) - SEG(J+1)'/	BINPUT
*	' J SYM PLOT JNT PIN', 2(6X,'X',8X,'Y',8X,'Z',3X),	BINPUT
*	2(5X,'YAW',5X,'PITCH',5X,'ROLL',1X) /)	BINPUT
733	FORMAT(///120X,'CARDS B.3'/	TGMOD5
*	3X,'JOINT',15X,'LOCATION(' ,A4,' ) - SEG(JNT)',	TGMOD5
*	3X,'LOCATION(' ,A4,' ) - SEG(J+1)',	TGMOD5
*	2X,'PRIN. AXIS(DEG) - SEG(JNT)',	TGMOD5
*	2X,'PRIN. AXIS(DEG) - SEG(J+1)'/	TGMOD5
*	' J SYM PLOT JNT PIN', 2(6X,'X',8X,'Y',8X,'Z',3X),	TGMOD5
*	'ID1 YAW ID2 PITCH ID3 ROLL ',	TGMOD5
*	'ID4 YAW ID5 PITCH ID6 ROLL ',/)	TGMOD5
DO 34	J=1,NJNT	BINPUT
	IF(IDYPRT.EQ.0)	TGMOD5
*WRITE (6,35)	J,JOINT(J),JS(J),JNT(J),JPIN(J),(SR(I,2*J-1),I-1,3),	TGMOD5
*	(SR(I,2*J),I-1,3),(YPR1(I,J),I-1,3),(YPR2(I,J),I-1,3)	BINPUT
	IF(IDYPRT.EQ.1)	TGMOD5
*WRITE(6,735)	J,JOINT(J),JS(J),JNT(J),JPIN(J),(SR(I,2*J-1),I-1,3),	TGMOD5
*	(SR(I,2*J),I-1,3),(IDYPR(I,J),YPR1(I,J),I-1,3),	TGMOD5
*	(IDYPR(I+3,J),YPR2(I,J),I-1,3)	TGMOD5
	IF (.NOT.EULER(J)) GO TO 34	SLIP
	IEULER(J) = 8	BINPUT
	IF (JPIN(J).EQ.4) GO TO 34	BINPUT
	IEULER(J) = 11 + JPIN(J)	BINPUT
	JPIN(J) = -4	BINPUT
34	CONTINUE	BINPUT
35	FORMAT(I3,1X,A4,2X,A1,2X,2I3,2(1X,3F9.3),2(1X,3F9.2) )	BINPUT
735	FORMAT(I3,1X,A4,2X,A1,2X,2I3,2(1X,3F9.3),2(1X,3(1X,11,F7.2)))	TGMOD5
	IF (.NOT.SLIP) GO TO 89	SLIP
	WRITE (6,83) UNITM,UNITM	SLIP
83	FORMAT(// ' UNLOCK CONDITIONS FOR SLIP JOINTS' /	SLIP
*	' JOINT TENSION COMPRESSION' /	SLIP
*	14X,'(' ,A4,' )',7X,'(' ,A4,' )' /)	SLIP
DO 85	J = 1,NJNT	SLIP
	IF (EULER(J)) GO TO 85	SLIP
	IF (IABS(JPIN(J)).LT.5) GO TO 85	SLIP
	WRITE (6,84) J,CONST(1,J),CONST(2,J)	SLIP
84	FORMAT(1X,16,4X,F10.3,3X,F10.3)	SLIP
85	CONTINUE	SLIP
C		BINPUT

C	SET UP HT MATRIX FROM YPR1 & YPR2 INPUT.	BINPUT
C	HA IS 3RD COLUMN & HB IS 2ND COLUMN OF HT.	BINPUT
C	FOR A SLIP JOINT(IPIN=7),HB IS 3RD COLUMN OF HT.	SLIP
C		BINPUT
89	IF (NPRT(23).NE.0) WRITE (6,36) NPG	SLIP
	IF (NPRT(23).NE.0) NPG=NPG+1	PAGE
36	FORMAT('1 HT ARRAY AS COMPUTED FROM YPR1 & YPR2 INPUT.',77X,	PAGE
	* 'PAGE',15)	PAGE
	DO 38 J=1,NJNT	BINPUT
	SR(4,2*J-1) = 0.0	SLIP
	SR(4,2*J ) = 0.0	SLIP
	CALL DRCYPR (TMP1,YPR1(1,J),IDYPR(1,J))	BINPUT
	CALL DRCYPR (TMP2,YPR2(1,J),IDYPR(4,J))	BINPUT
	DO 37 I=1,3	BINPUT
	ANGD(I,J) = 0.0	BINPUT
	HA(I,2*J-1) = 0.0	BINPUT
	HA(I,2*J ) = 0.0	BINPUT
	K = 2	SLIP
	IF (IABS(IPIN(J)).EQ.7) K = 3	SLIP
	HB(I,2*J-1) = TMP1(K,I)	SLIP
	HB(I,2*J ) = TMP2(K,I)	SLIP
	DO 77 K=1,3	SLIP
	HT(I,K,2*J-1) = TMP1(K,I)	SLIP
77	HT(I,K,2*J ) = TMP2(K,I)	SLIP
	IF (.NOT.EULER(J)) GO TO 37	SLIP
	CONST(I,J) = YPR3(I,J)*RADIAN	SLIP
	ANG(I,J) = ANG(I,J)*RADIAN - CONST(I,J)	SLIP
37	CONTINUE	SLIP
38	IF (NPRT(23).NE.0) WRITE (6,39) J,JOINT(J),	BINPUT
	* ((HT(I,K,2*J-1),K=1,3),(HT(I,K,2*J),K=1,3),I=1,3)	BINPUT
39	FORMAT('0',I4,2X,A4,3X,3F12.6,3X,3F12.6/(14X,3F12.6,3X,3F12.6))	BINPUT
C		BINPUT
C	PRINT CARDS B.4.J FOR EACH JOINT.	BINPUT
C		BINPUT
	WRITE (6,41) NPG,UNITL,UNITM,UNITL,UNITM	PAGE
	NPG=NPG+1	PAGE
41	FORMAT('1 JOINT TORQUE CHARACTERISTICS',93X,	PAGE
	* 'PAGE',15/120X,'CARDS B.4'/	PAGE
	*23X,'FLEXURAL SPRING CHARACTERISTICS',28X,'TORSIONAL SPRING' ,	BINPUT
	*' CHARACTERISTICS'//	BINPUT
	*15X,'SPRING COEF. (' ,2A4,'/DEG**J)',6X,'ENERGY JOINT',	BINPUT
	* 7X,'SPRING COEF. (' ,2A4,'/DEG**J)',6X,'ENERGY JOINT'/	JBINPUT
	*OINT ',2(8X.'LINEAR QUADRATIC CUBIC DISSIPATION STOP ')	BINPUT
	*/8X,2(8X,'(J=1)',7X,'(J=2)',7X,'(J=3)',7X,'COEF. (DEG)')/)	BINPUT
	DO 42 J=1,NJNT	BINPUT
	J1 = 3*J-2	BINPUT
	J2 = 3*J-1	BINPUT
	J3 = 3*J	BINPUT
	WRITE (6,43) J,JOINT(J),((SPRING(I,JJ),I=1,5),JJ=J1,J2)	BINPUT
42	IF (EULER(J)) WRITE (6,44) (SPRING(I,J3),I=1,5)	SLIP
43	FORMAT(I3,1X,A4,2(3X,3F12.3,2F10.3))	BINPUT
44	FORMAT(11X,3F12.3,2F10.3)	BINPUT

C		BINPUT
C	PRINT CARDS B.5.J FOR EACH JOINT.	BINPUT
C		BINPUT
	WRITE (6,46) (UNITL,UNITM,UNITT,I-1,2),(UNITL,UNITM,I-1,2),UNITT	BINPUT
46	FORMAT(///120X,'CARDS B.5'/	BINPUT
	*38X,'JOINT VISCOUS CHARACTERISTICS AND LOCK-UNLOCK CONDITIONS'//	BINPUT
	*14X,'VISCOUS',9X,'COULOMB',7X,'FULL FRICTION',5X,'MAX TORQUE FOR',	BINPUT
	*4X,'MIN TORQUE FOR',4X,'MIN. ANG. VELOCITY',6X,'IMPULSE'/	BINPUT
	*2X,'JOINT',5X,'COEFFICIENT',4X,'FRICTION COEF. ANGULAR VELOCITY',	BINPUT
	*4X,'A LOCKED JOINT',4X,'UNLOCKED JOINT',4X,'FOR UNLOCKED JOINT',	BINPUT
	*4X,'RESTITUTION'/	BINPUT
	*8X,'(' ,3A4,'/DEG) (' ,2A4,')' ,6X,'(DEG/' ,A4,')' ,10X,'(' ,2A4,')' ,	BINPUT
	*8X,'(' ,2A4,')' ,10X,'(RAD/' ,A4,')' ,8X,'COEFFICIENT'/ )	BINPUT
	DO 47 J=1,NJNT	BINPUT
	J1 = 3*J-2	BINPUT
	J2 = 3*J-1	BINPUT
	J3 = 3*J	BINPUT
	WRITE (6,48) J,JOINT(J),(VISC(I,J1),I-1,7)	BINPUT
47	IF (EULER(J)) WRITE (6,49) ((VISC(I,JJ),I-1,7),JJ-J2,J3)	SLIP
48	FORMAT(I3,1X,A4,F13.3,2F15.2,F22.2,F18.2,F20.2,F17.3)	BINPUT
49	FORMAT( 8X,F13.3,2F15.2,F22.2,F18.2,F20.2,F17.3)	BINPUT
C		BINPUT
C	PRINT CARDS B.6. FOR EACH SEGMENT.	BINPUT
C		BINPUT
50	WRITE (6,51) NPG,(UNITT,UNITL,UNITT,I-1,2)	PAGE
	NPG=NPG+1	PAGE
51	FORMAT('1',122X,'PAGE',I5/20X,	PAGE
	* 'SEGMENT INTEGRATION CONVERGENCE TEST INPUT',58X,'CARDS B.6'//PAGE	
	* 17X,'ANGULAR VELOCITIES', 11X,'LINEAR VELOCITIES',	BINPUT
	* 10X,'ANGULAR ACCELERATIONS',9X,'LINEAR ACCELERATIONS'//	BINPUT
	* 21X,'(RAD/' ,A4,')' , 18X,'(' ,A4,'/' ,A4,')' ,	BINPUT
	* 17X,'(RAD/' ,A4,'**2)' , 16X,'(' ,A4,'/' ,A4,'**2)'//	BINPUT
	* ' SEGMENT', 4(' MAG. ABS. REL. ' ) /	BINPUT
	* ' NO. SYM', 4(' TEST ERROR ERROR ' ) //	BINPUT
	DO 52 I=1,NSEG	BINPUT
52	WRITE (6,53) I,SEG(I),((SGTEST(J,K,I),J-1,3),K-1,4)	BINPUT
53	FORMAT(I3,1X,A4,4(F11.3,F9.3,F9.4) )	BINPUT
	IF (NFLX.EQ.0) GO TO 62	BINPUT
C		BINPUT
C	INPUT AND PRINT CARDS B.7	BINPUT
C	CARD B.7.A NFX: NO. OF INTERIOR SEGMENTS OF FLEXIBLE ELEMENTS.	BINPUT
C	KNT(J),J=1,NFX: THE SEGMENT NUMBERS.	BINPUT
C		BINPUT
	READ (5,54) NFX,(KNT(J),J=1,NFX)	BINPUT
54	FORMAT(18I4)	BINPUT
	IF (NFX.NE.NFLX) WRITE (6,55) NFX,NFLX	BINPUT
55	FORMAT('OINPUT ERROR ON CARD B.7.A, NFX =',I4, ' BUT NFLX =',I4/	BINPUT
	* ' AS COMPUTED FROM CARDS B.3. PROGRAM TERMINATED.')	BINPUT
	IF (NFX.NE.NFLX) STOP 4	BINPUT
	WRITE (6,56) NPG	PAGE
	NPG=NPG+1	PAGE
56	FORMAT('1',122X,'PAGE',I5/121X,'CARDS B.7')	PAGE

DO 60 JJ=1,NFX	BINPUT
DO 57 K=1,NFLX	BINPUT
IF (KNT(JJ).EQ.NFLEX(2,K)) GO TO 59	BINPUT
57 CONTINUE	BINPUT
WRITE (6,58) KNT(JJ)	BINPUT
58 FORMAT('OINPUT ERROR ON CARD B.7.J, SEGMENT NO.',I4,' IS NOT AN IN	BINPUT
*TERIOR SEGMENT OF A FLEXIBLE ELEMENT FROM DATA ON CARDS B.3.')	BINPUT
* ' PROGRAM TERMINATED.')	BINPUT
STOP 5	BINPUT
59 IF(NFLX.GT.MNFLX) STOP 99	TGMOD5
C	BINPUT
C CARDS B.7.J HF ARRAY FOR SEGMENT KNT(JJ)	BINPUT
C	BINPUT
READ (5,29) ((HF(I,J,K),J=1,12),I=1,4)	TGMOD5
DO 737 LL=1,3	TGMOD5
L = (LL-1)*4	TGMOD5
DO 737 I=1,4	TGMOD5
DO 737 J=1,4	TGMOD5
737 IF(HF(I,J+L,K).NE.HF(J,I+L,K)) STOP 100	TGMOD5
60 WRITE (6,61) KNT(JJ),K,(NFLEX(I,K),I=1,3),	BINPUT
* ((HF(I,J,K),J=1,12),I=1,4)	BINPUT
61 FORMAT('O HF ARRAY FOR INTERIOR SEGMENT NO.',I4,20X,	BINPUT
* '(NFLEX(I,',I1,')',I=1,3) =',3I6//	BINPUT
* (3X,4F10.4,3X,4F10.4,3X,4F10.4) )	BINPUT
62 IF (NJNT.EQ.0) GO TO 65	BINPUT
C	BINPUT
C CHANGE SPRING AND VISC FROM DEG TO RAD	BINPUT
C	BINPUT
DO 64 I=1,NJNT	BINPUT
J1 = 3*I-2	BINPUT
J2 = 3*I-1	BINPUT
IF (EULER(I)) J2= 3*I	SLIP
DO 63 J=J1,J2	BINPUT
SPRING(1,J) = SPRING(1,J)/RADIAN	BINPUT
SPRING(2,J) = SPRING(2,J)/RADIAN**2	BINPUT
SPRING(3,J) = SPRING(3,J)/RADIAN**3	BINPUT
SPRING(5,J) = SPRING(5,J)*RADIAN	BINPUT
63 CONTINUE	BINPUT
IF (.NOT.EULER(I)) J2 = J1	SLIP
DO 64 J=J1,J2	BINPUT
VISC (1,J) = VISC (1,J)/RADIAN	BINPUT
64 VISC (3,J) = VISC (3,J)*RADIAN	BINPUT
C	BINPUT
C W ARRAY HAS BEEN SUPPLIED IN LBS. SET UP RECIPROCAL MASS (RW)	BINPUT
C AND MOMENT OF INERTIA (RPHI) ARRAYS. HOWEVER, IF W OR ANY ELEMENT	BINPUT
C OF PHI IS ZERO, SEGMENT WILL BE CONSIDERED SINGULAR (ISING=1) AND	BINPUT
C ALL RECIPROCALLS WILL BE ZERO SO AS TO NULLIFY COMPUTATIONS IN THE	BINPUT
C DAUX ROUTINES. NS IS THE NUMBER OF SINGULAR SEGMENTS.	BINPUT
C	BINPUT
65 NS = 0	BINPUT
DO 68 I=1,NSEG	BINPUT
ISING(I) = 0	BINPUT

RW(I) = 0.0	BINPUT
IF (W(I).EQ.0.0) ISING(I) = 1	BINPUT
DO 66 K=1,3	BINPUT
IF (PHI(K,I).EQ.0.0) ISING(I) = 1	BINPUT
66 RPHI(K,I) = 0.0	BINPUT
IF (ISING(I).EQ.1) NS = NS+1	BINPUT
IF (ISING(I).EQ.1) GO TO 68	BINPUT
RW(I) = G/W(I)	BINPUT
DO 67 K=1,3	BINPUT
67 RPHI(K,I) = 1.0/PHI(K,I)	BINPUT
68 CONTINUE	BINPUT
C	BINPUT
C SET UP ELLIPSOID MATRIX AND INVERSE (ASSUME YAW,PITCH,ROLL = 0)	BINPUT
C FOR 1ST NSEG ELLIPSOIDS IN BD(7-15) AND BD(16-24).	BINPUT
C	BINPUT
DO 71 J=1,NSEG	BINPUT
DO 70 I=7,24	BINPUT
70 BD(I,J) = 0.0	BINPUT
DO 71 I=1,3	BINPUT
BD(4*I+3,J) = 1.0/BD(I,J)**2	BINPUT
71 BD(4*I+12,J) = BD(I,J)**2	BINPUT
RETURN	BINPUT
END	BINPUT

	SUBROUTINE BLKDTA		BLKDTA
		REV IV 07/23/86	TWOPI
C	THIS SUBROUTINE REPLACES THE BLOCK DATA SUBPROGRAM OF PREVIOUS		BLKDTA
C	VERSIONS OF CVS-III TO INITIALIZE COMMON/CNSNTS/ IN A MANNER		BLKDTA
C	THAT IS INDEPENDENT OF THE COMPUTER SYSTEM BEING UTILIZED.		BLKDTA
C			BLKDTA
	IMPLICIT REAL*8 (A-H,O-Z)		BLKDTA
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),		BLKDTA
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI		TWOPI
	COMMON/TEMPVS/ ZERO,ONE,THREE,TEN,ONE80,DMMY(35108)		80386
	DATA UM/8H LBS / , UT/8H SEC / , UL/8H IN /		BLKDTA
	ZERO = 0.0		BLKDTA
	ONE = 1.0		BLKDTA
	UNITM = UM		BLKDTA
	UNITT = UT		BLKDTA
	UNITL = UL		BLKDTA
	G = 386.088D0		BLKDTA
	GRAVITY(1) = ZERO		BLKDTA
	GRAVITY(2) = ZERO		BLKDTA
	GRAVITY(3) = G		BLKDTA
	THREE = 3.0		BLKDTA
	TEN = 10.0		BLKDTA
	ONE80 = 180.0		BLKDTA
	PI = DATAN2(ZERO,-ONE)		BLKDTA
	TWOPI = 2.0*PI		TWOPI
	RADIAN = PI/ONE80		BLKDTA
	THIRD = ONE/THREE		BLKDTA
	EPS(1) = ONE/TEN		BLKDTA
	DO 10 I=2,24		BLKDTA
10	EPS(I) = EPS(I-1)/TEN		BLKDTA
	RETURN		BLKDTA
	END		BLKDTA

	SUBROUTINE CFACTT(A,B,D)		CFACTT
C		REV 03	05/31/73CFACTT
C	GIVEN 3X3 MATRIX A		CFACTT
C	COMPUTE B TRANSPOSE OF COFACTORS (SIGNED MINORS)		CFACTT
C	AND D THE VALUE OF THE DETERMINANT OF A.		CFACTT
C	INVERSE OF A IS B(J,K)/D		CFACTT
C			CFACTT
	IMPLICIT REAL*8 (A-H,O-Z)		CFACTT
	DIMENSION A(3,3),B(3,3)		CFACTT
	M = 4		CFACTT
	L = 2		CFACTT
	N = 3		CFACTT
	D = 0.0		CFACTT
	DO 20 J=1,3		CFACTT
	B(J,J) = A(L,L)*A(N,N)-A(L,N)*A(N,L)		CFACTT
	IF (J.EQ.3) GO TO 20		CFACTT
	L = N		CFACTT
	N = J		CFACTT
	KK = J+1		CFACTT
	DO 15 K=KK,3		CFACTT
	M = M-1		CFACTT
	B(K,J) = A(K,M)*A(M,J)-A(K,J)*A(M,M)		CFACTT
15	B(J,K) = A(J,M)*A(M,K)-A(J,K)*A(M,M)		CFACTT
20	D = D+A(1,J)*B(J,1)		CFACTT
	RETURN		CFACTT
	END		CFACTT

	SUBROUTINE CHAIN(ISKIP)	JDRIFT
		REV IV 07/24/86SLIP
C	COMPUTES THE LINEAR POSITION AND VELOCITY IN INERTIAL REFERENCE	CHAIN
C	OF BODY SEGMENTS FROM THOSE OF THE REFERENCE SEGMENTS	CHAIN
C	(I.E., SEGMENT NO. 1 AND EACH SEGMENT J FOR WHICH JNT(J)=0).	CHAIN
C		CHAIN
	IMPLICIT REAL*8(A-H,O-Z)	CHAIN
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,	CHAIN
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),	CHAIN
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)	CHAIN
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),	SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),	CHAIN
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)	CHAIN
	COMMON/CEULER/ IEULER(30),HIR(3,3,90),ANG(3,30),ANGD(3,30),	SLIP
*	FE(3,30),TQE(3,30),CONST(5,30)	SLIP
	COMMON/TEMPVS/ T1(3),T2(3),T3(3),T4(3),T5(3),T6(3),T7(3)	SLIP
*	,DMMY(35092)	80386
	DATA IFIRST/1/	SLIP
	CALL ELTIME (1,11)	ATBIII
	IF (NJNT.EQ.0) GO TO 71	ATBIII
	IF(ISKIP.NE.0) CALL DRIFT	JDRIFT
	DO 70 J=1,NJNT	ATBIII
	K = IABS(JNT(J))	ATBIII
	IF (K.EQ.0) GO TO 70	ATBIII
	IF (ISING(J+1).LT.0) GO TO 70	ATBIII
C		ATBIII
C	COMPUTE SEGMENT POSITIONS BY	ATBIII
C	P(J+1) = P(K) + D(K)'*R(K,J) - D(J+1)'*R(J+1,J)	ATBIII
C		ATBIII
C	COMPUTE SEGMENT VELOCITIES BY	ATBIII
C	V(J+1) = V(K) + D(K)'*W(K) X R(K,J) - D(J+1)'*W(J+1) X R(J+1,J)	ATBIII
C		ATBIII
	CALL CROSS (WMEG(1,K),SR(1,2*J-1),T1)	JDRIFT
	CALL DOT31 (D(1,1,K),T1,T3)	ATBIII
	CALL CROSS (WMEG(1,J+1),SR(1,2*J),T2)	ATBIII
	CALL DOT31 (D(1,1,J+1),T2,T4)	ATBIII
	CALL DOT31 (D(1,1,K),SR(1,2*J-1),T1)	ATBIII
	CALL DOT31 (D(1,1,J+1),SR(1,2*J),T2)	ATBIII
	IF (IABS(IPIN(J)).LT.5) GO TO 50	SLIP
	IF (IEULER(J).EQ.-1)GO TO 50	SLIP
	IF (IFIRST.EQ.1) GO TO 50	SLIP
	DO 40 I = 1,3	SLIP
	T5(I) = SEGLP(I,J+1) + T2(I) - SEGLP(I,K) - T1(I)	SLIP
40	T6(I) = SEGLV(I,J+1) + T4(I) - SEGLV(I,K) - T3(I)	SLIP
	CALL DOT31 (D(1,1,K),HT(1,3,2*J-1),T7)	SLIP
	SR(4,2*J-1) = T5(1)*T7(1) + T5(2)*T7(2) + T5(3)*T7(3)	SLIP
	SR(4,2*J) = T6(1)*T7(1) + T6(2)*T7(2) + T6(3)*T7(3)	SLIP
	CALL CROSS (WMEG(1,K),HT(1,3,2*J-1),T5)	SLIP
	CALL DOT31 (D(1,1,K),T5,T6)	SLIP
	DO 45 I = 1,3	SLIP
	T1(I) = T1(I) + SR(4,2*J-1)*T7(I)	SLIP



45	T3(I) = T3(I) + SR(4,2*J )*T7(I) + SR(4,2*J-1)*T6(I)	SLIP
50	DO 60 I=1,3	SLIP
	SEGLP(I,J+1) = SEGLP(I,K) + T1(I) - T2(I)	ATBIII
60	SEGLV(I,J+1) = SEGLV(I,K) + T3(I) - T4(I)	ATBIII
70	CONTINUE	CHAIN
	IFIRST = 0	SLIP
C		CHAIN
C	OPTIONAL OUTPUT	CHAIN
C		CHAIN
71	IF (NPRT(20).NE.0) WRITE(6,90) TIME	CHAIN
*	,((SEGLP(I,J),I=1,3),J=1,NSEG)	CHAIN
*	,((SEGLV(I,J),I=1,3),J=1,NSEG)	CHAIN
90	FORMAT('0 LINEAR POSITIONS AND VELOCITIES OF BODY SEGMENTS FROM CH	CHAIN
	*AIN FOR TIME =',F12.6/(9F13.5))	CHAIN
	CALL ELTIME(2,11)	CHAIN
	RETURN	CHAIN
	END	CHAIN

	SUBROUTINE CINPUT	CINPUT
		REV III.2 08/08/84REVI
C		
C	INPUT CARDS E.1 - E.4 FOR THE FORCE-DEFLECTION, INERTIAL SPIKE,	CINPUT
C	R FACTOR, G FACTOR AND FRICTION COEFFICIENT FUNCTION DEFINITIONS	CINPUT
C		CINPUT
	IMPLICIT REAL*8(A-H,O-Z)	CINPUT
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,	PAGE
	* NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	PAGE
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)	DIMENB
	COMMON/TEMPVS/JTITL(5,51),NF(5),NT(3),KTITL(31),DDMY(34966)	80386
	REAL JTITL,KTITL	CINPUT
C		CINPUT
	IS = 0	CINPUT
	DO 10 I = 1,50	CINPUT
10	NTI(I) = 0	CINPUT
	J1 = 1	CINPUT
C		CINPUT
C	INPUT CARD E.1 - FUNCTION NO. AND TITLE, IF NO. > 50 SKIP OUT.	CINPUT
C		CINPUT
	11 READ(5,12) I,(KTITL(J ),J = 1,5)	CINPUT
	12 FORMAT (I4,4X,5A4)	CINPUT
	IF (I.GT.50) GO TO 30	CINPUT
	DO 13 J = 1,5	CINPUT
	13 JTITL(J,I) = KTITL(J)	CINPUT
C		CINPUT
C	HAS FUNCTION NO. BEEN ALREADY USED?	CINPUT
C		CINPUT
	IF (NTI(I).NE.0) WRITE(6,14) I	CINPUT
14	FORMAT('0 FUNCTION NO.',I4,' HAS ALREADY BEEN INPUTTED AND WILL BEC	CINPUT
	*REPLACED BY NEXT FUNCTION')	CINPUT
	NTI(I) = J1	CINPUT
	J2 = J1+4	CINPUT
C		CINPUT
C	INPUT CARD E.2	CINPUT
C		CINPUT
	READ(5,15) (TAB(J),J = J1,J2)	CINPUT
15	FORMAT (6F12.0)	CINPUT
	IS = 1-IS	CINPUT
	IF (IS.EQ.0) WRITE(6,16)	CINPUT
	IF (IS.EQ.0) GOTO 40	PAGE
	WRITE(6,41) NPG	PAGE
41	FORMAT('1',122X,'PAGE',I5)	PAGE
	NPG=NPG+1	PAGE
16	FORMAT(//////)	CINPUT
40	WRITE(6,17) I,(JTITL(J,I),J=1,5),I,NTI(I),(TAB(J),J=J1,J2)	PAGE
17	FORMAT(' FUNCTION NO.',I4,4X,5A4,20X,'NTI(',I2,') =',I5,45X,	PAGE
	* 'CARDS E'//10X,'D0',13X,'D1',13X,'D2',13X,'D3',13X,'D4'/5F15.4//)	CINPUT
	DO = TAB(J1)	CINPUT
	D1 = TAB(J1+1)	CINPUT
	D2 = TAB(J1+2)	CINPUT
	J1 = J2+1	CINPUT
	IF (D1) 22,18,20	CINPUT

C		CINPUT
C	FUNCTION IS CONSTANT D2 FOR ALL D.	CINPUT
C		CINPUT
	18 WRITE(6,19) D2	CINPUT
	19 FORMAT(7X,'FUNCTION IS CONSTANT',F12.6)	CINPUT
	GO TO 11	CINPUT
C		CINPUT
C	5TH ORDER POLYNOMIAL ... 1ST FUNCTION	CINPUT
C	INPUT CARD E.3	CINPUT
C		CINPUT
	20 J2 = J1+5	CINPUT
	READ(5,15)(TAB(J),J = J1,J2)	CINPUT
	WRITE(6,21) (TAB(J),J = J1,J2)	CINPUT
	21 FORMAT(7X,'FIRST PART OF FUNCTION - 5TH DEGREE POLYNOMIAL'//	CINPUT
	* 8X,'A0',13X,'A1',13X,'A2',13X,'A3',13X,'A4',13X,'A5',13X/	CINPUT
	* 6F15.6//)	CINPUT
	J1 = J2+1	CINPUT
	GO TO 25	CINPUT
C		CINPUT
C	TABLE LOAD ... 1ST FUNCTION	CINPUT
C	INPUT CARDS E.4.A-E.4.N	CINPUT
C		CINPUT
	22 READ(5,23) NPI	CINPUT
	23 FORMAT (12I6)	CINPUT
	TAB(J1) = NPI	CINPUT
	J1 = J1+1	CINPUT
	J2 = J1+2*NPI-1	CINPUT
	READ(5,15)(TAB(J),J = J1,J2)	CINPUT
	WRITE(6,24) NPI, (TAB(J), J = J1, J2)	CINPUT
	24 FORMAT(7X,'FIRST PART OF FUNCTION - ',I4,' TABULAR POINTS'//	CINPUT
	* 8X,'D',16X,'F(D)' /(F15.6,F15.4))	CINPUT
	J1 = J2+1	CINPUT
C		CINPUT
C	CHECK FOR SECOND FUNCTION	CINPUT
C		CINPUT
	25 IF(D2) 28,11,26	CINPUT
C		CINPUT
C	SECOND FUNCTION ... 5TH ORDER POLYNOMIAL	CINPUT
C	INPUT CARD E.3	CINPUT
C		CINPUT
	26 J2 = J1+5	CINPUT
	READ(5,15)(TAB(J),J = J1,J2)	CINPUT
	WRITE(6,27) (TAB(J),J = J1,J2)	CINPUT
	27 FORMAT(7X,'SECOND PART OF FUNCTION - 5TH DEGREE POLYNOMIAL'//	CINPUT
	* 8X,'B0',13X,'B1',13X,'B2',13X,'B3',13X,'B4',13X,'B5',13X/	CINPUT
	* 6F15.6//)	CINPUT
	J1 = J2+1	CINPUT
	GO TO 11	CINPUT
C		CINPUT
C	SECOND FUNCTION ... TABLE LOAD	CINPUT
C	INPUT CARDS E.4.A-E.4.N	CINPUT
C		CINPUT

28	READ(5,23) NPI	CINPUT
	TAB(J1) = NPI	CINPUT
	J1 = J1+1	CINPUT
	J2 = J1+2*NPI-1	CINPUT
	READ(5,15)(TAB(J),J = J1,J2)	CINPUT
	WRITE(6,29) NPI, (TAB(J), J = J1,J2)	CINPUT
29	FORMAT(7X,'SECOND PART OF FUNCTION - ',I4,' TABULAR POINTS'//	CINPUT
	* 8X,'D',16X,'F(D)' /(F15.6,F15.4))	CINPUT
	J1 = J2+1	CINPUT
	GO TO 11	CINPUT
30	MXTB1 = J1-1	CINPUT
	CALL KINPUT	CINPUT
	CALL FINPUT	CINPUT
	CALL HINPUT	CINPUT
	RETURN	CINPUT
	END	CINPUT



	SUBROUTINE CONTCT	REV III.2 08/08/84	CONTCT
C		REVIII	
C	CONTROLS THE CALLING OF SUBROUTINES REQUIRED TO COMPUTE THOSE		CONTCT
C	EXTERNAL FORCES AND TORQUES ACTING ON THE BODY SEGMENTS.		CONTCT
C			CONTCT
	IMPLICIT REAL*8 (A-H,O-Z)		CONTCT
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		CONTCT
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/JBARTZ/ MNPL( 30),MNBLT( 8),MNSEG( 30),MNBAG( 6),		CONTCT
*	MPL(3,5,30),MBLT(3,5,8),MSEG(3,5,30),MBAG(3,10,6),		CONTCT
*	NTPL( 5,30),NTBLT( 5,8),NTSEG( 5,30)		CONTCT
	COMMON/FORCES/PSF(7,70),BSF(4,20),SSF(10,40),BAGSF(3,20),		NCFORC
*	PRJNT(7,30),NPANEL(5),NPSF,NBSF,NSSF,NBGSF		CONTCT
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)		DIMENB
	COMMON/HRNESS/ BAR(15,100).BB(100).BBDOT(100),PLOSS(2,100),		CONTCT
,*	XLONG(20),HTIME(2),IBAR(5,100),NL(2,100),		CONTCT
*	NPTSPB(20),NPTPLY(20),NTHRNS(20),NBLTPH(5)		CONTCT
	COMMON/WINDFR/ WTIME(30),QFU(3,5),QFV(3,5),WF(3,30),IWIND(30),		WINDOP
*	MWSEG(7,30),NFVSEG(6),NFVNT(5),MOWSEG(30,30)		WINDOP
	DATA MAXPSF/70/,MAXBSF/20/,MAXSSF/46/		NCFORC
C			CHGIII
C	MAXSSF SHOULD BE 40 BUT IT IS ALLOWED TO OVERFLOW INTO BAGSF		NCFORC
C			CHGIII
	CALL ELTIME(1,12)		CONTCT
	NPSF = 0		CONTCT
	NBSF = 0		CONTCT
	NSSF = 0		CONTCT
	IF (NPL.LE.0) GO TO 21		CONTCT
C			CONTCT
C	CALL PLELP ROUTINE FOR EACH ALLOWED PLANE-SEGMENT CONTACT.		CONTCT
C			CONTCT
	DO 20 J=1,NPL		CONTCT
	IF(MNPL(J).EQ.0) GO TO 20		CONTCT
	KPL = MNPL(J)		CONTCT
	DO 19 I=1,KPL		CONTCT
	NPSF = NPSF+1		CONTCT
	IF(NPSF.GT.MAXPSF) STOP 57		CHGIII
	M1 = MPL(1,I,J)		CONTCT
	M2 = MPL(2,I,J)		CONTCT
	M3 = MPL(3,I,J)		CONTCT
	NT = NTPL(I,J)		CONTCT
	JT = NTAB(NT)		CONTCT
	TAB(JT) = 0.0		CONTCT
19	CALL PLELP(M2,M3,M1,J,NT)		CONTCT
20	CONTINUE		CONTCT
21	IF(NBLT.LE.0) GO TO 41		CONTCT
C			CONTCT
C	CALL BELTRT ROUTINE FOR EACH ALLOWED BELT-SEGMENT CONTACT.		CONTCT
C			CONTCT
	DO 30 J=1,NBLT		CONTCT
	IF(MNBLT(J).EQ.0) GO TO 30		CONTCT
	KBLT = MNBLT(J)		CONTCT

DO 29 I=1,KBLT	CONTCT
NBSF = NBSF+1	CONTCT
IF(NBSF.GT.MAXBSF) STOP 58	CHGIII
M1 = MBLT(1,I,J)	CONTCT
M2 = MBLT(2,I,J)	CONTCT
M3 = MBLT(3,I,J)	CONTCT
NT = NTBLT(I,J)	CONTCT
JT = NTAB(NT)	CONTCT
TAB(JT) = 0.0	CONTCT
NF = NTAB(NT+5)	CONTCT
IF (NF.NE.0) JT = NTAB(NT+6)	CONTCT
IF (NF.NE.0) TAB(JT) = 0.0	CONTCT
29 CALL BELTRT(M2,M3,M1,J,NT)	CONTCT
30 CONTINUE	CONTCT
C	CONTCT
C CALL SEGSEG ROUTINE FOR EACH ALLOWED SEGMENT-SEGMENT CONTACT.	CONTCT
C	CONTCT
41 DO 50 J=1,NSEG	CONTCT
IF(MNSEG(J).EQ.0) GO TO 50	CONTCT
KSEG = MNSEG(J)	CONTCT
DO 49 I=1,KSEG	CONTCT
NSSF = NSSF+1	CONTCT
IF(NSSF.GT.MAXSSF) STOP 59	CHGIII
M1 = MSEG(1,I,J)	CONTCT
M2 = MSEG(2,I,J)	CONTCT
M3 = MSEG(3,I,J)	CONTCT
NT = NTSEG(I,J)	CONTCT
JT = NTAB(NT)	CONTCT
TAB(JT) = 0.0	CONTCT
49 CALL SEGSEG(J,M1,M2,M3,NT)	CONTCT
50 CONTINUE	CONTCT
C	CONTCT
C CALL AIRBAG ROUTINE FOR ALLOWED BAG-SEGMENT CONTACTS, IF ANY.	CONTCT
C	CONTCT
IF (NBAG.NE.0) CALL AIRBAG	CONTCT
C	CONTCT
C CALL WINDY ROUTINE FOR WIND FORCES ON EACH SEGMENT.	CONTCT
C	CONTCT
DO 60 J=1,NSEG	CONTCT
IF (MWSEG(1,J).EQ.0) GO TO 60	CONTCT
M=MWSEG(1,J)	WINDOP
M1 = MWSEG(2,J)	CONTCT
M2 = MWSEG(3,J)	CONTCT
M3 = MWSEG(4,J)	CONTCT
NT = MWSEG(5,J)	CONTCT
CALL WINDY (M,M1,M2,M3,NT)	WINDOP
60 CONTINUE	CONTCT
C	CONTCT
C CALL WINDY FOR FORCE FUNCE FUNCTION CALCULATIONS.	CONTCT
C	CONTCT
NFORCE = NFVSEG(6)	CONTCT
IF (NFORCE.GT.0) CALL WINDY (0,M1,M2,M3,NT)	WINDOP

C		CONTCT
C	CALL HBELT ROUTINE FOR EACH HARNESS-BELT SYSTEM.	CONTCT
C		CONTCT
	IF (NHRNSS.LE.0) GO TO 80	CONTCT
	J1 = 1	CONTCT
	KNLO = 0	CONTCT
	DO 70 I=1,NHRNSS	CONTCT
	IF (NBLTPH(I).LE.0) GO TO 70	CONTCT
	J2 = J1 + NBLTPH(I) - 1	CONTCT
	CALL HBELT (J1,J2,KNLO,0)	CONTCT
	J1 = J2+1	CONTCT
	70 CONTINUE	CONTCT
C		CONTCT
C	CALL SPDAMP FOR SPRING DAMPER FORCES, IF ANY	CONTCT
C		CONTCT
	80 IF (NSD.NE.0) CALL SPDAMP	CONTCT
	CALL ELTIME (2,12)	CONTCT
	RETURN	CONTCT
	END	CONTCT



	SUBROUTINE CROSS(A,B,C)		CROSS
C		REV 03	05/31/73CROSS
C	COMPUTES VECTOR CROSS PRODUCT $C = A \times B$ .		CROSS
C			CROSS
C	ARGUMENTS		CROSS
C	A,B,C: VECTORS OF LENGTH 3 WHERE $C=AXB$ .		CROSS
C			CROSS
	IMPLICIT REAL*8 (A-H,O-Z)		CROSS
	DIMENSION A(3),B(3),C(3)		CROSS
	$C(1) = A(2)*B(3) - A(3)*B(2)$		CROSS
	$C(2) = A(3)*B(1) - A(1)*B(3)$		CROSS
	$C(3) = A(1)*B(2) - A(2)*B(1)$		CROSS
	RETURN		CROSS
	END		CROSS

	SUBROUTINE DAUX(I1)		DAUX
C		REV IV	07/24/86SLIP
C	COMPUTES DERIVATIVES FOR INTEGRATOR ROUTINE BY		DAUX
C	(1) SET UP INITIAL VALUES FOR ARRAY OF SYSTEM EQUATIONS.		DAUX
C	(2) MODIFY ARRAYS BY CONSTRAINTS.		DAUX
C	(3) SOLVE SYSTEM OF EQUATION FOR F,TQ,QQ AND V4.		DAUX
C	(4) EVALUATE DERIVATIVES SEGLA AND WMEGD.		DAUX
C			DAUX
	IMPLICIT REAL*8(A-H,O-Z)		DAUX
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		DAUX
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),		DAUX
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		DAUX
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),		SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),		DAUX
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)		DAUX
	COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),		DAUX
*	F(3,30),TQ(3,30),WJ(30),A11(3,3,30)		SLIP
	COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24),		DAUX
*	HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12),		DAUX
*	RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12),		DAUX
*	KQ1(12),KQ2(12),KQTYPE(12)		DAUX
	COMMON/FLXBLE/ HF(4,12,8),B42(3,3,24),V4(3,8),NFLEX(3,8)		DAUX
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),		DAUX
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI		TWOPI
	COMMON/RSAVE/ XSG(3,20,3),DPMI(3,3,30),LPMI(30),		ATBIII
*	NSG(9),MSG(20,9),MCG,MCGIN(24,5),KREF(20,9)		TTHKREF
C			DAUX
C	NOTE: DAUX SHARES /TEMPVS/ WITH DAUX11,12,22,31,32 &33.		DAUX
C			DAUX
	LOGICAL*1 FREE,LDMY		80386
	COMMON/TEMPVS/ C(3,3,600),RHS(3,54),IJK(54,54),IJ,NQ2S,		SLIP
*	IDUM(458),FREE(30),LDMY(2),DMY(27859)		80386
	DIMENSION T1(3),T2(3),T3(3)		TGMOD2
	CALL ELTIME(1,9)		DAUX
C			DAUX
C	IF I1#0, U1 AND U2 HAVE BEEN SET UP BY CALLING ROUTINE.		DAUX
C			DAUX
	IF (I1.NE.0) GO TO 8		DAUX
C			DAUX
C	SET UP INITIAL VALUES OF A & B ARRAYS AND U & V VECTORS.		DAUX
C	MODIFY U1 & U2 ARRAYS BY CONTACT AND JOINT FORCES.		DAUX
C			DAUX
	CALL CHAIN(NPRT(36))		JDRIFT
	CALL SETUP1		DAUX
	CALL VEHPOS		DAUX
	CALL CONTCT		DAUX
	CALL VISPR(0,0)		DAUX
	CALL EJOINT(0,0)		DAUX
	CALL SETUP2		DAUX
	IF (NFLX.GT.0) CALL FLXSEG		DAUX
C			DAUX

C	MODIFY U1,U2 AND ADD G TO U1.	DAUX
C		DAUX
	DO 5 J=1,NGRND	DAUX
	IF (ISING(J)) 1,3,5	DAUX
1	DO 2 I=1,3	DAUX
	U1(I,J) = SEGLA(I,J)	DAUX
2	U2(I,J) = WMEGD(I,J)	DAUX
	GO TO 5	DAUX
3	DO 4 I=1,3	DAUX
	U1(I,J) = U1(I,J)*RW(J) + GRAVITY(I)	DAUX
4	U2(I,J) = U2(I,J)*RPHI(I,J)	DAUX
5	CONTINUE	DAUX
C		DAUX
C	SET UP BODY SEGMENT SYMMETRY	DAUX
C	NSYM(J) = 0 3D MOTION	DAUX
C	NSYM(J) = J CENTRAL SEGMENT 2D MOTION, NO LATERAL MOTION	DAUX
C	NSYM(J) = K SEGMENT J SYMMETRIC TO SEGMENT K, ALL MOTION	DAUX
C	IN THE X-Z PLANE, NO LATERAL MOTION	DAUX
C	NSYM(J) = -K SEGMENT J MIRROR SYMMETRIC TO SEGMENT K, EQUAL	DAUX
C	BUT OPPOSITE LATERAL MOTION PERMITTED	DAUX
C		DAUX
	DO 20 J=1,NGRND	DAUX
	IF (NSYM(J).EQ.0) GO TO 20	DAUX
	K = IABS(NSYM(J))	DAUX
	DO 205 L=1,3	TGMOD2
	T1(L) = U2(L,J)	TGMOD2
	T2(L) = U2(L,K)	TGMOD2
	T3(L) = U2(L,J)	TGMOD2
205	CONTINUE	TGMOD2
	IF(LPMI(J).EQ.0.AND.LPMI(K).EQ.0) GO TO 201	TGMOD2
	IF(LPMI(J).NE.0.AND.LPMI(K).EQ.0) GO TO 202	TGMOD2
	IF(LPMI(J).EQ.0.AND.LPMI(K).NE.0) GO TO 203	TGMOD2
	CALL DOT31(DPMI(1,1,J),U2(1,J),T1)	TGMOD2
	CALL DOT31(DPMI(1,1,K),U2(1,K),T2)	TGMOD2
	GO TO 201	TGMOD2
202	CALL DOT31(DPMI(1,1,J),U2(1,J),T1)	TGMOD2
	GO TO 201	TGMOD2
203	CALL DOT31(DPMI(1,1,K),U2(1,K),T2)	TGMOD2
201	CONTINUE	TGMOD2
	IF (NSYM(J).EQ.J) GO TO 19	DAUX
	IF (K.LT.J) GO TO 16	DAUX
	U1(1,J) = 0.5*(U1(1,J) + U1(1,K))	DAUX
	U1(3,J) = 0.5*(U1(3,J) + U1(3,K))	DAUX
	T3(2) = 0.5*(T1(2) + T2(2))	TGMOD2
	GO TO 17	DAUX
16	U1(1,J) = U1(1,K)	DAUX
	U1(3,J) = U1(3,K)	DAUX
	T3(2) = T2(2)	DAUX
17	IF (NSYM(J).GT.0) GO TO 19	DAUX
	IF (K.LT.J) GO TO 18	DAUX
	U1(2,J) = 0.5*(U1(2,J) - U1(2,K))	DAUX
	T3(1) = 0.5*(T1(1) - T2(1))	TGMOD2

T3(3) = 0.5*(T1(3) - T2(3))	TGMOD2
GO TO 206	DAUX
18 U1(2,J) = -U1(2,K)	DAUX
T3(1) = -T2(1)	TGMOD2
T3(3) = -T2(3)	TGMOD2
GO TO 206	DAUX
19 U1(2,J) = 0.0	DAUX
T3(1) = 0.0	TGMOD2
T3(3) = 0.0	TGMOD2
206 IF(LPMI(J).EQ.0) GO TO 207	TGMOD2
CALL MAT31(DPMI(1,1,J),T3,U2(1,J))	TGMOD2
GO TO 20	TGMOD2
207 U2(1,J) = T3(1)	TGMOD2
U2(2,J) = T3(2)	TGMOD2
U2(3,J) = T3(3)	TGMOD2
20 CONTINUE	TGMOD2
C	DAUX
C INITIALIZE IJK ARRAY AND IJ COUNTER TO ZERO.	DAUX
C	DAUX
8 NQ2S = 2*NS + NFLX + NQ	DAUX
NJ2 = NQ2S + 2*NJNT	DAUX
IF (NJ2.GT.54) WRITE (6,11) NS,NFLX,NQ,NJNT,NJ2	DAUX
11 FORMAT('ONS=',I6,',NFLX=',I6,',NQ=',I6,',NJNT=',I6,', AND NJ2=',I6,/AFREVS	
*' THE VALUE OF NJ2 EXCEEDS THE ARRAY SIZES FOR RHS AND IJK IN SUBRDAUX	
*OUTLINE DAUX. PROGRAM TERMINATED.')	DAUX
IF (NJ2.GT.54) STOP 34	DAUX
MJ2 = NJ2	DAUX
DO 10 I=1,NJ2	DAUX
DO 10 J=1,NJ2	DAUX
10 IJK(I,J) = 0	DAUX
IJ = 0	DAUX
C	DAUX
C ELMINATE SEGLA AND WMEGD FROM SYSTEM OF EQUATIONS.	DAUX
C	DAUX
IF (NS.GT.0) CALL DAUX55	DAUX
IF (NJNT.EQ.0) GO TO 12	DAUX
IF (NFLX.GT.0) CALL DAUX44	DAUX
CALL DAUX11	DAUX
CALL DAUX12	DAUX
CALL DAUX22	DAUX
12 IF (NQ.LE.0) GO TO 15	DAUX
IF (NJNT.EQ.0) GO TO 13	DAUX
CALL DAUX31	DAUX
CALL DAUX32	DAUX
13 CALL DAUX33	DAUX
DO 14 I=1,NQ	DAUX
14 IF (KQTYPE(I).GE.4) MJ2 = -NJ2	DAUX
15 IF (NPRT(8).EQ.0) GO TO 28	DAUX
21 WRITE (6,22) NPG,(J,J=1,NJ2)	PAGE
NPG=NPG+1	PAGE
22 FORMAT('1 DAUX PRINT OF IJK MATRIX',97X,'PAGE',I5//6X,40I3)	PAGE
DO 23 I=1,NJ2	DAUX

23	WRITE (6,24) I,(IJK(I,J),J=1,NJ2)	DAUX
24	FORMAT(I3,3X,40I3)	DAUX
	WRITE (6,29)	DAUX
29	FORMAT('0 DAUX PRINT OF RHS ARRAY'//)	DAUX
	DO 30 K=1,NJ2	DAUX
30	WRITE (6,27) K,(RHS(I,K),I=1,3)	DAUX
	WRITE (6,25) NPG	PAGE
	NPG=NPG+1	PAGE
25	FORMAT('1 DAUX PRINT OF C ARRAY ELEMENTS',91X,'PAGE',15//)	PAGE
	DO 26 K=1,IJ	DAUX
26	WRITE (6,27) K,((C(I,J,K),J=1,3),I=1,3)	DAUX
27	FORMAT(I6,9G14.7)	DAUX
28	IF (NPRT(8).EQ.-2) GO TO 31	DAUX
C		DAUX
C	SOLVE SYSTEM OF EQUATIONS FOR F.TQ,QQ & V4.	DAUX
C		DAUX
	CALL FSMSOL (C,RHS,IJK,MJ2,IJ,54,600)	CHGIII
	IF (NPRT(8).EQ. 2) NPRT(8) = -2	DAUX
	IF (NPRT(8).EQ.-2) GO TO 21	DAUX
31	IF (NPRT(8).EQ.-2) NPRT(8) = 0	DAUX
	EPS12 = EPS(12)	JDRIFT
	IF (NJNT.EQ.0) GO TO 49	DAUX
	DO 51 I=1,NJNT	DAUX
	NJ = NQ2S + I	DAUX
	NI = NJ+NJNT	DAUX
	DO 51 K=1,3	DAUX
	IF (DABS(RHS(K,NJ)).LT.EPS12) RHS(K,NJ) = 0.0	DAUX
	IF (DABS(RHS(K,NI)).LT.EPS12) RHS(K,NI) = 0.0	DAUX
	TQ(K,I) = TQ(K,I) - RHS(K,NI)	DAUX
51	F(K,I) = RHS(K,NJ)	DAUX
49	IF (NQ.EQ.0) GO TO 53	DAUX
	DO 52 I=1,NQ	DAUX
	J = 2*NS + NFLX + I	DAUX
	DO 52 K=1,3	DAUX
	IF (KQTYPE(I).I.T.0) RHS(K,J) = 0.0	DAUX
	IF (DABS(RHS(K,J)).LT.EPS12) RHS(K,J) = 0.0	DAUX
52	QQ(K,I) = RHS(K,J)	DAUX
53	IF (NFLX.EQ.0) GO TO 70	DAUX
	DO 54 I=1,NFLX	DAUX
	J = 2*NS + I	DAUX
	DO 54 K=1,3	DAUX
	IF (DABS(RHS(K,J)).LT.EPS12) RHS(K,J) = 0.0	DAUX
54	V4(K,I) = RHS(K,J)	DAUX
C		DAUX
C	BACKUP SOLUTION FOR SEGIA AND WMEGD.	DAUX
C		DAUX
70	DO 71 J=1,NGRND	DAUX
	DO 71 I=1,3	DAUX
	SEGIA(I,J) = U1(I,J)	DAUX
71	WMEGD(I,J) = U2(I,J)	DAUX
	IF (NS.EQ.0) GO TO 79	DAUX
C		DAUX

C	SET UP SEGLA & WMEGD FOR SINGULAR SEGMENTS.	DAUX
C		DAUX
	IS = 0	DAUX
	DO 78 J=1,NGRND	DAUX
	IF (ISING(J).LE.0) GO TO 78	DAUX
	IS = IS+2	DAUX
	DO 77 I=1,3	DAUX
	IF (DABS(RHS(I,IS-1)).LT.EPS12) RHS(I,IS-1) = 0.0	DAUX
	SEGLA(I,J) = SEGLA(I,J) + RHS(I,IS-1)	DAUX
	IF (DABS(RHS(I,IS)).LT.EPS12) RHS(I,IS) = 0.0	DAUX
	77 WMEGD(I,J) = WMEGD(I,J) + RHS(I,IS)	DAUX
	78 CONTINUE	DAUX
	79 IF (NJNT.EQ.0) GO TO 80	DAUX
C		DAUX
C	ELIMINATE F	DAUX
C		DAUX
	DO 75 M=1,NJNT	DAUX
	N = IABS(JNT(M))	DAUX
	IF (N.EQ.0) GO TO 73	DAUX
	DO 72 I=1,3	DAUX
	DO 72 J=1,3	DAUX
	SEGLA(I,N) = SEGLA(I,N) - A11(I,J,M)*RW(N)*F(J,M)	SLIP
	SEGLA(I,M+1) = SEGLA(I,M+1) + A11(I,M)*RW(M+1)*F(J,M)	SLIP
	WMEGD(I,N) = WMEGD(I,N) - B1(I,J,2*M-1)*RPHI(I,N)*F(J,M)	DAUX
	72 WMEGD(I,M+1) = WMEGD(I,M+1) - B1(I,J,2*M)*RPHI(I,M+1)*F(J,M)	DAUX
C		DAUX
C	ELIMINATE TQ	DAUX
C		DAUX
	73 IF (FREE(M)) GO TO 75	SLIP
	L = NQ2S + NJNT + M	DAUX
	DO 74 I=1,3	DAUX
	DO 74 J=1,3	DAUX
	WMEGD(I,N) = WMEGD(I,N) - A22(I,J,2*M-1)*RPHI(I,N)*RHS(J,L)	DAUX
	74 WMEGD(I,M+1) = WMEGD(I,M+1) + A22(I,J,2*M)*RPHI(I,M+1)*RHS(J,L)	DAUX
	75 CONTINUE	DAUX
	80 IF (NQ.EQ.0) GO TO 83	DAUX
C		DAUX
C	ELIMINATE QQ	DAUX
C		DAUX
	DO 82 K=1,NQ	DAUX
	IF (KQTYPE(K).LT.0) GO TO 82	DAUX
	N = KQ1(K)	DAUX
	M = KQ2(K)	DAUX
	DO 81 I=1,3	DAUX
	DO 81 J=1,3	DAUX
	SEGLA(I,N) = SEGLA(I,N) - A13(I,J,2*K-1)*RW(N)*QQ(J,K)	DAUX
	SEGLA(I,M) = SEGLA(I,M) - A13(I,J,2*K)*RW(M)*QQ(J,K)	DAUX
	WMEGD(I,N) = WMEGD(I,N) - A23(I,J,2*K-1)*RPHI(I,N)*QQ(J,K)	DAUX
	81 WMEGD(I,M) = WMEGD(I,M) - A23(I,J,2*K)*RPHI(I,M)*QQ(J,K)	DAUX
	82 CONTINUE	DAUX
	83 IF (NFLX.EQ.0) GO TO 90	DAUX
C		DAUX

C	ELIMINATE V4 (TORQUES FOR FLEXIBLE SEGMENTS)	DAUX
C		DAUX
	DO 84 N=1,NFLX	DAUX
	N1 = NFLEX(1,N)	DAUX
	N2 = NFLEX(2,N)	DAUX
	N3 = NFLEX(3,N)	DAUX
	DO 84 I=1,3	DAUX
	DO 84 J=1,3	DAUX
	WMEGD(I,N1) = WMEGD(I,N1) - B42(J,I,3*N-2)*RPHI(I,N1)*V4(J,N)	DAUX
	WMEGD(I,N2) = WMEGD(I,N2) - B42(J,I,3*N-1)*RPHI(I,N2)*V4(J,N)	DAUX
	84 WMEGD(I,N3) = WMEGD(I,N3) - B42(J,I,3*N )*RPHI(I,N3)*V4(J,N)	DAUX
	90 DO 91 J=1,NGRND	DAUX
	DO 91 I=1,3	DAUX
	IF (DABS(WMEGD(I,J)).LE.EPS12) WMEGD(I,J) = 0.0	DAUX
	91 IF (DABS(SEGLA(I,J)).LE.EPS12) SEGLA(I,J) = 0.0	DAUX
C		DAUX
C	OPTIONAL OUTPUT OF FUNCTIONS AND DERIVATIVES.	DAUX
C		DAUX
	IF (NPRT(9).NE.0) CALL PRINT(6H DAUX )	DAUX
C		DAUX
	CALL ELTIME(2,9)	DAUX
	RETURN	DAUX
	END	DAUX

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SUBROUTINE DAUX11                                REV IV    07/24/86SLIP
C                                                     DAUX11
C CALLED BY SUBROUTINE DAUX TO COMPUTE              DAUX11
C                                                     DAUX11
C               -1                -1                DAUX11
C      (C11) = (B11)(M)   (A11) + (B12)(PHI)   (A21)  DAUX11
C                                                     DAUX11
C               -1                -1                DAUX11
C      (R1) = (B11)(M)   (U1) + (B12)(PHI)   (U2) - (V1) DAUX11
C                                                     DAUX11
C IMPLICIT REAL*8(A-H,O-Z)                          DAUX11
C COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND, DAUX11
C *          NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG PAGE
C COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30), DAUX11
C *          SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)     DAUX11
C COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60), SLIP
C *          RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),   DAUX11
C *          JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)  DAUX11
C COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60), DAUX11
C *          F(3,30),TQ(3,30),WJ(30),A11(3,3,30)             SLIP
C COMMON/TEMPVS/ C(3,3,600),RHS(3,54),IJK(54,54),IJ,NQ2S    CHGIII
C *          ,DN(3,3),DM(3,3),SN(3,3),SM(3,3),HH(3,3),BN(3)  DAUX11
C *          ,DDMY(28044)                                     80386
C CALL ELTIME(1,14)                                         DAUX11
C DO 30 M=1,NJNT                                           DAUX11
C N = IABS(JNT(M))                                          DAUX11
C MQ = NQ2S + M                                             DAUX11
C IJ = IJ+1                                                 DAUX11
C IJK(MQ,MQ) = IJ                                          DAUX11
C IF (N.GT.0) GO TO 13                                       DAUX11
C IF (N < 1) SET C11(M,M) = I                               DAUX11
C AND RHS(M) = V1(M)                                        DAUX11
C DO 12 I=1,3                                               DAUX11
C DO 11 J=1,3                                               DAUX11
C 11 C(I,J,IJ) = 0.0                                         DAUX11
C C(I,I,IJ) = 1.0                                           DAUX11
C 12 RHS(I,MQ) = V1(I,M)                                     DAUX11
C IJK(MQ,MQ) = -IJ                                          DAUX11
C GO TO 30                                                  DAUX11
C IF (N > 0) SET RHS(M) = U1(N) - U1(M+1) - V1(M)         DAUX11
C + B12(M,N)U2(N) + B12(M,M+1)U2(M+1)                     DAUX11
C AND C11(M,N) = RW(N) + RW(M+1)                           DAUX11
C + B12(M,N )PHI(N )'A21(N ,M)                            DAUX11
C + B12(M,M+1)PHI(M+1)'A21(M+1,M)                         DAUX11
C 13 DO 15 I=1,3                                            DAUX11
C T1 = -V1(I,M)                                             SLIP

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DO 15 J = 1,3	DAUX11
T1 = T1 + B12(I,J,2*M-1)*U2(J,N) + B12(I,J,2*M)*U2(J,M+1)	DAUX11
* + A11(I,J,M)*(U1(J,N) - U1(J,M+1))	SLIP
IF (J.LT.I) GO TO 15	DAUX11
T2 = 0.0	DAUX11
IF (J.EQ.I) T2 = RW(N) + RW(M+1)	DAUX11
DO 14 K=1,3	DAUX11
14 T2 = T2 + B12(I,K,2*M-1)*RPHI(K,N)*B12(J,K,2*M-1)	DAUX11
* + B12(I,K,2*M)*RPHI(K,M+1)*B12(J,K,2*M)	DAUX11
C(I,J,IJ) = T2	DAUX11
C(J,I,IJ) = T2	DAUX11
15 RHS(I,MQ) = T1	DAUX11
IF (ISING(N).NE.0) GO TO 30	DAUX11
L = 0	DAUX11
IF (N.GT.1) L = IABS(JNT(N-1))	DAUX11
IF (L.EQ.0) GO TO 18	DAUX11
C	DAUX11
C IF (N > 1) AND (L = JNT(N-1) > 0)	DAUX11
C	DAUX11
C SET C11(M,N-1) = -RW(N) + B12(M,N)PHI(N)'A21(N,N-1)	DAUX11
C	DAUX11
C AND C11(N-1,M) = C(M,N-1)	DAUX11
C	DAUX11
KJNT = NQ2S + N - 1	DAUX11
IJ = IJ+1	DAUX11
IJK(MQ,KJNT) = IJ	DAUX11
IJK(KJNT,MQ) = IJ+1	DAUX11
DO 17 I=1,3	DAUX11
DO 17 J=1,3	DAUX11
C(I,J,IJ) = 0.0	DAUX11
DO 16 K=1,3	DAUX11
16 C(I,J,IJ) = C(I,J,IJ) + B12(I,K,2*M-1)*RPHI(K,N)*B12(J,K,2*N-2)	DAUX11
* - A11(I,K,M)*RW(N)*A11(J,K,N-1)	SLIP
17 C(J,I,IJ+1) = C(I,J,IJ)	DAUX11
IJ = IJ+1	DAUX11
18 IF (M.EQ.NJNT) GO TO 30	DAUX11
M1 = M+1	DAUX11
DO 21 L=M1,NJNT	DAUX11
IF (IABS(JNT(L)).NE.N) GO TO 21	DAUX11
C	DAUX11
C IF (L > M) AND (JNT(L) = N)	DAUX11
C	DAUX11
C SET C11(M,L) = RW(N) + B12(M,N)PHI(N)'A21(N,L)	DAUX11
C	DAUX11
C AND C11(L,M) = C11(M,L)	DAUX11
C	DAUX11
KJNT = NQ2S + L	DAUX11
IJ = IJ+1	DAUX11
IJK(MQ,KJNT) = IJ	DAUX11
IJK(KJNT,MQ) = IJ+1	DAUX11

DO 20 I=1,3	DAUX11
DO 20 J=1,3	DAUX11
C(I,J,IJ) = 0.0	DAUX11
DO 19 K=1,3	DAUX11
19 C(I,J,IJ) = C(I,J,IJ) + B12(I,K,2*M-1)*RPHI(K,N)*B12(J,K,2*L-1)	DAUX11
*                    + A11(I,K,M)*RW(N)*A11(J,K,L)	SLIP
20 C(J,I,IJ+1) = C(I,J,IJ)	DAUX11
IJ = IJ+1	DAUX11
21 CONTINUE	DAUX11
30 CONTINUE	DAUX11
CALL ELTIME(2,14)	DAUX11
RETURN	DAUX11
END	DAUX11

	SUBROUTINE DAUX12		DAUX12
C		REV IV	07/24/86SLIP
C	CALLED BY SUBROUTINE DAUX TO COMPUTE		DAUX12
C			DAUX12
C	-1		DAUX12
C	(C12) = (B12)(PHI) (A22)		DAUX12
C			DAUX12
C	T		DAUX12
C	(C21) = (C12)		DAUX12
C			DAUX12
	IMPLICIT REAL*8(A-H,O-Z)		DAUX12
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NCRND,		DAUX12
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),		SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),		DAUX12
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)		DAUX12
	COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),		DAUX12
*	F(3,30),TQ(3,30),WJ(30),A11(3,3,30)		SLIP
	LOGICAL*1 FREE,LDMMY		80386
	COMMON/TEMPVS/ C(3,3,600),RHS(3,54),IJK(54,54),IJ,NQ2S		CHGIII
*	,DN(3,3),DM(3,3),SN(3,3),SM(3,3),HH(3,3),BN(3)		DAUX12
*	,IDUM(362),FREE(30),LDMMY(2),DDMY(27859)		80386
	CALL ELTIME(1,15)		DAUX12
	NQSJNT = NQ2S + NJNT		DAUX12
	DO 60 M=1,NJNT		DAUX12
	N = IABS(JNT(M))		DAUX12
	IF (N.EQ.0) GO TO 60		DAUX12
	MQ = NQ2S + M		DAUX12
	IF (FREE(M)) GO TO 37		SLIP
	MJNT = NQSJNT + M		DAUX12
	IJ = IJ+1		DAUX12
	IJK(MQ,MJNT) = IJ		DAUX12
	IJK(MJNT,MQ) = IJ+1		DAUX12
	DO 36 I=1,3		DAUX12
	DO 36 J=1,3		DAUX12
	SN(I,J) = 0.0		DAUX12
	SM(I,J) = 0.0		DAUX12
	DO 35 K=1,3		DAUX12
	SN(I,J) = SN(I,J) + B12(I,K,2*M-1) * RPHI(K,N ) * A22(K,J,2*M-1)		DAUX12
35	SM(I,J) = SM(I,J) + B12(I,K,2*M ) * RPHI(K,M+1) * A22(K,J,2*M )		DAUX12
	C(I,J,IJ ) = SN(I,J) - SM(I,J)		DAUX12
36	C(J,I,IJ+1) = C(I,J,IJ)		DAUX12
	IJ = IJ+1		DAUX12
37	IF (ISING(N).NE.0) GO TO 50		DAUX12
	IF (N.EQ.1) GO TO 43		DAUX12
	IF (FREE(N-1)) GO TO 43		SLIP
	MJNT = NQSJNT + N-1		DAUX12
	IJ = IJ+1		DAUX12
	IJK(MQ,MJNT) = IJ		DAUX12
	IJK(MJNT,MQ) = IJ+1		DAUX12
	DO 42 I=1,3		DAUX12
	DO 42 J=1,3		DAUX12

SN(I,J) = 0.0	DAUX12
DO 41 K=1,3	DAUX12
41 SN(I,J) = SN(I,J) + B12(I,K,2*M-1) * RPHI(K,N ) * A22(K,J,2*N-2)	DAUX12
C(I,J,IJ ) = -SN(I,J)	DAUX12
42 C(J,I,IJ+1) = -SN(I,J)	DAUX12
IJ = IJ+1	DAUX12
43 DO 49 L=N,NJNT	DAUX12
IF (L.EQ.M) GO TO 49	DAUX12
IF (IABS(JNT(L)).NE.N ) GO TO 49	DAUX12
IF (FREE(L)) GO TO 49	SLIP
MJNT = NQSJNT + L	DAUX12
IJ = IJ+1	DAUX12
IJK(MQ,MJNT) = IJ	DAUX12
IJK(MJNT,MQ) = IJ+1	DAUX12
DO 48 I=1,3	DAUX12
DO 48 J=1,3	DAUX12
SN(I,J) = 0.0	DAUX12
DO 47 K=1,3	DAUX12
47 SN(I,J) = SN(I,J) + B12(I,K,2*M-1) * RPHI(K,N ) * A22(K,J,2*L-1)	DAUX12
C(I,J,IJ ) = SN(I,J)	DAUX12
48 C(J,I,IJ+1) = SN(I,J)	DAUX12
IJ = IJ +1	DAUX12
49 CONTINUE	DAUX12
50 IF (M.EQ.NJNT) GO TO 60	DAUX12
IF (ISING(M+1).NE.0) GO TO 60	DAUX12
M1 = M+1	DAUX12
DO 59 L=M1,NJNT	DAUX12
IF (IABS(JNT(L)).NE.M1) GO TO 59	DAUX12
IF (FREE(L)) GO TO 59	SLIP
MJNT = NQSJNT + L	DAUX12
IJ = IJ+1	DAUX12
IJK(MQ,MJNT) = IJ	DAUX12
IJK(MJNT,MQ) = IJ+1	DAUX12
DO 58 I=1,3	DAUX12
DO 58 J=1,3	DAUX12
SM(I,J) = 0.0	DAUX12
DO 57 K=1,3	DAUX12
57 SM(I,J) = SM(I,J) + B12(I,K,2*M ) * RPHI(K,M+1) * A22(K,J,2*L-1)	DAUX12
C(I,J,IJ ) = SM(I,J)	DAUX12
58 C(J,I,IJ+1) = SM(I,J)	DAUX12
IJ = IJ +1	DAUX12
59 CONTINUE	DAUX12
60 CONTINUE	DAUX12
CALL ELTIME(2,15)	DAUX12
RETURN	DAUX12
END	DAUX12

	SUBROUTINE DAUX22		DAUX22
C		REV IV	07/24/86SLIP
C	CALLED BY SUBROUTINE DAUX TO COMPUTE		DAUX22
C			DAUX22
C			DAUX22
C			DAUX22
C		-1	DAUX22
C	(C22) - (B22)(PHI) (A22) - (B24)		DAUX22
C			DAUX22
C		-1	DAUX22
C	(R2) - (B22)(PHI) (U2) - (V2)		DAUX22
C			DAUX22
	IMPLICIT REAL*8(A-H,O-Z)		DAUX22
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		DAUX22
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),		DAUX22
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		DAUX22
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),		SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),		DAUX22
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)		DAUX22
	COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),		DAUX22
*	F(3,30),TQ(3,30),WJ(30),A11(3,3,30)		SLIP
	COMMON/CEULER/ IEULER(30),HIR(3,3,90),ANG(3,30),ANGD(3,30),		JDRIFT
*	FE(3,30),TQE(3,30),CONST(5,30)		JDRIFT
	LOGICAL*1 FREE,LDDMY		80386
	COMMON/TEMPVS/ C(3,3,600),RHS(3,54),IJK(54,54),IJ,NQ2S		CHGIII
*	,DN(3,3),DM(3,3),SN(3,3),SM(3,3),HH(3,3),BN(3)		DAUX22
*	,IDUM(362),FREE(30),LDDMY(2),DDMY(27859)		80386
	LOGICAL TEST		DAUX22
	CALL ELTIME(1,16)		DAUX22
	NQSJNT = NQ2S + NJNT		DAUX22
	DO 90 M=1,NJNT		DAUX22
	MJNT = NQSJNT + M		DAUX22
	DO 60 I=1,3		DAUX22
60	RHS(I,MJNT) = V2(I,M)		DAUX22
	N = IABS(JNT(M))		DAUX22
	IF (N.EQ.0) GO TO 90		DAUX22
	IF (FREE(M)) GO TO 90		SLIP
	IJ = IJ+1		DAUX22
	IJK(MJNT,MJNT) = IJ		DAUX22
	DO 61 J=1,3		DAUX22
	DO 61 I=1,3		DAUX22
61	HH(I,J) = 0.0		DAUX22
	LGO = IPIN(M)+8		SLIP
	TEST = .FALSE.		DAUX22
	GO TO (64,64,64,62,64,64,64,64,63,64,64,64,64,63,63),LGO		SLIP
62	IF (IEULER(M).GE.7) GO TO 64		DAUX22
	TEST = IEULER(M).LT.4		DAUX22
63	AN = 0.0		DAUX22
	DO 51 J=1,3		DAUX22
51	AN = AN + HB(J,2*M-1)**2 * RPHI(J,N)		DAUX22
*	+ HB(J,2*M)**2 * RPHI(J,M+1)		DAUX22
	IF (TEST) GO TO 64		DAUX22

CALL DOT31 (D(1,1,N),HB(1,2*M-1),BN)	DAUX22
DO 53 J=1,3	DAUX22
DO 53 I=1,3	DAUX22
53 HH(I,J) = AN*BN(I)*BN(J)	DAUX22
64 DO 67 I=1,3	DAUX22
RHS(I,MJNT) = -V2(I,M)	DAUX22
DO 66 J=1,3	DAUX22
RHS(I,MJNT) = RHS(I,MJNT) + A22(J,I,2*M-1)*U2(J,N )	DAUX22
* - A22(J,I,2*M )*U2(J,M+1)	DAUX22
SN(I,J) = 0.0	DAUX22
IF (TEST) GO TO 66	DAUX22
DO 65 K=1,3	DAUX22
65 SN(I,J) = SN(I,J) + A22(K,I,2*M-1) * RPHI(K,N ) * A22(K,J,2*M-1)	DAUX22
* + A22(K,I,2*M ) * RPHI(K,M+1) * A22(K,J,2*M )	DAUX22
66 C(I,J,IJ) = SN(I,J) + HH(I,J)	DAUX22
67 IF (TEST) C(I,I,IJ) = AN	DAUX22
IF (ISING(N).NE.0) GO TO 90	DAUX22
IF (N.EQ.1) GO TO 80	DAUX22
IF (FREE(N-1)) GO TO 80	DAUX22
N1JNT = NQSJNT + N -1	SLIP
IJ = IJ+1	DAUX22
IJK(MJNT,N1JNT) = IJ	DAUX22
IJK(N1JNT,MJNT) = IJ+1	DAUX22
DO 77 I=1,3	DAUX22
DO 77 J=1,3	DAUX22
SN(I,J) = 0.0	DAUX22
DO 76 K=1,3	DAUX22
76 SN(I,J) = SN(I,J) + A22(K,I,2*M-1) * RPHI(K,N ) * A22(K,J,2*N-2)	DAUX22
C(I,J,IJ) = -SN(I,J)	DAUX22
77 C(J,I,IJ+1) = -SN(I,J)	DAUX22
IJ = IJ+1	DAUX22
80 IF (M.EQ.NJNT) GO TO 90	DAUX22
M1 = M+1	DAUX22
DO 88 L=M1,NJNT	DAUX22
IF (IABS(JNT(L)).NE.N) GO TO 88	DAUX22
IF (FREE(L)) GO TO 88	DAUX22
LJNT = NQSJNT + L	SLIP
IJ = IJ+1	DAUX22
IJK(MJNT,LJNT) = IJ	DAUX22
IJK(LJNT,MJNT) = IJ+1	DAUX22
DO 87 I=1,3	DAUX22
DO 87 J=1,3	DAUX22
SN(I,J) = 0.0	DAUX22
DO 86 K=1,3	DAUX22
86 SN(I,J) = SN(I,J) + A22(K,I,2*M-1) * RPHI(K,N ) * A22(K,J,2*L-1)	DAUX22
C(I,J,IJ) = SN(I,J)	DAUX22
87 C(J,I,IJ+1) = SN(I,J)	DAUX22
IJ = IJ+1	DAUX22
88 CONTINUE	DAUX22
90 CONTINUE	DAUX22
CALL ELTIME(2,16)	DAUX22
RETURN	DAUX22

END

DAUX22

	SUBROUTINE DAUX31		DAUX31
C		REV IV	07/24/86SLIP
C	CALLED BY SUBROUTINE DAUX TO COMPUTE		DAUX31
C			DAUX31
C		-1	DAUX31
C	(C13) = (B11)(M) (A13) + (B12)(PHI) (A23)	-1	DAUX31
C			DAUX31
C		-1	DAUX31
C	(C31) = (B31)(M) (A11) + (B32)(PHI) (A21)	-1	DAUX31
C			DAUX31
	IMPLICIT REAL*8 (A-H,O-Z)		DAUX31
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		DAUX31
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),		SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),		DAUX31
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)		DAUX31
	COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),		DAUX31
*	F(3,30),TQ(3,30),WJ(30),A11(3,3,30)		SLIP
	COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24),		DAUX31
*	HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12),		DAUX31
*	RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12),		DAUX31
*	KQ1(12),KQ2(12),KQTYPE(12)		DAUX31
	COMMON/TEMPVS/ C(3,3,600),RHS(3,54),IJK(54,54),IJ,NQ2S,DMMY(28092)	80386	
	CALL ELTIME(1,17)		DAUX31
	DO 30 N=1,NQ		DAUX31
	IF (KQTYPE(N).LT.0) GO TO 30		DAUX31
	K1 = KQ1(N)		DAUX31
	K2 = KQ2(N)		DAUX31
	NNS = NQ2S - NQ + N		DAUX31
	IF (K1.LE.1) GO TO 13		DAUX31
	IF (IABS(JNT(K1-1)).EQ.0) GO TO 13		DAUX31
	IF (ISING(K1).NE.0) GO TO 13		DAUX31
C			DAUX31
C		-1	DAUX31
C	C13(K1-1,N) = B11(K1-1,K1)M (K1)A13(K1,N)		DAUX31
C		-1	DAUX31
C	+ B12(K1-1,K1)PHI (K1)A23(K1,N)		DAUX31
C			DAUX31
C		-1	DAUX31
C	C31(N,K1-1) = B31(N,K1)M (K1)A11(K1,K1-1)		DAUX31
C		-1	DAUX31
C	+ B32(N,K1)PHI (K1)A21(K1,K1-1)		DAUX31
C			DAUX31
	MQ = NQ2S + K1 - 1		DAUX31
	IJ = IJ+1		DAUX31
	IJK(MQ,NNS) = IJ		DAUX31
	IJK(NNS,MQ) = IJ+1		DAUX31
	DO 12 I=1,3		DAUX31
	DO 12 J=1,3		DAUX31
	SUM = 0.0		SLIP
	TUM = 0.0		SLIP
	DO 11 K=1,3		DAUX31



	SUM = SUM + B12(I,K,2*K1-2)*RPHI(K,K1)*A23(K,J,2*N-1 )	DAUX31
	* - A11(I,K,K1-1)*RW(K1)*A13(K,J,2*N-1)	SLIP
11	TUM = TUM + B32(I,K,2*N-1 )*RPHI(K,K1)*B12(J,K,2*K1-2)	DAUX31
	* - B31(I,K,2*N-1)*RW(K1)*A11(K,J,K1-1)	SLIP
	C(I,J,IJ) = SUM	DAUX31
12	C(I,J,IJ+1) = TUM	DAUX31
	IJ = IJ+1	DAUX31
13	IF (K2.LE.1) GO TO 16	DAUX31
	IF (IABS(JNT(K2-1)).EQ.0) GO TO 16	DAUX31
	IF (ISING(K2).NE.0) GO TO 16	DAUX31
C		DAUX31
C		DAUX31
C	C13(K2-1,N) = B11(K2-1,K2)M <sup>-1</sup> (K2)A13(K2,N)	DAUX31
C		DAUX31
C	+ B12(K2-1,K2)PHI <sup>-1</sup> (K2)A23(K2,N)	DAUX31
C		DAUX31
C		DAUX31
C	C31(N,K2-1) = B31(N,K2)M <sup>-1</sup> (K2)A11(K2,K2-1)	DAUX31
C		DAUX31
C	+ B32(N,K2)PHI <sup>-1</sup> (K2)A21(K2,K2-1)	DAUX31
C		DAUX31
	MQ = NQ2S + K2 - 1	DAUX31
	IJ = IJ+1	DAUX31
	IJK(MQ,NNS) = IJ	DAUX31
	IJK(NNS,MQ) = IJ+1	DAUX31
	DO 15 I=1,3	DAUX31
	DO 15 J=1,3	DAUX31
	SUM = 0.0	SLIP
	TUM = 0.0	SLIP
	DO 14 K=1,3	DAUX31
	SUM = SUM + B12(I,K,2*K2-2)*RPHI(K,K2)*A23(K,J,2*N )	DAUX31
	* - A11(I,K,K2-1)*RW(K2)*A13(K,J,2*N)	SLIP
14	TUM = TUM + B32(I,K,2*N )*RPHI(K,K2)*B12(J,K,2*K2-2)	DAUX31
	* - B31(I,K,2*N)*RW(K2)*A11(K,J,K2-1)	SLIP
	C(I,J,IJ) = SUM	DAUX31
15	C(I,J,IJ+1) = TUM	DAUX31
	IJ = IJ+1	DAUX31
16	IF (NJNT.LE.0) GO TO 30	DAUX31
	DO 26 L=1,NJNT	DAUX31
	IF (IABS(JNT(L)).NE.K1) GO TO 21	DAUX31
	IF (ISING(K1).NE.0) GO TO 21	DAUX31
C		DAUX31
C	FOR ANY L SUCH THAT JNT(L) = K1	DAUX31
C		DAUX31
C		DAUX31
C	C13(L,N) = B11(L,K1)M <sup>-1</sup> (K1)A13(K1,N)	DAUX31
C		DAUX31
C	+ B12(L,K1)PHI <sup>-1</sup> (K1)A23(K1,N)	DAUX31
C		DAUX31
C		DAUX31
C	C31(N,L) = B31(N,K1)M <sup>-1</sup> (K1)A11(K1,L)	DAUX31
C		DAUX31
C		DAUX31

C	+ B32(N,K1)PHI (K1)A21(K1,L)	DAUX31
C		DAUX31
	MQ = NQ2S + L	DAUX31
	IF (IJK(MQ,NNS).NE.0) GO TO 18	DAUX31
	IJ = IJ+1	DAUX31
	IJK(MQ,NNS) = IJ	DAUX31
	IJK(NNS,MQ) = IJ+1	DAUX31
	DO 17 J=1,3	DAUX31
	DO 17 I=1,3	DAUX31
	C(I,J,IJ) = 0.0	DAUX31
17	C(I,J,IJ+1) = 0.0	DAUX31
	IJ = IJ+1	DAUX31
18	JJ = IJK(MQ,NNS)	DAUX31
	DO 20 I=1,3	DAUX31
	DO 20 J=1,3	DAUX31
	SUM = C(I,J,JJ)	DAUX31
	TUM = C(I,J,JJ+1)	SLIP
	DO 19 K=1,3	SLIP
	SUM = SUM + B12(I,K,2*L-1)*RPHI(K,K1)*A23(K,J,2*N-1)	DAUX31
	* +A11(I,K,L)*RW(K1)*A13(K,J,2*N-1)	DAUX31
19	TUM = TUM + B32(I,K,2*N-1)*RPHI(K,K1)*B12(J,K,2*L-1)	SLIP
	* +B31(I,K,2*N-1)*RW(K1)*A11(J,K,L)	DAUX31
	C(I,J,JJ) = SUM	SLIP
20	C(I,J,JJ+1) = TUM	DAUX31
21	IF (IABS(JNT(L)).NE.K2) GO TO 26	DAUX31
	IF (ISING(K2).NE.0) GO TO 26	DAUX31
C		DAUX31
C	FOR ANY L SUCH THAT JNT(L) = K2	DAUX31
C		DAUX31
C		DAUX31
C		DAUX31
C	C13(L,N) = B11(L,K2)M <sup>-1</sup> (K2)A13(K2,N)	DAUX31
C		DAUX31
C	+ B12(L,K2)PHI <sup>-1</sup> (K2)A23(K2,N)	DAUX31
C		DAUX31
C		DAUX31
C	C31(N,L) = B31(N,K2)M <sup>-1</sup> (K2)A11(K2,L)	DAUX31
C		DAUX31
C	+ B32(N,K2)PHI <sup>-1</sup> (K2)A21(K2,L)	DAUX31
C		DAUX31
	MQ = NQ2S + L	DAUX31
	IF (IJK(MQ,NNS).NE.0) GO TO 23	DAUX31
	IJ = IJ+1	DAUX31
	IJK(MQ,NNS) = IJ	DAUX31
	IJK(NNS,MQ) = IJ+1	DAUX31
	DO 22 J=1,3	DAUX31
	DO 22 I=1,3	DAUX31
	C(I,J,IJ) = 0.0	DAUX31
22	C(I,J,IJ+1) = 0.0	DAUX31
	IJ = IJ+1	DAUX31
23	JJ = IJK(MQ,NNS)	DAUX31
	DO 25 I=1,3	DAUX31
	DO 25 J=1,3	DAUX31

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SUM = C(I,J,JJ)
TUM = C(I,J,JJ+1)
DO 24 K=1,3
SUM = SUM + B12(I,K,2*L-1)*RPHI(K,K2)*A23(K,J,2*N )
*
+ A11(I,K,L)*RW(K2)*A13(K,J,2*N)
24 TUM = TUM + B32(I,K,2*N )*RPHI(K,K2)*B12(J,K,2*L-1)
*
+ B31(I,K,2*N)*RW(K2)*A11(J,K,L)
C(I,J,JJ) = SUM
25 C(I,J,JJ+1) = TUM
26 CONTINUE
30 CONTINUE
CALL ELTIME(2,17)
RETURN
END

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SLIP
SLIP
DAUX31
DAUX31
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DAUX31

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	SUBROUTINE DAUX32	DAUX32
C		REV IV 07/24/86SLIP
C	CALLED BY SUBROUTINE DAUX TO COMPUTE	DAUX32
C		DAUX32
C	-1	DAUX32
C	(C23) - (B22)(PHI) (A23)	DAUX32
C		DAUX32
C	-1	DAUX32
C	(C32) - (B32)(PHI) (A22)	DAUX32
C		DAUX32
	IMPLICIT REAL*8 (A-H,O-Z)	DAUX32
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,	DAUX32
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	PAGE
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),	SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),	DAUX32
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)	DAUX32
	COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),	DAUX32
*	F(3,30),TQ(3,30),WJ(30),A11(3,3,30)	SLIP
	COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24),	DAUX32
*	HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12),	DAUX32
*	RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12),	DAUX32
*	KQ1(12),KQ2(12),KQTYPE(12)	DAUX32
	LOGICAL*1 FREE,LDDMY	80386
	COMMON/TEMPVS/ C(3,3,600),RHS(3,54),IJK(54,54),IJ,NQ2S	CHGIII
*	,DN(3,3),DM(3,3),BN(3),IDUM(416),FREE(30)	SLIP
*	,LDDMY(2),DDMY(27859)	80386
	CALL ELTIME(i,18)	DAUX32
	NQSJNT = NQ2S + NJNT	DAUX32
	DO 60 N=1,NQ	DAUX32
	IF (KQTYPE(N).LT.0) GO TO 60	DAUX32
	K1 = KQ1(N)	DAUX32
	K2 = KQ2(N)	DAUX32
	NNS = NQ2S - NQ + N	DAUX32
	IF (K1.LE.1) GO TO 43	DAUX32
	IF (IABS(JNT(K1-1)).EQ.0) GO TO 43	DAUX32
	IF (FREE(K1-1)) GO TO 43	SLIP
	IF (ISING(K1).NE.0) GO TO 43	DAUX32
C		DAUX32
C	-1	DAUX32
C	C23(K1-1,N) = B22(K1-1,K1)PHI (K1)A23(K1,N)	DAUX32
C		DAUX32
C	-1	DAUX32
C	C32(N,K1-1) = B32(N,K1)PHI (K1)A22(K1,K1-1)	DAUX32
C		DAUX32
	KJNT = NQSJNT + K1 - 1	DAUX32
	IJ = IJ+1	DAUX32
	IJK(KJNT,NNS) = IJ	DAUX32
	IJK(NNS,KJNT) = IJ+1	DAUX32
	DO 42 I=1,3	DAUX32
	DO 42 J=1,3	DAUX32
	SUM = 0.0	DAUX32
	TUM = 0.0	DAUX32

	DO 41 K=1,3	DAUX32
	SUM = SUM + A22(K,I,2*K1-2) * RPHI(K,K1) * A23(K,J,2*N-1 )	DAUX32
41	TUM = TUM + B32(I,K,2*N-1 ) * RPHI(K,K1) * A22(K,J,2*K1-2)	DAUX32
	C(I,J,IJ ) = -SUM	DAUX32
42	C(I,J,IJ+1) = -TUM	DAUX32
	IJ = IJ+1	DAUX32
43	IF (K2.LE.1) GO TO 46	DAUX32
	IF (IABS(JNT(K2-1)).EQ.0) GO TO 46	DAUX32
	IF (FREE(K2-1)) GO TO 46	SLIP
	IF (ISING(K2).NE.0) GO TO 46	DAUX32
C		DAUX32
C	-1	DAUX32
C	G23(K2-1,N) = B22(K2-1,K2)PHI (K2)A23(K2,N)	DAUX32
C		DAUX32
C	-1	DAUX32
C	G32(N,K2-1) = B32(N,K2)PHI (K2)A22(K2,K2-1)	DAUX32
C		DAUX32
	KJNT = NQSJNT + K2 - 1	DAUX32
	IJ = IJ+1	DAUX32
	IJK(KJNT,NNS) = IJ	DAUX32
	IJK(NNS,KJNT) = IJ+1	DAUX32
	DO 45 I=1,3	DAUX32
	DO 45 J=1,3	DAUX32
	SUM = 0.0	DAUX32
	TUM = 0.0	DAUX32
	DO 44 K=1,3	DAUX32
	SUM = SUM + A22(K,I,2*K2-2) * RPHI(K,K2) * A23(K,J,2*N )	DAUX32
44	TUM = TUM + B32(I,K,2*N ) * RPHI(K,K2) * A22(K,J,2*K2-2)	DAUX32
	C(I,J,IJ ) = -SUM	DAUX32
45	C(I,J,IJ+1) = -TUM	DAUX32
	IJ = IJ+1	DAUX32
46	IF (NJNT.LE.0) GO TO 60	DAUX32
	DO 56 L=1,NJNT	DAUX32
	IF (FREE(L)) GO TO 56	SLIP
	IF (IABS(JNT(L)).NE.K1) GO TO 51	DAUX32
	IF (ISING(K1).NE.0) GO TO 51	DAUX32
C		DAUX32
C	FOR ANY L SUCH THAT JNT(L) = K1	DAUX32
C		DAUX32
C	-1	DAUX32
C	G23(L,N) = B22(L,K1)PHI (K1)A23(K1,N)	DAUX32
C		DAUX32
C	-1	DAUX32
C	G32(N,L) = B32(N,K1)PHI (K1)A22(K1,L)	DAUX32
C		DAUX32
	KJNT = NQSJNT + L	DAUX32
	IF (IJK(KJNT,NNS).NE.0) GO TO 48	DAUX32
	IJ = IJ+1	DAUX32
	IJK(KJNT,NNS) = IJ	DAUX32
	IJK(NNS,KJNT) = IJ+1	DAUX32
	DO 47 J=1,3	DAUX32
	DO 47 I=1,3	DAUX32

	C(I,J,IJ ) = 0.0	DAUX32
47	C(I,J,IJ+1) = 0.0	DAUX32
	IJ = IJ+1	DAUX32
48	JJ = IJK(KJNT,NNS)	DAUX32
	DO 50 I=1,3	DAUX32
	DO 50 J=1,3	DAUX32
	SUM = C(I,J,JJ)	DAUX32
	TUM = C(I,J,JJ+1)	DAUX32
	DO 49 K=1,3	DAUX32
	SUM = SUM + A22(K,I,2*L-1 ) * RPHI(K,K1) * A23(K,J,2*N-1 )	DAUX32
49	TUM = TUM + B32(I,K,2*N-1 ) * RPHI(K,K1) * A22(K,J,2*L-1 )	DAUX32
	C(I,J,JJ) = SUM	DAUX32
50	C(I,J,JJ+1) = TUM	DAUX32
51	IF (IABS(JNT(L)).NE.K2) GO TO 56	DAUX32
	IF (ISING(K2).NE.0) GO TO 56	DAUX32
C		DAUX32
C	FOR ANY L SUCH THAT JNT(L) = K2	DAUX32
C		DAUX32
C	-1	DAUX32
C	C23(L,N) = B22(L,K2)PHI (K2)A23(K2,N)	DAUX32
C		DAUX32
C	-1	DAUX32
C	C32(N,L) = B32(N,K2)PHI (K2)A22(K2,L)	DAUX32
C		DAUX32
	KJNT = NQSJNT + L	DAUX32
	IF (IJK(KJNT,NNS).NE.0) GO TO 53	DAUX32
	IJ = IJ+1	DAUX32
	IJK(KJNT,NNS) = IJ	DAUX32
	IJK(NNS,KJNT) = IJ+1	DAUX32
	DO 52 J=1,3	DAUX32
	DO 52 I=1,3	DAUX32
	C(I,J,IJ ) = 0.0	DAUX32
52	C(I,J,IJ+1) = 0.0	DAUX32
	IJ = IJ+1	DAUX32
53	JJ = IJK(KJNT,NNS)	DAUX32
	DO 55 I=1,3	DAUX32
	DO 55 J=1,3	DAUX32
	SUM = C(I,J,JJ)	DAUX32
	TUM = C(I,J,JJ+1)	DAUX32
	DO 54 K=1,3	DAUX32
	SUM = SUM + A22(K,I,2*L-1 ) * RPHI(K,K2) * A23(K,J,2*N )	DAUX32
54	TUM = TUM + B32(I,K,2*N ) * RPHI(K,K2) * A22(K,J,2*L-1 )	DAUX32
	C(I,J,JJ) = SUM	DAUX32
55	C(I,J,JJ+1) = TUM	DAUX32
56	CONTINUE	DAUX32
60	CONTINUE	DAUX32
	CALL ELTIME(2,18)	DAUX32
	RETURN	DAUX32
	END	DAUX32

	SUBROUTINE DAUX33		DAUX33
C		REV IV	07/24/86SLIP
C	CALLED BY SUBROUTINE DAUX TO COMPUTE		DAUX33
C			DAUX33
C		-1	DAUX33
C	(C33) = (B31)(M) (A13) + (B32)(PHI) (A23) - (B35)	-1	DAUX33
C			DAUX33
C		-1	DAUX33
C	(R3) = (B31)(M) (U1) + (B32)(PHI) (U2) - (V3)	-1	DAUX33
C			DAUX33
	IMPLICIT REAL*8 (A-H,O-Z)		DAUX33
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		DAUX33
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),		DAUX33
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		DAUX33
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),		SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),		DAUX33
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)		DAUX33
	COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),		DAUX33
*	F(3,30),TQ(3,30),WJ(30),A11(3,3,30)		SLIP
	COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24),		DAUX33
*	HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12),		DAUX33
*	RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12),		DAUX33
*	KQ1(12),KQ2(12),KQTYPE(12)		DAUX33
	COMMON/TEMPVS/ C(3,3,600),RHS(3,54),IJK(54,54),IJ,NQ2S,DMMY(28092)	80386	
	CALL ELTIME(1,19)		DAUX33
	DO 90 N=1,NQ		DAUX33
	IF (KQTYPE(N).LT.0) GO TO 90		DAUX33
	K1 = KQ1(N)		DAUX33
	K2 = KQ2(N)		DAUX33
	NNS = NQ2S - NQ + N		DAUX33
C			DAUX33
C		-1	DAUX33
C	RHS(N) = B31(N,K1)M (K1)U1(K1) + B32(N,K1)PHI (K1)U2(K1)	-1	DAUX33
C		-1	DAUX33
C	+ B31(N,K2)M (K2)U1(K2) + B32(N,K2)PHI (K2)U2(K2)	-1	DAUX33
C			DAUX33
C	- V3(N)		DAUX33
C			DAUX33
	DO 63 I=1,3		DAUX33
	SUM = 0.0		DAUX33
	DO 62 K=1,3		DAUX33
62	SUM = SUM + B31(I,K,2*N-1)*U1(K,K1) + B32(I,K,2*N-1)*U2(K,K1)		DAUX33
*	+ B31(I,K,2*N )*U1(K,K2) + B32(I,K,2*N )*U2(K,K2)		DAUX33
63	RHS(I,NNS) = SUM - V3(I,N)		DAUX33
C			DAUX33
C		-1	DAUX33
C	C33(N,N) = B31(N,K1)M (K1)A13(K1,N) + B32(N,K1)PHI (K1)A23(K1,N)	-1	DAUX33
C		-1	DAUX33
C	+ B31(N,K2)M (K2)A13(K2,N) + B32(N,K2)PHI (K2)A23(K2,N)	-1	DAUX33
C			DAUX33
C	- B35(N,N)		DAUX33

C	IJ = IJ+1	DAUX33
	IJK(NNS,NNS) = IJ	DAUX33
	IF (KQTYPE(N).EQ.2) GO TO 51	DAUX33
	IF (KQTYPE(N).EQ.4) GO TO 51	DAUX33
	DO 65 I=1,3	DAUX33
	DO 65 J=1,3	DAUX33
	SUM = -HHT(I,J,N)	DAUX33
	IF (I.EQ.J) SUM = 1.0+SUM	DAUX33
	DO 64 K=1,3	DAUX33
64	SUM = SUM + B31(I,K,2*N-1)* RW( K1)*A13(K,J,2*N-1)	DAUX33
	* + B31(I,K,2*N )* RW( K2)*A13(K,J,2*N )	DAUX33
	* + B32(I,K,2*N-1)*RPHI(K,K1)*A23(K,J,2*N-1)	DAUX33
	* + B32(I,K,2*N )*RPHI(K,K2)*A23(K,J,2*N )	DAUX33
65	C(I,J,IJ) = SUM	DAUX33
	GO TO 59	DAUX33
C		DAUX33
C	FOR KQTYPE = 2 OR 4. SET C33(N,N) = B*I	DAUX33
C	WHERE B = SUM OF DIAGONAL ELEMENTS OF	DAUX33
C	-1 -1	DAUX33
C	(B31)(M) (A13) + (B32)(PHI) (A23)	DAUX33
C		DAUX33
51	SUM = 0.0	DAUX33
	DO 55 I=1,3	DAUX33
	DO 55 K=1,3	DAUX33
55	SUM = SUM + B31(I,K,2*N-1)* RW( K1)*A13(K,I,2*N-1)	DAUX33
	* + B31(I,K,2*N )* RW( K2)*A13(K,I,2*N )	DAUX33
	* + B32(I,K,2*N-1)*RPHI(K,K1)*A23(K,I,2*N-1)	DAUX33
	* + B32(I,K,2*N )*RPHI(K,K2)*A23(K,I,2*N )	DAUX33
	DO 57 I=1,3	DAUX33
	DO 56 J=1,3	DAUX33
56	C(I,J,IJ) = 0.0	DAUX33
57	C(I,I,IJ) = SUM	DAUX33
59	IF (N.EQ.NQ) GO TO 90	DAUX33
	N1 = N+1	DAUX33
	DO 85 M=N1,NQ	DAUX33
	IF (KQTYPE(M).LT.0) GO TO 85	DAUX33
	MNS = NQ2S - NQ + M	DAUX33
	IF (ISING(K1).NE.0) GO TO 75	DAUX33
	IF (K1.NE.KQ1(M)) GO TO 70	DAUX33
	IF (IJK(MNS,NNS).NE.0) GO TO 67	DAUX33
C		DAUX33
C	FOR ANY M>N SUCH THAT K1(N) = K1(M)	DAUX33
C		DAUX33
C	-1	DAUX33
C	C33(N,M) = C(N,M) + B31(N,K1) M (K1)A13(K1,M)	DAUX33
C	-1	DAUX33
C	+ B32(N,K1)PHI (K1)A23(K1,M)	DAUX33
C		DAUX33
C	-1	DAUX33
C	C33(M,N) = C(M,N) + B31(M,K1) M (K1)A13(K1,N)	DAUX33
C	-1	DAUX33



C		+ B32(M,K1)PHI (K1)A23(K1,N)	DAUX33
C			DAUX33
	IJ - IJ+1		DAUX33
	IJK(MNS,NNS) - IJ		DAUX33
	IJK(NNS,MNS) - IJ+1		DAUX33
	DO 66 J-1,3		DAUX33
	DO 66 I-1,3		DAUX33
	C(I,J,IJ) = 0.0		DAUX33
66	C(I,J,IJ+1) = 0.0		DAUX33
	IJ - IJ+1		DAUX33
67	JJ - IJK(MNS,NNS)		DAUX33
	DO 69 I-1,3		DAUX33
	DO 69 J-1,3		DAUX33
	SUM = C(I,J,JJ)		DAUX33
	TUM = C(I,J,JJ+1)		DAUX33
	DO 68 K-1,3		DAUX33
	SUM = SUM + B31(I,K,2*N-1)* RW( K1)*A13(K,J,2*M-1)		DAUX33
	* + B32(I,K,2*N-1)*RPHI(K,K1)*A23(K,J,2*M-1)		DAUX33
68	TUM = TUM + B31(I,K,2*M-1)* RW( K1)*A13(K,J,2*N-1)		DAUX33
	* + B32(I,K,2*M-1)*RPHI(K,K1)*A23(K,J,2*N-1)		DAUX33
	C(I,J,JJ) = SUM		DAUX33
69	C(I,J,JJ+1) = TUM		DAUX33
70	IF (K1.NE.KQ2(M)) GO TO 75		DAUX33
	IF (IJK(MNS,NNS).NE.0) GO TO 72		DAUX33
C			DAUX33
C	FOR ANY M>N SUCH THAT K1(N) = K2(M)		DAUX33
C			DAUX33
C		-1	DAUX33
C	C33(N,M) = C(N,M) + B31(N,K1) M (K1)A13(K2,M)		DAUX33
C		-1	DAUX33
C	+ B32(N,K1)PHI (K1)A23(K2,M)		DAUX33
C			DAUX33
C		-1	DAUX33
C	C33(M,N) = C(M,N) + B31(M,K2) M (K1)A13(K1,N)		DAUX33
C		-1	DAUX33
C	+ B32(M,K2)PHI (K1)A23(K1,N)		DAUX33
C			DAUX33
	IJ - IJ+1		DAUX33
	IJK(MNS,NNS) - IJ		DAUX33
	IJK(NNS,MNS) - IJ+1		DAUX33
	DO 71 J-1,3		DAUX33
	DO 71 I-1,3		DAUX33
	C(I,J,IJ) = 0.0		DAUX33
71	C(I,J,IJ+1) = 0.0		DAUX33
	IJ - IJ+1		DAUX33
72	JJ - IJK(MNS,NNS)		DAUX33
	DO 74 I-1,3		DAUX33
	DO 74 J-1,3		DAUX33
	SUM = C(I,J,JJ)		DAUX33
	TUM = C(I,J,JJ+1)		DAUX33
	DO 73 K-1,3		DAUX33
	SUM = SUM + B31(I,K,2*N-1)* RW( K1)*A13(K,J,2*M )		DAUX33

	* + B32(I,K,2*N-1)*RPHI(K,K1)*A23(K,J,2*M )	DAUX33
73	TUM = TUM + B31(I,K,2*M )* RW( K1)*A13(K,J,2*N-1)	DAUX33
	* + B32(I,K,2*M )*RPHI(K,K1)*A23(K,J,2*N-1)	DAUX33
	C(I,J,JJ ) = SUM	DAUX33
74	C(I,J,JJ+1) = TUM	DAUX33
75	IF (ISING(K2).NE.0) GO TO 85	DAUX33
	IF (K2.NE.KQ1(M)) GO TO 80	DAUX33
	IF (IJK(MNS,NNS).NE.0) GO TO 77	DAUX33
C		DAUX33
C	FOR ANY M>N SUCH THAT K2(N) = K1(M)	DAUX33
C		DAUX33
C		DAUX33
C	C33(N,M) = C(N,M) + B31(N,K2) M <sup>-1</sup> (K2)A13(K1,M)	DAUX33
C		DAUX33
C	+ B32(N,K2)PHI <sup>-1</sup> (K2)A23(K1,M)	DAUX33
C		DAUX33
C		DAUX33
C	C33(M,N) = C(M,N) + B31(M,K1) M <sup>-1</sup> (K2)A13(K2,N)	DAUX33
C		DAUX33
C	+ B32(M,K1)PHI <sup>-1</sup> (K2)A23(K2,N)	DAUX33
C		DAUX33
	IJ = IJ+1	DAUX33
	IJK(MNS,NNS) = IJ	DAUX33
	IJK(NNS,MNS) = IJ+1	DAUX33
	DO 76 J=1,3	DAUX33
	DO 76 I=1,3	DAUX33
	C(I,J,IJ ) = 0.0	DAUX33
76	C(I,J,IJ+1) = 0.0	DAUX33
	IJ = IJ+1	DAUX33
77	JJ = IJK(MNS,NNS)	DAUX33
	DO 79 I=1,3	DAUX33
	DO 79 J=1,3	DAUX33
	SUM = C(I,J,JJ)	DAUX33
	TUM = C(I,J,JJ+1)	DAUX33
	DO 78 K=1,3	DAUX33
	SUM = SUM + B31(I,K,2*N )* RW( K2)*A13(K,J,2*M-1)	DAUX33
	* + B32(I,K,2*N )*RPHI(K,K2)*A23(K,J,2*M-1)	DAUX33
78	TUM = TUM + C(I,J,2*M-1)* RW( K2)*A13(K,J,2*N )	DAUX33
	* + C(I,J,2*M-1)*RPHI(K,K2)*A23(K,J,2*N )	DAUX33
	C(I,J,JJ ) = TUM	DAUX33
79	C(I,J,JJ+1) = TUM	DAUX33
80	IF (K2.NE.KQ2(M)) GO TO 85	DAUX33
	IF (IJK(MNS,NNS).NE.0) GO TO 82	DAUX33
C		DAUX33
C	FOR ANY M>N SUCH THAT K2(N) = K2(M)	DAUX33
C		DAUX33
C		DAUX33
C	C33(N,M) = C(N,M) + B31(N,K2) M <sup>-1</sup> (K2)A13(K2,M)	DAUX33
C		DAUX33
C	+ B32(N,K2)PHI <sup>-1</sup> (K2)A23(K2,M)	DAUX33
C		DAUX33
C		DAUX33

C	C33(M,N) = C(M,N) + B31(M,K2) M (K2)A13(K2,N)	DAUX33
C	-1	DAUX33
C	+ B32(M,K2)PHI (K2)A23(K2,N)	DAUX33
C		DAUX33
	IJ = IJ+1	DAUX33
	IJK(MNS,NNS) = IJ	DAUX33
	IJK(NNS,MNS) = IJ+1	DAUX33
	DO 81 J=1,3	DAUX33
	DO 81 I=1,3	DAUX33
	C(I,J,IJ) = 0.0	DAUX33
81	C(I,J,IJ+1) = 0.0	DAUX33
	IJ = IJ+1	DAUX33
82	JJ = IJK(MNS,NNS)	DAUX33
	DO 84 I=1,3	DAUX33
	DO 84 J=1,3	DAUX33
	SUM = C(I,J,JJ)	DAUX33
	TUM = C(I,J,JJ+1)	DAUX33
	DO 83 K=1,3	DAUX33
	SUM = SUM + B31(I,K,2*N) * RW( K2)*A13(K,J,2*M )	DAUX33
	* + B32(I,K,2*N) *RPHI(K,K2)*A23(K,J,2*M )	DAUX33
83	TUM = TUM + B31(I,K,2*M) * RW( K2)*A13(K,J,2*N )	DAUX33
	* + B32(I,K,2*M) *RPHI(K,K2)*A23(K,J,2*N )	DAUX33
	C(I,J,JJ) = SUM	DAUX33
84	C(I,J,JJ+1) = TUM	DAUX33
85	CONTINUE	DAUX33
90	CONTINUE	DAUX33
	CALL ELTIME(2,19)	DAUX33
	RETURN	DAUX33
	END	DAUX33

	SUBROUTINE DAUX44		DAUX44
C		REV IV 07/24/86	SLIP
	IMPLICIT REAL*8(A-H,O-Z)		DAUX44
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		DAUX44
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),		DAUX44
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		DAUX44
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),		SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),		DAUX44
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)		DAUX44
	COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),		DAUX44
*	F(3,30),TQ(3,30),WJ(30),A11(3,3,30)		SLIP
	COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24),		DAUX44
*	HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12),		DAUX44
*	RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12),		DAUX44
*	KQ1(12),KQ2(12),KQTYPE(12)		DAUX44
	COMMON/FLXBLE/ HF(4,12,8),B42(3,3,24),V4(3,8),NFLEX(3,8)		DAUX44
	LOGICAL*1 FREE,LDDMY		80386
	COMMON/TEMPVS/ C(3,3,600),RHS(3,54),IJK(54,54),IJ,NQ2S		CHGIII
*	,IDUM(458),FREE(30),LDDMY(2),DDMY(27859)		80386
	IF (NFLX.EQ.0) GO TO 99		DAUX44
	CALL ELTIME(1,33)		DAUX44
	DO 90 L=1,NFLX		DAUX44
	N1 = NFLEX(1,L)		DAUX44
	N2 = NFLEX(2,L)		DAUX44
	N3 = NFLEX(3,L)		DAUX44
	IJ = IJ+1		DAUX44
	DO 10 I=1,3		DAUX44
	DO 10 J=1,3		DAUX44
	C(I,J,IJ) = 0.0		DAUX44
	DO 10 K=1,3		DAUX44
10	C(I,J,IJ) = C(I,J,IJ) + B42(I,K,3*L-2)*RPHI(K,N1)*B42(J,K,3*L-2)		DAUX44
*	+ B42(I,K,3*L-1)*RPHI(K,N2)*B42(J,K,3*L-1)		DAUX44
*	+ B42(I,K,3*L)*RPHI(K,N3)*B42(J,K,3*L)		DAUX44
	NSL = 2*NS+L		DAUX44
	IJK(NSL,NSL) = IJ		DAUX44
	DO 20 I=1,3		DAUX44
	RHS(I,NSL) = -V4(I,L)		DAUX44
	DO 20 J=1,3		DAUX44
20	RHS(I,NSL) = RHS(I,NSL) + B42(I,J,3*L-2)*U2(I,N1)		DAUX44
*	+ B42(I,J,3*L-1)*U2(I,N2)		DAUX44
*	+ B42(I,J,3*L)*U2(I,N3)		DAUX44
	IF (L.EQ.NFLX) GO TO 30		DAUX44
	LP1 = L+1		DAUX44
	DO 29 M=LP1,NFLX		DAUX44
	DO 28 II=1,3,2		DAUX44
	IL = NFLEX(II,L)		DAUX44
	IF (ISING(IL).NE.0) GO TO 28		DAUX44
	DO 27 JJ=1,3,2		DAUX44
	IF (NFLEX(II,L).NE.NFLEX(JJ,M)) GO TO 27		DAUX44
	NSM = 2*NS+M		DAUX44
	JK = IJK(NSL,NSM)		DAUX44

KJ = IJK(NSM,NSL)	DAUX44
IF (JK.GT.0) GO TO 22	DAUX44
IJK(NSL,NSM) = IJ+1	DAUX44
IJK(NSM,NSL) = IJ+2	DAUX44
JK = IJ+1	DAUX44
KJ = IJ+2	DAUX44
IJ = IJ+2	DAUX44
DO 21 I=1,3	DAUX44
DO 21 J=1,3	DAUX44
21 C(I,J,JK) = 0.0	DAUX44
22 LI = 3*L+II-3	DAUX44
MJ = 3*M+JJ-3	DAUX44
DO 24 I=1,3	DAUX44
DO 24 J=1,3	DAUX44
DO 23 K=1,3	DAUX44
23 C(I,J,JK) = C(I,J,JK) + B42(I,K,LI)*RPHI(K,IL)*B42(J,K,MJ)	DAUX44
24 C(J,I,KJ) = C(I,J,JK)	DAUX44
27 CONTINUE	DAUX44
28 CONTINUE	DAUX44
29 CONTINUE	DAUX44
30 IF (NQ.EQ.0) GO TO 40	DAUX44
DO 39 M=1,NQ	DAUX44
IF (KQTYPE(M).LT.0) GO TO 39	DAUX44
DO 38 II=1,3	DAUX44
LM = 0	DAUX44
IF (NFLEX(II,L).EQ.KQ1(M)) LM = 2*M-1	DAUX44
IF (NFLEX(II,L).EQ.KQ2(M)) LM = 2*M	DAUX44
IF (LM.EQ.0) GO TO 38	DAUX44
IL = NFLEX(II,L)	DAUX44
IF (ISING(IL).NE.0) GO TO 38	DAUX44
NSM = 2*NS+NFLX+M	DAUX44
JK = IJK(NSL,NSM)	DAUX44
KJ = IJK(NSM,NSL)	DAUX44
IF (JK.GT.0) GO TO 32	DAUX44
IJK(NSL,NSM) = IJ+1	DAUX44
IJK(NSM,NSL) = IJ+2	DAUX44
JK = IJ+1	DAUX44
KJ = IJ+2	DAUX44
IJ = IJ+2	DAUX44
DO 31 I=1,3	DAUX44
DO 31 J=1,3	DAUX44
C(I,J,JK) = 0.0	DAUX44
31 C(I,J,KJ) = 0.0	DAUX44
32 LI = 3*L+II-3	DAUX44
DO 33 I=1,3	DAUX44
DO 33 J=1,3	DAUX44
DO 33 K=1,3	DAUX44
C(I,J,JK) = C(I,J,JK) + B42(I,K,LI)*RPHI(K,IL)*A23(K,J,LM)	DAUX44
33 C(I,J,KJ) = C(I,J,KJ) + B32(I,K,LM)*RPHI(K,IL)*B42(J,K,LI)	DAUX44
38 CONTINUE	DAUX44
39 CONTINUE	DAUX44
40 IF (NJNT.EQ.0) GO TO 90	DAUX44

DO 59 M=1,NJNT	DAUX44
IF (JNT(M).EQ.0) GO TO 59	DAUX44
DO 58 II=1,3	DAUX44
LM = 0	DAUX44
IF (NFLEX(II,L).EQ.IABS(JNT(M))) LM = 2*M-1	DAUX44
IF (NFLEX(II,L).EQ.M+1) LM = 2*M	DAUX44
IF (LM.EQ.0) GO TO 58	DAUX44
IL = NFLEX(II,L)	DAUX44
IF (ISING(IL).NE.0) GO TO 58	DAUX44
NSM = 2*NS+NFLX+NQ+M	DAUX44
JK = IJK(NSL,NSM)	DAUX44
KJ = IJK(NSM,NSL)	DAUX44
IF (JK.GT.0) GO TO 42	DAUX44
IJK(NSL,NSM) = IJ+1	DAUX44
IJK(NSM,NSL) = IJ+2	DAUX44
JK = IJ+1	DAUX44
KJ = IJ+2	DAUX44
IJ = IJ+2	DAUX44
DO 41 I=1,3	DAUX44
DO 41 J=1,3	DAUX44
41 C(I,J,JK) = 0.0	DAUX44
42 LI = 3*L+II-3	DAUX44
DO 44 I=1,3	DAUX44
DO 44 J=1,3	DAUX44
DO 43 K=1,3	DAUX44
43 C(I,J,JK) = C(I,J,JK) + B42(I,K,LI)*RPHI(K,IL)*B12(J,K,LM)	DAUX44
44 C(J,I,KJ) = C(I,J,JK)	DAUX44
IF (FREE(M)) GO TO 58	SLIP
NSM = 2*NS+NFLX+NQ+NJNT+M	DAUX44
JK = IJK(NSL,NSM)	DAUX44
KJ = IJK(NSM,NSL)	DAUX44
IF (JK.GT.0) GO TO 52	DAUX44
IJK(NSL,NSM) = IJ+1	DAUX44
IJK(NSM,NSL) = IJ+2	DAUX44
JK = IJ+1	DAUX44
KJ = IJ+2	DAUX44
IJ = IJ+2	DAUX44
DO 51 I=1,3	DAUX44
DO 51 J=1,3	DAUX44
51 C(I,J,JK) = 0.0	DAUX44
52 SET = 1.0	DAUX44
IF (IL.EQ.M+1) SET = -1.0	DAUX44
DO 54 I=1,3	DAUX44
DO 54 J=1,3	DAUX44
DO 53 K=1,3	DAUX44
53 C(I,J,JK) = C(I,J,JK) + SET*B42(I,K,LI)*RPHI(K,IL)*A22(K,J,LM)	DAUX44
54 C(J,I,KJ) = C(I,J,JK)	DAUX44
58 CONTINUE	DAUX44
59 CONTINUE	DAUX44
90 CONTINUE	DAUX44
CALL ELTIME(2,33)	DAUX44
99 RETURN	DAUX44

END

DAUX44

	SUBROUTINE DAUX55	DAUX55
C		REV IV 07/24/86SLIP
	IMPLICIT REAL*8(A-H,O-Z)	DAUX55
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,	DAUX55
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),	DAUX55
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)	DAUX55
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),	SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),	DAUX55
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)	DAUX55
	COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),	DAUX55
*	F(3,30),TQ(3,30),WJ(30),A11(3,3,30)	SLIP
	COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24),	DAUX55
*	HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12),	DAUX55
*	RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12),	DAUX55
*	KQ1(12),KQ2(12),KQTYPE(12)	DAUX55
	COMMON/FLXBLE/ HF(4,12,8),B42(3,3,24),V4(3,8),NFLEX(3,8)	DAUX55
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),	DAUX55
*	UNITL,UNITM,UNITT,GRAVTY(3),TWOPI	TWOPI
	LOGICAL*1 FREE,LDDMY	80386
	COMMON/TEMPVS/ C(3,3,600),RHS(3,54),IJK(54,54),IJ,NQ2S	CHG111
*	,IDUM(458),FREE(30),LDDMY(2),DDMY(27859)	80386
	CALL ELTIME(1,30)	DAUX55
	IS = 0	DAUX55
	DO 99 I=1,NGRND	DAUX55
	IF (ISING(I).LE.0) GO TO 99	DAUX55
	IS = IS+1	DAUX55
	IJ = IJ+1	DAUX55
	IJK(IS,IS) = IJ	DAUX55
	IJK(IS+1,IS+1) = IJ+1	DAUX55
	DO 11 J=1,3	DAUX55
	RHS(J,IS) = U1(J,I) + W(I)*GRAVTY(J)/G	DAUX55
	RHS(J,IS+1) = U2(J,I)	DAUX55
	U1(J,I) = 0.0	DAUX55
	U2(J,I) = 0.0	DAUX55
	DO 10 K=1,3	DAUX55
	C(J,K,IJ) = 0.0	DAUX55
10	C(J,K,IJ+1) = 0.0	DAUX55
	C(J,J,IJ) = W(I)/G	DAUX55
11	C(J,J,IJ+1) = PHI(J,I)	DAUX55
	IJ = IJ+1	DAUX55
	IF (NFLX.EQ.0) GO TO 19	DAUX55
	DO 15 N=1,NFLX	DAUX55
	LN = 0	DAUX55
	IF (NFLEX(1,N).EQ.1) LN = 3*N-2	DAUX55
	IF (NFLEX(2,N).EQ.1) LN = 3*N-1	DAUX55
	IF (NFLEX(3,N).EQ.1) LN = 3*N	DAUX55
	IF (LN.EQ.0) GO TO 15	DAUX55
	DO 14 J=1,3	DAUX55
	DO 14 K=1,3	DAUX55
	C(J,K,IJ+1) = B42(K,J,LN)	DAUX55
14	C(J,K,IJ+2) = B42(J,K,LN)	SLIP



NNS = 2*NS+N	DAUX55
IJK(IS+1,NNS) = IJ+1	DAUX55
IJK(NNS,IS+1) = IJ+2	DAUX55
IJ = IJ+2	DAUX55
15 CONTINUE	DAUX55
19 IF (NQ.EQ.0) GO TO 30	DAUX55
DO 25 N=1,NQ	DAUX55
IF (KQTYPE(N).LT.0) GO TO 25	DAUX55
LN = 0	DAUX55
IF (I.EQ.KQ1(N)) LN = 2*N-1	DAUX55
IF (I.EQ.KQ2(N)) LN = 2*N	DAUX55
IF (LN.EQ.0) GO TO 25	DAUX55
DO 20 J=1,3	DAUX55
DO 20 K=1,3	DAUX55
C(J,K,IJ+1) = A13(J,K,LN)	DAUX55
C(J,K,IJ+2) = A23(J,K,LN)	DAUX55
C(J,K,IJ+3) = B31(J,K,LN)	SLIP
20 C(J,K,IJ+4) = B32(J,K,LN)	SLIP
NNS = 2*NS+NFLX+N	DAUX55
IJK(IS ,NNS) = IJ+1	DAUX55
IJK(IS+1,NNS) = IJ+2	DAUX55
IJK(NNS,IS ) = IJ+3	DAUX55
IJK(NNS,IS+1) = IJ+4	DAUX55
IJ = IJ+4	DAUX55
25 CONTINUE	DAUX55
30 IF (NJNT.EQ.0) GO TO 98	DAUX55
DO 65 N=1,NJNT	DAUX55
IF (JNT(N).EQ.0) GO TO 65	DAUX55
LN = 0	DAUX55
IF (I.EQ.IABS(JNT(N))) LN = 2*N-1	DAUX55
IF (I.EQ.N+1) LN = 2*N	DAUX55
IF (LN.EQ.0) GO TO 65	DAUX55
SET = 1.0	DAUX55
IF (I.EQ.N+1) SET = -1.0	DAUX55
DO 40 J=1,3	DAUX55
DO 40 K=1,3	SLIP
C(J,K,IJ+1) = SET*A11(J,K,N)	SLIP
C(J,K,IJ+3) = SET*A11(K,J,N)	SLIP
C(J,K,IJ+2) = B12(K,J,LN)	DAUX55
40 C(J,J,IJ+4) = B12(J,K,LN)	SLIP
NNS = NQ2S + N	DAUX55
IJK(IS ,NNS) = IJ+1	DAUX55
IJK(IS+1,NNS) = IJ+2	DAUX55
IJK(NNS,IS ) = IJ+3	DAUX55
IJK(NNS,IS+1) = IJ+4	DAUX55
IJ = IJ+4	DAUX55
IF (FREE(N)) GO TO 65	SLIP
DO 60 J=1,3	DAUX55
DO 60 K=1,3	DAUX55
C(J,K,IJ+1) = SET*A22(J,K,LN)	DAUX55
60 C(J,K,IJ+2) = SET*A22(K,J,LN)	SLIP
NNS = NQ2S + NJNT + N	DAUX55

IJK(IS+1,NNS) = IJ+1	DAUX55
IJK(NNS,IS+1) = IJ+2	DAUX55
IJ = IJ+2	DAUX55
65 CONTINUE	DAUX55
98 IS = IS+1	DAUX55
99 CONTINUE	DAUX55
CALL ELTIME(2,30)	DAUX55
RETURN	DAUX55
END	DAUX55

	SUBROUTINE DHHPIN(DD,BN,L,M,N)		DHHPIN
C		REV IV	07/24/86SLIP
C	SETS DD = D(L) IF JOINT M IS NOT PINNED		DHHPIN
C	OR DD = (I-HH.)(D(L)) IF PINNED		DHHPIN
C			DHHPIN
	IMPLICIT REAL*8 (A-H,O-Z)		DHHPIN
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),		DHHPIN
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		DHHPIN
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),		SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),		DHHPIN
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)		DHHPIN
	COMMON/CEULER/ IEULER(30),HIR(3,3,90),ANG(3,30),ANGD(3,30),		JDRIFT
*	FE(3,30),TQE(3,30),CONST(5,30)		JDRIFT
	DIMENSION DD(3,3),BN(3)		DHHPIN
	DO 10 J=1,3		DHHPIN
	BN(J) = 0.0		DHHPIN
	DO 10 I=1,3		DHHPIN
10	DD(I,J) = D(I,J,L)		DHHPIN
	LGO = IPIN(M)+8		SLIP
	TSIGN = -1.0		DHHPIN
	GO TO (90,90,90,20,90,90,90,90,30,90,90,90,90,30,30),LGO		SLIP
20	IF (IEULER(M).GE.7) GO TO 90		DHHPIN
	IF (IEULER(M).GE.4) GO TO 30		DHHPIN
	TSIGN = 1.0		DHHPIN
	DO 21 J=1,3		DHHPIN
	DO 21 I=1,3		DHHPIN
21	DD(I,J) = 0.0		DHHPIN
30	DO 31 J=1,3		DHHPIN
	BN(J) = HB(1,N)*D(1,J,L) + HB(2,N)*D(2,J,L) + HB(3,N)*D(3,J,L)		DHHPIN
	DO 31 I=1,3		DHHPIN
31	DD(I,J) = DD(I,J) + TSIGN*BN(J)*HB(I,N)		DHHPIN
90	RETURN		DHHPIN
	END		DHHPIN

	SUBROUTINE DINT		DINT
C		REV IV 07/23/86	TWOPI
	IMPLICIT REAL*8 (A-H,O-Z)		DINT
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		DINT
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/INTEST/ SGTEST(3,4,30),XTEST(360 ),SEGT(120),REGT(120)		DINT
C	NOTE: XTEST SINGLY DIMENSIONED HERE.		DINT
	REAL SEGT		DINT
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),		DINT
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI		TWOPI
	COMMON/CDINT/ UU(4),GH(3,4),		DINT
*	E(3,240), F(5,240),GG(5,240),Y(5,240),U(5,240),		DINT
*	H,HPRINT,HS,TPRINT,TSTART,ICNT,IDBL,IFLAG,IDMMY		80386
	COMMON/COMAIN/ VAR(240),DER(240),DT,H0,HMAX,HMIN,RSTIME,		DINT
*	ISTEP,NSTEPS,NDINT,NEQ,IRSIN,IRSOUT		DINT
	LOGICAL LNRT		TGMOD1
	CALL ELTIME(1,3)		DINT
	IF (ISTEP.NE.0) GO TO 11		DINT
C			DINT
C	IN=0: INITIAL CALL TO INTEGRATOR - INITIALIZE AND RESET PARAMETERS		DINT
C	NOTE: FOR EARLIER VERSIONS OF CVS, THE VARIABLE 'IN'(ISTEP IN THE		DINT
C	CALLING PROGRAM) RAN FROM 1 TO NSTEPS+1, NOW IT RUNS FROM		DINT
C	0 TO NSTEPS.		DINT
C			DINT
	TPRINT = TIME		DINT
	IDBL = 2		DINT
	K = 0		DINT
	GO TO 13		DINT
C			DINT
C	IN#0: ADVANCE TPRINT - TIME TO RETURN TO CALLING PROGRAM.		DINT
C			DINT
11	TPRINT = TPRINT + DT		DINT
	H = HPRINT		DINT
C			DINT
C	ENTRY TO ADVANCE INTEGRATOR		DINT
C			DINT
12	K = 1		DINT
	CALL UPDATE(K)		DINT
C			DINT
C	NEGATIVE K FROM UPDATE IS INDICATOR TO RESET INTEGRATOR.		DINT
C			DINT
	IF (K.EQ.1) GO TO 15		DINT
C			DINT
C	RESET OR INITIALIZE INTEGRATOR.		DINT
C			DINT
13	H = H0		DINT
	HPRINT = H0		DINT
	HS = 0.0		DINT
	ICNT = -2		DINT
	IF (ISTEP.EQ.0 .OR. NPRT(26).EQ.2) CALL OUTPUT(0)		DINT
	CALL PDAUX (VAR,DER,NEQ,K)		DINT
	IF (ISTEP.NE.0 .AND. NPRT(26).EQ.2) CALL OUTPUT(1)		DINT

	DO 14 I=1,NEQ	DINT
	F(1,I) = VAR(I)	DINT
	F(2,I) = DER(I)	DINT
	DO 14 J=3,5	DINT
	F(J,I) = 0.0	DINT
	U(J,I) = 0.0	DINT
14	Y(J,I) = 0.0	DINT
	IF (ISTEP.EQ.0) GO TO 65	DINT
	K = 1	DINT
C		DINT
C	ADJUST H (CURRENT TIME STEP) IF IT WILL ADVANCE T BEYOND TPRINT.	DINT
C		DINT
15	IF (H+EPS(8).GE.TPRINT-TIME) H = TPRINT-TIME	DINT
C		DINT
C	BACKUP ENTRY POINT IF H HAS BEEN HALVED.	DINT
C		DINT
16	D1 = 0.5*H	D1
	CALL TRIGFS	DINT
	TSTART = TIME	DINT
	DO 20 I=1,NEQ	DINT
	U(3,I) = Y(5,I)	DINT
	U(4,I) = U(5,I)	DINT
	DO 20 J=1,5	DINT
20	GG(J,I) = F(J,I)	DINT
	CALL CMPUTE (K,1,D1)	DINT
	IF (K.LT.0) GO TO 50	DINT
	CALL ADJUST (1,D1)	DINT
	K = 2	DINT
	CALL CMPUTE (K,0,D1)	DINT
	IF (K.LT.0) GO TO 50	DINT
	CALL ADJUST (2,D1)	DINT
	NQUAT = K	DINT
	K = 3	DINT
	CALL CMPUTE (K,1, H)	DINT
	IF (K.LT.0) GO TO 50	DINT
	CALL ADJUST (3,D1)	DINT
	DO 49 L=1,NDINT	DINT
	M = 1	DINT
	IF (L.EQ.1) M = 0	DINT
	IF (NPRT(26).NE.2) CALL OUTPUT(0)	DINT
	CALL CMPUTE (K,M, H)	DINT
	IF (K.LT.0) GO TO 50	DINT
	FAIL = 1.0	DINT
	JJ = 0	DINT
	DO 47 II=1,NEQ,3	DINT
	JJ = JJ+1	DINT
	IF (XTEST(II).LE.0.0) GO TO 47	DINT
	TT = DER(II)**2 + DER(II+1)**2 + DER(II+2)**2	DINT
	TX = VAR(II)**2 + VAR(II+1)**2 + VAR(II+2)**2	DINT
	TE = 0.0	DINT
	TY = 0.0	DINT
	I2 = II+2	DINT

DO 45 I=II,I2	DINT
Z = GG(5,I)*(VAR(I)-GG(1,I)) + GG(2,I) + H*(GG(3,I)+H*GG(4,I))	DINT
TE = TE + (DER(I)-Z)**2	DINT
TYD = TT + TX*GG(5,I)**2	DINT
IF (TYD.EQ.0.0) TYD = 1.0	DINT
45 TY = TY + (DER(I)-Z)**2/TYD	DINT
TM = 1000.0*TIME	DINT
IF (NPRT(25).NE.0) WRITE (6,46) TM,SEGT(JJ),REGT(JJ),TT,TE,TY,	DINT
* (XTEST(I),I-II,I2)	DINT
46 FORMAT ('O DINT CONV. TEST',F10.3,2X,A4,2X,A8,6G12.4)	DINT
IF (TT.LT.XTEST(II)) GO TO 47	DINT
IF (XTEST(II+1).GT.0.0 .AND. TE.LT.XTEST(II+1)) GO TO 47	DINT
IF (TY.GT.XTEST(II+2)) GO TO 48	DINT
47 CONTINUE	DINT
FAIL = 0.0	DINT
48 CALL ADJUST (4,D1)	DINT
IF (FAIL.EQ.0.0) GO TO 60	DINT
IF (L.EQ.NDINT) GO TO 49	DINT
CALL CMPUTE (K,1,D1)	DINT
IF (K.LT.0) GO TO 50	DINT
CALL ADJUST (5,D1)	DINT
49 CONTINUE	DINT
IF (NPRT(25).EQ.0) WRITE (6,46) TM,SEGT(JJ),REGT(JJ),TT,TE,TY,	DINT
* (XTEST(I),I-II,I2)	DINT
50 WRITE (6,51) TIME,H	DINT
51 FORMAT('O TEST FAILED AT TIME = ',F10.6,' FOR H = ',F10.6)	DINT
ICNT = 0	DINT
IDBL = IDBL+2	DINT
IF (IDBL.GT.6) IDBL = 6	DINT
IF (K.GE.0) GO TO 58	DINT
IF (H.GT.HMIN+EPS(8)) GO TO 59	DINT
WRITE (6,52)	DINT
52 FORMAT('O PROGRAM TERMINATED. PDAUX NEG SQRT. H < HMIN+EPS8.'/	DINT
* ' RERUN PROGRAM WITH SMALLER HMIN ON INPUT CARD A.4')	DINT
STOP 31	DINT
58 IF (H.LE.HMIN+EPS(8)) GO TO 61	DINT
IF (NPRT(26).EQ.2) CALL OUTPUT(1)	DINT
59 TIME = TSTART	DINT
H = 0.5*H	DINT
HPRINT = 0.5*HPRINT	DINT
K = 2	DINT
GO TO 16	DINT
60 IF (H.GT.0.74*HPRINT) ICNT = ICNT+1	DINT
61 K = 4	DINT
M = 0	DINT
IF (H.GT.HMIN .AND. IDBL.GT.2) IDBL = IDBL-1	DINT
GG4 = 2.0*H	DINT
GG5 = DEXP(-1600.0*H)	DINT
DO 63 I=1,NEQ	DINT
F(3,I) = GG(3,I) + GG4*GG(4,I)	DINT
F(4,I) = GG(4,I)	DINT
F(5,I) = GG(5,I)	DINT

Y(3,I) - Y(1,I)	DINT
Y(4,I) - Y(2,I)	DINT
Y(5,I) - GG5*U(3,I)	DINT
63 U(5,I) - GG5*U(4,I)	DINT
CALL QSET(F,Y,VAR,DER,NQUAT)	DINT
CALL PDAUX (VAR,DER,M,K)	DINT
DO 64 I=1,NEQ	DINT
F(1,I) - VAR(I)	DINT
64 F(2,I) - DER(I)	DINT
HS = H	DINT
IF (ICNT.LT.IDBL) GO TO 65	DINT
ICNT = 0	DINT
H = DMIN1(2.0*H,HMAX)	DINT
HPRINT = DMIN1(2.0*HPRINT,HMAX)	DINT
65 CALL UPDATE(2)	DINT
XPRINT = TPRINT - TIME	TGMOD1
IF(XPRINT.GE.EPS(8).AND.NPRT(26).NE.3.AND.NPRT(26).GE.0)	TGMOD1
* CALL OUTPUT(1)	TGMOD1
IF(XPRINT.GE.EPS(8)) GO TO 12	TGMOD1
LNRT = .FALSE.	TGMOD1
IF(NPRT(26).GE.0) LNRT = .TRUE.	TGMOD1
IF(NPRT(26).LT.0) INRT = IABS(NPRT(26))	TGMOD1
IF(NPRT(26).LT.0) LNRT = (MOD(ISTEP,INRT).EQ.0)	TGMOD1
IF(LNRT) CALL OUTPUT(1)	TGMOD1
CALL ELTIME(2,3)	DINT
RETURN	DINT
END	DINT

	SUBROUTINE DOTT31 (A,B,C)		DOTT31
C		REV 17	12/20/76DOTT31
C	PERFORMS MATRIX MULTIPLICATION C = AB'		DOTT31
C	WHERE C IS A 3X3 MATRIX, AND A AND B ARE VECTORS OF LENGTH 3.		DOTT31
C			DOTT31
	IMPLICIT REAL*8 (A-H,O-Z)		DOTT31
	DIMENSION A(3) , B(3) , C(3,3)		DOTT31
	DO 10 I=1,3		DOTT31
	DO 10 J=1,3		DOTT31
10	C(I,J) = A(I)*B(J)		DOTT31
	RETURN		DOTT31
	END		DOTT31



	SUBROUTINE DOTT33 (A,B,C)		DOTT33
C		REV 17	01/03/77DOTT33
C	PERFORMS MATRIX MULTIPLICATION C = AB'		DOTT33
C	WHERE A, B AND C ARE ALL 3X3 MATRICEES.		DOTT33
C			DOTT33
	IMPLICIT REAL*8 (A-H,O-Z)		DOTT33
	DIMENSION A(3,3) , B(3,3) , C(3,3)		DOTT33
	DO 10 I=1,3		DOTT33
	DO 10 J=1,3		DOTT33
10	C(I,J) = A(I,1)*B(J,1) + A(I,2)*B(J,2) + A(I,3)*B(J,3)		DOTT33
	RETURN		DOTT33
	END		DOTT33

	SUBROUTINE DOT31 (A,B,C)	DOT31
C		REV 17 01/03/77DOT31
C	PERFORMS MATRIX MULTIPLICATION $C = A'B$	DOT31
C	WHERE A IS A 3X3 MATRIX, AND B AND C ARE VECTORS OF LENGTH 3.	DOT31
C		DOT31
	IMPLICIT REAL*8 (A-H,O-Z)	DOT31
	DIMENSION A(3,3) , B(3) , C(3)	DOT31
	$C(1) = A(1,1)*B(1) + A(2,1)*B(2) + A(3,1)*B(3)$	DOT31
	$C(2) = A(1,2)*B(1) + A(2,2)*B(2) + A(3,2)*B(3)$	DOT31
	$C(3) = A(1,3)*B(1) + A(2,3)*B(2) + A(3,3)*B(3)$	DOT31
	RETURN	DOT31
	END	DOT31

	SUBROUTINE DOT33 (A,B,C)		DOT33
C		REV 17	01/03/77DOT33
C	PERFORMS MATRIX MULTIPLICATION $C = A'B$		DOT33
C	WHERE A, B AND C ARE ALL 3X3 MATRICES.		DOT33
C			DOT33
	IMPLICIT REAL*8 (A-H,O-Z)		DOT33
	DIMENSION A(3,3) , B(3,3) , C(3,3)		DOT33
	DO 10 I=1,3		DOT33
	DO 10 J=1,3		DOT33
10	C(I,J) = A(1,I)*B(1,J) + A(2,I)*B(2,J) + A(3,I)*B(3,J)		DOT33
	RETURN		DOT33
	END		DOT33

	SUBROUTINE DRCIJK (D,ANG,ID,HT,J)		DRCIJK
C		REV 18	02/24/78DRCIJK
	IMPLICIT REAL*8 (A-H,O-Z)		DRCIJK
	DIMENSION D(9,22),HT(9,42),ANG(3,2-),ID(4,22),T1(9),T2(9)		DRCIJK
	M = ID(4,J)		DRCIJK
	IF (M.NE.0) GO TO 10		DRCIJK
	CALL DRCYPR (D(1,J),ANG(1,J),ID(1,J))		DRCIJK
	GO TO 99		DRCIJK
10	CALL DRCYPR (T1,ANG(1,J),ID(1,J))		DRCIJK
	IF (M.LT.0) GO TO 20		DRCIJK
	CALL MAT33 (T1,D(1,M),D(1,J))		DRCIJK
	GO TO 99		DRCIJK
20	M = -M		DRCIJK
	CALL DOT33 (HT(1,2*J-3),D(1,M),D(1,J))		DRCIJK
	CALL MAT33 (T1,D(1,J),T2)		DRCIJK
	CALL MAT33 (HT(1,2*J-2),T2,D(1,J))		DRCIJK
99	RETURN		DRCIJK
	END		DRCIJK

	SUBROUTINE DRCQUA(DC,Q)	
C		DRCQUA
		REV III.5 07/31/85JTF785
C	COMPUTES DIRECTION COSINE MATRIX FROM QUATERNIONS	DRCQUA
	IMPLICIT REAL*8(A-H,O-Z)	DRCQUA
	DIMENSION DC(3,3),Q(4)	DRCQUA
	C = Q(1)**2 - Q(2)**2 - Q(3)**2 - Q(4)**2	JTF785
	DO 12 I = 1,3	DRCQUA
	DO 10 J = 1,3	DRCQUA
10	DC(I,J) = 2.0*Q(I+1)*Q(J+1)	DRCQUA
12	DC(I,I) = DC(I,I) + C	DRCQUA
	E = Q(1) + Q(1)	DRCQUA
	DO 14 I = 1,3	DRCQUA
	J = 1 + MOD(I,3)	DRCQUA
	K = 1 + MOD(I+1,3)	DRCQUA
	D = E*Q(I+1)	DRCQUA
	DC(K,J) = DC(K,J) - D	DRCQUA
14	DC(J,K) = DC(J,K) + D	DRCQUA
	DO 18 I = 1,3	DRCQUA
	DO 18 J = 1,3	DRCQUA
18	IF(DABS(DC(I,J)).GT.1.0D0)DC(I,J) = DSIGN(1.0D0,DC(I,J))	DRCQUA
	RETURN	DRCQUA
	END	DRCQUA

	SUBROUTINE DRCYPR (D,A,ID)		DRCYPR
		REV IV 07/23/86	TWOPI
C	SETS UP 3X3 DIRECTION COSINE MATRIX FOR GIVEN YAW,PITCH AND ROLL.		DRCYPR
C			DRCYPR
C	ARGUMENTS:		DRCYPR
C	D: 3X3 DIRECTION COSINE MATRIX TO BE COMPUTED.		DRCYPR
C	A: ARRAY OF LENGTH 3 CONTAINING ROTATION ANGLES (DEGREES).		DRCYPR
C	I1: AXIS OF ROTATION FOR 1ST ANGLE (1,2,3 = X,Y,Z)		DRCYPR
C	I2: AXIS OF ROTATION FOR 2ND ANGLE (1,2,3 = X,Y,Z)		DRCYPR
C	I3: AXIS OF ROTATION FOR 3RD ANGLE (1,2,3 = X,Y,Z)		DRCYPR
C			DRCYPR
	IMPLICIT REAL*8 (A-H,O-Z)		DRCYPR
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),		DRCYPR
	* UNITL,UNITM,UNITT,GRAVITY(3),TWOPI		DRCYPR
	DIMENSION D(3,3),A(3),ID(3),T(3,3),B(3),S(3)		TWOPI
	IDSUM = ID(1) + ID(2) + ID(3)		DRCYPR
	DO 12 I=1,3		DRCYPR
	B(I) = A(I)*RADIAN		DRCYPR
	DO 11 J=1,3		DRCYPR
11	D(I,J) = 0.0		DRCYPR
12	D(I,I) = 1.0		DRCYPR
	DO 30 N=1,3		DRCYPR
	IDN = IABS(ID(N))		DRCYPR
	M = 4 - IDN		DRCYPR
	IF (ID(N).LT.0) M = IDSUM - ID(N) - 2		DRCYPR
	IF (B(M).EQ.0.0) GO TO 30		DRCYPR
	CALL ROT (T,IDN,B(M))		DRCYPR
	DO 23 J=1,3		DRCYPR
	DO 21 K=1,3		DRCYPR
	S(K) = D(K,J)		DRCYPR
21	D(K,J) = 0.0		DRCYPR
	DO 22 I=1,3		DRCYPR
	DO 22 K=1,3		DRCYPR
22	D(I,J) = D(I,J) + T(I,K)*S(K)		DRCYPR
23	CONTINUE		DRCYPR
30	CONTINUE		DRCYPR
	RETURN		DRCYPR
	END		DRCYPR

' SUBROUTINE DRIFT

REV IV 07/24/86SLIP

C		DRIFT
C	CORRECTS FOR DRIFT IN CONSTRAINED JOINTS	DRIFT
C		DRIFT
C		DRIFT
	IMPLICIT REAL*8(A-H,O-Z)	DRIFT
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,	DRIFT
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	DRIFT
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),	DRIFT
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)	DRIFT
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),	SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),	DRIFT
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)	DRIFT
	COMMON/CEULER/ IEULER(30),HIR(3,3,90),ANG(3,30),ANGD(3,30),	DRIFT
*	FE(3,30),TQE(3,30),CONST(5,30)	DRIFT
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),	DRIFT
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI	TWOPI
	COMMON/TEMPVS/ T1(3),T2(3),T3(3),T4(3),TP(3,3),H1(3),H2(3)	DRIFT
*	,DDMY(35086)	80386
	IF (NJNT.EQ.0) GO TO 51	DRIFT
	DO 50 J=1,NJNT	DRIFT
	K = IABS(JNT(J))	DRIFT
	IF (K.EQ.0) GO TO 50	DRIFT
	IF (ISING(J+1).LT.0) GO TO 50	DRIFT
C		DRIFT
	M = 0	DRIFT
	IF (IPIN(J).EQ.1) M = 4	DRIFT
	IF (IPIN(J).EQ.6) M = 4	SLIP
	IF (IPIN(J).EQ.7) M = 4	SLIP
	IF (IABS(IPIN(J)).NE.4) GO TO 15	DRIFT
	IF (IEULER(J).EQ.1) M = 2	DRIFT
	IF (IEULER(J).EQ.2) M = 3	DRIFT
	IF (IEULER(J).EQ.3) M = 1	DRIFT
	IF (IEULER(J).EQ.4) M = 4	DRIFT
	IF (IEULER(J).EQ.5) M = 4	DRIFT
	IF (IEULER(J).EQ.6) M = 4	DRIFT
15	IF (M.EQ.0) GO TO 50	DRIFT
	IF(M.EQ.4)GO TO 23	DRIFT
	IF(M.NE.3)GO TO 21	DRIFT
	CALL EJOINT(-1,J)	DRIFT
	CALL CROSS(HIR(1,2,2*J+29),HIR(1,1,2*J+29),T1)	DRIFT
	DO 17 I = 1,3	DRIFT
	H1(I) = CONST(4,J)*HIR(I,1,2*J+29) + CONST(5,J)*T1(I)	DRIFT
17	H2(I) = HIR(I,3,2*J+30)	DRIFT
	GO TO 25	DRIFT
21	DO 22 I = 1,3	DRIFT
	H1(I) = HIR(I,M,2*J+29)	DRIFT
22	H2(I) = HIR(I,M+1,2*J+30)	DRIFT
	GO TO 25	DRIFT
23	DO 24 I = 1,3	DRIFT
	H1(I) = HB(I,2*J-1)	DRIFT
24	H2(I) = HB(I,2*J)	DRIFT

C		DRIFT
C	** ADJUST DC MATRIX FOR CONSTRAINED JOINTS **	DRIFT
C		DRIFT
	25 CALL DOT31(D(1,1,K),H1,T1)	DRIFT
	CALL MAT31 (D(1,1,J+1),T1,T2)	DRIFT
	CT = T2(1)*H2(1) + T2(2)*H2(2) + T2(3)*H2(3)	DRIFT
	IF(M.GE.3)GO TO 28	DRIFT
	ST = 1.0/DSQRT((1.0 - CT)*(1.0 + CT))	DRIFT
	DO 27 I = 1,3	DRIFT
	27 T2(I) = (H2(I) - CT*T2(I))*ST	DRIFT
	CT = 1.0/ST	DRIFT
	28 CALL CROSS(H2,T2,T3)	DRIFT
	DO 30 L=1,3	DRIFT
	CALL CROSS (T3,D(1,L,J+1),T4)	DRIFT
	ST = T3(1)*D(1,L,J+1) + T3(2)*D(2,L,J+1) + T3(3)*D(3,L,J+1)	DRIFT
	ST = ST/(1.0 + CT)	DRIFT
	DO 30 I=1,3	DRIFT
	30 D(I,L,J+1) = CT*D(I,L,J+1) - T4(I) + ST*T3(I)	DRIFT
C		DRIFT
C	** RENORMALIZATION OF DIRECTION COSINE MATRIX BY **	DRIFT
C	** AVERAGING MATRIX AND TRANSPOSE OF ITS INVERSE **	DRIFT
C		DRIFT
	DO 33 ITER= 1,10	DRIFT
	CALL CFACTT (D(1,1,J+1),TP,DET)	DRIFT
	DO 32 L = 1,3	DRIFT
	DO 32 I = 1,3	DRIFT
	D(I,L,J+1) = 0.5*(D(I,L,J+1)+TP(L,I)/DET)	DRIFT
	32 IF (DABS(D(I,L,J+1)).LT.EPS(15)) D(I,L,J+1) = 0.0	DRIFT
	IF (DABS(DET-1.0).LT.EPS(6)) GO TO 41	DRIFT
	33 CONTINUE	DRIFT
	WRITE (6,34) J,TIME,DET	DRIFT
	34 FORMAT (44H0 DRIFT RENORMALIZATION DID NOT CONVERGE FOR,	DRIFT
	* 10H JOINT NO.,I3,7H TIME =,F10.6,6H DET =,F10.6)	DRIFT
C		DRIFT
C	** ADJUST WMEG FOR CONSTRAINED JOINTS **	DRIFT
C		DRIFT
	41 IF(M.NE.4)GO TO 43	DRIFT
	HW = H2(1)*WMEG(1,J+1) - H1(1)*WMEG(1,K)	DRIFT
	* + H2(2)*WMEG(2,J+1) - H1(2)*WMEG(2,K)	DRIFT
	* + H2(3)*WMEG(3,J+1) - H1(3)*WMEG(3,K)	DRIFT
	CALL DOT31 (D(1,1,K),WMEG(1,K),T1)	DRIFT
	CALL MAT31 (D(1,1,J+1),T1,WMEG(1,J+1))	DRIFT
	DO 42 I=1,3	DRIFT
	42 WMEG(I,J+1) = WMEG(I,J+1) + HW*H2(I)	DRIFT
	GO TO 50	DRIFT
	43 IF(M.NE.3)GO TO 47	DRIFT
	CALL DOT31(D(1,1,K),HIR(1,2,2*J+29),T1)	DRIFT
	CALL MAT31(D(1,1,J+1),T1,H1)	DRIFT
	GO TO 48	DRIFT
	47 CALL MAT31(D(1,1,J+1),T1,T2)	DRIFT
	CALL CROSS(T2,H2,H1)	DRIFT
	48 CALL DOT31(D(1,1,K),WMEG(1,K),T1)	DRIFT



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      CALL MAT31(D(1,1,J+1),T1,T2)
      HW = H1(1)*(T2(1) - WMEG(1,J+1))
      *   + H1(2)*(T2(2) - WMEG(2,J+1))
      *   + H1(3)*(T2(3) - WMEG(3,J+1))
      DO 49 I = 1,3
49 WMEG(I,J+1) = WMEG(I,J+1) + HW*H1(I)
50 CONTINUE
51 RETURN
      END

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DRIFT
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SUBROUTINE DSETD(D,TH,T)                                DSETD
C                                                         REV IV    07/23/86TWOPI
C   UPDATES A DIRECTION COSINE MATRIX (D)                DSETD
C   USING AN INCREMENTAL ANGULAR MOTION (TH).            DSETD
C       ARGUMENTS D: 3X3 DIRECTION COSINE MATRIX TO BE UPDATED. DSETD
C                   TH: 3 COMPONENTS OF INCREMENTAL ANGULAR MOTION DSETD
C                   ABOUT LOCAL X,Y AND Z AXIS RESPECTIVELY.     DSETD
C                   T: MAGNITUDE OF VECTOR TH COMPUTED BY ROUTINE. DSETD
C                                                         DSETD
      IMPLICIT REAL*8(A-H,O-Z)                             DSETD
      DIMENSION D(3,3),TH(3),S(3),TEMP(3,3)              DSETD
      COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),          DSETD
*               UNITL,UNITM,UNITT,GRAVITY(3),TWOPI        TWOPI
      T=DSQRT(TH(1)**2+TH(2)**2+TH(3)**2)                 DSETD
      IF(T.EQ.0.)RETURN                                     DSETD
      ST=DSIN(T)                                            DSETD
      CT=L~COS(T)                                           DSETD
      STT=ST/T                                              DSETD
      CTT=STT**2/(1.+CT)                                    DSETD
      DO 10 J=1,3                                          DSETD
        S(1)= -TH(3)*D(2,J)+TH(2)*D(3,J)                  DSETD
        S(2)= TH(3)*D(1,J)-TH(1)*D(3,J)                    DSETD
        S(3)= -TH(2)*D(1,J)+TH(1)*D(2,J)                    DSETD
        DTT=(TH(1)*D(1,J)+TH(2)*D(2,J)+TH(3)*D(3,J))*CTT DSETD
        DO 5 K=1,3                                         DSETD
          5 D(K,J)=D(K,J)*CT-STT*S(K)+TH(K)*DTT           DSETD
      10 CONTINUE                                           DSETD
C                                                         DSETD
C   RENORMALIZATION OF DIRECTION COSINE MATRIX             DSETD
C   BY AVERAGING MATRIX AND TRANSPOSE OF ITS INVERSE.     DSETD
C                                                         DSETD
      DO 23 ITER=1,10                                       DSETD
      CALL CFACTT(D,TEMP,DET)                               DSETD
      DO 22 I=1,3                                           DSETD
      DO 22 J=1,3                                           DSETD
        D(I,J) = 0.5*(D(I,J)+TEMP(J,I)/DET)                DSETD
      22 IF (DABS(D(I,J)).LT.EPS(15)) D(I,J)=0.0           DSETD
        IF (DABS(DET-1.0).LT.EPS(6)) GO TO 24              DSETD
      23 CONTINUE                                           DSETD
      WRITE (6,27) DET                                       DSETD
      27 FORMAT('O DSETD RENORMALIZATION DID NOT CONVERGE, DET =',1PD25.15)DSETD
      24 RETURN                                             DSETD
      END                                                    DSETD

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SUBROUTINE DSETQ(E,TH,ES,EC,D)                                DSETQ
C                                                                REV IV 07/23/86TWOPI
C COMPUTES NEW DIRECTION MATRIX (D), GIVEN ORIGINAL MATRIX (E) DSETQ
C AND INCREMENTAL MOTION EXPRESSED IN QUATERNION FORM. DSETQ
C DSETQ
C ARGUMENTS: DSETQ
C DSETQ
C E : ORIGINAL DIRECTION COSINE MATRIX. DSETQ
C TH : COMPONENTS OF Q ( UX SIN A/2, UY SIN A/2, UZ SIN A/2) DSETQ
C ES : SIN**2(A/2) DSETQ
C EC : COS (A/2) DSETQ
C D : NEW DIRECTION COSINE MATRIX. DSETQ
C DSETQ
C IMPLICIT REAL*8(A-H,O-Z) DSETQ
C DIMENSION D(3,3),TH(3),S(3),TEMP(3,3),E(3,3) DSETQ
C COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24), DSETQ
C * UNITL,UNITM,UNITT,GRAVITY(3),TWOPI TWOPI
C CT = 1.0 - 2.0*ES DSETQ
C DO 10 J=1,3 DSETQ
C S(1) = TH(2)*E(3,J) - TH(3)*E(2,J) DSETQ
C S(2) = TH(3)*E(1,J) - TH(1)*E(3,J) DSETQ
C S(3) = TH(1)*E(2,J) - TH(2)*E(1,J) DSETQ
C DTT = TH(1)*E(1,J) + TH(2)*E(2,J) + TH(3)*E(3,J) DSETQ
C DO 5 K=1,3 DSETQ
C 5 D(K,J) = E(K,J)*CT + 2.0*(TH(K)*DTT - EC*S(K)) DSETQ
C 10 CONTINUE DSETQ
C DSETQ
C RENORMALIZATION OF DIRECTION COSINE MATRIX DSETQ
C BY AVERAGING MATRIX AND TRANSPOSE OF ITS INVERSE. DSETQ
C DSETQ
C DO 23 ITER=1,10 DSETQ
C CALL CFACTT(D,TEMP,DET) DSETQ
C DO 22 I=1,3 DSETQ
C DO 22 J=1,3 DSETQ
C D(I,J) = 0.5*(D(I,J)+TEMP(J,I)/DET) DSETQ
C 22 IF (DABS(D(I,J)).LT.EPS(15)) D(I,J)=0.0 DSETQ
C IF (DABS(DET-1.0).LT.EPS(6)) GO TO 24 DSETQ
C 23 CONTINUE DSETQ
C WRITE (6,27) DET DSETQ
C 27 FORMAT('0 DSETQ RENORMALIZATION DID NOT CONVERGE, DET =',1PD25.15) DSETQ
C 24 RETURN DSETQ
C END DSETQ

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	SUBROUTINE DSMSOL (A, KK, LL)		DSMSOL
C		REV 03	07/08/74 DSMSOL
C	SOLVES A SET OF SIMULTANEOUS LINEAR EQUATIONS AX=B.		DSMSOL
C			DSMSOL
C	ARGUMENTS:		DSMSOL
C	A: 2-DIMENSIONAL(KK, KK+1) MATRIX OF COEFFICIENTS.		DSMSOL
C	KK: NUMBER OF EQUATIONS AND UNKNOWN.		DSMSOL
C	LL: 1ST DIMENSION OF A IN CALLING PROGRAM.		DSMSOL
C			DSMSOL
C	CALLING PROGRAM SETUP:		DSMSOL
C	A(I, J) FOR I, J=1, KK		DSMSOL
C	A(I, KK+1) = B(I) FOR I=1, KK		DSMSOL
C	THE SOLUTION X IS RETURNED IN COLUMN KK+1 OF A.		DSMSOL
C	MATRIX A IS DESTROYED BY SUBROUTINE.		DSMSOL
C			DSMSOL
	IMPLICIT REAL*8(A-H, O-Z)		DSMSOL
	DIMENSION A(LL, 1)		DSMSOL
	N = KK		DSMSOL
	N1 = N+1		DSMSOL
	DO 50 L=1, N		DSMSOL
	L1 = L+1		DSMSOL
	BIG = 0.0		DSMSOL
	DO 25 I=L, N		DSMSOL
	IF (DABS(A(I, L)).LE.DABS(BIG)) GO TO 25		DSMSOL
	K = I		DSMSOL
	BIG = A(I, L)		DSMSOL
25	CONTINUE		DSMSOL
	IF (BIG.NE.0.0) GO TO 30		DSMSOL
	WRITE (6, 26)		DSMSOL
26	FORMAT('O DSMSOL MATRIX SINGULAR, PROGRAM TERMINATED.')		DSMSOL
	STOP 41		DSMSOL
30	BIG = 1.0/BIG		DSMSOL
	DO 40 J=L, N1		DSMSOL
	B = A(K, J)		DSMSOL
	A(K, J) = A(L, J)		DSMSOL
40	A(L, J) = B*BIG		DSMSOL
	IF (L.EQ.N) GO TO 50		DSMSOL
	DO 48 I=L1, N		DSMSOL
	IF (A(I, L).EQ.0.0) GO TO 48		DSMSOL
	DO 45 J=L1, N1		DSMSOL
45	A(I, J) = A(I, J)-A(I, L)*A(L, J)		DSMSOL
48	CONTINUE		DSMSOL
50	CONTINUE		DSMSOL
	IF (N.EQ.1) GO TO 71		DSMSOL
	N2 = N-1		DSMSOL
	DO 60 L=1, N2		DSMSOL
	I = N-L		DSMSOL
	L1 = I+1		DSMSOL
	DO 60 J=L1, N		DSMSOL
60	A(I, N1) = A(I, N1)-A(I, J)*A(J, N1)		DSMSOL
71	CONTINUE		DSMSOL
	RETURN		DSMSOL

END

DSMSOL

	' SUBROUTINE DZP(N,X,GG,E,R,M)		DZP
		REV IV	07/23/86TWOPI
C	COMPUTES THE STATE VARIABLES (X) FROM THE PARAMETRIC FORM ASSUMED		DZP
C	IN THE INTEGRATION ROUTINE DINT. ALSO EVALUATES THE EXPONENTIAL		DZP
C	WEIGHTS (E) IF M IS NOT ZERO.		DZP
C			DZP
	IMPLICIT REAL*8 (A-H,O-Z)		DZP
	DIMENSION X(1),GG(5,1),E(3,1)		DZP
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),		DZP
	* UNITL,UNITM,UNITT,GRAVITY(3),TWOPI		TWOPI
C			DZP
	CALL ELTIME(1,5)		DZP
	IF(M.NE.0) GO TO 10		DZP
C			DZP
C	COMPUTE STATE VARIABLES ONLY.		DZP
C			DZP
	DO 5 I=1,N		DZP
5	X(I) = GG(1,I) + R*(GG(2,I)*E(1,I)		DZP
	+ R*(GG(3,I)*E(2,I)		DZP
	+ R*(GG(4,I)*E(3,I) )))		DZP
	GO TO 90		DZP
C			DZP
C	COMPUTE EXPONENTIAL WEIGHTS AND STATE VARIABLES.		DZP
C			DZP
10	DO 50 I=1,N		DZP
	E(1,I) = 1.0		DZP
	E(2,I) = 0.5		DZP
	E(3,I) = THIRD		DZP
	IF (GG(5,I).EQ.0.0) GO TO 50		DZP
	Z = R*GG(5,I)		DZP
	W = 0.		DZP
	IF (DABS(Z).GT.0.004) GO TO 20		DZP
	W = 4.		DZP
	A = E(3,I)		DZP
	E(3,I) = 0.		DZP
15	E(3,I) = E(3,I)+A		DZP
	A = A*Z/W		DZP
	W = W+1.0		DZP
	IF(E(3,I)+A.NE.E(3,I)) GO TO 15		DZP
	E(2,I) = 0.5+0.5*Z*E(3,I)		DZP
	E(1,I) = 1.+Z*E(2,I)		DZP
	GO TO 50		DZP
20	IF(Z.GT.-40.) W = DEXP(Z)		DZP
	E(1,I) = (W-1.)/Z		DZP
	E(2,I) = (E(1,I)-1.)/Z		DZP
	E(3,I) = (2.*E(2,I)-1.)/Z		DZP
50	X(I) = GG(1,I) + R*(GG(2,I)*E(1,I)		DZP
	+ R*(GG(3,I)*E(2,I)		JZP
	+ R*(GG(4,I)*E(3,I) )))		DZP
C			DZP
	90 CALL ELTIME(2,5)		DZP
	RETURN		DZP

END

DZP

```

C      SUBROUTINE EDEPTH (A,B,XM,T,Y,XA,XB,XL,XU)                                EDEPTH
C                                                                                   REV IV 07/23/86TWOPI
C      DETERMINES XA AND XB, THE POINTS OF MAXIMUM PENETRATION OF TWO            EDEPTH
C      INTERSECTING ELLIPSOIDS A AND B.                                         EDEPTH
C      ARGUMENTS A,B,XM,T AND X SAME AS FOR SUBROUTINE INTERS.                 EDEPTH
C      ARGUMENTS XL AND XU, IF NONZERO, ARE FINAL RESULTS OF LAST CALL.          EDEPTH
C                                                                                   EDEPTH
C      IMPLICIT REAL*8 (A-H,O-Z)                                                EDEPTH
C      DIMENSION A(3,3),B(3,3),XM(3),Y(3),XA(3),XB(3)                          EDEPTH
C      COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,                  EDEPTH
C      *      NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG                   PAGE
C      COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),                               EDEPTH
C      *      UNITL,UNITM,UNITT,GRAVITY(3),TWOPI                               TWOPI
C      DIMENSION C1(3,4),C2(3,4),C3(3,4),XBM(3),PXBL(3),PXAU(3),AB(3,3)         EDEPTH
C      DIMENSION AXA(3),BXXBM(3),PXAL(?),PXB(3)                                EDEPTH
C      EQUIVALENCE (XBM(1),C1(1,4)), (PXBL(1),C2(1,4)), (PXAU(1),C3(1,4))      EDEPTH
C                                                                                   EDEPTH
C                                                                                   INITIAL GUESSES
C                                                                                   EDEPTH
C      XA = Y/T                                                                  EDEPTH
C      XB = M+(Y-M)/T                                                            EDEPTH
C      L = -!XB-XA!/!AXA!                                                        EDEPTH
C      U = -!XB-XA!/!B(XB-M)!                                                    EDEPTH
C                                                                                   EDEPTH
C      D1 = 0.0                                                                  EDEPTH
C      D2 = 0.0                                                                  EDEPTH
C      DO 9 I=1,3                                                                EDEPTH
C      XA(I) = Y(I)/T                                                            EDEPTH
C      XBM(I) = (Y(I)-XM(I))/T                                                    EDEPTH
C      XB(I) = XBM(I)+XM(I)                                                       EDEPTH
C 9 D1 = D1+(XB(I)-XA(I))**2                                                      EDEPTH
C      IF (DABS(T-1.0).LE.EPS(6)) GO TO 31                                       EDEPTH
C      ITER = 0                                                                    EDEPTH
C      CALL MAT33 (A,B,AB)                                                        EDEPTH
C      IF (XL.NE.0.0) GO TO 11                                                    EDEPTH
C      IF (XU.NE.0.0) GO TO 11                                                    EDEPTH
C      D3 = 0.0                                                                    EDEPTH
C      DO 10 I=1,3                                                                EDEPTH
C      AXA(I) = A(I,1)*XA(1)                                                      EDEPTH
C      *      + A(I,2)*XA(2)                                                      EDEPTH
C      *      + A(I,3)*XA(3)                                                      EDEPTH
C      D2 = D2 + AXA(I)**2                                                         EDEPTH
C      BXXBM(I) = B(I,1)*XBM(1)                                                    EDEPTH
C      *      + B(I,2)*XBM(2)                                                      EDEPTH
C      *      + B(I,3)*XBM(3)                                                      EDEPTH
C 10 D3 = D3+BXXBM(I)**2                                                           EDEPTH
C      XL = -DSQRT(D1/D2)                                                          EDEPTH
C      XU = -DSQRT(D1/D3)                                                          EDEPTH
C                                                                                   EDEPTH
C                                                                                   START OF ITERATION
C                                                                                   EDEPTH
C      11 ITER = ITER+1                                                            EDEPTH
C      IF (NPRT(17).NE.0) WRITE (6,12) ITER,XL,XU,XA,XB                        EDEPTH

```



12	FORMAT(' EDEPTH ITER',I6,8G14.6)	EDEPTH
	IF (ITER.LE.50) GO TO 14	EDEPTH
	WRITE (6,13)	EDEPTH
13	FORMAT(' EDEPTH ITERATION DID NOT CONVERGE')	EDEPTH
	GO TO 31	EDEPTH
C		EDEPTH
C		EDEPTH
C	FORM MATRICES	EDEPTH
C	C1 = LUAB + LA + UB	EDEPTH
C	C2 = C1	EDEPTH
C	C3 = C1'	EDEPTH
C		EDEPTH
14	XLAU = XU*XL	EDEPTH
	DO 22 I=1,3	EDEPTH
	XBM(I) = 0.0	EDEPTH
	DO 22 J=1,3	EDEPTH
	C1(I,J) = XLAU*AB(I,J) + XL*A(I,J) + XU*B(I,J)	EDEPTH
	C2(I,J) = C1(I,J)	EDEPTH
	C3(J,I) = C1(I,J)	EDEPTH
22	XBM(I) = XBM(I) - XL*A(I,J)*XM(J)	EDEPTH
C		EDEPTH
C		EDEPTH
C	SOLVE FOR (XB-M)	EDEPTH
C	C1(XB-M) = -LAM	EDEPTH
C		EDEPTH
	CALL DSMSOL(C1,3,3)	EDEPTH
C		EDEPTH
C		EDEPTH
C	EVALUATE	EDEPTH
C	XB = (XB-M)+M	EDEPTH
C	B(XB-M)	EDEPTH
C	AXA	EDEPTH
C	C13 = (1-XA'AXA)/2	EDEPTH
C	C23 = (1-(XB-M)'B(XB-M))/2	EDEPTH
C		EDEPTH
	C13 = 0.0	EDEPTH
	C23 = 0.0	EDEPTH
	DO 23 I=1,3	EDEPTH
	XB(I) = XBM(I)+XM(I)	EDEPTH
	BXBM(I) = B(I,1)*XBM(1)	EDEPTH
	* + B(I,2)*XBM(2)	EDEPTH
	* + B(I,3)*XBM(3)	EDEPTH
23	XA(I) = XB(I) + XU*BXBM(I)	EDEPTH
	DO 24 I=1,3	EDEPTH
	AXA(I) = A(I,1)*XA(1)	EDEPTH
	* + A(I,2)*XA(2)	EDEPTH
	* + A(I,3)*XA(3)	EDEPTH
	C13 = C13 + XA(I)*AXA(I)	EDEPTH
	C23 = C23 + XBM(I)*BXBM(I)	EDEPTH
24	PXBL(I) = -AXA(I)	EDEPTH
	C13 = (1.0-C13)/2.0	EDEPTH
	C23 = (1.0-C23)/2.0	EDEPTH
C		EDEPTH
C	* DXB	EDEPTH
C	SOLVE FOR ---	EDEPTH
C	* DL	EDEPTH

C			EDEPTH
C		* DXB	EDEPTH
C		C2--- = -AXA	EDEPTH
C		* DL	EDEPTH
C	CALL DSMSOL(C2,3,3)		EDEPTH
C			EDEPTH
C		CALCULATE	EDEPTH
C		DXA DXB DXB	EDEPTH
C		--- = --- + UB---	EDEPTH
C		DL DL DL	EDEPTH
C			EDEPTH
C		* DXA	EDEPTH
C		C11 = XA'A---	EDEPTH
C		* DL	EDEPTH
C			EDEPTH
C		* EXB	EDEPTH
C		C21 = (XB-M)'B---	EDEPTH
C		* DL	EDEPTH
C			EDEPTH
C	C11 = 0.0		EDEPTH
C	C21 = 0.0		EDEPTH
C	DO 25 I=1,3		EDEPTH
C	PXAL(I) = B(I,1)*PXBL(1)		EDEPTH
C	* + B(I,2)*PXBL(2)		EDEPTH
C	* + B(I,3)*PXBL(3)		EDEPTH
C	PXAL(I) = PXBL(I) + XU*PXAL(I)		EDEPTH
C	C11 = C11 + AXA(I)*PXAL(I)		EDEPTH
C	C21 = C21 + BXBM(I)*PXBL(I)		EDEPTH
C	25 PXAU(I) = -BXBM(I)		EDEPTH
C			EDEPTH
C		* DXA	EDEPTH
C		SOLVE FOR ---	EDEPTH
C		* DU	EDEPTH
C			EDEPTH
C		* DXA	EDEPTH
C		C3--- = -B(XB-M)	EDEPTH
C		* DU	EDEPTH
C	CALL DSMSOL(C3,3,3)		EDEPTH
C			EDEPTH
C		CALCULATE	EDEPTH
C		DXB DXA DXA	EDEPTH
C		--- = --- + LA---	EDEPTH
C		DU DU DU	EDEPTH
C			EDEPTH
C		* DXA	EDEPTH
C		C12 = XA'A---	EDEPTH
C		* DU	EDEPTH
C			EDEPTH
C		* DXB	EDEPTH
C		C22 = (XB-M)'B---	EDEPTH

C		*	DU	EDEPTH
C				EDEPTH
	C12 = 0.0			EDEPTH
	C22 = 0.0			EDEPTH
	DO 26 I=1,3			EDEPTH
	PXBU(I) = PXAU(I) + XL*(A(I,1)*PXAU(1)			EDEPTH
	* + A(I,2)*PXAU(2) + A(I,3)*PXAU(3) )			EDEPTH
	C12 = C12 + AXA(I)*PXAU(I)			EDEPTH
	26 C22 = C22 + BXBM(I)*PXBU(I)			EDEPTH
C				EDEPTH
C		SOLVE FOR DL AND DU		EDEPTH
C		C11*DL + C12*DU = C13		EDEPTH
C		C21*DL + C22*DU = C23		EDEPTH
C				EDEPTH
	DET = C11*C22-C12*C21			EDEPTH
	DL = (C13*C22-C12*C23)/DET			EDEPTH
	DU = (C11*C23-C13*C21)/DET			EDEPTH
C				EDEPTH
C		INCREMENT L AND U		EDEPTH
C		TEST FOR CONVERGENCE		EDEPTH
C				EDEPTH
	XL = XL + DL			EDEPTH
	XU = XU + DU			EDEPTH
	IF (DABS(DL/XL).GT.EPS(12)) GO TO 11			EDEPTH
	IF (DABS(DU/XU).GT.EPS(12)) GO TO 11			EDEPTH
	31 CONTINUE			EDEPTH
	RETURN			EDEPTH
	END			EDEPTH

	DOUBLE PRECISION FUNCTION EFUNCT (TH,THD,SPR,JSTOP)	EFUNCT
C	REV 20	04/29/80EFUNCT
C	COMPUTES NONLINEAR SRRING TORQUE FOR EULER JOINTS.	EFUNCT
C		EFUNCT
C	ARGUMENTS:	EFUNCT
C	TH - THETA IS THE ANGLE OF THE EULER AXIS	EFUNCT
C	THD - THETA DOT	EFUNCT
C	SPR - ARRAY OF 5 VALUES DESCRIBING FUNCTION EVALUATION	EFUNCT
C	JSTOP - INDICATOR TO BE SET TO ONE IF IN STOP	EFUNCT
C		EFUNCT
	IMPLICIT REAL*8(A-H,O-Z)	EFUNCT
	DIMENSION SPR(5)	EFUNCT
	JSTOP = 0	EFUNCT
	EFUNCT = TH*SPR(1)	EFUNCT
	TEN = 10.0	EFUNCT
	Q = DSIGN(TEN*THD,TH*THD)	EFUNCT
	IF (Q.GT.1.0) Q = 1.0	EFUNCT
	IF (Q.LT.-1.0) Q = -1.0	EFUNCT
	X = 0.5*(1.0+SPR(4)+Q*(1.0-SPR(4)))	EFUNCT
	IF (SPR(5).GT.0.0) GO TO 10	EFUNCT
	EFUNCT = X*EFUNCT	EFUNCT
	GO TO 99	EFUNCT
10	IF (DABS(TH).LT.SPR(5)) GO TO 99	EFUNCT
	JSTOP = 1	EFUNCT
	Z = DABS(TH) - SPR(5)	EFUNCT
	EFUNCT = EFUNCT + DSIGN(X*(SPR(2)+Z*SPR(3))*Z**2,TH)	EFUNCT
99	RETURN	EFUNCT
	END	EFUNCT

```

SUBROUTINE EJOINT(IJ,NK)
C
C COMPUTES THE TORQUES ACTING ON AN EULER JOINT
C AND ADDS THEM TO THE U2 ARRAY.
C
C ARGUMENTS:
C     NK = 0 - REGULAR COMPUTATION FOR ALL EULER JOINTS
C     # 0 - COMPUTE ONLY FOR JOINT NJ IMPULSE
C
C     IJ = 1 IMPULSE ON PRECESSION AXIS ONLY
C     = 2 IMPULSE ON NUTATION AXIS ONLY
C     = 3 IMPULSE ON SPIN AXIS ONLY
C     = 4 IMPULSE ON GLOBALGRAPHIC AXIS
C     NK = 0, IJ # 0, SPECIAL COMPUTATIONS OF HIR AND HB ONLY
C
C IMPLICIT REAL*8(A-H,O-Z)
COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,
* NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG
COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),
* SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)
COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),
* RPH1(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),
* JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)
COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),
* F(3,30),TQ(3,30),WJ(30),A11(3,3,30)
COMMON/CEULER/ IEULER(30),HIR(3,3,90),ANG(3,30),ANGD(3,30),
* FE(3,30),TQE(3,30),CONST(5,30)
COMMON/FORCES/PSF(7,70),BSF(4,20),SSF(10,40),BAGSF(3,20),
* PRJNT(7,30),NPANEL(5),NPSF,NBSF,NSSF,NBGSF
COMMON/TEMPVI/ CREST,TTI(3),R1I(3),R2I(3),JSTOP(4,2,30)
COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),
* UNITL,UNITM,UNITT,GRAVITY(3),TWOPI
COMMON/TEMPVS/ DH1(3,3),DH4(3,3),TH(3,3),HIM(3,3),HIJ(3,3),
* HDT(3,3),H2(3,3),SH(3),TM(3),TJ(3),WMJ(3),AD(3),
* CV(3),CS(3),ANGL(3),HD3(3),CC(3),T9(3),LSKIP(3)
* ,IDMMY,DMMY(35015)
LOGICAL LSKIP
IF (NJNT.LE.0) GO TO 99
CALL ELTIME(1,31)
J1 = 1
J2 = NJNT
NJ = NK
IF (NJ.EQ.0) GO TO 11
J1 = NJ
J2 = NJ
IF(IJ.LT.0) NJ = 0
11 DO 98 J=J1,J2
IF (IABS(IPIN(J)).NE.4) GO TO 98
M = IABS(JNT(J))
CALL DOT33(D(1.1,M),HT(1,1,2*J-1),DH1)
CALL DOT33(D(1.1,J+1),HT(1,1,2*J),DH4)
CALL DOT33(DH4,DH1,TH)

```

DO 12 I=1,3	EJOINT
12 ANG(I,J) = ANG(I,J) + CONST(I,J)	EJOINT
IC = IEULER(J)	EJOINT
CALL EULRAD (TH,ANG(1,J),IC)	EJOINT
CALL ROT(H2,3,-ANG(1,J))	EJOINT
DO 13 I=1,3	EJOINT
ANG(I,J) = ANG(I,J) - CONST(I,J)	EJOINT
HIR(I,1,J) = DH1(I,3)	EJOINT
HIR(I,3,J) = DH4(I,3)	EJOINT
HIM(I,1) = HT(I,3,2*J-1)	EJOINT
HIJ(I,3) = HT(I,3,2*J)	EJOINT
LSKIP(I) = .FALSE.	EJOINT
FE(I,J) = 0.0	EJOINT
CV(I) = 0.0	EJOINT
CS(I) = 0.0	EJOINT
V2(I,J) = 0.0	EJOINT
TQE(I,J) = 0.0	EJOINT
13 TQ(I,J) = 0.0	EJOINT
WJ(J) = 0.0	EJOINT
TQC = 0.0	EJOINT
IF (IJ.EQ.4) GO TO 55	EJOINT
CALL MAT31 (HT(1,1,2*J-1),H2(1,1),HIM(1,2))	EJOINT
CALL MAT31 (HT(1,1,2*J-1),H2(1,2),HIM(1,3))	EJOINT
CALL DOT31 (D(1,1,M),HIM(1,2),H2(1,2))	EJOINT
CALL DOT31 (D(1,1,M),HIM(1,3),H2(1,3))	EJOINT
CALL CROSS (H2(1,2),HIR(1,3,J),H2(1,1))	EJOINT
CALL DOT31 (D(1,1,M ),WMEG(1,M ),TM)	EJOINT
CALL DOT31 (D(1,1,J+1),WMEG(1,J+1),TJ)	EJOINT
SWJ = 0.0	EJOINT
DO 14 I=1,3	EJOINT
HIR(I,2,J) = H2(I,2)	EJOINT
WMJ(I) = TJ(I) - TM(I)	EJOINT
14 SWJ = SWJ + WMJ(I)**2	EJOINT
WJ(J) = DSQRT(SWJ)	EJOINT
CALL DOT31 (HIR(1,1,J),WMJ,AD)	EJOINT
CALL CROSS (TM,HIR(1,1,J),HDT(1,1))	EJOINT
CALL CROSS (TM,HIR(1,2,J),HDT(1,2))	EJOINT
CALL CROSS (TJ,HIR(1,3,J),HDT(1,3))	EJOINT
CALL MAT31 (D(1,1,J+1),HIR(1,1,J),HIJ(1,1))	EJOINT
CALL MAT31 (D(1,1,J+1),HIR(1,2,J),HIJ(1,2))	EJOINT
CALL MAT31 (D(1,1,M ),HIR(1,3,J),HIM(1,3))	EJOINT
N = IEULER(J)	EJOINT
DO 15 I=1,3	EJOINT
SH(I) = AD(I)	JDRIFT
DO 15 K=1,3	JDRIFT
HIR(I,K,2*J+29) = HIM(I,K)	JDRIFT
15 HIR(I,K,2*J+30) = HIJ(I,K)	JDRIFT
IF (N.EQ.8) GO TO 19	EJOINT
IF (N.GT.3) GO TO 16	EJOINT
SH(N) = 0.0	EJOINT
GO TO 18	EJOINT
16 DO 17 I=1,3	EJOINT

17 IF (I.NE.N-3) SH(I) = 0.0	EJOINT
18 IF (N.NE.2) GO TO 21	EJOINT
19 HX = H2(1,1)*HIR(1,1,J) + H2(2,1)*HIR(2,1,J) + H2(3,1)*HIR(3,1,J)	EJOINT
IF (DABS(HX).GE.EPS(6)) GO TO 20	EJOINT
SH(1) = ANG(1,J) *	EJOINT
SH(3) = ANG(3,J)	EJOINT
GO TO 21	EJOINT
20 CALL DOT31 (H2,WMJ,SH)	EJOINT
SH(1) = SH(1)/HX	EJOINT
IF (N.EQ.2) SH(2) = 0.0	EJOINT
SH(3) = SH(3)/HX	EJOINT
21 DO 22 I=1,3	EJOINT
ANG(I,J) = SH(I)	EJOINT
22 HDT(I,2) = HDT(I,2) + SH(1)*H2(I,3)	EJOINT
IF (NJ.NE.0) N = IJ+3	EJOINT
IF (N.GT.3) GO TO 30	EJOINT
N4 = 4-N	EJOINT
IF (N.EQ.2) AHDT = HDT(1,2)*WMJ(1)+HDT(2,2)*WMJ(2)+HDT(3,2)*WMJ(3)	EJOINT
IF (N.NE.2) AHDT = -(SH(2)*HDT(1,2)+SH(N4)*HDT(1,N4))*H2(1,N)	EJOINT
* -(SH(2)*HDT(2,2)+SH(N4)*HDT(2,N4))*H2(2,N)	EJOINT
* -(SH(2)*HDT(3,2)+SH(N4)*HDT(3,N4))*H2(3,N)	EJOINT
CALL MAT31 (D(1,1,M ),H2(1,N),HB(1,2*J-1))	EJOINT
CALL MAT31 (D(1,1,J+1),H2(1,N),HB(1,2*J ))	EJOINT
DO 25 I=1,3	EJOINT
V2(I,J) = AHDT*H2(I,N)	EJOINT
25 IF (N.EQ.1) LSKIP(I) = .TRUE.	EJOINT
GO TO 42	EJOINT
30 IF (N.GT.6) GO TO 40	EJOINT
K3J = 3*J-2	EJOINT
DO 32 I=1,3	EJOINT
IF (NJ.EQ.0) GO TO 31	EJOINT
IF (I.EQ.N-3) CREST = VISC(7,K3J)	EJOINT
TQE(I,J) = H2(I,N-3)	EJOINT
GO TO 32	EJOINT
31 V2(I,J) = -HDT(I,N-3)*AD(N-3)	EJOINT
HB(I,2*J-1) = HIM(I,N-3)	EJOINT
HB(I,2*J ) = HIJ(I,N-3)	EJOINT
IF (I.NE.N-3) LSKIP(I) = .TRUE.	EJOINT
32 K3J = K3J + 1	EJOINT
IF (NJ) 35,42,35	EJOINT
40 IF (N.EQ.7) GO TO 97	EJOINT
42 IF(IJ.NE.0) GOTO 98	JDRIFT
DO 41 I=1,3	JDRIFT
IF (LSKIP(I)) GO TO 41	EJOINT
K3J = 3*J-3+I	EJOINT
CV(I) = ANG(I,J)*VISCOS(DABS(ANG(I,J)),VISC(1,K3J),HA(I,2*J))	EJOINT
CS(I) = EFUNCT(ANG(I,J),ANG(I,J),SPRING(1,K3J),JSTOP(I,1,J))	EJOINT
FE(I,J) = CS(1) + CV(I) + HA(I,2*J)*HA(I,2*J-1)	EJOINT
41 CONTINUE	EJOINT
CALL MAT31(HIR(1,1,J),FE(1,J),TQE(1,J))	EJOINT
IF(NJ.GT.0) GO TO 34	EJOINT
55 IF (IGLOB(J).EQ.0) GO TO 34	EJOINT

HD3(1) = TH(3,1)	EJOINT
HD3(2) = TH(3,2)	EJOINT
HD3(3) = TH(3,3)	EJOINT
CALL GLOBAL (J,HD3,DH1,TQC,T9,ANGL)	EJOINT
34 CONTINUE	EJOINT
C	EJOINT
C ADD TORQUE CONVERTED TO LOCAL REFERENCE TO U2 ARRAY BY	EJOINT
C U2(M ) = U2(M ) + D(M )*TQ	EJOINT
C U2(J+1) = U2(J+1) - D(J+1)*TQ	EJOINT
C	EJOINT
35 DO 51 I=1,3	EJOINT
TQ(I,J) = TQE(I,J)+TQC*T9(I)	EJOINT
TTI(I) = TQ(I,J)	EJOINT
DO 51 K=1,3	EJOINT
U2(K,M ) = U2(K,M ) + D(K,I,M )*TQ(I,J)	EJOINT
51 U2(K,J+1) = U2(K,J+1) - D(K,I,J+1)*TQ(I,J)	EJOINT
C	EJOINT
C STORE DATA INTO PRJNT ARRAY FOR OUTPUT ROUTINE	EJOINT
C	EJOINT
97 PRJNT(1,J) = IEULER(J)	EJOINT
PRJNT(2,J) = ANG(1,J)	EJOINT
PRJNT(3,J) = ANG(2,J)	EJOINT
PRJNT(4,J) = ANG(3,J)	EJOINT
PRJNT(5,J)=CS(1)**2+CS(3)**2+2.0*CS(1)*CS(3)*TH(3,3)+CS(2)**2	JTF785
PRJNT(6,J)=CV(1)**2+CV(3)**2+2.0*CV(1)*CV(3)*TH(3,3)+CV(2)**2	JTF785
PRJNT(7,J) = TQ(1,J)**2 + TQ(2,J)**2 + TQ(3,J)**2	EJOINT
98 CONTINUE	EJOINT
CALL ELTIME(2,31)	EJOINT
99 RETURN	EJOINT
END	EJOINT



	DOUBLE PRECISION FUNCTION ELONG(A,B,C,D,E)		ELONG
C		REV 01 10/05/72	ELONG
C	COMPUTES ARC LENGTH OF ELLIPSE	$AX^2 + 2BXY + CY^2 = 1$	ELONG
C	FROM THETA=0 (POSITIVE X AXIS) TO THETA=E (RADIAN)		ELONG
C	WHERE D IS NOMINAL INCREMENT OF INTEGRATION.		ELONG
C			ELONG
	IMPLICIT REAL*8(A-H,O-Z)		ELONG
	N=DABS(E/D)		ELONG
	N=N+N		ELONG
	IF(N.EQ.0)N=2		ELONG
	Z=N		ELONG
	T=E/Z		ELONG
	F = DSQRT ((1.+(B/A)**2)/A)		ELONG
	CS=1.		ELONG
	SN=0.		ELONG
	DCS=DCOS(T)		ELONG
	DSN=DSIN(T)		ELONG
	S=F/2.		ELONG
	AC = A+C		ELONG
	BAC = B*B-A*C		ELONG
	DO 10 I=1,N,2		ELONG
	CSS=CS*DCS-SN*DSN		ELONG
	SN=SN*DCS+CS*DSN		ELONG
	CS=CSS		ELONG
	G=(A*CS+B*SN)*CS+(B*CS+C*SN)*SN		ELONG
	G = G**2/(AC + BAC/G)		ELONG
	F=(F+1./(F*G))/2.		ELONG
	S=S+F+F		ELONG
	CSS=CS*DCS-SN*DSN		ELONG
	SN=SN*DCS+CS*DSN		ELONG
	CS=CSS		ELONG
	G=(A*CS+B*SN)*CS+(B*CS+C*SN)*SN		ELONG
	G = G**2/(AC + BAC/G)		ELONG
	F=(F+1./(F*G))/2.		ELONG
	S=S+F		ELONG
10	CONTINUE		ELONG
	ELONG=(S+S-F)*T/3.		ELONG
	RETURN		ELONG
	END		ELONG

	SUBROUTINE ELTIME(L,N)	ELTIME
C		REV III.2 08/08/84REVIII
C	COUNTS THE NUMBER OF TIMES CERTAIN BASIC SUBROUTINES ARE CALLED	ELTIME
C	AND ACCOUNTS FOR ALL COMPUTER CPU TIME USED BY THESE ROUTINES.	ELTIME
C		ELTIME
C	ARGUMENTS L: 1 INDICATES CALL IS AT START OF ROUTINE	ELTIME
C	2 INDICATES CALL IS AT END OF ROUTINE.	ELTIME
C	>2 PAGE NUMBER FOR CALL AT END OF RUN	PAGE
C	N: THE SUBROUTINE IDENTIFICATION NUMBER.	ELTIME
C		ELTIME
C	ASSUMES FUNCTION LTIME(1) IS GIVING ELAPSED CPU TIME IN INTEGER	ELTIME
C	UNITS OF 0.01 SECONDS SINCE FUNCTION LTIME(0) WAS CALLED.	ELTIME
C		ELTIME
	DIMENSION NT(40),MTIN(40),NC(40),IND(40)	ELTIME
	REAL*8 SUB(40)	ELTIME
	DATA SUB/	ELTIME
	* 8H MAIN3D ,8H INPUT ,8H DINT ,8H PRIPLT ,8H DZP ,	ELTIME
	* 8H PDAUX ,8H UPDATE ,8H OUTPUT ,8H DAUX ,8H SETUP1 ,	ELTIME
	* 8H CHAIN ,8H CONTCT ,8H VISPR ,8H DAUX11 ,8H DAUX12 ,	ELTIME
	* 8H DAUX22 ,8H DAUX31 ,8H DAUX32 ,8H DAUX33 ,8H FSMSOL ,	ELTIME
	* 8H PLELP ,8H BELTRT ,8H SEGSEG ,8H AIRBAG ,8H RSTART ,	ELTIME
	* 8H SETUP2 ,8H IMPULS ,3H IMPLS2 ,8H AIRBG3 ,8H DAUX55 ,	ELTIME
	* 8H EJOINT ,8H SPDAMP ,8H DAUX44 ,8H FLXSEG ,8H EQUILB ,	ELTIME
	* 8H POSTPR ,8H WINDY ,8H HBELT ,8H HPTURB ,8H /	ELTIME
	IF (N.GT.1) GO TO 20	ELTIME
	IF (L.GT.1) GO TO 40	ELTIME
C		ELTIME
C	INITIAL CALL AT BEGINNING OF MAIN PROGRAM.	ELTIME
C		ELTIME
C	MTIN(1) = LTIME(0)	80386
	DO 11 I=1,40	ELTIME
	IND(I) = 0	ELTIME
	NC(I) = 0	ELTIME
	MTIN(I) = -1	ELTIME
11	NT(I) = 0	ELTIME
	NSUB = 1	ELTIME
	IND(1) = 1	ELTIME
	NC(1) = 1	ELTIME
	MTIN(1) = 0	ELTIME
	CALL TIMER(ISTART)	80386
	GO TO 99	ELTIME
C		ELTIME
C	CALL AT BEGINNING OF NTH SUBROUTINE.	ELTIME
C		ELTIME
20	IF (L.GT.1) GO TO 30	ELTIME
	CALL TIMER(INOW)	80386
	MTIN(N) = INOW-ISTART	80386
	IF (NC(N).NE.0) GO TO 21	ELTIME
	NSUB = NSUB+1	ELTIME
	IND(NSUB) = N	ELTIME
21	NC(N) = NC(N)+1	ELTIME
	GO TO 99	ELTIME

C		ELTIME
C	CALL AT END OF NTH SUBROUTINE.	ELTIME
C		ELTIME
	30 CALL TIMER(INOW)	80386
	MTOUT = INOW-ISTART	80386
	NDIFF = MTOUT-MTIN(N)	ELTIME
	MTIN(N) = -1	ELTIME
	IF (NDIFF.EQ.0) GO TO 99	80386
	NT(N) = NT(N) + NDIFF	ELTIME
	DO 31 I=1,40	ELTIME
	IF (MTIN(I).NE.-1) MTIN(I) = MTIN(I) + NDIFF	ELTIME
	31 CONTINUE	ELTIME
	GO TO 99	80386
C		ELTIME
C	SUBSEQUENT CALLS FROM MAIN PROGRAM, PRINT SUMMARY TABLE.	ELTIME
C		ELTIME
	40 CALL TIMER(INOW)	80386
	NTSUM = INOW-ISTART	80386
	NT(1) = NTSUM - MTIN(1)	ELTIME
	TIME = FLOAT(NTSUM)/100.0	ELTIME
	WRITE (6,41) TIME,L	PAGE
	41 FORMAT('1 ELAPSED CPU TIME =',F10.2,' SECONDS',85X,'PAGE',I5//	PAGE
	* ' SUB CALLS TIME % '//)	ELTIME
	PCSUM = 0.0	ELTIME
	NTSUM = 0	ELTIME
	DO 42 I=1,NSUB	ELTIME
	J = IND(I)	ELTIME
	PC = FLOAT(NT(J))/TIME	ELTIME
	PCSUM = PCSUM + PC	ELTIME
	NTSUM = NTSUM + NT(J)	ELTIME
	42 WRITE (6,43) SUB(J),NC(J),NT(J),PC	ELTIME
	43 FORMAT(A10,2I10,F10.2)	ELTIME
	WRITE (6,44) NTSUM,PCSUM	ELTIME
	44 FORMAT('0TOTAL',14X,I10,F10.2)	ELTIME
	99 RETURN	ELTIME
	END	ELTIME

	* SUBROUTINE EQUILB (YPR,IYPR)	EQUILB
		REV IV 02/01/88MISDOT
C		EQUILB
C	ADJUSTS INITIAL INPUT POSITION PARAMETERS SUPPLIED ON CARDS G.2	EQUILB
C	AND G.3 SUCH THAT INITIAL NORMAL CONTACT FORCES ARE EQUAL TO	EQUILB
C	EITHER SUPPLIED VALUES OR THOSE COMPUTED BY CONSTRAINT FORCES.	EQUILB
C		EQUILB
	IMPLICIT REAL*8(A-H,O-Z)	EQUILB
	DIMENSION YPR(3,30) , IYPR(4,30)	EQUILB
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,	EQUILB
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),	EQUILB
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)	EQUILB
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),	SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),	EQUILB
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)	EQUILB
	COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),	EQUILB
*	F(3,30),TQ(3,30),WJ(30),A11(3,3,30)	SLIP
	COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24),	EQUILB
*	HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12),	EQUILB
*	RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12),	EQUILB
*	KQ1(12),KQ2(12),KQTYPE(12)	EQUILB
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)	DIMENB
	COMMON/JBARTZ/ MNPL( 30),MNBLT( 8),MNSEG( 30),MNBAG( 6),	EQUILB
*	MPL(3,5,30),MBLT(3,5,8),MSEG(3,5,30),MBAG(3,10,6),	EQUILB
*	NTPL( 5,30),NTBLT( 5,8),NTSEG( 5,30)	EQUILB
	COMMON/CNTRSF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)	EDGE
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),	EQUILB
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI	TWOPI
	COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),	EQUILB
*	BLTTTL(5,8),PLTTL(5,30),BAGTTL(5,6),SEG(30),	EQUILB
*	JOINT(30),CGS(30),JS(30)	EQUILB
	COMMON/FORCES/PSF(7,70),BSF(4,20),SSF(10,40),BAGSF(3,20),	EDGE
*	PRJNT(7,30),NPANEL(5),NPSF,NBSF,NSSF,NBSF	EDGE
	REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTL,BAGTTL,SEG,JOINT	EQUILB
	LOGICAL*1 CGS,JS	EQUILB
	COMMON/TEMPVS/ DMNT(3,3),XMN(3),XMM(3),TM(3),RM(3),DMMY(35092)	80386
	DIMENSION TEMP(3),T(5),FX(10),FX1(10)	EDGE
	DIMENSION X(10),GX(10),DX(10),DXP(10),DPN(5,10)	EQUILB
	DIMENSION JPL(10),JSG(10),JX(10),M1(10),M2(10),M3(10),MT(10)	EQUILB
	DIMENSION NTV(10),N11(10),NSG(10),NAV(10),KSG(5,10)	EQUILB
	DIMENSION ISG(5),IPL(5),LTYPE(5),INDGX(5),NTNQ(5)	EQUILB
	DIMENSION SX(10),SGX(10),XDEV(10),WORD(2)	EQUILB
	DATA BLANK/' '/ , WORD/' SEGLP' , ' YPR'/	EQUILB
	CALL ELTIME (1,35)	EQUILB
C		EQUILB
C	INPUT CARDS G.4, G.5.A-G.5.N, AND G.6.A-G.6.M	EQUILB
C		EQUILB
	READ (5,60) NVAR,NCON	EQUILB
	WRITE (6,51) NVAR,NCON,NPG	PAGE
	NPG=NPG+1	PAGE
51	FORMAT('1',5X,'NVAR =',I3,3X,'NCON =',I3,96X,	PAGE

*	'PAGE',15/120X,'CARD G.4'/)	PAGE
	ICARD = 4	EQUILB
	JCARD = 0	EQUILB
	IF (NVAR.LT.1 .OR. NVAR.GT.10) GO TO 65	EQUILB
	IF (NCON.LT.0 .OR. NCON.GT.5 ) GO TO 65	EQUILB
	WRITE (6,52)	EQUILB
52	FORMAT('0',4X,'J',4X,'NTV',3X,'N11',3X,'NSG',8X,'GX',12X,'XDEV',	EQUILB
	*7X,'JPL',3X,'JSG',3X,'NAV',3X,'KSG(I,J),I=1,NAV',28X,'CARDS G.5'/)	EQUILB
	ICARD = 5	EQUILB
	DO 58 J=1,NVAR	EQUILB
	JCARD = J	EQUILB
	READ (5,53) NTV(J),N11(J),NSG(J),GX(J),XDEV(J),	EQUILB
	* JPL(J),JSG(J),IAV,(KSG(I,J),I=1,IAV)	EQUILB
53	FORMAT(3I4,2F8.0,8I4)	EQUILB
	NAV(J) = IAV	EQUILB
	WRITE (6,54) J,NTV(J),N11(J),NSG(J),GX(J),XDEV(J),	EQUILB
	* JPL(J),JSG(J),IAV,(KSG(I,J),I=1,IAV)	EQUILB
54	FORMAT(4I6,2F15.6,8I6)	EQUILB
	IF (NTV(J).LT.1 .OR. NTV(J).GT.2 ) GO TO 65	EQUILB
	IF (N11(J).LT.1 .OR. N11(J).GT.3 ) GO TO 65	EQUILB
	IF (NSG(J).LT.1 .OR. NSG(J).GT.NSEG) GO TO 65	EQUILB
	IF (NAV(J).LT.0 .OR. NAV(J).GT.5 ) GO TO 65	EQUILB
	IF (JPL(J).LT.1 .OR. JPL(J).GT.NPL ) GO TO 65	EQUILB
	IF (JSG(J).LT.1 .OR. JSG(J).GT.NSEG) GO TO 65	EQUILB
	K = JPL(J)	EQUILB
	NNPL = MNPL(K)	EQUILB
	IF (NNPL.LT.1 .OR. NNPL.GT.5) GO TO 65	EQUILB
	DO 55 I=1,NNPL	EQUILB
	IF (JSG(J).NE.MPL(2,I,K)) GO TO 55	EQUILB
	JSG(J) = I	EQUILB
	GO TO 56	EQUILB
55	CONTINUE	EQUILB
	GO TO 65	EQUILB
56	IF (NAV(J).LE.0) GO TO 58	EQUILB
	DO 57 I=1,IAV	EQUILB
	IF (KSG(I,J).LT.1 .OR. KSG(I,J).GT.NSEG) GO TO 65	EQUILB
57	CONTINUE	EQUILB
58	CONTINUE	EQUILB
	IF (NCON.LE.0) GO TO 17	EQUILB
	WRITE (6,59)	EQUILB
59	FORMAT('0',4X,'I',4X,'IPL',3X,'ISG',2X,'LTYPE',2X,'INDGX',	EQUILB
	* 87X,'CARDS G.6'/)	EQUILB
	ICARD = 6	EQUILB
	DO 64 I=1,NCON	EQUILB
	JCARD = I	EQUILB
	READ (5,60) IPL(I),ISG(I),LTYPE(I),INDGX(I)	EQUILB
	WRITE (6,61) I,IPL(I),ISG(I),LTYPE(I),INDGX(I)	EQUILB
60	FORMAT(4I4)	EQUILB
61	FORMAT(5I6)	EQUILB
	IF ( IPL(I).LT.1 .OR. IPL(I).GT.NPL ) GO TO 65	EQUILB
	IF ( ISG(I).LT.1 .OR. ISG(I).GT.NSEG) GO TO 65	EQUILB
	IF (LTYPE(I).LT.3 .OR. LTYPE(I).GT.4 ) GO TO 65	EQUILB

IF (INDGX(I).LT.0 .OR. INDGX(I).GT.NVAR) GO TO 65	EQUILB
J = IPL(I)	EQUILB
NNPL = MNPL(J)	EQUILB
IF (NNPL.LT.1 .OR. NNPL.GT.5) GO TO 65	EQUILB
DO 62 K=1,NNPL	EQUILB
IF (ISG(I).NE.MPL(2,K,J)) GO TO 62	EQUILB
ISG(I) = K	EQUILB
GO TO 63	EQUILB
62 CONTINUE	EQUILB
GO TO 65	EQUILB
63 IF (INDGX(I).LE.0) GO TO 64	EQUILB
K = INDGX(I)	EQUILB
IF (IPL(I).NE.JPL(K) .OR. ISG(I).NE.JSG(K)) GO TO 65	EQUILB
64 CONTINUE	EQUILB
GO TO 17	EQUILB
C	EQUILB
C INPUT ERROR - PRINT MESSAGE AND TERMINATE PROGRAM.	EQUILB
C	EQUILB
65 WRITE (6,66) ICARD,JCARD	EQUILB
66 FORMAT('0 INPUT ERROR ON CARD G.',I2,'.',I2,	EQUILB
* ' . PROGRAM TERMINATED.')	EQUILB
STOP 26	EQUILB
C	EQUILB
C DATA INITIALIZATION.	EQUILB
C	EQUILB
17 NQORG = NQ	EQUILB
DO 19 K=1,NVAR	EQUILB
J = JPL(K)	EQUILB
I = JSG(K)	EQUILB
M1(K) = MPL(1,I,J)	EQUILB
M2(K) = MPL(2,I,J)	EQUILB
M3(K) = MPL(3,I,J)	EQUILB
MT(K) = NTPL (I,J)	EQUILB
JX(K) = 1	EQUILB
DXP(K) = 0.0	EQUILB
I1 = NI1(K)	EQUILB
I2 = NSG(K)	EQUILB
IF (NTV(K).EQ.1) X(K) = SEGLP(I1,I2)	EQUILB
IF (NTV(K).EQ.2) X(K) = YPR(I1,I2)	EQUILB
SX (K) = X(K)	EQUILB
SGX(K) = GX(K)	EQUILB
IF (NAV(K).LE.0) GO TO 19	EQUILB
IAV = NAV(K)	EQUILB
DO 18 L=1,IAV	EQUILB
J2 = KSG(L,K)	EQUILB
IF (NTV(K).EQ.1) DPN(L,K) = SEGLP(I1,I2) - SEGLP(I1,J2)	EQUILB
18 IF (NTV(K).EQ.2) DPN(L,K) = YPR(I1,I2) - YPR(I1,J2)	EQUILB
19 CONTINUE	EQUILB
IF (NPRT(27).EQ.0) GO TO 20	EQUILB
C	EQUILB
C LET'S SEE WHAT USER INPUT LOOKS LIKE.	EQUILB
C	EQUILB

	CALL OUTPUT(0)	EQUILB
	CALL DAUX(0)	EQUILB
	CALL PRINT(6H USER )	EQUILB
	CALL OUTPUT(1)	EQUILB
C		EQUILB
C	START FDF FORCE -> CONSTRAINT FORCE ITERATION	EQUILB
C		EQUILB
20	PENDOT = 0.0	EQUILB
	DO 50 JITTER=1,10	EQUILB
C		EQUILB
C	ITERATE INPUT (X) SUCH THAT F(X) = G(X)	EQUILB
C		EQUILB
	MVAR = 2	EQUILB
	IF (NVAR.EQ.1) MVAR = 1	EQUILB
	DO 32 M=1,2	EQUILB
	DO 32 I=MVAR,NVAR	EQUILB
	DO 32 J=1,I	EQUILB
	NITER = 10	EQUILB
	IF (DXP(J).EQ.0.0) NITER = 50	EQUILB
	DX(J) = 0.25	EQUILB
	N1 = M1(J)	EQUILB
	N2 = M2(J)	EQUILB
	N3 = M3(J)	EQUILB
	NP = JPL(J)	EQUILB
	NT = MT(J)	EQUILB
	I1 = NI1(J)	EQUILB
	I2 = NSG(J)	EQUILB
	IAV = NAV(J)	EQUILB
	IF (NTV(J).NE.2) GO TO 15	EQUILB
	CALL DRCIJK (D,YPR,IYPR,HT,I2)	EQUILB
	IF (NAV(J).LE.0) GO TO 15	EQUILB
	DO 14 K=1,IAV	EQUILB
	J2 = KSG(K,J)	EQUILB
14	CALL DRCIJK (D,YPR,IYPR,HT,J2)	EQUILB
15	DO 29 ITER=1,NITER	EQUILB
	CALL CHAIN(0)	JDRIFT
	PEN1 = PEN	EQUILB
	NPSF = 1	EDGE
	CALL PLELP(N2,N3,N1,NP,NT)	MISDOT
	PEN = PSF(1,1)	EDGE
	FX1(J) = FX(J)	EQUILB
	FXJ = 0.0	EQUILB
	IF (PEN.GT.0.0) FXJ = PSF(2,1)	EDGE
	IF (PEN.GT.0.0) CALL FRCDFL (PEN,PENDOT,NT,1,FXJ,ELOSS)	EQUILB
	FX(J) = FXJ	EQUILB
	IF (JX(J)-2) 23,21,25	EQUILB
21	IF (FX(J)*FX1(J).GT.0.0) GO TO 22	EQUILB
	IF (FX1(J).EQ.0.0) JX(J) = 1	EQUILB
	FX(J) = FX1(J)	EQUILB
	PEN = PEN1	EQUILB
	DX(J) = 0.5*DX(J)	EQUILB
	X(J) = X(J) - DX(J)	EQUILB

	GO TO 27	EQUILB
22	F2 = FX(J) - GX(J)	EQUILB
	F1 = FX1(J) - GX(J)	EQUILB
	IF (F1*F2.LE.0.0) GO TO 24	EQUILB
	IF (DABS(F2).LT.DABS(F1)) GO TO 23	EQUILB
26	FX(J) = FX1(J)	EQUILB
	DX(J) = -DX(J)	EQUILB
	PEN = PEN1	EQUILB
	X(J) = X(J) + 2.0*DX(J)	EQUILB
	GO TO 27	EQUILB
23	JX(J) = 1	EQUILB
	IF (PEN.GT.0.0) JX(J) = 2	EQUILB
	IF (ITER.GT.1 .AND. PEN.LT.0.0 .AND. PEN.LT.PEN1) GO TO 26	EQUILB
	X(J) = X(J) + DX(J)	EQUILB
	GO TO 27	EQUILB
24	DXP(J) = DX(J)/(FX(J)-FX1(J))	EQUILB
	JX(J) = 3	EQUILB
25	IF (DABS(FX(J)-GX(J)).LT.EPS(6)) GO TO 30	EQUILB
	IF (PEN.LT.0.0) CALL FRCDL (-PEN,PENDOT,NT,1,FXJ,ELOSS)	EQUILB
	IF (PEN.LT.0.0) FX(J) = -FXJ	EQUILB
	X(J) = X(J) - DXP(J)*(FX(J)-GX(J))	EQUILB
27	IF (XDEV(J).LE.0.0) GO TO 42	EQUILB
	IF (DABS(X(J)-SX(J)).LE.XDEV(J)) GO TO 42	EQUILB
	WRITE (6,41) J,X(J),SX(J),XDEV(J)	EQUILB
41	FORMAT('O PROGRAM IS BEING TERMINATED IN SUBROUTINE EQUILB.'//	EQUILB
	* ' ITERATION FOR VARIABLE NO.',I3,' IS NOT CONVERGING.'//	EQUILB
	* ' VALUE OF X IS OUT OF RANGE. VALUES OF X,SX,XDEV ARE'//	EQUILB
	* 3G20.8)	EQUILB
	STOP 27	EQUILB
42	IF (NTV(J).EQ.1) SEGLP(I1,I2) = X(J)	EQUILB
	IF (NTV(J).EQ.2) YPR(I1,I2) = X(J)	EQUILB
	IF (NTV(J).EQ.2) CALL DRCIJK (D,YPR,IYPR,HT,I2)	EQUILB
	IF (NAV(J).LE.0) GO TO 29	EQUILB
	DO 28 K=1,IAV	EQUILB
	J2 = KSG(K,J)	EQUILB
	IF (NTV(J).EQ.1) SEGLP(I1,J2) = X(J) - DPN(K,J)	EQUILB
	IF (NTV(J).EQ.2) YPR(I1,J2) = X(J) - DPN(K,J)	EQUILB
28	IF (NTV(J).EQ.2) CALL DRCIJK (D,YPR,IYPR,HT,J2)	EQUILB
29	CONTINUE	EQUILB
30	IF (NPRT(27).NE.0) WRITE (6,31) M,I,J,ITER,X(J),FX(J)	EQUILB
31	FORMAT(4I3,4X,2F12.6)	EQUILB
32	CONTINUE	EQUILB
	IF (NQ.LE.0) GO TO 40	EQUILB
C		EQUILB
C	COMPUTE VEHICLE COORDINATES FOR FIXED POINT CONSTRAINTS.	EQUILB
C		EQUILB
	DO 35 K=1,NQ	EQUILB
	IF (KQTYPE(K).NE.1) GO TO 35	EQUILB
	IF (KQ2(K).NE.NVEH) GO TO 35	EQUILB
	L = KQ1(K)	EQUILB
	CALL DOT31(D(1,1,L),RK1(1,K),T)	EQUILB
	DO 34 I=1,3	EQUILB



34	T(I) = T(I) + SEGLP(I,L) - SEGLP(I,NVEH)	EQUILB
	CALL MAT31(D(1,1,NVEH),T,RK2(1,K))	EQUILB
35	CONTINUE	EQUILB
40	IF (NPRT(27).EQ.0) GO TO 36	EQUILB
C		EQUILB
C	SOLVE SYSTEM EQUATIONS WITH CONSTRAINTS OFF.	EQUILB
C		EQUILB
	CALL OUTPUT(0)	EQUILB
	CALL DAUX(0)	EQUILB
	CALL PRINT(6HEQUIL2)	EQUILB
	CALL OUTPUT(1)	EQUILB
C		EQUILB
C	SET UP CONSTRAINTS TO PRODUCE ZERO ACCELERATIONS.	EQUILB
C		EQUILB
36	NQ = NQORG	EQUILB
	IF (NCON.LE.0) GO TO 81	EQUILB
	DO 37 I=1,NCON	EQUILB
	NQ = NQ+1	EQUILB
	J = IPL(I)	EQUILB
	K = ISG(I)	EQUILB
	NT = NTPL(K,J)	EQUILB
	NTNQ(I) = NTAB(NT+1)	EQUILB
	NTAB(NT+1) = -NQ	EQUILB
	KQ1(NQ) = MPL(2,K,J)	EQUILB
	KQ2(NQ) = MPL(1,K,J)	EQUILB
37	KQTYPE(NQ) = LTYPE(I)	EQUILB
C		EQUILB
C	SOLVE SYSTEM EQUATIONS WITH CONSTRAINTS ON.	EQUILB
C		EQUILB
	CALL OUTPUT(0)	EQUILB
	CALL DAUX(0)	EQUILB
	IF (NPRT(27).NE.0.AND.JITTER.EQ.1) CALL PRINT(6HEQUIL1)	EQUILB
C		EQUILB
C	FETCH CONSTRAINTS FORCES NORMAL TO PLANE SURFACES.	EQUILB
C	STORE FRICTION FORCE AND TURN OFF CONSTRAINTS.	EQUILB
C		EQUILB
	CONV = 1.0	EQUILB
	DO 39 I=1,NCON	EQUILB
	MQ = NQORG+I	EQUILB
	J = IPL(I)	EQUILB
	K = ISG(I)	EQUILB
	NT = NTPL(K,J)	EQUILB
	NTAB(NT+1) = NTNQ(I)	EQUILB
	M = MPL(2,K,J)	EQUILB
	N = MPL(1,K,J)	EQUILB
	CALL DOT31(D(1,1,N),PL(1,J),TEMP)	EQUILB
	T(I) = TEMP(1)*QQ(1,MQ) + TEMP(2)*QQ(2,MQ) + TEMP(3)*QQ(3,MQ)	EQUILB
	I1 = INDGX(I)	EQUILB
	IF (I1.GT.0 .AND. DABS(GX(I1)+T(I)).GT.EPS(2)) CONV = 0.0	EQUILB
	IF (I1.GT.0) GX(I1) = 0.5*(GX(I1)-T(I))	EQUILB
	DO 38 L=1,3	EQUILB
38	TEMP(L) = QQ(L,MQ) - T(I)*TEMP(L)	EQUILB

```

      LT = NTAB(NT)
39  CALL MAT31(D(1,1,M),TEMP,TAB(LT+19))
      NQ = NQORG
      IF (CONV.EQ.1.0) GO TO 81
50  CONTINUE
C
C      PRINT INPUT AND CHANGES MADE.
C
81  IF (NJNT.LE.0) GO TO 86
      CALL OUTPUT(0)
      CALL DAUX(0)
      IPRINT = 0
      DO 84 J=1,NJNT
      IF (IPIN(J).GE.0) GO TO 84
      IF (VISC(4,3*J-2).GT.0.0) GO TO 84
      IF (IPIN(J).EQ.-1) T1 = DABS(XDY(HB(1,2*J),D(1,1,J+1),TQ(1,J)))
      IF (IPIN(J).LE.-2) T1 = DSQRT(TQ(1,J)**2+TQ(2,J)**2+TQ(3,J)**2)
      VISC(4,3*J-2) = 1.5*T1
      IF (IPRINT.EQ.0) WRITE (6,82)
82  FORMAT('0 THE FOLLOWING VALUES FOR THE MAX TORQUE FOR A LOCKED JOEQUILB
*INT ON CARDS B.5 HAVE BEEN SET UP BY SUBROUTINE EQUILB: '//
      *      ' J SYM LPIN T1=VISC(4)' /)
      IPRJNT = 1
      WRITE (6,83) J,JOINT(J),IPIN(J),VISC(4,3*J-2)
83  FORMAT(I6,1X,A4,I6,F15.6)
84  CONTINUE
86  IF (NQ.LE.0) GO TO 91
      IPRINT = 0
      DO 89 K=1,NQ
      IF (KQTYPE(K).NE.1) GO TO 89
      IF (KQ2(K).NE.NVEH) GO TO 89
      IF (IPRINT.EQ.0) WRITE (6,87)
87  FORMAT('0 THE FOLLOWING VALUES FOR RK2 ON CARDS D.6 FOR FIXED POIEQUILB
*NT CONSTRAINTS HAVE BEEN CHANGED BY SUBROUTINE EQUILB: '//
      *      5X,'K',3X,'KQTYPE',4X,'KQ1',5X,'KQ2',8X,'RK2(X)',
      *      9X,'RK2(Y)',9X,'RK2(Z)') /)
      IPRINT = 1
      WRITE (6,88) K,KQTYPE(K),KQ1(K),KQ2(K),(RK2(I,K),I=1,3)
88  FORMAT(I6,3I8,3F15.6)
89  CONTINUE
91  WRITE (6,92)
92  FORMAT('0 THE FOLLOWING VARIABLES ON CARDS G.2 AND G.3 ',
*      'HAVE BEEN CHANGED BY SUBROUTINE EQUILB: '//)
      DO 95 J=1,NVAR
      IO = NTV(J)
      I1 = NI1(J)
      I2 = NSG(J)
      WRITE (6,93) WORD(IO),I1,I2,SX(J),X(J),BLANK,J,SGX(J),GX(J)
93  FORMAT(4X,A6,'(' ,I2,',',I2,') FROM',F12.6,' TO',F12.6,
*      A4,'AND GX(' ,I2,') FROM',F12.6,' TO',F12.6)
      IF (NAV(J).LE.0) GO TO 95
      IAV = NAV(J)

```

```

      DO 94 I=1,IAV
      J2 = KSG(I,J)
      ZSX = SX(J) - DPN(I,J)
      ZXX = X(J) - DPN(I,J)
94  WRITE (6,93) WORD(I0),I1,J2,ZSX,ZXX
95  CONTINUE
      CALL ELTIME (2,35)
      RETURN
      END

```

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EQUILB
EQUILB
EQUILB
EQUILB
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EQUILB
EQUILB

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SUBROUTINE EULRAD(D,A,IC)                                EULRAD
C                                                         REV IV    07/23/86TWOPI
C COMPUTES EULER ANGLES PRECESSION, NUTATION, AND SPIN IN RADIANS EULRAD
C AND PLACES THEM INTO THE A ARRAY FOR GIVEN DIRECTION COSINE MATRIXEULRAD
C                                                         EULRAD
C ASSUMES  $D = D(S)D(N)D(P)$ , WHERE EULRAD
C                                                         EULRAD
C          CS SS 0           1 0 0           CP SP 0 EULRAD
C D(S)=--SS CS 0 , D(N)= 0 CN SN , D(P)--SP CP 0 EULRAD
C          0 0 1           0 -SN CN           0 0 1 EULRAD
C                                                         EULRAD
C AND P=A(1), N=A(2), S=A(3) EULRAD
C                                                         EULRAD
C ROUTINE WILL ALWAYS WORK IN THE MEMORY MODE, I.E., WILL PRODUCE A EULRAD
C NEW SET OF A'S THAT DIFFER THE LEAST FROM THE INPUTTED A ARRAY. EULRAD
C TO USE IN NON-MEMORY MODE,SET ALL A'S TO ZERO, CALL WITH IC = 8. EULRAD
C                                                         EULRAD
C NEW N IS ALWAYS COMPUTED. EULRAD
C IF N OR PI-N < 10**-6, IC IS USED TO RESOLVE AMBIGUITIES ON P & S, EULRAD
C EXCEPT FOR IC = 2 OR 8 WHERE THEY ARE NOT CHANGED. EULRAD
C                                                         EULRAD
C IMPLICIT REAL*8(A-H,O-Z) EULRAD
C DIMENSION A(3),D(3,3),T(6) EULRAD
C COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24), EULRAD
C * UNITL,UNITM,UNITT,GRAVITY(3),TWOPI TWOPI
C IF (D(3,3).GT. 1.0) D(3,3) = 1.0 EULRAD
C IF (D(3,3).LT. -1.0) D(3,3) = -1.0 EULRAD
C B = DACOS(D(3,3)) EULRAD
C T(2) = B-A(2) EULRAD
C T(5) = -B-A(2) EULRAD
C Z = 0.0 EULRAD
C IF ( B.LT.EPS(6)) Z = 1.0 EULRAD
C IF (PI-B.LT.EPS(6)) Z = -1.0 EULRAD
C IF (Z.NE.0.0) GO TO 11 EULRAD
C T(1) = DATAN2(D(3,1),-D(3,2)) - A(1) EULRAD
C T(4) = T(1) + PI EULRAD
C T(3) = DATAN2(D(1,3), D(2,3)) - A(3) EULRAD
C T(6) = T(3) + PI EULRAD
C GO TO 26 EULRAD
11 T(1) = DATAN2(D(1,2)-Z*D(2,1) , D(1,1)+Z*D(2,2)) - A(1) - Z*A(3) EULRAD
C T(3) = T(1) EULRAD
C GO TO (21,22,23,23,22,21,22,22) , IC EULRAD
C                                                         EULRAD
C SET T(1) = 0 EXCEPT FOR IC=3,4 EULRAD
C SET T(3) = 0 EXCEPT FOR IC=1,6 EULRAD
C                                                         EULRAD
21 T(1) = 0.0 EULRAD
C GO TO 25 EULRAD
22 T(1) = 0.0 EULRAD
23 T(3) = 0.0 EULRAD
25 T(4) = T(1) EULRAD
C T(6) = T(3) EULRAD

```

26	TMAX = 0.0	EULRAD
	J = 3	EULRAD
	DO 30 I=1,6	EULRAD
	T(I) = DMOD(T(I),TWOPI)	EULRAD
	IF (DABS(T(I)).GT.PI ) T(I) = T(I) - DSIGN(TWOPI,T(I))	EULRAD
	IF (DABS(T(I)).LT.TMAX) GO TO 30	EULRAD
	TMAX = DABS(T(I))	EULRAD
	IF (I.GT.3) J = 0	EULRAD
30	CONTINUE	EULRAD
	IF (Z.LT.0.0) T(J+3) = -T(J+3)	EULRAD
	DO 40 I=1,3	EULRAD
	IJ = I+J	EULRAD
40	A(I) = A(I) + T(IJ)	EULRAD
	RETURN	EULRAD
	END	EULRAD

```

C      DOUBLE PRECISION FUNCTION EVALFD (D,N,L)                                EVALFD
C                                                                                   REV IV 07/23/86JTF786
C      EVALUATE FUNCTION THAT IS DEFINED AT LOCATION N OF TAB ARRAY              EVALFD
C      FOR ABSCISSA VALUE D. EVALUATES DERIVATIVE, FUNCTION OR INTEGRAL          EVALFD
C      AS L EQUALS 0, 1, OR 2. TAB ARRAY IS DEFINED AS FOLLOWS:                 EVALFD
C      TAB(N) - DO (NO RESTRICTIONS ON DO)                                       JTF786
C      TAB(N+1) - D1 (F1 DEFINED FOR  $DO < D < |D1|$ )                             JTF786
C      TAB(N+2) - D2 (F2 DEFINED FOR  $|D1| < D < |D2|$ )                             JTF786
C      TAB(N+3) - (NOT CURRENTLY USED)                                           EVALFD
C      TAB(N+4) - (NOT CURRENTLY USED)                                           EVALFD
C      TAB(N+5) - START OF DEFINITION OF 1ST PART OF FUNCTION (F1)              EVALFD
C      WHICH IS FOLLOWED BY DEFINITION OF 2ND PART OF FUNCTION (F2),              EVALFD
C      IF ANY.                                                                    EVALFD
C      2ND PART OF FUNCTION EXISTS IF D2 IS NON-ZERO.                          EVALFD
C      SIGN OF D1 DETERMINES FORM OF DEFINITION FOR 1ST PART OF                 EVALFD
C      THE FUNCTION.                                                             EVALFD
C                                                                                   EVALFD
C      D1 ZERO INDICATES THAT FUNCTION IS CONSTANT D2 FOR ALL D.                EVALFD
C                                                                                   EVALFD
C      D1 POSITIVE INDICATES THAT TAB(N+5)-TAB(N+10) CONTAINS                   EVALFD
C      A0,A1,...A5. THE COEFFICIENTS OF A 5TH ORDER POLYNOMIAL.                 EVALFD
C                                                                                   EVALFD
C      D1 NEGATIVE INDICATES THAT TAB(N+5) CONTAINS NP (REAL)                   EVALFD
C      FOLLOWED BY D(1), F(1), D(2), F(2) ..., D(NP), F(NP)                     EVALFD
C                                                                                   EVALFD
C      WARNING- TABULAR FUNCTION MUST BE DEFINED FOR WHOLE RANGE,              EVALFD
C      THAT IS, FROM DO TO D1 INCLUSIVE, OR D1 TO D2 INCLUSIVE.                 EVALFD
C                                                                                   EVALFD
C      SIMILARLY, THE SIGN OF D2 (IF NON-ZERO) DETERMINES FORM OF              EVALFD
C      DEFINITION OF 2ND PART OF FUNCTION, IF ANY.                             EVALFD
C                                                                                   EVALFD
C      IF D < DO AND D1# 0, DERIVATIVE = 0 OR FUNCTION = F1(DO)                 JTF786
C      IF D > !D1! AND D2=0, DERIVATIVE = 0 OR FUNCTION = F1(|D1|)              JTF786
C      IF D > !D2! AND D2#0, DERIVATIVE = 0 OR FUNCTION = F2(|D2|)              JTF786
C                                                                                   EVALFD
C      NOTE: PREVIOUS VERSIONS ASSUMED THAT DO WAS NON-NEGATIVE AND              JTF786
C      THAT F = 0 FOR D < DO.                                                    JTF786
C                                                                                   JTF786
C      IMPLICIT REAL*8(A-H,O-Z)                                                  EVALFD
C      COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)        EVALFD
C      F = 0.0                                                                    EVALFD
C      IOUTr = 0                                                                    EVALFD
C      DO = TAB(N)                                                                EVALFD
C      D1 = TAB(N+1)                                                              EVALFD
C      D2 = TAB(N+2)                                                              EVALFD
C      IF (D1.NE.0.0) GO TO 26                                                    EVALFD
C      IF (L-1) 40,24,25                                                         JTF786
24 F = D2                                                                    EVALFD
      GO TO 40                                                                    EVALFD
25 F = (D-DO)*D2                                                                EVALFD

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	GO TO 40	EVALFD
C		EVALFD
C	COMPUTE INDEX OF F1 DEFINITION	EVALFD
C		EVALFD
26	NP = N+5	EVALFD
	IF (L.EQ.2) GO TO 41	EVALFD
C		EVALFD
C	DERIVATIVES AND FUNCTIONS HERE, INTEGRALS HAVE OTHER LOGIC	EVALFD
C		EVALFD
	IF (D.GE.D0) GOTO 22	JTF786
C		JTF786
C	D < D0, RETURN F=0 FOR L=0, OR F=F1(D0) FOR L=1.	JTF786
C		JTF786
	IF (L.EQ.0) GOTO 40	JTF786
	X = D0	JTF786
	IF (D1.GT.0.0) GOTO 37	JTF786
	F = TAB(NP+2)	JTF786
	GOTO 40	JTF786
22	IF (D.LT.DABS(D1)) GOTO 31	EVALFD
	IF (D2.NE.0.0) GO TO 32	EVALFD
C		EVALFD
C	D .GE. !D1! , D2 = 0	EVALFD
C		EVALFD
	IF (D1.LE.0.0) GO TO 33	EVALFD
C		EVALFD
C	IOUTR.EQ.1 INDICATES D BEYOND RANGE. DERIVATIVE = 0.	EVALFD
C	IOUTR.EQ.0 INDICATES D.LE. !D1!. COMPUTE POLY DERIVATIVE	EVALFD
C		EVALFD
	IF (D.GT.DABS(D1)) IOUTR = 1	EVALFD
	X = D1	EVALFD
	GO TO 37	EVALFD
C		EVALFD
C	D0 < D < !D1!	EVALFD
C		EVALFD
31	IF (D1.LT.0.0) GO TO 35	EVALFD
	X = D	EVALFD
	GO TO 37	EVALFD
C		EVALFD
C	D .GE. !D1!, D2 NON-ZERO, USE F2	EVALFD
C		EVALFD
32	MP = 6	EVALFD
C		EVALFD
C	COMPUTE INDEX OF F2 DEFINITION	EVALFD
C		EVALFD
	IF (D1.LT.0.0) MP = 2.0 * TAB(NP)+1.0	EVALFD
	NP = NP+MP	EVALFD
	IF (D.LT.DABS(D2)) GO TO 34	EVALFD
	IF (D2.LT.0.0) GO TO 33	EVALFD
C		EVALFD
C	IOUTR.EQ.1 INDICATES D BEYOND RANGE. DERIVATIVE = 0.	EVALFD
C	IOUTR.EQ.0 INDICATES D.LE. !D2!. COMPUTE POLY DERIVATIVE	EVALFD
C		EVALFD

	IF (D.GT.DABS(D2)) IOUTR = 1	EVALFD
C		EVALFD
C	D .GE. D2 (POSITIVE), EVALUATE F2 FOR D2	EVALFD
C		EVALFD
	X = D2	EVALFD
	GO TO 37	EVALFD
C		EVALFD
C	D EXCEEDS TABULAR DEFINITION, SET F = F(NP)	EVALFD
C	IF TABLE DEFINITION EXTENDS BEYOND RANGE, USE TABLE VALUES	EVALFD
C		EVALFD
	33 MB = TAB(NP)	EVALFD
	NB = NP+MB+MB	EVALFD
	IF (D .LE. TAB(NB-1)) GO TO 35	EVALFD
	IF (L.EQ.1) F=TAB(NB)	EVALFD
	GO TO 40	EVALFD
C		EVALFD
C	!D1! .LE. D < !D2!	EVALFD
C		EVALFD
	34 IF (D2.LT.0.0) GO TO 35	EVALFD
	X = D	EVALFD
	GO TO 37	EVALFD
C		EVALFD
C	EVALUATE F FROM TABULAR DEFINITION	EVALFD
C		EVALFD
	35 MB = TAB(NP)	EVALFD
	K1 = NP+3	EVALFD
	K2 = NP+MB+MB	EVALFD
	DO 36 K=K1,K2,2	EVALFD
	IF (D.GT.TAB(K)) GO TO 36	EVALFD
	IF (L-1) 28,27,40	EVALFD
C		EVALFD
C	EVALUATE DERIVATIVE FROM TABLE	EVALFD
C		EVALFD
	28 F = (TAB(K+1)-TAB(K-1))/(TAB(K)-TAB(K-2)) .	EVALFD
	GO TO 40	EVALFD
C		EVALFD
C	EVALUATE FUNCTION FROM TABLE	EVALFD
C		EVALFD
	27 R2 = TAB(K)-TAB(K-2)	EVALFD
	R1 = (D-TAB(K-2))/R2	EVALFD
	R2 = (TAB(K)-D)/R2	EVALFD
	F = R1*TAB(K+1)+R2*TAB(K-1)	EVALFD
	GO TO 40	EVALFD
	36 CONTINUE	EVALFD
	IF (L.EQ.1) F = TAB(K2)	EVALFD
	GO TO 40	EVALFD
	37 IF (IOUTR.EQ.1 .AND. L.EQ.0 ) GO TO 40	EVALFD
	IF (L-1) 38,39,40	EVALFD
C		EVALFD
C	EVALUATE DERIVATIVE OF 5TH DEGREE POLYNOMIAL	EVALFD
C		EVALFD
	38 F = TAB(NP+1)+X*(2.0*TAB(NP+2)+X*(3.0*TAB(NP+3)+X*(4.0*TAB(NP+4)+	EVALFD



	* X*5.0*TAB(NP+5))))	EVALFD
	GO TO 40	EVALFD
C		EVALFD
C	EVALUATE 5TH DEGREE POLYNOMIAL	EVALFD
C		EVALFD
	39 F = TAB(NP) + X*(TAB(NP+1)+X*(TAB(NP+2)	EVALFD
	* +X*(TAB(NP+3)+X*(TAB(NP+4)+X*TAB(NP+5))))	EVALFD
	GO TO 40	EVALFD
C		EVALFD
C	L-2: COMPUTE INTEGRAL OF FUNCTION FROM D0 TO T.	EVALFD
C		EVALFD
	41 IF (D.EQ.D0) GO TO 40	EVALFD
	X0 = D0	EVALFD
	X1 = D1	EVALFD
	DO 50 I=1,2	EVALFD
	IF (X1) 43,49,42	EVALFD
	42 A0 = TAB(NP)	EVALFD
	A1 = TAB(NP+1)/2.0	EVALFD
	A2 = TAB(NP+2)/3.0	EVALFD
	A3 = TAB(NP+3)/4.0	EVALFD
	A4 = TAB(NP+4)/5.0	EVALFD
	A5 = TAB(NP+5)/6.0	EVALFD
	NP = NP+6	EVALFD
	X = X0	EVALFD
	IF (X.NE.0.0) F=F-X*(A0+X*(A1+X*(A2+X*(A3+X*(A4+X*A5))))	EVALFD
	X = DMIN1(D,X1)	EVALFD
	IF (X.NE.0.0) F=F+X*(A0+X*(A1+X*(A2+X*(A3+X*(A4+X*A5))))	EVALFD
	IF(D.LE.X1) GO TO 40	EVALFD
	IF(I.EQ.1.AND.D2.NE.0.0) GO TO 49	EVALFD
C		EVALFD
C	NOTE - NP WAS UPDATED NP=NP+6 BEFORE THIS, READY FOR SECOND PASS	EVALFD
C		EVALFD
	F = F + (D-X1)*(TAB(NP-6)+X1*(TAB(NP-5)+X1*(TAB(NP-4)	EVALFD
	* +X1*(TAB(NP-3)+X1*(TAB(NP-2)+X1*TAB(NP-1))))	EVALFD
	GO TO 40	EVALFD
	43 MB = TAB(NP)	EVALFD
	K1 = NP+3	EVALFD
	K2 = NP+MB+MB	EVALFD
	NP = K2+1	EVALFD
	DL = DMIN1(D,DABS(X1))	EVALFD
	DO 44 K=K1,K2,2	EVALFD
	IF (X0.GE.TAB(K)) GO TO 44	EVALFD
	Z1 = DMAX1(X0,TAB(K-2))	EVALFD
	Z2 = DMIN1(DL,TAB(K))	EVALFD
	FYX = TAB(K-1)*TAB(K) - TAB(K+1)*TAB(K-2)	EVALFD
	FY = TAB(K+1) - TAB(K-1)	EVALFD
	F = F + (FYX + 0.5*FY*(Z1+Z2)) *(Z2-Z1)/ (TAB(K)-TAB(K-2))	EVALFD
	IF (Z2.NE.DL) GO TO 44	EVALFD
	IF(I.EQ.1.AND.D2.NE.0.0) GO TO 49	EVALFD
	IF(Z2.EQ.0) GO TO 40	EVALFD
	F = F + (D-Z2)*(FYX+Z2*FY)/ (TAB(K)-TAB(K-2))	EVALFD
	GO TO 40	EVALFD

44 CONTINUE  
49 X0 = DABS(D1)  
50 X1 = D2  
40 EVALFD = F  
RETURN  
END

EVALFD  
EVALFD  
EVALFD  
EVALFD  
EVALFD  
EVALFD

	SUBROUTINE FDINIT	FDINIT
		REV III.2 08/08/84REVIII
C	REPLACES CODE PREVIOUSLY IN SUBROUTINES FINPUT AND HINPUT.	FDINIT
C	FROM FIVE FUNCTION NUMBERS IN NF ARRAY	FDINIT
C	1. SET UP KTITLE.	FDINIT
C	2. SET UP NTAB AND TAB ARRAYS	FDINIT
C	3. INCREMENT COUNTERS MXNTB AND MXTB2	FDINIT
C		FDINIT
	IMPLICIT REAL*8 (A-H,O-Z)	FDINIT
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)	DIMENB
	COMMON/TEMPVS/ JTITLE(5,51),NF(5),MS(3),KTITLE(31),DMMY(34966)	80386
C	NOTE: THIS IS SHARED BY SUBS CINPUT, FINPUT, HINPUT AND FDINIT.	FDINIT
	REAL JTITLE,KTITLE	FDINIT
	J1 = MXTB2 + 1	FDINIT
	NT = MXNTB + 1	FDINIT
	NTAB(NT) = J1	FDINIT
	NT = NT+1	FDINIT
	DO 56 L=1,5	FDINIT
	NX = IABS(NF(L))	FDINIT
	NTAB(NT) = 0	FDINIT
	IF (NX.EQ.0) GO TO 56	FDINIT
	NTAB(NT) = ISIGN(NTI(NX),NF(L))	FDINIT
	DO 51 KK = 1,5	FDINIT
	KJ = 5*L+KK+1	FDINIT
51	KTITLE(KJ) = JTITLE(KK,NX)	FDINIT
	IF (NTI(NX).NE.0) GO TO 56	FDINIT
	WRITE(6,54) NX	FDINIT
54	FORMAT ('0 FUNCTION NO.',I4,' HAS NOT BEEN DEFINED. ',	FDINIT
	* ' PROGRAM TERMINATED.')	FDINIT
	STOP 15	FDINIT
56	NT = NT+1	FDINIT
C		FDINIT
C	INITIALIZE TAB ARRAY TO ZERO EXCEPT FOR DMAX, DINER, FDMAX.	FDINIT
C		FDINIT
	J2 = J1+29	FDINIT
	DO 57 JJ=J1,J2	FDINIT
57	TAB(JJ) = 0.0	FDINIT
	NX = NTAB(NT-5)	FDINIT
	IF (NX.LE.0) GO TO 58	BUTLER1
	TAB(J1+8) = DABS(TAB(NX+1))	FDINIT
	IF (TAB(NX+2).NE.0.0) TAB(J1+8) = DABS(TAB(NX+2))	FDINIT
	DX = TAB(J1+8)	FDINIT
	TAB(J1+10) = EVALFD(DX,NX,1)	FDINIT
	NX = NTAB(NT-4)	FDINIT
	IF (NX.LE.0) GO TO 58	FDINIT
	TAB(J1+9) = DABS(TAB(NX+1))	FDINIT
	IF (TAB(NX+2).NE.0.0) TAB(J1+9) = DABS(TAB(NX+2))	FDINIT
58	J1 = J2+1	FDINIT
	MXNTB = NT-1	FDINIT
	MXTB2 = J1-1	FDINIT
	IF (MXTB2.GT.4500) WRITE (6,62) MXTB2	DIMENB
62	FORMAT ('0 ERROR IN SUBROUTINE FDINIT, SIZE OF TAB ARRAY =',I8//	FDINIT

<pre> *          ' PROGRAM TERMINATED.'   IF (MXNTB.GT.1250) WRITE (6,63) MXNTB 63 FORMAT ('0 ERROR IN SUBROUTINE FDINIT, SIZE OF NTAB ARRAY =',I8// *          ' PROGRAM TERMINATED.')   IF (MXTB2.GT.4500.OR.MXNTB.GT.1250) STOP 16   RETURN END </pre>	<pre> FDINIT DIMENB FDINIT FDINIT DIMENB FDINIT FDINIT </pre>
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SUBROUTINE FINPUT                                FINPUT
C                                                    REV IV    02/01/88MISDOT
C INPUT CARDS F.1-F.5 SPECIFYING THE ALLOWED CONTACTS OF THE CRASH FINPUT
C VICTIM BODY SEGMENTS WITH VEHICLE PANELS, BELTS, AIRBAGS AND OTHERFINPUT
C BODY SEGMENTS ALONG WITH THE ASSOCIATED FUNCTIONS TO BE USED FOR FINPUT
C EACH CONTACT. FINPUT
C ALSO SETS UP TABLES TO CONTROL TIME HISTORY INFORMATION FOR FINPUT
C EACH FUNCTION FOR EACH ALLOWED CONTACT. FINPUT
C FINPUT
C IMPLICIT REAL*8(A-H,O-Z) FINPUT
COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND, FINPUT
* NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG PAGE
COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60), SLIP
* RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90), FINPUT
* JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30) FINPUT
COMMON/JBARTZ/ MNPL( 30),MNBLT( 8),MNSEG( 30),MNBAG( 6), FINPUT
* MPL(3,5,30),MBLT(3,5,8),MSEG(3,5,30),MBAG(3,10,6), FINPUT
* NTPL( 5,30),NTBLT( 5,8),NTSEG( 5,30) FINPUT
COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)DIMENB
COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5), FINPUT
* BLTTTL(5,8),PLTTL(5,30),BAGTTL(5,6),SEG(30), FINPUT
* JOINT(30),CGS(30),JS(30) FINPUT
REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTL,BAGTTL,SEG,JOINT FINPUT
LOGICAL*1 CGS,JS FINPUT
COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24), FINPUT
* HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12), FINPUT
* RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12), FINPUT
* KQ1(12),KQ2(12),KQTYPE(12) FINPUT
COMMON/WINDFR/ WTIME(30),QFU(3,5),QFV(3,5),WF(3,30),IWIND(30), WINDOP
* MWSEG(7,30),NFVSEG(6),NFVNT(5),MOWSEG(30,30) WINDOP
COMMON/TEMPVS/JTITL(5,51),NF(5),MS(3),KTITL(31),DMMY(34966) 80386
C FINPUT
REAL JTITL,KTITL,BLANK,SURFCE(2,3) FINPUT
DATA BLANK/4H / FINPUT
DATA SURFCE/4H PL,4HANE ,4H BE,4HLT ,4H SEG,4HMENT/ FINPUT
C FINPUT
MXNTI = 50 FINPUT
MXNTB = 0 FINPUT
MXTB2 = MXTB1 FINPUT
C FINPUT
C INPUT ALLOWED CONTACTS AND FUNCTIONS BY REF. NO. FINPUT
C FINPUT
WRITE (6,31) NPG PAGE
NPG=NPG+1 PAGE
31 FORMAT('1 ALLOWED CONTACTS AND ASSOCIATED FUNCTIONS',80X, PAGE
* 'PAGE',I5) PAGE
DO 61 I=1,4 FINPUT
IJK = 0 FINPUT
GO TO (32,34,35,36),I FINPUT
32 IF (NPL.LE.0) GO TO 61 FINPUT
C FINPUT
C INPUT NO. OF SEGMENTS TO CONTACT EACH PLANE. FINPUT

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C	INPUT CARD F.1.A	FINPUT
C		FINPUT
	READ (5,33) (MNPL(J),J=1,NPL)	FINPUT
33	FORMAT(1814)	FINPUT
	NJJ = NPL	FINPUT
	GO TO 37	FINPUT
34	IF (NBLT.LE.0) GO TO 61	FINPUT
C		FINPUT
C	INPUT NO. OF SEGMENTS TO CONTACT EACH BELT.	FINPUT
C	INPUT CARD F.2.A	FINPUT
C		FINPUT
	READ (5,33) (MNBLT(J),J=1,NBLT)	FINPUT
	NJJ = NBLT	FINPUT
	GO TO 37	FINPUT
35	IF (NSEG.LE.0) GO TO 61	FINPUT
C		FINPUT
C	INPUT NO. OF SEGMENTS TO CONTACT EACH SEGMENT.	FINPUT
C	INPUT CARD F.3.A	FINPUT
C		FINPUT
	READ (5,33) (MNSEG(J),J=1,NSEG)	FINPUT
	NJJ = NSEG	FINPUT
	NSEG1 = NSEG+1	FINPUT
	DO 26 J=NSEG1,NGRND	FINPUT
26	MNSEG(J) = 0	FINPUT
	GO TO 37	FINPUT
36	IF (NJNT.LE.0) GO TO 61	FINPUT
C		FINPUT
C	INPUT CARD F.4.A	FINPUT
C	SUPPLY IGLOB(J)=1 FOR EACH GLOBALGRAPHIC JOINT J=1,NJNT	FINPUT
C		FINPUT
	READ (5,33) (IGLOB(J),J=1,NJNT)	FINPUT
	NJJ = NJNT	FINPUT
C		FINPUT
C	START OF LOOP TO READ CONTACTS FOR PLANES (I-1), BELTS (I-2),	FINPUT
C	SEGMENTS (I-3) AND FUNCTIONS FOR GLOBALGRAPHIC JOINTS (I-4).	FINPUT
C		FINPUT
37	DO 60 J=1,NJJ	FINPUT
	IF (I.EQ.1) NK = MNPL(J)	FINPUT
	IF (I.EQ.2) NK = MNBLT(J)	FINPUT
	IF (I.EQ.3) NK = MNSEG(J)	FINPUT
	IF (I.EQ.4) NK = IGLOB(J)	FINPUT
	IF (NK.LE.0) GO TO 60	FINPUT
	DO 59 K=1,NK	FINPUT
	IF (IJK.EQ.0) WRITE (6,38) I	FINPUT
38	FORMAT('0',119X,'CARDS F.',I1)	FINPUT
	IF (IJK.EQ.0 .AND. I.NE.4) WRITE (6,39) SURFCE(1,I),SURFCE(2,I)	FINPUT
39	FORMAT('0',3X,2A4,8X,'SEGMENT',2X,'FORCE DEFLECTION',6X,'INERTIAL	FINPUT
	*SPIKE',10X,'R FACTOR',13X,'G FACTOR',10X,'FRICTION COEF. OPT')	EDGE
	IF (IJK.EQ.0 .AND. I.EQ.4) WRITE (6,40)	FINPUT
40	FORMAT('0',5X,'JOINT (GLOBALGRAPHIC)',2X,'TORQUE DEFLECTION',6X,'HF	FINPUT
	*ERRON FORMULA',10X,'R FACTOR',13X,'G FACTOR',10X,'FRICTION COEF.')	FINPUT
	IJK = 1	FINPUT

C		FINPUT
C	INPUT CONTACT SURFACE NO., SEGMENT NO., AND FUNCTION NOS.	FINPUT
C	INPUT CARD F.(I).(K)	FINPUT
C		FINPUT
	READ (5,33) NJ,MS,NF,NX	EDGE
	WRITE (6,41) NJ,MS,NF,NX	EDGE
41	FORMAT('0',I7,'-',I3,I11,'-',I3,I8,4I21,I12)	EDGE
	IF (NJ.NE.J) WRITE (6,42)	FINPUT
42	FORMAT(' CONTACT INPUT ERROR. PROGRAM TERMINATED.')	FINPUT
	IF (NJ.NE.J) STOP 14	FINPUT
	IF (I.NE.2.AND.NF(5).EQ.0) WRITE(6,20)	MISDOT
20	FORMAT(' FRICTION FUNCTION NUMBER CAN NOT BE ZERO FOR THIS TYPE OF	MISDOT
	* CONTACT')	MISDOT
	IF (I.NE.2.AND.NF(5).EQ.0) STOP 105	MISDOT
	NLT = 1	FINPUT
	DO 43 JJ = 1,31	FINPUT
43	KTITLE(JJ) = BLANK	FINPUT
	GO TO (44,46,48,49),I	FINPUT
C		FINPUT
C	PLACE SEGMENT NO. AND INDEX TO NTAB ARRAY INTO M- AND NT- ARRAYS.	FINPUT
C		FINPUT
44	MPL(1,K,J) = MS(1)	FINPUT
	MPL(2,K,J) = MS(2)	FINPUT
	MPL(3,K,J) = MS(3)	FINPUT
	NTPL(K,J) = MXNTB+1	FINPUT
	DO 45 JJ = 1,5	FINPUT
45	KTITLE(JJ) = PLTTL (JJ,J)	FINPUT
	GO TO 50	FINPUT
46	MBLT(1,K,J) = MS(1)	FINPUT
	MBLT(2,K,J) = MS(2)	FINPUT
	MBLT(3,K,J) = MS(3)	FINPUT
	NTBLT(K,J) = MXNTB+1	FINPUT
	DO 47 JJ = 1,5	FINPUT
47	KTITLE(JJ) = BLTTTL (JJ,J)	FINPUT
C		FINPUT
C	SET UP TWO TABLES FOR FULL BELT FRICTION	FINPUT
C		FINPUT
	IF (NF(5).NE.0) NLT = 2	FINPUT
	GO TO 50	FINPUT
48	MSEG(1,K,J) = MS(1)	FINPUT
	MSEG(2,K,J) = MS(2)	FINPUT
	MSEG(3,K,J) = MS(3)	FINPUT
	NTSEG(K,J) = MXNTB+1	FINPUT
	KTITLE (3) = SEG(J)	FINPUT
	GO TO 50	FINPUT
C		FINPUT
C	NOTE: GLOBALGRAPHIC JOINT WILL SAVE NT IN IGLOB ARRAY	FINPUT
C		FINPUT
49	IGLOB(J) = MXNTB+1	FINPUT
	KTITLE(2) = JOINT(J)	FINPUT
C		FINPUT
C	SET UP POINTERS TO TAB ARRAY IN NTAB ARRAY.	FINPUT

C		FINPUT
	50 NFJ = MS(2)	FINPUT
	IF (NFJ.GT.0) KTITLE(6) = SEG(NFJ)	FINPUT
	DO 51 JJ=1,NLT	FINPUT
	51 CALL FDINIT	FINPUT
	WRITE (6,53) KTITLE	FINPUT
	53 FORMAT(1X,5A4,1X,A4,5(1X,5A4))	FINPUT
	LT = NTAB(MXNTB-5)	EDGE
	IF (I.EQ.1) TAB(LT+22) = NX	EDGE
	IF (NF(1).NE.0) GO TO 59	EDGE
C		FINPUT
C	IF FORCE DEFLECTION FUNCTION NO. IS ZERO,	FINPUT
C	SET UP FOR ROLLING CONSTRAINT	FINPUT
C		FINPUT
	NQ = NQ+1	FINPUT
	NTAB(MXNTB-4) = -NQ	FINPUT
	KQTYPE(NQ) = -4	FINPUT
	KQ1(NQ) = MS(2)	FINPUT
	KQ2(NQ) = MS(1)	FINPUT
	IF (I.NE.3) GO TO 59	EDGE
	KQ1(NQ) = J	FINPUT
	KQ2(NQ) = MS(2)	FINPUT
	59 CONTINUE	FINPUT
	60 CONTINUE	FINPUT
	61 CONTINUE	FINPUT
C		FINPUT
C	INPUT CARD F.5 - JOINT FUNCTIONS TO BE USED.	FINPUT
C		FINPUT
	IF (NJNT.LE.0) GO TO 81	FINPUT
	IF (NJNTF.NE.0) GO TO 76	FINPUT
	DO 75 J=1,NJNT	FINPUT
	75 JOINTF(J) = 0	FINPUT
	GO TO 81	FINPUT
	76 READ (5,33) (JOINTF(J),J=1,NJNT)	FINPUT
	IJK = 0	FINPUT
	DO 80 J=1,NJNT	FINPUT
	IF (JOINTF(J).EQ.0) GO TO 80	FINPUT
	IF (IJK.EQ.0) WRITE (6,77) NPG	PAGE
	IF (IJK.EQ.0) NPG=NPG+1	PAGE
	77 FORMAT('1',122X,'PAGE',15/120X,'CARD F.5'/	PAGE
	* ' THE FOLLOWING JOINT RESTORING FORCE FUNCTIONS AS DEFINED	FINPUT
	*ON CARDS E.7 WILL BE USED.'//4X,'JOINT',10X,'FUNCTION'//)	FINPUT
	JF = JOINTF(J)	FINPUT
	IJK = 1	FINPUT
	WRITE (6,78) J,JOINT(J),JF,(JTITLE(I,JF),I=1,5)	FINPUT
	78 FORMAT(I6,'-',A4,I10,'-',5A4)	FINPUT
	IF (NTI(JF).EQ.0) WRITE (6,42)	FINPUT
	IF (NTI(JF).EQ.0) STOP 17	FINPUT
	80 CONTINUE	FINPUT
C		FINPUT
C	INPUT CONTACT SEGMENTS FOR AIRBAG, IF ANY.	FINPUT
C		FINPUT



81	IF (NBAG.LE.0) GO TO 69	FINPUT
	IJK = 0	FINPUT
	DO 68 J=1,NBAG	FINPUT
C		FINPUT
C	INPUT CARD F.6.(J)*	FINPUT
C		FINPUT
	READ (5,63) K,NK,(MBAG(2,I,J),MBAG(3,I,J),I=1,NK)	FINPUT
63	FORMAT(2I4,20I2)	FINPUT
	MNBAG(J) = NK	FINPUT
	IF (NK.EQ.0) GO TO 68	FINPUT
	IF (IJK.EQ.0) WRITE (6,64)	FINPUT
64	FORMAT(////5X,'AIRBAG',4X,'VS.',4X,'SEGMENTS',90X,'CARDS F.6')	FINPUT
	IF (K.NE.J) WRITE (6,42)	FINPUT
	IF (K.NE.J) STOP 20	FINPUT
	WRITE (6,65) J,(MBAG(2,I,J),MBAG(3,I,J),I=1,NK)	FINPUT
65	FORMAT('0 NO.',I2,12X,10(I3,'-',I3))	FINPUT
	DO 66 I=1,NK	FINPUT
	K = MBAG(2,I,J)	FINPUT
66	KTITLE(I) = SEG(K)	FINPUT
	WRITE (6,67) (BAGTTL(I,J),I=1,5),(KTITLE(I),I=1,NK)	FINPUT
67	FORMAT(1X,5A4,10(3X,A4))	FINPUT
68	CONTINUE	FINPUT
C		FINPUT
C	INPUT CARDS F.7.A F.7.B FOR SUBROUTINE WINDY.	FINPUT
C		FINPUT
69	DO 85 J=1,NGRND	FINPUT
85	MWSEG(1,J) = 0	FINPUT
	IF (NWINDF.EQ.0) GO TO 99	FINPUT
	READ (5,33) (MWSEG(1,J),J=1,NSEG)	FINPUT
	IPAGE = 0	FINPUT
	DO 73 J=1,NSEG	FINPUT
	IWIND(J) = 0	FINPUT
	WTIME(J) = 0.0	FINPUT
	IF (MWSEG(1,J).EQ.0) GO TO 73	FINPUT
	IF (IPAGE.EQ.0) WRITE (6,70) NPG	PAGE
	IF (IPAGE.EQ.0) NPG=NPG+1	PAGE
70	FORMAT('1 SEGMENT WIND FORCES',102X,'PAGE',I5/120X,'CARDS F.7'/	PAGE
*	75X,'DRAG COEFFICIENT BLOCKING'/	WINDOP
*	' SEGMENT-ELLIPSOID SEGMENT-PLANE',	WINDOP
*	16X,'WIND FORCE FUNCTION',10X,'FUNCTION',9X,	WINDOP
*	'SEGMENTS-ELLIPSOID')	WINDOP
	IPAGE = 1	FINPUT
	READ(5,86)(MWSEG(I,J),I=1,7),(MOWSEG(J,K),K=1,2*MWSEG(7,J))	WINDOP
86	FORMAT (7I4,22I2/(I30,7I2))	WINDOP
	WRITE(6,71)(MWSEG(I,J),I=1,6)	OUT385
71	FORMAT(1H0,I6,2H -,I3,I13,2H ,I3,I31,I23)	OUT385
	IF (IABS(MWSEG(1,J)).NE.J) WRITE (6,42)	WINDOP
	IF (IABS(MWSEG(1,J)).NE.J) STOP 21	WINDOP
	M3 = MWSEG(3,J)	FINPUT
	M4 = MWSEG(4,J)	FINPUT
	M5 = MWSEG(5,J)	FINPUT
	M6 = MWSEG(6,J)	WINDOP

M7 = MWSEG(7,J)	OUT385
DO 172 II=1,5	FIXWBS
KTITLE(II)=BLANK	FIXWBS
172 IF (M6.NE.0) KTITLE(II)=JTITLE(II,M6)	FIXWBS
WRITE (6,72) SEG(J),SEG(M3),(PLTTL(I,M4),I=1,5)	FINPUT
* , (JTITLE(I,M5),I=1,5), (KTITLE(I),I=1,5)	FIXWBS
* , (MOWSEG(J,K),K=1,2*M7)	OUT385
72 FORMAT(3X,A4,14X,A4,1H-,5A4,3X,5A4,3X,5A4,2X,3(5(I3,1H-,I3)/94X))	OUT385
73 CONTINUE	FINPUT
99 RETURN	FINPUT
END	FINPUT

C

## 'SUBROUTINE FLXSEG

REV IV 07/23/86TWOPI

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      IMPLICIT REAL*8(A-H,O-Z)
      COMMON/CONTRL/ TIME,NSEG,NJNT,NPI,NBLT,NBAG,NVEH,NGRND,
*      NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG
      COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),
*      SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)
      COMMON/FLXBLE/ HF(4,12,8),B42(3,3,24),V4(3,8),NFLEX(3,8)
      COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),
*      UNITL,UNITM,UNITT,GRAVITY(3),TWOPI
      COMMON/TEMPVS/ TT(3,3),THN(4),CN1(3,3),CN(3,3),WNM1(3),
*      THND(4),PTD(3),WCSN(3),RHSN(3),RHS1(3),
*      RHS2(3),GF(3,4),GC(3,3),CGC(3,3),THA(3),
*      THAD(3),THADEG(3),DN2N1(3,3),RMG(3),DDMY(35009)
      DIMENSION IDYPR(3)
      DATA IDYPR/3,2,1/
      IF (NFLX.EQ.0) GO TO 99
      CALL ELTIME(1,34)
      IFX = 1
11  N1 = NFLEX(1,IFX)
      N3 = NFLEX(3,IFX)
      CALL DOT33(D(1,1,N3),D(1,1,N1),TT)
      THN(1) = DATAN2(TT(1,2),TT(1,1))
      THN(2) = -DASIN(TT(1,3))
      THN(3) = DATAN2(TT(2,3),TT(3,3))
      THN(4) = 1.0
      CT22 = 1.0-TT(1,3)**2
      CT2 = DSQRT(CT22)
      ST2 = -TT(1,3)
      CT1 = TT(1,1)/CT2
      ST1 = TT(1,2)/CT2
      CN1(1,1) = -TT(1,1)*TT(1,3)/CT22
      CN1(1,2) = -TT(1,2)*TT(1,3)/CT22
      CN1(1,3) = 1.0
      CN1(2,1) = -ST1
      CN1(2,2) = CT1
      CN1(2,3) = 0.0
      CN1(3,1) = TT(1,1)/CT22
      CN1(3,2) = TT(1,2)/CT22
      CN1(3,3) = 0.0
      CALL DOT31(TT,WMEG(1,N3),WNM1)
      DO 12 I=1,3
12  WNM1(I) = WNM1(I) - WMEG(I,N1)
      CALL MAT31(CN1,WNM1,THND)
      THND(4) = 0.0
      CALL CROSS(WMEG(1,N1),WNM1,WCSN)
      RHSN(1) = ( (-THND(1)*ST1*ST2 + THND(2)*CT1/CT2)*WNM1(1)
*      +( THND(1)*CT1*ST2 + THND(2)*ST1/CT2)*WNM1(2) )/CT2
      RHSN(2) = -THND(1)*(CT1*WNM1(1) + ST1*WNM1(2))
      RHSN(3) = ( (-THND(1)*ST1 + THND(2)*CT1*ST2/CT2)*WNM1(1)
*      +( THND(1)*CT1 + THND(2)*ST1*ST2/CT2)*WNM1(2) )/CT2
13  N2 = NFLEX(2,IFX)

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'M = 0	FLXSEG
DO 15 I=1,3	FLXSEG
DO 14 J=1,4	FLXSEG
JM = J+M	FLXSEG
GF(I,J) = 0.0	FLXSEG
DO 14 K=1,4	FLXSEG
14 GF(I,J) = GF(I,J) + HF(K,JM,IFX)*THN(K)	FLXSEG
15 M = M+4	FLXSEG
DO 17 I=1,3	FLXSEG
THA(I) = 0.0	FLXSEG
THAD(I) = 0.0	FLXSEG
DO 16 J=1,4	FLXSEG
THA(I) = THA(I) + GF(I,J)*THN(J)	FLXSEG
16 THAD(I) = THAD(I) + GF(I,J)*THND(J)	FLXSEG
THA(I) = 0.5*THA(I)	FLXSEG
17 THADEG(I) = THA(I)/RADIAN	FLXSEG
CALL DRCYPR(DN2N1,THADEG,IDYPR)	FLXSEG
CALL MAT33(DN2N1,D(1,1,N1),D(1,1,N2))	FLXSEG
CSC = DCOS(THA(2))	FLXSEG
CSS = DSIN(THA(2))	FLXSEG
CN(1,1) = 0.0	FLXSEG
CN(2,1) = 0.0	FLXSEG
CN(3,1) = 1.0	FLXSEG
CN(1,2) = -DSIN(THA(1))	FLXSEG
CN(2,2) = DCOS(THA(1))	FLXSEG
CN(3,2) = 0.0	FLXSEG
CN(1,3) = CSC*CN(2,2)	FLXSEG
CN(2,3) = -CSC*CN(1,2)	FLXSEG
CN(3,3) = -CSS	FLXSEG
CALL MAT33(GF,CN1,GC)	FLXSEG
CALL MAT33(CN,GC,CGC)	FLXSEG
CALL DOT33(D(1,1,N1),CGC,B42(1,1,3*IFX-2))	FLXSEG
CALL DOTT33(B42(1,1,3*IFX-2),TT,B42(1,1,3*IFX))	FLXSEG
DO 20 I=1,3	FLXSEG
DO 20 J=1,3	FLXSEG
B42(I,J,3*IFX-2) = B42(I,J,3*IFX-2) - D(J,I,N1)	FLXSEG
B42(I,J,3*IFX-1) = D(J,I,N2)	FLXSEG
20 B42(I,J,3*IFX) = -B42(I,J,3*IFX)	FLXSEG
C	FLXSEG
C	FLXSEG
C	FLXSEG
COMPUTE V4	FLXSEG
CALL MAT31(CGC,WNM1,RHS1)	FLXSEG
DO 21 I=1,3	FLXSEG
21 RMG(I) = RHS1(I) + WMEG(I,N1)	FLXSEG
CALL MAT31(DN2N1,RMG,WMEG(1,N2))	FLXSEG
CALL CROSS(WMEG(1,N1),RHS1,RHS2)	FLXSEG
CALL MAT31(CGC,WCSN,RHS1)	FLXSEG
DO 25 I=1,3	FLXSEG
25 RHS1(I) = RHS2(I) - RHS1(I)	FLXSEG
CALL MAT31(GC,WNM1,RHS2)	FLXSEG
RHS1(1) = RHS1(1) - THAD(1)*(CN(2,2)*RHS2(2) - CN(1,2)*CSC*RHS2(3))	FLXSEG
* - THAD(2)*CN(2,2)*CSS*RHS2(3)	FLXSEG

RHS1(2) = RHS1(2) + THAD(1)*(CN(1,2)*RHS2(2)+CN(2,2)*CSC*RHS2(3))	FLXSEG
* + THAD(2)*CN(1,2)*CSS*RHS2(3)	FLXSEG
RHS1(3) = RHS1(3) - THAD(2)*CSC*RHS2(3)	FLXSEG
CALL MAT31(GF, RSHN, RHS2)	FLXSEG
M = 1	FLXSEG
DO 30 I=1,3	FLXSEG
DO 26 J=1,3	FLXSEG
PTD(J) = 0.0	FLXSEG
DO 26 K=1,3	FLXSEG
KK = K+M-1	FLXSEG
26 PTD(J) = PTD(J) + HF(J,KK,IFX)*THND(K)	FLXSEG
RHS2(I) = RHS2(I) + XDY(PTD,CN1,WM1)	FLXSEG
30 M = M+4	FLXSEG
CALL MAT31(CN, RHS2, PTD)	FLXSEG
DO 35 I=1,3	FLXSEG
35 RHS1(I) = RHS1(I) + PTD(I)	FLXSEG
CALL DOT31(D(1,1,N1),RHS1,V4(1,IFX))	FLXSEG
IF (IFX.EQ.NFLX) GO TO 98	FLXSEG
IFX = IFX+1	FLXSEG
IF (NFLEX(1,IFX).EQ.N1 .AND. NFLEX(3,IFX).EQ.N3) GO TO 13	FLXSEG
GO TO 11	FLXSEG
98 CALL ELTIME(2,34)	FLXSEG
99 RETURN	FLXSEG
END	FLXSEG

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C      DOUBLE PRECISION FUNCTION FINTERP(THETA,PHI,NT)                                FINTERP
C                                                                                   REV IV    04/10/87FNFIX
C      COMPUTES THE RESTORING TORQUE OF A JOINT AS A FUNCTION OF THE              FINTERP
C      FLEXURE ANGLE (THETA) AND THE AZIMUTH ANGLE (PHI) AS DEFINED BY            FINTERP
C      FUNCTION NO. NT .                                                           FINTERP
C                                                                                   FINTERP
C      ASSUMES  0 < THETA < PI                                                    FINTERP
C               -PI < PHI < PI                                                    FINTERP
C               DATA IN TAB ARRAY CONTAINS NTHETA,NPHI FOLLOWED BY              FINTERP
C               TWO DIMENSIONAL ARRAY OF FUNCTIONAL VALUES (NTHETA > 0)        FINTERP
C               OR POLYNOMIAL COEFFICIENTS (NTHETA < 0) FOR EQUALLY              FINTERP
C               SPACED VALUES OF PHI.                                           FINTERP
C                                                                                   FINTERP
C               THETA(I) = (I-1)*PI/(NTHETA-1) FOR I=1,NTHETA                  FINTERP
C               PHI(J) = -PI + (J-1)*2*PI/NPHI FOR J=1,NPHI                   FINTERP
C               F(THETA,PI) = F(THETA,-PI)                                       FINTERP
C                                                                                   FINTERP
C      SUBROUTINE EVALUATES G1(THETA) = F(THETA,PHI(J) )                        FINTERP
C               G2(THETA) = F(THETA,PHI(J+1))                                  FINTERP
C               FOR PHI(J) < PHI < PHI(J+1)                                     FINTERP
C      BY LINEAR INTERPOLATION OR POLYNOMIAL EVALUATION AND THEN LINEAR          FINTERP
C      INTERPOLATES BETWEEN G1 AND G2 TO OBTAIN F(THETA,PHI).                  FINTERP
C      IF F < 0. F IS SET TO ZERO, THEREFORE A DEAD BAND IS OBTAINED           FINTERP
C      BY NEGATIVE VALUES IN THE TABLE.                                       FINTERP
C                                                                                   FINTERP
C      IMPLICIT REAL*8 (A-H,O-Z)                                                FINTERP
C      COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),                               FINTERP
C      *      UNITL,UNITM,UNITT,GRAVTY(3),TWOPI                                TWOPI
C      COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)DIMENB
C      IERROR = 0                                                                FINTERP
C      IF (PHI.LT.-PI) IERROR = 1                                                FINTERP
C      IF (PHI.GT. PI) IERROR = 2                                                FINTERP
C      IF (THETA.LT.0.0) IERROR = 3                                              FINTERP
C      IF (THETA.GT.PI ) IERROR = 4                                              FINTERP
C      IF (IERROR.NE.0) WRITE (6,11) IERROR,THETA,PHI,NT                      FINTERP
11  FORMAT('O IMPROPER ARGUMENTS TO FUNCTION FINTERP. ERROR CODE =',I4)FINTERP
C      *      'O THETA =',G25.15, ' PHI =',G25.15, ' NT =',I6)                FINTERP
C      IF (IERROR.NE.0) STOP 36                                                  FINTERP
C      NF = NTI(NT) + 5                                                         FINTERP
C      NTHETA = TAB(NF)                                                         FINTERP
C      NPHI   = TAB(NF+1)                                                       FINTERP
C                                                                                   FINTERP
C      DETERMINE INDEX AND INTERPOLATION PARAMETERS FOR PHI.                  FINTERP
C                                                                                   FINTERP
C      IF (PHI.GE.PI-EPS(15)) PHI=0.0-PI                                       FNFIX
C      XNP = (PHI+PI)/TWOPI*TAB(NF+1)                                           TWOPI
C      NP1 = XNP                                                                FINTERP
C      NP2 = NP1+1                                                             FINTERP
C      IF (NP2.GE.NPHI) NP2 = 0                                                FINTERP
C      RP2 = XNP - DFLOAT(NP1)                                                 FINTERP
C      RP1 = 1.0 - RP2                                                         FINTERP
C      NTH = IABS(NTHETA)                                                       FINTERP

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	IP1 = NF+1+NP1*NTH	FNTERP
	IP2 = NF+1+NP2*NTH	FNTERP
C		FNTERP
C	DETERMINE INDEX AND INTERPOLATION PARAMETERS FOR THETA.	FNTERP
C		FNTERP
	IF (NTHETA.LT.0) GO TO 20	FNTERP
	XNT = THETA/PI*(TAB(NF)-1.0)	FNTERP
	NT1 = XNT	FNTERP
	RT2 = XNT - DFLOAT(NT1)	FNTERP
	RT1 = 1.0 - RT2	FNTERP
	IT1 = IP1 + NT1	FNTERP
	IT2 = IP2 + NT1	FNTERP
	G1 = RT1*TAB(IT1+1) + RT2*TAB(IT1+2)	FNTERP
	G2 = RT1*TAB(IT2+1) + RT2*TAB(IT2+2)	FNTERP
	GO TO 23	FNTERP
C		FNTERP
C	COMPUTE FOR POLYNOMIALS IN THETA FOR FIXED PHI.	FNTERP
C		FNTERP
20	NPOLY = -NTHETA-1	FNTERP
	IT1 = IP1 + NPOLY + 2	FNTERP
	IT2 = IP2 + NPOLY + 2	FNTERP
	THETA1 = THETA - TAB(IP1+1)	FNTERP
	THETA2 = THETA - TAB(IP2+1)	FNTERP
	G1 = 0.0	FNTERP
	G2 = 0.0	FNTERP
	DO 21 I=1,NPOLY	FNTERP
	IT1 = IT1-1	FNTERP
	IT2 = IT2-1	FNTERP
	G1 = THETA1*(TAB(IT1)+G1)	FNTERP
21	G2 = THETA2*(TAB(IT2)+G2)	FNTERP
	IF (THETA1.LT.0.0) G1=0.0	FNFIX
	IF (THETA2.LT.0.0) G2=0.0	FNFIX
23	FNTERP = RP1*G1 + RP2*G2	FNTERP
	IF (FNTERP.LT.0.0) FNTERP = 0.0	FNTERP
	RETURN	FNTERP
	END	FNTERP

	SUBROUTINE FRCDFL (D,RATE,M,N,FRCDF,ELOSS)		FRCDFL
C		REV III.2 08/08/84	REV III
C	EVALUATE FORCE DEFLECTION FUNCTION AT POINT D, WHERE DEFINITION		FRCDFL
C	OF FUNCTION IS CONTROLLED BY M INDEX OF NTAB ARRAY.		FRCDFL
C	DERIVATIVE, FUNCTION OR INTEGRAL IS EVALUATED AS N = 0,1 OR 2.		FRCDFL
C	NTAB(M) - INDEX TO TAB ARRAY FOR REAL DATA		FRCDFL
C	NTAB(M+1) - INDEX TO TAB ARRAY FOR BASE FUNCTION		FRCDFL
C	NTAB(M+2) - INDEX TO TAB ARRAY FOR INERTIAL FUNCTION, IF ANY		FRCDFL
C			FRCDFL
C	ASSUMES 0 < DG < DCUBIC < DREF < DMAX		FRCDFL
C	BUT ANY < MAY BE LESS THAN OR EQUAL TO		FRCDFL
C			FRCDFL
	IMPLICIT REAL*8(A-H,O-Z)		FRCDFL
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)		DIMENB
	F = 0.0		FRCDFL
	ELOSS = 0.0		FRCDFL
	L = NTAB(M)		FRCDFL
	TAB(L) = D		FRCDFL
	IF (D.LT.0.0) GO TO 99		FRCDFL
	DMAX = TAB(L+8)		FRCDFL
	IF (D.LT.DMAX) GO TO 10		FRCDFL
C			FRCDFL
C	DMAX < D , USE MAX VALUE		FRCDFL
C			FRCDFL
	IF (N-1) 99,9,99		FRCDFL
	9 FDMAX = TAB(L+10)		FRCDFL
	F = FDMAX		FRCDFL
	GO TO 40		FRCDFL
	10 DREF = TAB(L+7)		FRCDFL
	IF (D.GE.DREF) GO TO 30		FRCDFL
	DCUBIC = TAB(L+6)		FRCDFL
	IF (DCUBIC GE.DREF) GO TO 20		FRCDFL
	IF (D.LE.DCUBIC) GO TO 20		FRCDFL
C			FRCDFL
C	DCUBIC < D < DREF , USE CUBIC		FRCDFL
C			FRCDFL
	LC = L+14		FRCDFL
	DCO = TAB(L+18)		FRCDFL
	X = D-DCO		FRCDFL
	IF (N-1) 12,11,99		FRCDFL
C			FRCDFL
C	USE CUBIC DEFINITION		FRCDFL
C			FRCDFL
	11 F = TAB(LC) + X *(TAB(LC+1)+X*(TAB(LC+2)+X*TAB(LC+3)))		FRCDFL
	GO TO 40		FRCDFL
C			FRCDFL
C	USE DERIVATIVE OF CUBIC		FRCDFL
C			FRCDFL
	12 F = TAB(LC+1)+X*(2.0*TAB(LC+2)+X*3.0*TAB(LC+3))		FRCDFL
	GO TO 99		FRCDFL
	20 DG = TAB(L+5)		FRCDFL
	IF (D.LE.DG) GO TO 40		FRCDFL



C		FRCDFL
C	DG < D < DCUBIC , USE QUADRATIC	FRCDFL
C		FRCDFL
	LQ = L+11	FRCDFL
	X = D-DG	FRCDFL
	IF (N-1) 22,21,99	FRCDFL
C		FRCDFL
C	USE QUADRATIC DEFINITION	FRCDFL
C		FRCDFL
21	F = TAB(LQ)+X*(TAB(LQ+1)+X*TAB(LQ+2))	FRCDFL
	GO TO 40	FRCDFL
C		FRCDFL
C	USE DERIVATIVE OF QUADRATIC.	FRCDFL
C		FRCDFL
22	F = TAB(LQ+1)+X*2.0*TAB(LQ+2)	FRCDFL
	GO TO 99	FRCDFL
C		FRCDFL
C	DREF < D < DMAX, USE BASE FUNCTION	FRCDFL
C		FRCDFL
30	IF (N-1) 31,31,99	FRCDFL
31	NB = NTAB(M+1)	FRCDFL
C		FRCDFL
C	EVALUATE BASE FUNCTION	FRCDFL
C		FRCDFL
	IF (NB.GT.0) F = EVALFD(D,NB,N)	FRCDFL
	NI = NTAB(M+2)	FRCDFL
C		FRCDFL
C	ADD INERTIAL FUNCTION , IF ANY	FRCDFL
C		FRCDFL
	IF (NI.GT.0) F = F+EVALFD(D,NI,N)	FRCDFL
40	IF (N.NE.1) GO TO 99	FRCDFL
C		FRCDFL
C	COMPUTE AND ADD RATE DEPENDENT FUNCTIONS, IF ANY.	FRCDFL
C		FRCDFL
C	CURRENT RESTRICTIONS:	FRCDFL
C		FRCDFL
C	1) COMPUTED FOR N=1 (FUNCTION) ONLY.	FRCDFL
C		FRCDFL
C	2) FUNCTION NOS. M+2,M+3 AND M+4 (USED FOR INERTIAL SPIKE,	FRCDFL
C	R FACTOR AND G FACTOR FUNCTIONS) MUST BE NEGATIVE OR ZERO,	FRCDFL
C	I.E., THESE FUNCTIONS CANNOT BE USED IN CONJUNCTION WITH	FRCDFL
C	THE RATE DEPENDENT FUNCTIONS.	FRCDFL
C		FRCDFL
C	3) ASSUMES THE FUNCTIONAL FORM	FRCDFL
C		FRCDFL
C	$F(D,D') = F1(D) + F2(D)*F3(D') + F4(D')$	FRCDFL
C		FRCDFL
C	WHERE F1(D) IS DEFINED BY FUNCTION NTAB(M+1)>0,	FRCDFL
C	I.E., NORMAL FORCE DEFLECTION FUNCTION WITH NO	FRCDFL
C	INERTIAL SPIKE FUNCTION AND DEFAULT VALUES	FRCDFL
C	R=1 AND G=0 (UNLOADING AND RELOADING SAME AS	FRCDFL
C	ORIGINAL LOADING);	FRCDFL

C		FRCDFL
C	F2(D ) IS DEFINED BY FUNCTION NTAB(M+2)<0,	FRCDFL
C	IF NTAB(M+2)=0, F2(D )=0;	FRCDFL
C		FRCDFL
C	F3(D') IS DEFINED BY FUNCTION NTAB(M+3)<0,	FRCDFL
C	IF NTAB(M+3)=0, F3(D')=0;	FRCDFL
C		FRCDFL
C	AND F4(D') IS DEFINED BY FUNCTION NTAB(M+4)<0,	FRCDFL
C	IF NTAB(M+4)=0, F4(D')=0.	FRCDFL
C		FRCDFL
C	NOTE: FUNCTIONAL FORM CAN BE CHANGED BY REVISING PROGRAM	FRCDFL
C	BETWEEN STATEMENTS 40 AND 99.	FRCDFL
C		FRCDFL
	F2 = 0.0	FRCDFL
	F3 = 0.0	FRCDFL
	F4 = 0.0	FRCDFL
	N2 = -NTAB(M+2)	FRCDFL
	N3 = -NTAB(M+3)	FRCDFL
	N4 = -NTAB(M+4)	FRCDFL
	IF (N2.GT.0) F2 = EVALFD (D, N2,N)	FRCDFL
	IF (N3.GT.0) F3 = EVALFD (RATE,N3,N)	FRCDFL
	IF (N4.GT.0) F4 = EVALFD (RATE,N4,N)	FRCDFL
	F = F + F2*F3 + F4	FRCDFL
	ELOSS = RATE*(F2*F3+F4)	FRCDFL
99	FRCDF = F	FRCDFL
	RETURN	FRCDFL
	END	FRCDFL

	SUBROUTINE FSMSOL (C,R,NN,MX,MAXN,JN,MAXDIM)	FSMSOL
C		REV III.2 08/08/84REVIII
C	SOLVES A SET OF SIMULTANEOUS EQUATIONS OF SIZE 3*MM	FSMSOL
C	WHERE THE MATRIX CONSISTS OF A SET OF 3*3 SUBMATRICES	FSMSOL
C	STORED IN C(3,3,IJ). THE LOCATION OF THE I,J ELEMENT	FSMSOL
C	IS STORED IN NN(I,J). I.E. IJ= NN(I,J)	FSMSOL
C		FSMSOL
C	A NEGATIVE IJ IMPLIES THAT C( , ,!IJ!) IS AN	FSMSOL
C	IDENTITY AND THE RIGHT SIDE IS ZERO. A NEGATIVE	FSMSOL
C	IJ WILL ONLY OCCUR ON A DIAGONAL ENTRY OF NN.	FSMSOL
C		FSMSOL
C	THE BASIC EQUATION IS CX=R	FSMSOL
C		FSMSOL
C	DURING THE SOLUTION THE C MATRIX IS DESTROYED ,IT MAY	FSMSOL
C	BE NECESSARY TO ADD TO THE C ARRAY.	FSMSOL
C	THE SOLUTION IS STORED IN R.	FSMSOL
C		FSMSOL
C	INPUT	FSMSOL
C		FSMSOL
C	C(3,3,K) GIVEN ARRAY	FSMSOL
C	R(3,MM) GIVEN RIGHT HAND SIDE	FSMSOL
C	NN(JJ,JJ) GIVEN ARRAY CONTAINING LOCATIONS OF I,J,ELEMENT	FSMSOL
C	MX SIZE OF SYSTEM OF SUBMATRICES (POSITIVE INDICATES	FSMSOL
C	THAT C MATRIX IS SYMMETRIC, NEGATIVE IT IS NOT.)	FSMSOL
C	MAXN LARGEST VALUE IN NN ARRAY	FSMSOL
C	JN DIMENSION OF NN	FSMSOL
C	MAXDIM THIRD DIMENSION OF C IN CALLING ROUTINE	FSMSOL
C		FSMSOL
	IMPLICIT REAL*8 (A-H,O-Z)	FSMSOL
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,	PAGE
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	PAGE
	DIMENSION C(3,3,1),R(3,1),NN(JN,1)	FSMSOL
	CALL ELTIME(1,20)	FSMSOL
	MM = IABS(MX)	FSMSOL
	IF (MM.LE.0) GO TO 99	FSMSOL
	MM1 = MM-1	FSMSOL
	MP1 = MM+1	FSMSOL
	DO 50 II=1,MM	FSMSOL
	I = MP1-II	FSMSOL
C		FSMSOL
C	START PIVOT AT BOTTOM - FIND PIVOT - INVERT.	FSMSOL
C		FSMSOL
	L = NN(I,I)	FSMSOL
	IF (L.LE.0) GO TO 50	FSMSOL
	DO 14 M=1,3	FSMSOL
	B = 1.0/C(M,M,L)	FSMSOL
	C(M,M,L) = 1.0	FSMSOL
	C(M,1,L) = B*C(M,1,L)	FSMSOL
	C(M,2,L) = B*C(M,2,L)	FSMSOL
	C(M,3,L) = B*C(M,3,L)	FSMSOL
	R(M,I) = B*R(M,I)	FSMSOL
	DO 13 N=1,3	FSMSOL

[illegible]

IF (KI.EQ.0 .OR. IJ.EQ.0) GO TO 24	FSMSOL
KJ = NN(K,J)	FSMSOL
IF (KJ.NE.0) GO TO 22	FSMSOL
MAXN = MAXN+1	FSMSOL
IF (MAXN.GT.MAXDIM) GO TO 41	FSMSOL
KJ = MAXN	FSMSOL
NN(K,J) = KJ	FSMSOL
DO 21 M=1,3	FSMSOL
DO 21 N=1,3	FSMSOL
21 C(N,M,KJ) = 0.0	FSMSOL
22 DO 23 M=1,3	FSMSOL
DO 23 N=1,3	FSMSOL
23 C(N,M,KJ) = C(N,M,KJ) - C(N,1,KI)*C(1,M,IJ)	FSMSOL
* - C(N,2,KI)*C(2,M,IJ)	FSMSOL
* - C(N,3,KI)*C(3,M,IJ)	FSMSOL
24 IF (J.EQ.K) GO TO 30	FSMSOL
IF (JI.EQ.0 .OR. IK.EQ.0) GO TO 30	FSMSOL
JK = NN(J,K)	FSMSOL
IF (JK.NE.0) GO TO 26	FSMSOL
MAXN = MAXN+1	FSMSOL
IF (MAXN.GT.MAXDIM) GO TO 41	FSMSOL
JK = MAXN	FSMSOL
NN(J,K) = JK	FSMSOL
DO 25 M=1,3	FSMSOL
DO 25 N=1,3	FSMSOL
25 C(N,M,JK) = 0.0	FSMSOL
26 IF (MX.LT.0) GO TO 28	FSMSOL
DO 27 M=1,3	FSMSOL
DO 27 N=1,3	FSMSOL
27 C(N,M,JK) = C(M,N,KJ)	FSMSOL
GO TO 30	FSMSOL
28 DO 29 M=1,3	FSMSOL
DO 29 N=1,3	FSMSOL
29 C(N,M,JK) = C(N,M,JK) - C(N,1,JI)*C(1,M,IK)	FSMSOL
* - C(N,2,JI)*C(2,M,IK)	FSMSOL
* - C(N,3,JI)*C(3,M,IK)	FSMSOL
30 CONTINUE	FSMSOL
IF (KI.EQ.0) GO TO 40	FSMSOL
DO 35 N=1,3	FSMSOL
35 R(N,K) = R(N,K) - C(N,1,KI)*R(1,I)	FSMSOL
* - C(N,2,KI)*R(2,I)	FSMSOL
* - C(N,3,KI)*R(3,I)	FSMSOL
40 CONTINUE	FSMSOL
50 CONTINUE	FSMSOL
GO TO 51	FSMSOL
41 WRITE (6,49) MAXDIM,NPG,(L,L=1,MM)	FSMSOL
NPG=NPG+1	PAGE
DO 42 I=1,MM	PAGE
42 WRITE (6,43) I,(NN(I,L),L=1,MM)	FSMSOL
43 FORMAT(I3,3X,40I3,3X/6X,40I3)	FSMSOL
WRITE (6,44) NPG	FSMSOL
NPG=NPG+1	PAGE
	PAGE

44	FORMAT('1 FSMSOL PRINT OF RHS ARRAY',96X,'PAGE',15//)	PAGE
	DO 45 K=1,MM	FSMSOL
45	WRITE (6,46) K,(R(I,K),I=1,3)	FSMSOL
46	FORMAT(I6,9G14.7)	FSMSOL
	WRITE (6,47) NPG	PAGE
	NPG=NPG+1	PAGE
47	FORMAT('1 FSMSOL PRINT OF C ARRAY ELEMENTS',89X,'PAGE',15//)	PAGE
	DO 48 K=1,MAXN	FSMSOL
48	WRITE (6,46) K,((C(I,L,K),L=1,3),I=1,3)	FSMSOL
49	FORMAT('1 MAXIMUM DIMENSION OF',14,' ON C ARRAY HAS BEEN EXCEEDED	FSMSOL
	*IN SUBROUTINE FSMSOL.',46X,'PAGE',15// IF 600, CALL IS FROM SUBRO	PAGE
	*UTINE DAUX. IF 200'	PAGE
	* , ' CALL IS FROM SUBROUTINE HPTURB.'/// PROGRAM IS BEING TERMINATE	PAGE
	*D. COMPLETE PRINT-OUT OF IJK, RHS AND C ARRAYS FOLLOW.'//	FSMSOL
	*' FSMSOL PRINT OF IJK MATRIX'//(6X,40I3))	FSMSOL
	STOP 35	FSMSOL
C		FSMSOL
C	BACKDOWN SOLUTION	FSMSOL
C		FSMSOL
51	IF (MM.EQ.1) GO TO 99	FSMSOL
	DO 90 J=1,MM1	FSMSOL
	IP = J+1	FSMSOL
	DO 80 I=IP,MM	FSMSOL
	IF (NN(I,J).EQ.0) GO TO 80	FSMSOL
	IJ = NN(I,J)	FSMSOL
	DO 75 N=1,3	FSMSOL
75	R(N,I) = R(N,I) - C(N,1,IJ)*R(1,J)	FSMSOL
	* - C(N,2,IJ)*R(2,J)	FSMSOL
	* - C(N,3,IJ)*R(3,J)	FSMSOL
80	CONTINUE	FSMSOL
90	CONTINUE	FSMSOL
99	CALL ELTIME(2,20)	FSMSOL
	RETURN	FSMSOL
	END	FSMSOL



	SUBROUTINE HBELT (J1,J2,KNLO,IND)		HBELT
C		REV IV	02/01/88MISDOT
C	ARGUMENTS:		HBELT
C	J1,J2 - FIRST AND LAST INDEX FOR BELTS.		HBELT
C	KNLO - ZERO VALUE FOR KNL INDEX.		HBELT
C	IND - 0: CALL IS FROM SUBROUTINE CONTCT		HBELT
C	1: CALL IS FROM SUBROUTINE UPDATE		HBELT
C			HBELT
	IMPLICIT REAL*8 (A-H,O-Z)		HBELT
	COMMON/CNTRSF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)		EDGE
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),		MISDOT
	* UNITL,UNITM,UNITT,GRAVITY(3),TWOPI		MISDOT
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),		HBELT
	* SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		HBELT
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)		DIMENB
	COMMON/FORCES/PSF(7,70),BSF(4,20),SSF(10,40),BAGSF(3,20),		NCFORC
	* PRJNT(7,30),NPANEL(5),NPSF,NBSF,NSSF,NBGSF		HBELT
	COMMON/HRNESS/ BAR(15,100),BB(100),BBDOT(100),PLOSS(2,100),		HBELT
	* XLONG(20),HTIME(2),IBAR(5,100),NL(2,100),		HBELT
	* NPTSPB(20),NPTPLY(20),NTHRNS(20),NBLTPH(5)		HBELT
C	THIS COMMON/TEMPVS/ IS SHARED BY HPTURB, HBPLAY, HBELT AND HSETC.		HBELT
	COMMON/TEMPVS/ B(3,3,3),S(3,3),T(3),R(3),V(3),T1(3),T2(3),		HBELT
	* E(3,3,50),EDOT(3,50),FCE(3,50),FR(3,50),ZR(3,50),		HBELT
	* TR(3,50),U(3,50),PTLOSS(2,50),BL(50),FB(50),FP(50),		HBELT
	* OLDBB(100),RHS(3,54),C(3,3,200),IJK(54,54)		HBELT
	* ,DMMY(29942)		80386
	CALL ELTIME (1,38)		HBELT
	NTP = 0		HBELT
	K2 = 0		HBELT
	DO 31 JB=J1,J2		HBELT
	IF (IND.EQ.0) NBSF = NBSF + 1		HBELT
	IF (NPTPLY(JB).LE.0) GO TO 31		HBELT
C			HBELT
C	FIRST LOOP ON K		HBELT
C	COMPUTE Z(K),ZR(K),E3(K),U(K-1),BL(K-1),FB(K-1)		HBELT
C	NEED NL(K),BB(K-1)		HBELT
C	NOTE: AN INDEX K-1 REFERS TO BELT SEGMENT BETWEEN K-1 AND K.		HBELT
C			HBELT
	K1 = K2 + 1		HBELT
	K2 = K2 + NPTPLY(JB)		HBELT
	DO 20 K=K1,K2		HBELT
	KNL = KNLO + K		HBELT
	KI = NL(1,KNL)		HBELT
C			HBELT
C	HERE K IS INDEX OF POINTS IN PLAY ON EACH HARNESS		HBELT
C	KNL IS INDEX OF ALL POINTS IN PLAY		HBELT
C	KI IS INDEX OF ALL POINTS		HBELT
C			HBELT
	KS = IABS(IBAR(1,KI))		HBELT
	IF (KS.GT.100) NTP = 1		HBELT
	IF (KS.GT.100) KS = MOD(KS,100)		HBELT
	KE = IBAR(2,KI)		HBELT



CALL DOT31 (D(1,1,KS),BAR(4,KI),T1)	HBELT
CALL DOT31 (D(1,1,KS),BAR(7,KI),T2)	HBELT
DO 11 J=1,3	HBELT
R(J) = V(J)	HBELT
V(J) = BAR(J+3,KI) + BAR(J+6,KI)	HBELT
TR(J,K) = T1(J)	HBELT
ZR(J,K) = T1(J) + T2(J)	HBELT
S (J,2) = S(J,1)	HBELT
11 S (J,1) = SEGLP(J,KS) + ZR(J,K)	HBELT
CALL CROSS (WMEG(1,KS),V,T)	HBELT
IF (KE.EQ.0) GO TO 12	HBELT
CALL MAT31 (BD(7,KE),BAR(4,KI),T2)	HBELT
CALL DOT31 (D(1,1,KS),T2,T1)	HBELT
12 DO 13 J=1,3	HBELT
T(J) = T(J) + BAR(J+12,KI)	HBELT
13 E(J,3,K) = T1(J)	HBELT
CALL DOT31 (D(1,1,KS),T,V)	HBELT
DO 14 J=1,3	HBELT
14 V(J) = V(J) + SEGLV(J,KS)	HBELT
FB(K) = 0.0	HBELT
FP(K) = 0.0	HBELT
IF (K.EQ.K1) GO TO 20	HBELT
DO 15 J=1,3	HBELT
15 U(J,K-1) = S(J,1) - S(J,2)	HBELT
BL(K-1) = DSQRT(U(1,K-1)**2 + U(2,K-1)**2 + U(3,K-1)**2)	HBELT
DO 16 J=1,3	HBELT
16 U(J,K-1) = U(J,K-1)/BL(K-1)	HBELT
STRAIN = (BL(K-1)/BB(KNL-1)) - 1.0	HBELT
IF (STRAIN.LT.EPS(12)) STRAIN = 0.0	HBELT
NT = NL(2,KNL)	MISDOT
BLDOT = U(1,K-1)*(V(1)-R(1))	HBELT
* + U(2,K-1)*(V(2)-R(2))	HBELT
* + U(3,K-1)*(V(3)-R(3))	HBELT
STRDOT = (BB(KNL-1)*BLDOT-BL(K-1)*BBDOT(KNL-1))/BB(KNL-1)**2	HBELT
CALL FRCDL (STRAIN,STRDOT,NT,0,FBK,ELOSS)	HBELT
CALL FRCDL (STRAIN,STRDOT,NT,1,FBK,ELOSS)	HBELT
PTLOSS(1,K-1) = BB(KNL-1)*ELOSS	HBELT
FP(K-1) = FP	HBELT
FB(K-1) = FBK	HBELT
IF (IND.NE.0) GO TO 20	HBELT
IF (K.NE.K1+1) GO TO 19	ENDPFX
BSF(1,NBSF) = STRAIN	ENDPFX
BSF(2,NBSF) = FBK	ENDPFX
19 IF (K.NE.K2) GO TO 20	ENDPFX
BSF(3,NBSF) = STRAIN	ENDPFX
BSF(4,NBSF) = FBK	ENDPFX
20 CONTINUE	HBELT
C	HBELT
C SECOND LOOP ON K	HBELT
C COMPUTE FCE(K),E1(K),E2(K),EDOT(K),FR(K),U1(KS),U2(KS)	HBELT
C NEED FB(K&K-1),U(K&K-1),ZR(K),E3(K)	HBELT
C	HBELT

DO 30 K=K1,K2	HBELT
KNL = KNLO + K	HBELT
KI = NL(1,KNL)	HBELT
KS = IABS(IBAR(1,KI))	HBELT
IF (KS.GT.100) KS = MOD(KS,100)	HBELT
DO 21 J=1,3	HBELT
FCE(J,K) = 0.0	HBELT
IF (K.NE.K2) FCE(J,K) = FB(K)*U(J,K)	BUTLER1
21 IF (K.NE.K1) FCE(J,K) = FCE(J,K) - FB(K-1)*U(J,K-1)	EJTLER1
NT = IBAR(3,KI)	HBELT
NF = NTAB(NT+5)	HBELT
IF (NF.EQ.0 .AND. IND.EQ.0) GO TO 30	HBELT
IF (IBAR(4,KI).EQ.0) GO TO 22	HBELT
CALL DOT31 (D(1,1,KS),BAR(10,KI),T1)	HBELT
GO TO 24	HBELT
22 DO 23 J=1,3	HBELT
T1(J) = 0.0	HBELT
IF (K.NE.K2) T1(J) = U(J,K)	HBELT
23 IF (K.NE.K1) T1(J) = T1(J) + U(J,K-1)	HBELT
24 CALL CROSS (T1,E(1,3,K),E(1,1,K))	HBELT
CALL CROSS (E(1,3,K),E(1,1,K),E(1,2,K))	HBELT
DO 25 J=1,3	HBELT
EDOT(J,K) = DSQRT(E(1,J,K)**2 + E(2,J,K)**2 + E(3,J,K)**2)	HBELT
DO 25 I=1,3	HBELT
25 E(I,J,K) = E(I,J,K)/EDOT(J,K)	HBELT
CALL DOT31 (E(1,1,K),FCE(1,K),FR(1,K))	HBELT
30 CONTINUE	HBELT
31 CONTINUE	HBELT
IF (NTP.LE.0) GO TO 41	HBELT
C	HBELT
C SUM FCE,FR FOR TIE-POINTS	HBELT
C	HBELT
KNL1 = KNLO + 2	HBELT
KNL2 = KNLO + K2	HBELT
DO 40 KNL=KNL1,KNL2	HBELT
KI = NL(1,KNL)	HBELT
KS = IABS(IBAR(1,KI))	HBELT
IF (KS.LT.100) GO TO 40	HBELT
KS1 = KS/100	HBELT
KH = KNL - KNLO	HBELT
MH = 0	HBELT
DO 38 JNL=KNL1,KNL	HBELT
K1 = NL(1,JNL-1)	HBELT
KS = IABS(IBAR(1,KI))	HBELT
IF (KS.LT.100) GO TO 38	HBELT
KS2 = KS/100	HBELT
IF (KS2.NE.KS1) GO TO 38	HBELT
JH = JNL - KNLO	HBELT
IF (MH.EQ.0) MH = JH	HBELT
DO 37 J=1,3	HBELT
IF (MH.EQ.JH) FCE(J,MH) = FCE(J,MH) + FCE(J,KH)	HBELT
37 FCE(J,JH) = FCE(J,MH)	HBELT

	CALL DOT31 (E(1,1,JH),FCE(1,JH),FR(1,JH))	HBELT
38	CONTINUE	HBELT
	IF (MH.EQ.0) GO TO 40	HBELT
	KI = NL(1,KNL)	HBELT
	IBAR(1,KI) = -IABS(IBAR(1,KI))	HBELT
	DO 39 J=1,3	HBELT
39	FCE(J,KH) = FCE(J,MH)	HBELT
	CALL DOT31 (E(1,1,KH),FCE(1,KH),FR(1,KH))	HBELT
40	CONTINUE	HBELT
C		HBELT
C	IF CALL IS FROM SUBROUTINE CONTCCT,	HBELT
C	ADD FORCES (FCE) MODIFIED BY FRICTION TO U1,U2 ARRAYS.	HBELT
C		HBELT
41	IF (IND.NE.0) GO TO 52	HBELT
	K2 = 0	HBELT
	DO 51 JB=J1,J2	HBELT
	IF (NPTPLY(JB).LE.0) GO TO 51	HBELT
	K1 = K2 + 1	HBELT
	K2 = K2 + NPTPLY(JB)	HBELT
	DO 50 K=K1,K2	HBELT
	KNL = KNLO + K	HBELT
	KI = NL(1,KNL)	HBELT
	IF (IBAR(1,KI).LT.0) GO TO 50	HBELT
	KS = IBAR(1,KI)	HBELT
	IF (KS.GT.100) KS = MOD(KS,100)	HBELT
	NT = IBAR(3,KI)	HBELT
	NF = NTAB(NT+5)	HBELT
	IF (NF.EQ.0) GO TO 43	HBELT
	DO 42 J=1,3	HBELT
42	T1(J) = FR(J,K)	HBELT
	FR1 = TAB(NF+2)*DABS(T1(3))	HBELT
	FR2 = TAB(NF+4)*DABS(T1(3))	HBELT
	IF (DABS(T1(1)).GT.FR1) T1(1) = DSIGN(FR1,T1(1))	HBELT
	IF (DABS(T1(2)).GT.FR2) T1(2) = DSIGN(FR2,T1(2))	HBELT
	CALL MAT31 (E(1,1,K),T1,FCE(1,K))	HBELT
43	CALL CROSS (ZR(1,K),FCE(1,K),T2)	HBELT
	CALL MAT31 (D(1,1,KS),T2,T1)	HBELT
	DO 44 J=1,3	HBELT
	U1(J,KS) = U1(J,KS) + FCE(J,K)	HBELT
44	U2(J,KS) = U2(J,KS) + T1(J)	HBELT
50	CONTINUE	HBELT
51	CONTINUE	HBELT
52	KNLO = KNLO + K2	HBELT
	CALL ELTIME (2,38)	HBELT
	RETURN	HBELT
	END	HBELT

	SUBROUTINE HBPLAY	REV III.5 10/17/85	EDGE	HBPLAY
C	IMPLICIT REAL*8 (A-H,O-Z)			HBPLAY
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,			HBPLAY
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG			PAGE
	COMMON/CNTRSF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)			EDGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),			HBPLAY
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)			HBPLAY
	COMMON/HRNESS/ BAR(15,100),BB(100),BBDOT(100),PLOSS(2,100),			HBPLAY
*	XLONG(20),HTIME(2),IBAR(5,100),NL(2,100),			HBPLAY
*	NPTSPB(20),NPTPLY(20),NTHRNS(20),NBLTPH(5)			HBPLAY
C	THIS COMMON/TEMPVS/ IS SHARED BY HPTURB, HBPLAY, HBELT AND HSETC.			HBPLAY
	COMMON/TEMPVS/ B(3,3,3),S(3,3),T(3),R(3),V(3),T1(3),T2(3),			HBPLAY
*	E(3,3,50),EDOT(3,50),FCE(3,50),FR(3,50),ZR(3,50).			HBPLAY
*	TR(3,50),U(3,50),PTLOSS(2,50),BL(50),FB(50),FP(50),			HBPLAY
*	OLDBB(100),RHS(3,54),C(3,3,200),IJK(54,54)			HBPLAY
*	,DMMY(29942)			80386
	IF (NHRNSS.LE.0) GO TO 99			HBPLAY
C				HBPLAY
C	SAVE PREVIOUS NL,BB AND PLOSS ARRAYS.			HBPLAY
C	USE IJK,OLDBB AND PTLOSS AS TEMP STORAGE.			HBPLAY
C				HBPLAY
	DO 10 I=1,100			HBPLAY
	IJK(I,1) = NL(1,I)			HBPLAY
	PTLOSS(I,1) = PLOSS(1,I)			HBPLAY
10	OLDBB(I) = BB(I)			HBPLAY
	JNL = 1			HBPLAY
	J1 = 1			HBPLAY
	J1 = 1			HBPLAY
	LL = 0			HBPLAY
	DO 90 NH=1,NHRNSS			HBPLAY
	IF (NBLTPH(NH).LE.0) GO TO 90			HBPLAY
	J2 = J1 + NBLTPH(NH) - 1			HBPLAY
	DO 80 NB=J1,J2			HBPLAY
	L1 = LL			HBPLAY
	IF (NPTSPB(NB).LE.0) GO TO 80			HBPLAY
	K2 = K1 + NPTSPB(NB) - 1			HBPLAY
	KB = 0			HBPLAY
	DO 30 K=K1,K2			HBPLAY
	KB = KB + 1			HBPLAY
C				HBPLAY
C	HERE K IS INDEX OF ALL POINTS			HBPLAY
C	KB IS INDEX OF POINTS ON A SINGLE BELT			HBPLAY
C	LL IS INDEX OF ALL POINTS IN PLAY			HBPLAY
C	JB IS INDEX OF PREVIOUS POINT ON BELT IN PLAY			HBPLAY
C				HBPLAY
	KS = IABS(IBAR(1,K))			HBPLAY
	IF (KS.GT.100) KS = MOD(KS,100)			HBPLAY
	CALL DOT31 (D(1,1,KS),BAR(4,K),T1)			HBPLAY
	CALL DOT31 (D(1,1,KS),BAR(7,K),T2)			HBPLAY
	DO 11 J=1,3			HBPLAY
11	U(J,KB) = SEGLP(J,KS) + T1(J) + T2(J)			HBPLAY

IF (K.EQ.K1) GO TO 30	HBPLAY
LL = LL + 1	HBPLAY
12 JJ = NL(1,LL)	HBPLAY
JB = JJ - K1 + 1	HBPLAY
DSS = 0.0	HBPLAY
DO 13 J=1,3	HBPLAY
ZR(J,KB) = U(J,KB) - U(J,JB)	HBPLAY
13 DSS = DSS + ZR(J,KB)**2	HBPLAY
BL(LL) = DSQRT(DSS)	HBPLAY
IF (JJ.EQ.K1 .OR. IABS(IBAR(1,JJ)).GT.100) GO TO 30	HBPLAY
JS = IBAR(1,JJ)	HBPLAY
JE = IBAR(2,JJ)	HBPLAY
IF (JE.LE.0) GO TO 30	HBPLAY
CALL MAT31 (BD(7,JE),BAR(4,JJ),T2)	HBPLAY
CALL DOT31 (D(1,1,JS),T2,R)	HBPLAY
DPR = 0.0	HBPLAY
DO 17 J=1,3	HBPLAY
17 DPR = DPR + R(J)*(ZR(J,KB)/BL(LL) - ZR(J,JB)/BL(LL-1))	HBPLAY
IF (DPR.LT.0.0) GO TO 30	HBPLAY
LL = LL - 1	HBPLAY
GO TO 12	HBPLAY
30 NL(1,LL+1) = K	HBPLAY
L2 = L1 + 1	HBPLAY
LL = LL + 1	HBPLAY
L3 = LL-1	HBPLAY
DO 31 J=L2,LL	HBPLAY
31 NL(2,J) = NTHRNS(NB)	HBPLAY
IF (XLONG(NB).EQ.0.0) GO TO 35	HBPLAY
C	HBPLAY
C FIRST TIME IN ROUTINE, SET INITIAL BB ARRAY.	HBPLAY
C INPUT XLONG MUST BE NON-ZERO TO TRIGGER THIS TEST.	HBPLAY
C	HBPLAY
XLG = 0.0	HBPLAY
DO 32 J=L2,L3	HBPLAY
32 XLG = XLG + BL(J)	HBPLAY
XLG = 1.0 + XLONG(NB)/XLG	HBPLAY
DO 33 J=L2,L3	HBPLAY
33 BB(J) = XLG*BL(J)	HBPLAY
XLONG(NB) = 0.0	HBPLAY
GO TO 52	HBPLAY
C	HBPLAY
C DETERMINE IF NEW NL ARRAY IS DIFFERENT FROM PREVIOUS NL ARRAY.	HBPLAY
C IF SO, RECOMPUTE BB ELEMENTS FOR POINTS THAT ARE DIFFERENT.	HBPLAY
C	HBPLAY
35 IF (NL(1,L2).EQ.IJK(JNL,1)) GO TO 61	HBPLAY
WRITE (6,62)	HBPLAY
62 FORMAT ('0 LOGIC ERROR IN SUB HBPLAY. PROGRAM TERMINATED.')	HBPLAY
STOP 42	HBPLAY
61 LTEST = 0	HBPLAY
M = L2	HBPLAY
N = JNL	HBPLAY
36 IF (NL(1,M+1)-IJK(N+1,1)) 39,37,41	HBPLAY

37	BB(M) = OLDBB(N)	HBPLAY
	PLOSS(1,M) = PTLOSS(N,1)	HBPLAY
38	M = M+1	HBPLAY
	N = N+1	HBPLAY
	IF (M-LL) 36,51,51	HBPLAY
C		HBPLAY
C	POINT M+1 IS NEW.	HBPLAY
C		HBPLAY
39	M0 = M	HBPLAY
	N0 = N	HBPLAY
	LTEST = 1	HBPLAY
40	M = M+1	HBPLAY
C		HBPLAY
C	MODIFY NEW POINT TO LIE IN BELT PLANE	CHGIII
C		CHGIII
	IP1 = N - 1	CHGIII
	IF (N.GT.JNL) GO TO 63	CHGIII
	IP1 = N	CHGIII
C	(IS THIRD POINT AVAILABLE FROM OLD POINTS IN PLAY?)	CHGIII
	IF (IJK(N+1,1).EQ.NL(1,LL)) GO TO 43	CHGIII
63	DO 64 I=1,3	CHGIII
	IP = IP1 + I - 1	CHGIII
C	(USE OLD POINTS IP = N-1,N,N+1 IF N > JNL	CHGIII
C	OR IP = N,N+1,N+2 IF N = JNL AND N+2 EXISTS)	CHGIII
	NI = IJK(IP,1)	CHGIII
	NSI = IABS(IBAR(1,NI))	NSFIX
	IF (NSI.GT.100) NSI = MOD(NSI,100)	NSFIX
	CALL DOT31 (D(1,1,NSI),BAR(4,NI),T1)	NSFIX
	CALL DOT31 (D(1,1,NSI),BAR(7,NI),T2)	NSFIX
	DO 64 J=1,3	CHGIII
64	S(J,I) = SEGLP(J,NSI)+ T1(J) + T2(J)	NSFIX
	DO 65 J=1,3	CHGIII
	S(J,3) = S(J,3) - S(J,2)	CHGIII
65	S(J,2) = S(J,2) - S(J,1)	CHGIII
C	(S(*,1) IS POINT P1 IN INERTIAL REFERENCE)	CHGIII
C	(S(*,2) IS VECTOR (P2-P1) IN INERTIAL REFERENCE)	CHGIII
C	(S(*,3) IS VECTOR (P3-P2) IN INERTIAL REFERENCE)	CHGIII
	CALL CROSS (S(1,3),S(1,2),T2)	CHGIII
	ABST = DSQRT(T2(1)**2 + T2(2)**2 + T2(3)**2)	CHGIII
	DO 66 J=1,3	CHGIII
66	T2(J) = T2(J)/ABST	CHGIII
C	(T2 IS T, THE NORMALIZED PLANE VECTOR IN INERTIAL REFERENCE)	CHGIII
	MI = NL(1,M)	CHGIII
	MS = IABS(IBAR(1,MI))	CHGIII
	IF (MS.GT.100) MS = MOD(MS,100)	CHGIII
	ME = IBAR(2,MI)	CHGIII
	CALL MAT31 (D(1,1,MS),T2,T1)	CHGIII
C	(T1 IS T IN ELLIPSOID REFERENCE OF NEW POINT M)	CHGIII
	D1 = T2(1)*S(1,1) + T2(2)*S(2,1) + T2(3)*S(3,1)	CHGIII
	D2 = T1(1)*BAR(7,MI) + T1(2)*BAR(8,MI) + T1(3)*BAR(9,MI)	CHGIII
	D3 = T2(1)*SEGLP(1,MS) + T2(2)*SEGLP(2,MS) + T2(3)*SEGLP(3,MS)	CHGIII
	DD = D1 - D2 - D3	CHGIII

C	(DD IS D, THE DISTANCE OF ELLIPSOID CENTER TO PLANE)	CHGIII
	CALL MAT31 (BD(16,ME),T1,R)	CHGIII
	BX = DD/(T1(1)*R(1) + T1(2)*R(2) + T1(3)*R(3))	CHGIII
	D4 = T1(1)*BAR(4,MI) + T1(2)*BAR(5,MI) + T1(3)*BAR(6,MI)	CHGIII
	DO 67 J=1,3	CHGIII
	R(J) = BX*R(J)	CHGIII
C	(R IS S, THE CENTER OF THE ELLIPSE)	CHGIII
67	V(J) = BAR(J+3,MI) + (DD-D4)*T1(J)	CHGIII
C	(BAR(J+3,MI) IS P, THE NEW POINT TO BE ADDED)	CHGIII
C	(V IS Q, THE PROJECTION OF POINT P ONTO THE PLANE)	CHGIII
	AX = DSQRT( (BX*DD-1.0) / (BX*DD-XDY(V,BD(7,ME),V)) )	CHGIII
	DO 68 J=1,3	CHGIII
68	BAR(J+3,MI) = R(J) + AX*(V(J)-R(J))	CHGIII
C	(BAR(J+3,MI) IS R = S + A(Q - S), Q EXTENDED TO ELLIPSOID)	CHGIII
	GO TO 43	HBPLAY
C		HBPLAY
C	POINT N+1 IS DROPPED.	HBPLAY
C		HBPLAY
41	M0 = M	HBPLAY
	N0 = N	HBPLAY
	LTEST = 1	HBPLAY
42	N = N+1	HBPLAY
43	IF (NL(1,M+1)-IJK(N+1,1)) 40,44,42	HBPLAY
C		HBPLAY
C	POINTS N0 TO N+1 ARE BEING REPLACED WITH POINTS M0 TO M+1.	HBPLAY
C		HBPLAY
44	SUMBL = 0.0	HBPLAY
	DO 45 J=M0,M	HBPLAY
45	SUMBL = SUMBL + BL(J)	HBPLAY
	SUMPL = 0.0	HBPLAY
	SUMBB = 0.0	HBPLAY
	DO 46 J=N0,N	HBPLAY
	SUMPL = SUMPL + PTLOSS(J,1)	HBPLAY
46	SUMBB = SUMBB + OLDBB(J)	HBPLAY
	RATPL = SUMPL/SUMBL	HBPLAY
	RATIO = SUMBB/SUMBL	HBPLAY
	DO 47 J=M0,M	HBPLAY
	PLOSS(1,J) = RATPL*BL(J)	HBPLAY
47	BB(J) = RATIO*BL(J)	HBPLAY
	GO TO 38	HBPLAY
51	JNL = N+1	HBPLAY
	IF (LTEST.EQ.0) GO TO 79	HBPLAY
C		HBPLAY
C	PRINT NEW POINT ARRAY IF DIFFERENT.	HBPLAY
C		HBPLAY
52	NPTS = LL - L1	HBPLAY
	USEC = 1000.0*TIME	HBPLAY
	WRITE (6,53) USEC,NH,NB,NPTS,NTHRNS(NB)	HBPLAY
53	FORMAT ('0 HBPLAY TIME =',F10.3,' MSEC. NH,NB,NPTS NT=',4I6)	HBPLAY
	WRITE (6,54) (NL(1,J),J=L2,LL)	HBPLAY
54	FORMAT (' NL(1)=',15I8/(8X,15I8))	HBPLAY
	WRITE (6,55) (BB(J),J=L2,L3)	HBPLAY

```
55  FORMAT ('  BB   =',6X,14F8.3/(6X,15F8.3))
79  K1 = K2 + 1
80  NPTPLY(NB) = LL - L1
    J1 = J2 + 1
90  CONTINUE
99  RETURN
    END
```

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HBPLAY
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	SUBROUTINE HEDING (LINES,LPP)		HEDING
C		REV IV 02/01/88MISDOT	
	IMPLICIT REAL*8 (A-H,O-Z)		HEDING
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		HEDING
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/JBARTZ/ MNPL( 30),MNBLT( 8),MNSEG( 30),MNBAG( 6),		HEDING
*	MPL(3,5,30),MBLT(3,5,8),MSEG(3,5,30),MBAG(3,10,6),		HEDING
*	NTPL( 5,30),NTBLT( 5,8),NTSEG( 5,30)		HEDING
	COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),		HEDING
*	BLTTTL(5,8),PLTTL(5,30),BAGTTL(5,6),SEG(30),		HEDING
*	JOINT(30),CGS(30),JS(30)		HEDING
	REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTL,BAGTTL,SEG,JOINT		HEDING
	LOGICAL*1 CGS,JS		HEDING
	COMMON/FORCES/PSF(7,70),BSF(4,20),SSF(10,40),BAGSF(3,20),		NCFORC
*	PRJNT(7,30),NPANEL(5),NPSF,NBSF,NSSF,NBSGF		HEDING
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),		HEDING
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI		TWOPI
	COMMON/RSAVE/ XSG(3,20,3),DPMI(3,3,30),LPMI(30),		ATBIII
*	NSG(9),MSG(20,9),MCG,MCGIN(24,5),KREF(20,9)		TTHKREF
	COMMON/DAMPER/ APSDM(3,20),APSDN(3,20),ASD(5,20),MSDM(20),MSDN(20)		HEDING
	COMMON/HRNESS/ BAR(15,100),BB(100),BBDOT(100),PLOSS(2,100),		HEDING
*	XLONG(20),HTIME(2),IBAR(5,100),NL(2,100),		HEDING
*	NPTSPB(20),NPTPLY(20),NTHRNS(20),NBLTPH(5)		HEDING
C	NOTE: SUBROUTINES POSTPR & HEDING SHARE THIS COMMON/TEMPVS/.		HEDING
C	SEE COMMENT IN POSTPR ABOUT FIRST DIMENSION OF PLDATA.		HEDING
	REAL HEAD,PHED,BLANK,PLDATA,USEC,ZTTH,AHED,AHEAD,GHED,ZZZ		PLTINC
	COMMON/TEMPVS/ TDATA(14,65),HEAD(20),NOPL(150),MOPL(150),		CHGIII
*	M1PL(150),PLDATA(97,20),USEC(45),ZZZ(1000,25),ZTTH(14,45,65)		MISDOT
*	,IDMMY		80386
	LOGICAL LOLD , LNEW		HEDING
	DIMENSION PHED(5),HEDJ(4,2),HEADJJ(4,2),HEADR(20)		TTHKREF
	DATA HEDJ/8HIPIN FL,8HEXURE A,8HZIMUTH ,8HTORSION ,		HEDING
*	8HIEULER ,8HPREC. N,8HUTATION ,8H SPIN /		HEDING
	DIMENSION AHED(5,2),AHEAD(5,20),GHED(2)		ACCEL
	DATA AHED/4H IN ,4H ,4H REF,4HEREN,4HCE ,		ACCEL
*	4H AC,4HCELE,4HROME,4HTER ,4H /		ACCEL
	DATA GHED/4H(OG),4H(1G)/		ACCEL
	DATA BLANK/4H /		HEDING
	DATA PHED/4HSPRF,4HPNL1,4HPNL2,4HPNL3,4HPNL4/		HEDING
	NPRT4 = NPRT(4) + 4		HEDING
	IF (NPRT4.LE.0 .OR. NPRT4.GT.8) STOP 40		HEDING
	GO TO (11,11,82,12,12,11,11,12) , NPRT4		HEDING
11	LOLD = .FALSE.		HEDING
	LNEW = .TRUE.		HEDING
	GO TO 13		HEDING
12	LOLD = .TRUE.		HEDING
	LNEW = .FALSE.		HEDING
13	MT = 20		HEDING
	NLINES = MOD(LINES-1,LPP)+1		HEDING
	XPAGE = 0.01*FLOAT((LINES + LPP-1)/LPP)		HEDING
C			HEDING
C	NOTE: MT WILL BE THE PAGE OR OUTPUT UNIT COUNTER		HEDING

C	NT WILL BE THE ACTUAL OUTPUT UNIT NUMBER	HEDING
C	IT WILL BE THE INDEX TO THE DATA ARRAY	HEDING
C	NLINES WILL BE THE NUMBER OF LINES TO BE PRINTED	HEDING
C		HEDING
C		HEDING
C	EVERY LPP LINES PRINT HEADINGS FOR 9 TYPES OF OUTPUT ABOVE.	WINDOP
C		HEDING
	DO 20 K=1,9	WINDOP
	IF (NSG(K).LE.0) GO TO 20	HEDING
	KSG = NSG(K)	HEDING
	IF (K.EQ.9) GO TO 455	WINDOP
	J3 = 3	HEDING
	IF (K.EQ.7) J3 = 2	HEDING
	DO 19 J1=1,KSG,J3	HEDING
	MT = MT + 1	HEDING
	NT = MT	HEDING
	IF (LNEW) NT = 6	HEDING
	IT = MT - 20	HEDING
	PAGE = FLOAT(MT) + XPAGE	HEDING
C	P & E PRINTER CARRIAGE CONTROL	PECONV
C	CALL CARCON(NT,1)	80386
	IF (NT.EQ.6) WRITE(NT,121) DATE,BLANK,NPG	PAGE
	IF (NT.NE.6) WRITE(NT,121) DATE	PAGE
	IF (NT.EQ.6) NPG=NPG+1	PAGE
	WRITE (NT,21) COMENT,PAGE,VPSTTL,BDYTTL	PAGE
	IF (K.EQ.1) WRITE (NT,22)	TTHKREF
	IF (K.EQ.2) WRITE (NT,23) UNITL,UNITT	TTHKREF
	IF (K.EQ.3) WRITE (NT,24) UNITL	TTHKREF
	IF (K.EQ.4) WRITE (NT,25) UNITT	TTHKREF
	IF (K.EQ.5) WRITE (NT,26) UNITT	TTHKREF
	IF (K.EQ.6) WRITE (NT,27)	TTHKREF
	IF (K.EQ.7) WRITE (NT,28)	HEDING
	IF (K.EQ.8) WRITE(NT,200) UNITM	TTHKREF
	J2 = MINO(J1+J3-1,KSG)	HEDING
	DO 14 J=J1,J2	HEDING
	KK = MSG(J,K)	HEDING
	HEAD(J) = SEG(IABS(KK))	ACCEL
	IF ((K.LT.7).OR.(K.EQ.8)) GO TO 214	TTHKREF
	KK = IABS(KK)	HEDING
	HEAD(J) = JOINT(KK)	HEDING
	JJ2 = J-J1+1	HEDING
	K2 = 1	HEDING
	IF (MSG(J,K).LT.0) K2 = 2	HEDING
	DO 35 K1=1,4	HEDING
	35 HEADJJ(K1,JJ2) = HEDJ(K1,K2)	HEDING
	GO TO 14	TTHKREF
	214 IF (MSG(J,K).LT.0) GOTO 302	ACCEL
	IF (KREF(J,K).EQ.0) HEADR(J)=SEG(NVEH)	ACCEL
	IF (K.EQ.8) HEADR(J)=SEG(NGRND)	TTHKREF
	IF (K.EQ.1 .OR. K.EQ.4) HEADR(J)=SEG(KK)	TTHKREF
	IF (KREF(J,K).NE.0) HEADR(J)=SEG(KREF(J,K))	TTHKREF
	DO 301 II=1,5	ACCEL

301	AHEAD(II,J)=AHED(II,1)	ACCEL
	AHEAD(2,J)=HEADR(J)	ACCEL
	GOTO 14	ACCEL
302	HEADR(J)=SEG(IABS(KK))	ACCEL
	DO 303 II=1,4	ACCEL
303	AHEAD(II,J)=AHED(II,2)	ACCEL
	AHEAD(5,J)=GHED(KREF(J,K)+1)	ACCEL
14	CONTINUE	HEDING
	IF (K.LE.3) WRITE (NT,29) (BLANK,(XSG(I,J,K),I=1,3),J=J1,J2)	HEDING
	IF (K.LE.6) WRITE (NT,30) (BLANK,MSG(J,K),HEAD(J),J=J1,J2)	HEDING
	IF (K.EQ.8) WRITE (NT,30) (BLANK,MSG(J,K),HEAD(J),J=J1,J2)	WINDOP
	IF (K.LE.6 .OR. K.EQ.8) WRITE (NT,230)	ACCEL
	* (BLANK,(AHEAD(II,J),II=1,5),J=J1,J2)	ACCEL
	IF ((K.LE.5).OR.(K.EQ.8)) WRITE (NT,31) (BLANK,J=J1,J2)	WINDOP
	IF (K.EQ.6) WRITE (NT,32) (BLANK,J=J1,J2)	HEDING
	IF ((K.LT.7).OR.(K.EQ.8)) GOTO 15	WINDOP
	WRITE (NT,33) (BLANK,MSG(J,K),HEAD(J),J=J1,J2)	HEDING
	WRITE (NT,36) (BLANK,UNITL,UNITM,J=J1,J2)	HEDING
	WRITE (NT,37) (BLANK,(HEADJJ(K1,J),K1=1,4),J=1,JJ2)	HEDING
15	WRITE (NT,38)	HEDING
	IF (.NOT.LNEW) GO TO 19	HEDING
	IF (K.EQ.7) GO TO 17	HEDING
	JJ = 4*(J2-J1+1)	HEDING
	DO 16 I=1,NLINES	HEDING
16	WRITE (NT,39) USEC(I),(ZTTH(J,I,IT),J=1,JJ)	HEDING
	GO TO 19	HEDING
17	JJ = 7*(J2-J1+1)	HEDING
	DO 18 I=1,NLINES	HEDING
18	WRITE (NT,40) USEC(I),(ZTTH(J,I,IT),J=1,JJ)	HEDING
19	CONTINUE	HEDING
	GO TO 20	CHGIII
C		CHGIII
C	PRINT HEADING FOR JOINT FORCES & TORQUES	CHGIII
C		CHGIII
455	CONTINUE	CHGIII
	DO 860 II=1,KSG	CHGIII
	IF(KREF(II,K).EQ.0) KRF = NVEH	TTHKREF
	IF(KREF(II,K).NE.0) KRF = KREF(II,K)	TTHKREF
	JRF = MSG(II,9)	WINDOP
	MT = MT + 1	CHGIII
	NT = MT	CHGIII
	IF (LNEW) NT = 6	CHGIII
C	P & E CARRIAGE CONTROL	PECONV
C	CALL CARCON(NT,1)	80386
	IT = MT - 20	CHGIII
	PAGE = FLOAT (MT) + XPAGE	CHGIII
	IF (NT.EQ.6) WRITE(NT,121) DATE,BLANK,NPG	PAGE
	IF (NT.NE.6) WRITE(NT,121) DATE	PAGE
	IF (NT.EQ.6) NPG=NPG+1	PAGE
	WRITE (NT,21) COMENT,PAGE,VPSTTL,BDYTTL	PAGE
	WRITE (NT,850) JOINT(JRF),SEG(JRF+1),SEG(KRF)	OUT385
	WRITE (NT,38)	CHGIII

WRITE (NT,851) UNITM,UNITL,UNITM	CHGIII
WRITE (NT,852)	CHGIII
WRITE (NT,38)	CHGIII
IF (.NOT.LNEW) GO TO 857	CHGIII
DO 858 JK=1,NLINES	CHGIII
WRITE (NT,856) USEC(JK),(ZTTH(J,JK,IT),J=1,6)	CHGIII
858 CONTINUE	CHGIII
857 CONTINUE	CHGIII
850 FORMAT(' '/47X,	TTHKREF
* A4,' JOINT FORCES & TORQUES ON ',A4,' IN ',A4,' REFERENCE')	OUT385
851 FORMAT(4X,4HTIME,7X,13HJOINT FORCE (,A4,7H 10**2),10X,	CHGIII
*14HJOINT TORQUE (,A4,1H-,A4,7H 10**2))	CHGIII
852 FORMAT(3X,6H(MSEC),8X,1HX,8X,1HY,8X,1HZ,14X,1HX,11X,1HY,11X,1HZ)	CHGIII
856 FORMAT(F9.3,3X,3F9.3,3X,3(2X,D10.3))	CHGIII
860 CONTINUE	CHGIII
20 CONTINUE	HEDING
121 FORMAT('1',18X,'DATE:',3X,4A4,80X,'PAGE',I5)	PAGE
21 FORMAT(8X,'RUN DESCRIPTION:',3X,20A4/27X,20A4,'PAGE:',F6.2/	PAGE
* 3X,'VEHICLE DECELERATION:',3X,20A4/	HEDING
* 11X,'CRASH VICTIM:',3X,5A4 )	HEDING
22 FORMAT(' '47X,	TTHKREF
* 'POINT TOTAL ACCELERATION (G'S)'/)	TTHKREF
23 FORMAT(' '47X,	TTHKREF
* 'POINT REL. VELOCITY (' ,A4,'/' ,A4,')'/)	TTHKREF
24 FORMAT(' '47X,	TTHKREF
* 'POINT REL. LINEAR DISPLACEMENT (' ,A4,')'/)	TTHKREF
25 FORMAT(' '/47X,	TTHKREF
* 'SEGMENT ANGULAR ACCELERATION (REV/' ,A4,'**2)'/)	TTHKREF
26 FORMAT(' '/47X,	TTHKREF
* 'SEGMENT REL. ANGULAR VELOCITY (REV/' ,A4,')'/)	TTHKREF
27 FORMAT(' '/47X,	TTHKREF
* 'SEGMENT REL. ANGULAR DISPLACEMENT (DEG)'/)	TTHKREF
28 FORMAT(' '/47X,'JOINT PARAMETERS'//)	TTHKREF
200 FORMAT(' '/47X,'SEGMENT WIND FORCE (' ,A4,')'/)	TTHKREF
29 FORMAT(9X,3(A4,3X,'POINT (' ,F6.2,' ,F6.2,' ,F6.2,') ON '))	HEDING
30 FORMAT(' ' ,3(A4,9X,'SEGMENT NO.',I3,' - ' ,A4,5X) )	TTHKREF
230 FORMAT(' TIME ' ,3(A4,9X,5A4,6X))	ACCEL
31 FORMAT(' (MSEC)' ,3(A4,5X,'X',8X,'Y',8X,'Z',7X,'RES',1X) )	HEDING
32 FORMAT(' (MSEC)' ,3(A4,4X,'YAW',5X,'PITCH',5X,'ROLL',5X,'RES '))	HEDING
33 FORMAT(9X,2(A1,21X,'JOINT NO.',I3,' - ' ,A4,20X) )	HEDING
36 FORMAT(' TIME ' ,2(A1,'STATE',5X,'JOINT ANGLES (DEG)',8X,	HEDING
* 'TOTAL TORQUE (' ,2A4,') '))	HEDING
37 FORMAT(' (MSEC)' ,2(A1,4A8,4X,'SPRING VISCOUS RES. '))	HEDING
38 FORMAT(1X)	HEDING
39 FORMAT(F9.3,3(3X,4F9.3) )	HEDING
40 FORMAT(F9.3,2(F5.0,3F9.3,2X,3F9.3))	HEDING
C	ATBIII
C PRINT BODY PROPERTIES CONTROLLED BY H.10 CARDS	WINDOP
C	ATBIII
IF (MCG.EQ.0) GO TO 131	ATBIII
DO 130 NCG=1,MCG	ATBIII
MT = MT +1	ATBIII

	NT = MT	ATBIII
	IF (LNEW) NT = 6	ATBIII
C	P & E CARRIAGE CONTROL	PECONV
C	CALL CARCON(NT,1)	80386
	IT = MT - 20	ATBIII
	PAGE = FLOAT(MT) + XPAGE	ATBIII
	IF (NT.EQ.6) WRITE(NT,121) DATE,BLANK,NPG	PAGE
	IF (NT.NE.6) WRITE(NT,121) DATE	PAGE
	IF (NT.EQ.6) NPG=NPG+1	PAGE
	WRITE (NT,21) COMENT,PAGE,VPSTTL,BDYTTL	PAGE
	M = MCGIN(1,NCG)	ATBIII
	WRITE (NT,132) M,SEG(M)	ATBIII
	N = MCGIN(2,NCG)	ATBIII
	WRITE (NT,133) (MCGIN(I+2,NCG),I-1,N)	ATBIII
	WRITE (NT,38)	ATBIII
	WRITE (NT,134) UNITL,UNITM,UNITT,UNITL,UNITM,UNITT,UNITM,UNITL	KINETIC
	WRITE (NT,38)	ATBIII
	IF (.NOT.LNEW) GO TO 130	ATBIII
	DO 129 I=1,NLINES	ATBIII
	129 WRITE (NT,135) USEC(I),(ZTTH(J,I,IT),J=1,12)	KINETIC
	130 CONTINUE	ATBIII
	131 CONTINUE	ATBIII
	132 FORMAT(' ',47X,39HBODY PROPERTIES - REFERENCE SEGMENT NO.,	TTMKREF
	* I3,2H(,A4,1H) )	ATBIII
	133 FORMAT(15X,21HINCLUDED SEGMENT NOS: ,20I3)	ATBIII
	134 FORMAT(14X,17HCENTER OF GRAVITY,13X,15HLINEAR MOMENTUM,17X,	KINETIC
	* 16HANGULAR MOMENTUM,18X,14HKINETIC ENERGY/	KINETIC
	* 4X,4HTIME,11X,1H(,A4,1H),21X,1H(,A4,1H-,A4,1H),19X,	KINETIC
	* 1H(,A4,1H-,A4,1H-,A4,1H),20X,1H(,A4,1H-,A4,1H)/	MISC
	* 3X,6H(MSEC),5X,1HX,7X,1HY,7X,1HZ,	KINETIC
	* 2(10X,1HX,10X,1HY,10X,1HZ),6X,6HLINEAR,5X,	KINETIC
	* 7HANGULAR,5X,5HTOTAL)	KINETIC
	135 FORMAT(F9.3,3F8.3,9(1X,D10.3))	KINETIC
C		HEDING
C	PLANE FORCES HEADINGS	HEDING
C		HEDING
	MPSF = 0	HEDING
	IF (NPL.EQ.0) GO TO 52	HEDING
	IF (NPRT(18).EQ.1.OR.NPRT(18).EQ.7) GO TO 52	VARTTH
	IF (NPRT(18).EQ.10.OR.NPRT(18).EQ.11) GO TO 52	VARTTH
	IF (NPRT(18).GE.14) GO TO 52	VARTTH
	DO 42 J=1,NPL	HEDING
	IF (MNPL(J).EQ.0) GO TO 42	HEDING
	KPL = MNPL(J)	HEDING
	DO 41 I=1,KPL	HEDING
	MPSF = MPSF+1	HEDING
	NOPL(MPSF) = J	HEDING
	IF (MPL(3,I,J).LT.0) M1PL(MPSF) = MPL(2,I,J)	CHGIII
	IF (MPL(3,I,J).GE.0) M1PL(MPSF) = MPL(1,I,J)	CHGIII
	41 MOPL(MPSF) = MPL(2,I,J)	HEDING
	42 CONTINUE	HEDING
	IF (MPSF.EQ.0) GO TO 52	HEDING

	DO 44 J1=1,MPSF,2	HEDING
	J2 = MINO(J1+1,MPSF)	HEDING
	MT = MT + 1	HEDING
	NT = MT	HEDING
	IF (LNEW) NT = 6	HEDING
C	P & E CARRIAGE CONTROL	PECONV
C	CALL CARCON(NT,1)	80386
	IT = MT - 20	HEDING
	PAGE = FLOAT(MT) + XPAGE	HEDING
	IF (NT.EQ.6) WRITE(NT,121) DATE,BLANK,NPG	PAGE
	IF (NT.NE.6) WRITE(NT,121) DATE	PAGE
	IF (NT.EQ.6) NPG=NPG+1	PAGE
	WRITE (NT,21) COMENT,PAGE,VPSTTL,BDYTTL	PAGE
	WRITE (NT,45)	HEDING
	N1 = NOPL(J1)	HEDING
	N2 = NOPL(J2)	HEDING
	M1 = MOPL(J1)	HEDING
	M2 = MOPL(J2)	HEDING
	MM1 = M1PL(J1)	CHGIII
	MM2 = M1PL(J2)	CHGIII
	IF (J1.EQ.J2) WRITE (NT,46)	HEDING
*	BLANK,N1,( PLTTL(I,N1),I=1,5),M1,SEG(M1)	HEDING
	IF (J1.NE.J2) WRITE (NT,46)	HEDING
*	BLANK,N1,( PLTTL(I,N1),I=1,5),M1,SEG(M1),	HEDING
*	BLANK,N2,( PLTTL(I,N2),I=1,5),M2,SEG(M2)	HEDING
	WRITE (NT,47) (BLANK,UNITL,J=J1,J2)	HEDING
	IF (J1.EQ.J2) WRITE (NT,48) BLANK,SEG(MM1)	CHGIII
	IF (J1.NE.J2) WRITE (NT,448) BLANK,SEG(MM1),BLANK,SEG(MM2)	CHGIII
	WRITE (NT,49) (BLANK,UNITL,UNITM,UNITM,UNITM,J=J1,J2)	HEDING
	WRITE (NT,38)	HEDING
	IF (.NOT.LNEW) GO TO 44	HEDING
	JJ = 7*(J2-J1+1)	HEDING
	DO 43 I=1,NLINES	HEDING
	43 WRITE (NT,50) USEC(I),(ZTTH(J,I,IT),J=1,JJ)	HEDING
	44 CONTINUE	HEDING
	45 FORMAT(27X,'CONTACT FORCES - SEGMENT PANELS VS. SEGMENTS' )	CHGIII
	46 FORMAT(' '/8X,2(A4,' PANEL',I3,' (' ,5A4,' ) VS. SEGMENT',I3,	HEDING
	* ' (' ,A4,' ) ' )	HEDING
	47 FORMAT(' ',8X,A4,'DEFL- NORMAL FRICTION RESULTANT CONTACT LOCATHEDING	HEDING
	*ION (' ,A4,' )',A2,'DEFL- NORMAL FRICTION RESULTANT CONTACT LOCATHEDING	HEDING
	*ION (' ,A4,' )')	HEDING
	48 FORMAT(' TIME',A4,'ECTION FORCE FORCE FORCE (' ,A4 CHGIII	CHGIII
	*,' REFERENCE')' )	CHGIII
	448 FORMAT(' TIME',A4,'ECTION FORCE FORCE FORCE (' ,A4 CHGIII	CHGIII
	*,' REFERENCE'),'2X,A4,'ECTION FORCE FORCE FORCE (' ,A4 CHGIII	CHGIII
	*,' REFERENCE')' )	CHGIII
	49 FORMAT(' (MSEC)',2(A3,' (' ,A4,' )',2X,' (' ,A4,' )',4X,' (' ,A4,' )',3X,	HEDING
	* ' (' ,A4,' , X Y Z ' ) )	HEDING
	50 FORMAT(F9.3,2(F9.3,3F9.2,3F8.3) )	HEDING
	51 FORMAT(3X,'(MSEC)',4(A1,9X,'X',8X,'Y',8X,'Z',1X))	HEDING
C		HEDING
C	BELT FORCES HEADINGS	HEDING

C		HEDING
	52 MBSF = 0	HEDING
	IF (NPRT(18).EQ.2.OR.NPRT(18).GE.13) GO TO 83	VARTTH
	IF (NPRT(18).GE.7.AND.NPRT(18).LE.9) GO TO 83	VARTTH
	IF (NBLT.EQ.0) GO TO 83	HEDING
	DO 54 J=1,NBLT	HEDING
	IF (MNBLT(J).EQ.0) GO TO 54	HEDING
	MBSF = MBSF+1	HEDING
	NOPL(MBSF) = J	HEDING
	MOPL(MBSF) = MBLT(2,1,J)	HEDING
	54 CONTINUE	HEDING
	IF (MBSF.EQ.0) GO TO 83	HEDING
	DO 56 J1=1,MBSF,2	HEDING
	J2 = MINO(J1+1,MBSF)	HEDING
	MT = MT + 1	HEDING
	NT = MT	HEDING
	IF (LNEW) NT = 6	HEDING
C	P & E CARRIAGE CONTROL	PECONV
C	CALL CARCON(NT,1)	80386
	IT = MT - 20	HEDING
	PAGE = FLOAT(MT) + XPAGE	HEDING
	IF (NT.EQ.6) WRITE(NT,121) DATE,BLANK,NPG	PAGE
	IF (NT.NE.6) WRITE(NT,121) DATE	PAGE
	IF (NT.EQ.6) NPG=NPG+1	PAGE
	WRITE (NT,21) COMENT,PAGE,VPSTTL,RDYTTL	PAGE
	WRITE (NT,57)	HEDING
	N1 = NOPL(J1)	HEDING
	N2 = NOPL(J2)	HEDING
	M1 = MOPL(J1)	HEDING
	M2 = MOPL(J2)	HEDING
	IF (J1.EQ.J2) WRITE (NT,58)	HEDING
	* BLANK,N1,(BLTTTL(I,N1),I=1,5),M1,SEG(M1)	HEDING
	* IF (J1.NE.J2) WRITE (NT,58)	HEDING
	* BLANK,N1,(BLTTTL(I,N1),I=1,5),M1,SEG(M1),	HEDING
	* BLANK,N2,(BLTTTL(I,N2),I=1,5),M2,SEG(M2)	HEDING
	WRITE (NT,59) (BLANK,J=J1,J2)	HEDING
	WRITE (NT,60) (BLANK,J=J1,J2)	HEDING
	WRITE (NT,61) (BLANK,UNITL,UNITL,UNITM,UNITL,UNITL,UNITM,J=J1,J2)	HEDING
	WRITE (NT,38)	HEDING
	IF (.NOT.LNEW) GO TO 56	HEDING
	JJ = 4*(J2-J1+1)	HEDING
	DO 55 I=1,NLINES	HEDING
	55 WRITE (NT,62) USEC(I),(ZTTH(J,I,IT),J=1,JJ)	HEDING
	56 CONTINUE	HEDING
	57 FORMAT('0',26X,'CONTACT FORCES - BELTS VS. SEGMENTS')	HEDING
	58 FORMAT(' ',7X,2(A4,' BELT',I3,' (' ,5A4,' ) VS. SEGMENT',I3,	HEDING
	* ' (' ,A4,' ) ' )	HEDING
	59 FORMAT(' ',2X,2(A4,11X,'ANCHOR POINT A',14X,'ANCHOR POINT B'))	HEDING
	60 FORMAT(4X,'TIME',2(A4,5X,'STRAIN',7X,'FORCE',12X,	HEDING
	* 'STRAIN',7X,'FORCE',3X) )	HEDING
	61 FORMAT(3X,'(MSEC)',2(A4,2X,' (' ,A4,' / ' ,A4,' )',4X,' (' ,A4,' )',9X,	HEDING
	* ' (' ,A4,' / ' ,A4,' )',4X,' (' ,A4,' )',3X) )	HEDING

62	FORMAT(F9.3,4(F15.6,F12.2,3X) )	HEDING
C		HEDING
C	HARNES BELT ENDPOINTS FORCES HEADINGS	HEDING
C		HEDING
83	IF (NHRNSS.LE.0) GO TO 91	HEDING
	MBSF = 0	HEDING
	IF (NPRT(18).EQ.3.OR.NPRT(18).EQ.11) GO TO 91	VARTTH
	IF (NPRT(18).EQ.9.OR.NPRT(18).EQ.8) GO TO 91	VARTTH
	IF (NPRT(18).EQ.13.OR.NPRT(18).EQ.14) GO TO 91	VARTTH
	IF (NPRT(18).EQ.16) GO TO 91	VARTTH
	J1 = 1	HEDING
	K1 = 1	HEDING
	DO 85 I=1,NHRNSS	HEDING
	IF (NBLTPH(I).LE.0) GO TO 85	HEDING
	J2 = J1 + NBLTPH(I) - 1	HEDING
	DO 84 J=J1,J2	HEDING
	MBSF = MBSF + 1	HEDING
	IF (NPTSPB(J).LE.0) GO TO 84	HEDING
	K2 = K1 + NPTSPB(J) - 1	HEDING
	NOPL(2*MBSF-1) = J	HEDING
	NOPL(2*MBSF ) = I	HEDING
	MOPL(2*MBSF-1) = K1	HEDING
	MOPL(2*MBSF ) = K2	HEDING
	K1 = K2 + 1	HEDING
84	CONTINUE	HEDING
	J1 = J2 + 1	HEDING
85	CONTINUE	HEDING
	DO 87 J1=1,MBSF,2	HEDING
	J2 = MINO(J1+1,MBSF)	HEDING
	MT = MT + 1	HEDING
	NT = MT	HEDING
	IF (LNEW) NT = 6	HEDING
C	P & E CARRIAGE CONTROL	PECONV
C	CALL CARCON(NT,1)	80386
	IT = MT - 20	HEDING
	PAGE = FLOAT(MT) + XPAGE	HEDING
	IF (NT.EQ.6) WRITE(NT,121) DATE,BLANK,NPG	PAGE
	IF (NT.NE.6) WRITE(NT,121) DATE	PAGE
	IF (NT.EQ.6) NPG=NPG+1	PAGE
	WRITE (NT,21) COMENT,PAGE,VPSTTL,BDYTTL	PAGE
	WRITE (NT,88)	HEDING
	WRITE (NT,89) (BLANK,NOPL(2*J-1),NOPL(2*J),J=J1,J2)	HEDING
	WRITE (NT,90) (BLANK,MOPL(2*J-1),MOPL(2*J),J=J1,J2)	HEDING
	WRITE (NT,60) (BLANK,J=1,J2)	HEDING
	WRITE (NT,61) (BLANK,UNITL,UNITL,UNITM,UNITL,UNITL,UNITM,J=J1,J2)	HEDING
	WRITE (NT,38)	HEDING
	IF (.NOT.LNEW) GO TO 87	HEDING
	JJ = 4*(J2-J1+1)	HEDING
	DO 86 I=1,NLINES	HEDING
86	WRITE (NT,62) USEC(I),(ZTTH(J,I,IT),J=1,JJ)	HEDING
87	CONTINUE	HEDING
88	FORMAT('0',26X,'HARNES SYSTEM BELT ENDPOINT FORCES')	HEDING



	89	FORMAT(9X,2(A4,11X,'BELT NO.',14,' OF HARNESS NO.',13,15X))	HEDING
	90	FORMAT(9X,2(A4,6X,'POINT NO.',15,16X,'POINT NO.',15,6X))	HEDING
C			HEDING
C		SPRING DAMPER FORCES HEADINGS	HEDING
C			HEDING
	91	IF (NSD.LE.0) GO TO 63	HEDING
		IF (NPRT(18).EQ.4.OR NPRT(18).EQ.9) GO TO 63	VARTTH
		IF (NPRT(18).GE.12) GO TO 63	VARTTH
		DO 94 J1=1,NSD,4	HEDING
		J2 = MINO(J1+3,NSD)	HEDING
		MT = MT + 1	HEDING
		NT = MT	HEDING
		IF (LNEW) NT = 6	HEDING
C		P & E CARRIAGE CONTROL	PECONV
C		CALL CARCON(NT,1)	80386
		IT = MT - 20	HEDING
		PAGE = FLOAT(MT) + XPAGE	HEDING
		IF (NT.EQ.6) WRITE(NT,121) DATE,BLANK,NPG	PAGE
		IF (NT.NE.6) WRITE(NT,121) DATE	PAGE
		IF (NT.EQ.6) NPG=NPG+1	PAGE
		WRITE (NT,21) COMENT,PAGE,VPSTTL,BDYTTL	PAGE
		WRITE (NT,95) (BLANK,J,J=J1,J2)	HEDING
		DO 92 J=J1,J2	HEDING
		M1 = MSDM(J)	HEDING
		N1 = MSDN(J)	HEDING
C		POSSIBLE OVERFLOW INTO NOPL ARRAY IS INTENTIONAL.	HEDING
		HEAD(2*J-1) = SEG(M1)	HEDING
	92	HEAD(2*J ) = SEG(N1)	HEDING
		WRITE (NT,96) (BLANK,MSDM(J),HEAD(2*J-1),MSDN(J),HEAD(2*J),J=J1,J2)	HEDING
		WRITE (NT,97) (BLANK,J=J1,J2)	HEDING
		WRITE (NT,98) (BLANK,UNITL,UNITM,J=J1,J2)	HEDING
		WRITE (NT,38)	HEDING
		IF (.NOT.LNEW) GO TO 94	HEDING
		JJ = 2*(J2-J1+1)	HEDING
		DO 93 I=1,NLINES	HEDING
	93	WRITE (NT,99) USEC(I),(ZTTH(J,I,IT),J=1,JJ)	HEDING
	94	CONTINUE	HEDING
	95	FORMAT('0',26X,'SPRING DAMPER FORCES'/	HEDING
		* 9X,4(A3,3X,'SPRING DAMPER NO.',13,4X))	HEDING
	96	FORMAT(9X,4(A3,'SEG',I3,'(' ,A4,') - SEG',I3,'(' ,A4,')'))	HEDING
	97	FORMAT(4X,'TIME',1X,4(A3,5X,'LENGTH',7X,'FORCE',4X))	HEDING
	98	FORMAT(3X,'(MSEC)',4(A3,5X,'(' ,A4,') ',6X,'(' ,A4,') ',4X))	HEDING
	99	FORMAT (F9.3,4(F14.3,F12.2,4X))	HEDING
C			HEDING
C		SEGMENT FORCES HEADINGS	HEDING
C			HEDING
	63	MSSF = 0	HEDING
		IF (NPRT(18).EQ.5.OR.NPRT(18).EQ.13) GO TO 161	VARTTH
		IF (NPRT(18).EQ.10.OR.NPRT(18).EQ.11) GO TO 161	VARTTH
		IF (NPRT(18).GE.15) GO TO 161	VARTTH
		DO 65 J=1,NSEG	HEDING
		IF (MNSEG(J).EQ.0) GO TO 65	HEDING

LSEG = MNSEG(J)	HEDING
DO 64 I=1,LSEG	HEDING
MSSF = MSSF+1	HEDING
NOPL(MSSF) = J	HEDING
64 MOPL(MSSF) = MSEG(2,I,J)	HEDING
65 CONTINUE	HEDING
IF (MSSF.EQ.0) GO TO 70	HEDING
DO 67 J=1,MSSF	HEDING
MT = MT + 1	HEDING
NT = MT	HEDING
IF (LNEW) NT = 6	HEDING
C P & E CARRIAGE CONTROL	PECONV
C CALL CARCON(NT,1)	80386
IT = MT - 20	HEDING
PAGE = FLOAT(MT) + XPAGE	HEDING
IF (NT.EQ.6) WRITE(NT,121) DATE,BLANK,NPG	PAGE
IF (NT.NE.6) WRITE(NT,121) DATE	PAGE
IF (NT.EQ.6) NPG=NPG+1	PAGE
WRITE (NT,21) COMENT,PAGE,VPSTTL,BDYTTL	PAGE
N1 = NOPL(J)	HEDING
M1 = MOPL(J)	HEDING
WRITE (NT,68) N1,SEG(N1),M1,SEG(M1),UNITL,N1,M1	HEDING
* ,UNITL,UNITM,UNITM,UNITM	HEDING
IF (.NOT.LNEW) GO TO 67	HEDING
DO 66 I=1,NLINES	HEDING
66 WRITE (NT, 69) USEC(I),(ZTTH(JJ,I,IT),JJ=1,10)	HEDING
67 CONTINUE	HEDING
68 FORMAT('0',26X,'CONTACT FORCES - SEGMENT NO.',I3,' ('',A4,	HEDING
* ' ) VS. SEGMENT NO.',I3,' ('',A4,'')'//	HEDING
* 13X,'DEFL- NORMAL FRICTION RESULTANT',	HEDING
* 14X,'CONTACT LOCATION ('',A4,'')'/	HEDING
* 4X,'TIME ECTION',3(3X,'FORCE',1X),	HEDING
* 2(' SEG.',I3,' LOCAL REFERENCE ')/	HEDING
* 3X,'(MSEC)',3X,'('',A4,'')', 3(3X,'('',A4,'')'),	HEDING
* 2(5X,'X',7X,'Y',7X,'Z',4X)/1X)	HEDING
69 FORMAT(2F9.3,3F9.2,3F8.3,2X,3F8.3)	HEDING
161 CONTINUE	VARTTH
C	HEDING
C AIRBAG FORCES HEAD!	HEDING
C	HEDING
70 IF (NBAG.EQ.0) GO TO 82	HEDING
IF (NPRT(18).EQ.6.OR.NPRT(18).EQ.9) GO TO 82	VARTTH
IF (NPRT(18).GE.12) GO TO 82	VARTTH
DO 77 J=1,NBAG	HEDING
IF (MNBAG(J).EQ.0) GO TO 77	HEDING
MT = MT + 1	HEDING
NT = MT	HEDING
IF (LNEW) NT = 6	HEDING
C P & E CARRIAGE CONTROL	PECONV
C CALL CARCON(NT,1)	80386
IT = MT - 20	HEDING
PAGE = FLOAT(MT) + XPAGE	HEDING

IF (NT.EQ.6) WRITE(NT,121) DATE,BLANK,NPG	PAGE
IF (NT.NE.6) WRITE(NT,121) DATE	PAGE
IF (NT.EQ.6) NPG=NPG+1	PAGE
WRITE (NT,21) COMENT,PAGE,VPSTTL,BDYTTL	PAGE
WRITE (NT,78) J,(BAGTTL(I,J),I=1,5)	HEDING
IF (.NOT.LNEW) GO TO 72	HEDING
DO 71 I=1,NLINES	HEDING
71 WRITE (NT, 79) USEC(I),(ZTTH(JJ,I,IT),JJ=1,12)	HEDING
72 KBAG = 0	HEDING
KP = NPANEL(J)+1	HEDING
DO 73 K=1,KP	HEDING
KBAG = KBAG+1	HEDING
73 HEAD(KBAG) = PHED(K)	HEDING
KP = MNBAG(J)	HEDING
DO 74 K=1,KP	HEDING
KBAG = KBAG+1	HEDING
M = MBAG(2,K,J)	HEDING
74 HEAD(KBAG) = SEG(M)	HEDING
DO 76 J1=1,KBAG,4	HEDING
J2 = MINO(J1+3,KBAG)	HEDING
MT = MT + 1	HEDING
NT = MT	HEDING
IF (LNEW) NT = 6	HEDING
C P & E CARRIAGE CONTROL	PECONV
C CALL CARCON(NT,1)	80386
IT = MT - 20	HEDING
PAGE = FLOAT(MT) + XPAGE	HEDING
IF (NT.EQ.6) WRITE(NT,121) DATE,BLANK,NPG	PAGE
IF (NT.NE.6) WRITE(NT,121) DATE	PAGE
IF (NT.EQ.6) NPG=NPG+1	PAGE
WRITE (NT,21) COMENT,PAGE,VPSTTL,BDYTTL	PAGE
WRITE (NT,80)UNITM,J,(BAGTTL(I,J),I=1,5),(BLANK,J,HEAD(K),K=J1,J2)	HEDING
WRITE (NT,51) (BLANK,K=J1,J2)	HEDING
WRITE (NT,38)	HEDING
IF (.NOT.LNEW) GO TO 76	HEDING
JJ = 3*(J2-J1+1)	HEDING
DO 75 I=1,NLINES	HEDING
75 WRITE (NT, 81) USEC(I),(ZTTH(K,I,IT),K=1,JJ)	HEDING
76 CONTINUE	HEDING
77 CONTINUE	HEDING
78 FORMAT('0',26X,'PARAMETERS FOR AIRBAG NO.',I2,4X,5A4//	HEDING
* 16X,'SUPPLY CYLINDER STATIC'/	HEDING
* 4X,'TIME',8X,'PRES.',4X,'TEMP.',4X,'PRES.',12X,'AIRBAG',	HEDING
* 3X,'CENTER',14X,'AIRBAG SEMIAXES',12X,'ORIENTATION (DEG.)'/	HEDING
* 3X,'(MSEC)',7X,'(PSIG) (DEG.R) (PSIG)',8X,'X',8X,'Y',8X,'Z',	HEDING
* 11X,'A',8X,'B',8X,'C',10X,'YAW',4X,'PITCH',5X,'ROLL'/ )	HEDING
79 FORMAT (F9.3,3X,3F9.2,2(3X,3F9.3).3X,3F9.2)	HEDING
80 FORMAT('0',26X,'CONTACT FORCES ('A4,') ON AIRBAG NO.',I2,4X,5A4//	HEDING
* /4X,'TIME',4(A1,11X,'AIRBAG',I2,' VS. ',A4,1X))	HEDING
81 FORMAT (F9.3,4(3X,3F9.2))	HEDING
82 RETURN	HEDING
END	HEDING

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SUBROUTINE HERRON(HD3,NT1,THETO,THETOP)                                HERRON
                                                                 REV IV    07/23/86TWOPI
COMPUTES THETO - ANGLE OF JOINT STOP                                  HERRON
      THETOP- DERIVATIVE OF THETO WITH RESPECT TO PHI                HERRON
      *                                                              HERRON
FROM HD3   - COMPONENTS OF VECTOR DEFINING PHI                      HERRON
      NT1   - INDEX TO TAB ARRAY DEFINING FUNCTION                  HERRON
                                                                 HERRON
IMPLICIT REAL*8(A-H,O-Z)                                            HERRON
COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)DIMENB
COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),                          HERRON
*          UNITL,UNITM,UNITT,GRAVITY(3),TWOPI                       TWOPI
DIMENSION HD3(3)                                                    HERRON
IF (TAB(NT1+1).LE.0.0) GO TO 30                                     HERRON
IF (TAB(NT1+2).LE.0.0) GO TO 30                                     HERRON
C                                                                    HERRON
C THETO = P1(CP) + SP*P2(CP)                                         HERRON
C                                                                    HERRON
C THETOP = -SP*P1'(CP) + CP*P2(CP) - SP**2*P2'(CP)                 HERRON
C                                                                    HERRON
C WHERE P1(X),P2(X) ARE THE TWO 5TH ORDER POLYNOMIALS DEFINED       HERRON
C           IN TAB(NT1+5) AND TAB(NT1+11)                           HERRON
C           P1'(X),P2'(X) ARE THEIR DERIVATIVES WITH RESPECT TO PHI HERRON
C           AND SP,CP ARE SIN(PHI) AND COS(PHI)                     HERRON
C                                                                    HERRON
STH2 = 1.0-HD3(3)**2                                                HERRON
STH  = DSQRT(STH2)                                                  HERRON
CP   = HD3(1)/STH                                                   HERRON
SP   = HD3(2)/STH                                                   HERRON
P1   = TAB(NT1+5 )+ CP*(TAB(NT1+6 )                               HERRON
*               + CP*(TAB(NT1+7 )                               HERRON
*               + CP*(TAB(NT1+8 )                               HERRON
*               + CP*(TAB(NT1+9 )                               HERRON
*               + CP*(TAB(NT1+10) ))))) .                            HERRON
P2   = TAB(NT1+11)+ CP*(TAB(NT1+12)                               HERRON
*               + CP*(TAB(NT1+13)                               HERRON
*               + CP*(TAB(NT1+14)                               HERRON
*               + CP*(TAB(NT1+15)                               HERRON
*               + CP*(TAB(NT1+16) )))))                             HERRON
P1P  = TAB(NT1+6 )+ CP*(2.0*TAB(NT1+7 )                             HERRON
*               + CP*(3.0*TAB(NT1+8 )                             HERRON
*               + CP*(4.0*TAB(NT1+9 )                             HERRON
*               + CP*(5.0*TAB(NT1+10) )))                         HERRON
P2P  = TAB(NT1+12)+ CP*(2.0*TAB(NT1+13)                             HERRON
*               + CP*(3.0*TAB(NT1+14)                             HERRON
*               + CP*(4.0*TAB(NT1+15)                             HERRON
*               + CP*(5.0*TAB(NT1+16) )))                         HERRON
THETO = P1 + SP*P2                                                  HERRON
THETOP = CP*P2 - SP*(P1P + SP*P2P)                                 HERRON
GO TO 99                                                            HERRON
C                                                                    HERRON
C EVALUATE THETO AND THETOP FROM REGULAR FUNCTION DEFINITION WHERE HERRON

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C	· THETO (ORDINATE) IS A FUNCTION OF PHI (ABSCISSA) (0 < PHI < 2*PI)	HERRON
C		HERRON
30	PHI = DATAN2(HD3(2),HD3(1))	HERRON
	IF (PHI.LT.0.0) PHI = PHI + TWOPI	TWOPI
	THETO = EVALFD(PHI,NT1,1)	HERRON
	THETOP = EVALFD(PHI,NT1,0)	HERRON
99	RETURN	HERRON
	END	HERRON

	SUBROUTINE HICCSI(NPTS)	HICCSI
C		REV IV 10/08/87PLTINC
C		HICCSI
C	COMPUTES HIC, HSI AND CSI FOR CVS PROGRAM.	HICCSI
C		HICCSI
C	ASSUMES Z ARRAY CONTAINS	HICCSI
C	Z(I,1),I=1,NPTS : TIME POINTS (SECONDS)	HICCSI
C	Z(I,JH),I=1,NPTS : HEAD RESULTANT ACCELERATIONS (G'S)	HICCSI
C	Z(I,JC),I=1,NPTS : CHEST RESULTANT ACCELERATIONS (G'S)	HICCSI
C		HICCSI
C	NOTE:	HICCSI
C	IF JDTPTS(1)=0, HEAD RESULTANT IS NOT AVAILABLE (JH=NULL,JC=2).	HICCSI
C	IF JDTPTS(2)=0, CHEST RESULTANT IS NOT AVAILABLE (JH=2,JC=NULL).	HICCSI
C	OTHERWISE, JH=2 AND JC=3.	HICCSI
C		HICCSI
	COMMON/CDINT/ JDTPTS(18),Z(1000,3),DMY(8068)	80386
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,	PAGE
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	PAGE
	REAL*8 TIME	PAGE
	DIMENSION AREA(1000)	PLTINC
	IF (NPTS.LT.25) GO TO 25	HICCSI
	WRITE (6,14) NPG	PAGE
	NPG=NPG+1	PAGE
14	FORMAT (1H1, ' HIC, HSI AND CSI RESULTS',96X,'PAGE',15)	PAGE
	JH = 2	HICCSI
	JC = 3	HICCSI
	IF (JDTPTS(1).EQ.0) JC = 2	HICCSI
	CSI = 0.0	HICCSI
	HSI = 0.0	HICCSI
	HIC = 0.0	HICCSI
	CMX = Z(1,JC)	HICCSI
	HMX = Z(1,JH)	HICCSI
	IF (JDTPTS(2).EQ.0) GO TO 16	HICCSI
C		HICCSI
C	COMPUTE CSI - CHEST SEVERITY INDEX	HICCSI
C		HICCSI
	H1 = SQRT(Z(1,JC)) * Z(1,JC)**2	HICCSI
	DO 15 I=2,NPTS	HICCSI
	H2 = SQRT(Z(I,JC)) * Z(I,JC)**2	HICCSI
	DT = Z(I,1) - Z(I-1,1)	HICCSI
	CSI = CSI + 0.5*DT*(H1+H2)	HICCSI
	IF (CMX.GT.Z(I,JC)) GO TO 15	HICCSI
	CMX = Z(I,JC)	HICCSI
	CMT = Z(I,1)	HICCSI
15	H1 = H2	HICCSI
	CSI = 0.001*CSI	HICCSI
16	IF (JDTPTS(1).EQ.0) GO TO 23	HICCSI
C		HICCSI
C	COMPUTE HSI - HEAD SEVERITY INDEX - AND AREA TABLE	HICCSI
C		HICCSI
	AREA(1) = 0.0	HICCSI
	H1 = SQRT(Z(1,JH)) * Z(1,JH)**2	HICCSI

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DO 17 I=2,NPTS
H2 = SQRT(Z(I,JH)) * Z(I,JH)**2
DT = 0.5*(Z(I,1) - Z(I-1,1))
AREA(I) = AREA(I-1) + DT*(Z(I-1,JH)+Z(I,JH))
HSI = HSI + DT*(H1+H2)
IF (HMX.GT.Z(I,JH)) GO TO 17
HMX = Z(I,JH)
HMT = Z(I,1)
17 H1 = H2
HSI = 0.001*HSI
C
C COMPUTE HIC - HEAD INJURY CRITERION - AND TIME DURATION HT1,HT2
C
DO 19 K=2,NPTS
DO 18 L=K,NPTS
DT = Z(L,1) - Z(K-1,1)
DH = AREA(L) - AREA(K-1)
HT = DH/DT
HM = DT*SQRT(HT)*HT**2
IF (HM.LE.HIC) GO TO 18
HIC = HM
HT1 = Z(K-1,1)
HT2 = Z(L,1)
HA2 = Z(L,JH)
HA1 = Z(K-1,JH)
AVE = HT
18 CONTINUE
19 CONTINUE
HIC = 0.001*HIC
WRITE (6,21) HIC,HT1,HT2,HA1,HA2,AVE
21 FORMAT (1H0, ' HEAD INJURY CRITERION'//
* ' HIC = ', F8.2,
* 9X, 'TIME DURATION = ', F9.3, ' TO ', F9.3, ' MSEC'//
* 20X, 'WITH HEAD RESULTANTS = ', F9.3, ' AND ', F9.3, ' G''S'//
*14X, 'AVERAGE HEAD RESULTANT FOR TIME DURATION = ', F9.3, ' G''S')
WRITE (6,22) HSI,HMX,HMT
22 FORMAT (1H0, ' HEAD SEVERITY INDEX'//
* ' HSI = ', F8.2//
* ' MAX HEAD RESULTANT = ', F9.3, ' G''S AT ', F9.3, ' MSEC')
23 IF (JDTPTS(2).EQ.0) GO TO 25
WRITE (6,24) CSI,CMX,CMT
24 FORMAT (1H0, ' CHEST SEVERITY INDEX'//
* ' CSI = ', F8.2//
* ' MAX CHEST RESULTANT = ', F9.3, ' G''S AT ', F9.3, ' MSEC')
25 CONTINUE
IF(NPTS.LT.25) WRITE(6,101) NPTS
101 FORMAT(1X,/,2X,'HIC, HSI AND CSI NOT COMPUTED BECAUSE THE NUMBER
*OF POINTS TO BE USED IN THE COMPUTATION =',12,',',/,2X
* 'WHICH IS LESS THAN THE MINIMUM REQUIREMENT OF 25 POINTS.',/)
RETURN
END

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	SUBROUTINE HINPUT	HINPUT
C		REV IV 07/23/86TWOPI
C	CONTROLS THE INPUT OF CARDS F.8.A - F.8.D CONTAINING THE SETUP AND	HINPUT
C	CONTROL OF THE HARNESS BELT SYSTEM.	HINPUT
C		HINPUT
C		HINPUT
	IMPLICIT REAL*8(A-H,O-Z)	HINPUT
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,	HINPUT
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	PAGE
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),	HINPUT
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI	TWOPI
	COMMON/HRNESS/ BAR(15,100),BB(100),BBDOT(100),PLOSS(2,100),	HINPUT
*	XLONG(20),HTIME(2),IBAR(5,100),NL(2,100),	HINPUT
*	NPTSPB(20),NPTPLY(20),NTHRNS(20),NBLTPH(5)	HINPUT
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)	DIMENB
	COMMON/CNTRSF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)	EDGE
	COMMON/TITLES/ DATE(3),COMENT(40),VPS TTL(20),BDYTTL(5),	HINPUT
*	BLTTTL(5,8),PLTTTL(5,30),BAGTTL(5,6),SEG(30),	HINPUT
*	JOINT(30),CGS(30),JS(30)	HINPUT
	REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTTL,BAGTTL,SEG,JOINT	HINPUT
	LOGICAL*1 CGS,JS	HINPUT
C	THIS COMMON/TEMTVS/ IS SHARED BY CINPUT, FINPUT, HINPUT AND FDINIT	HINPUT
	COMMON/TEMPVS/ JTITLE(5,51),NF(5),MS(3),KTITLE(31),DDMY(34966)	80386
	REAL JTITLE,KTITLE	HINPUT
	IF (NHRNSS.EQ.0) GO TO 99	HINPUT
C		HINPUT
C	INPUT CARD F.8.A	HINPUT
C	(NOTE: NHRNSS NOW SUPPLIED ON INPUT CARD D.1)	HINPUT
C	NBLTPH - NO. OF BELTS PER HARNESS	HINPUT
C		HINPUT
	READ (5,11) (NBLTPH(I),I=1,NHRNSS)	HINPUT
11	FORMAT(18I4)	HINPUT
	WRITE (6,12) NPG,NHRNSS,(NBLTPH(I),I=1,NHRNSS)	PAGE
	NPG=NPG+1	PAGE
12	FORMAT('1 HARNESS-BELT SYSTEM INPUT',96X,'PAGE',15/120X,	PAGE
*	'CARDS F.8/' NO. OF HARNESSES =',I4//	PAGE
*	' NO. OF BELTS PER HARNESS =',5I6)	HINPUT
	J1 = 1	HINPUT
	K1 = 1	HINPUT
	DO 90 I=1,NHRNSS	HINPUT
	IF (NBLTPH(I).LE.0) GO TO 90	HINPUT
	J2 = J1 + NBLTPH(I) -1	HINPUT
C		HINPUT
C	INPUT CARD F.8.B - NPTSPB - NO. OF POINTS PER BELT.	HINPUT
C		HINPUT
	READ (5,11) (NPTSPB(J),J=J1,J2)	HINPUT
	WRITE (6,13) I,(NPTSPB(J),J=J1,J2)	HINPUT
13	FORMAT('0 FOR HARNESS NO.',13,' NO. OF POINTS PER BELT =',20I4)	HINPUT
	DO 80 J=J1,J2	HINPUT
	IF (NPTSPB(J).EQ.0) GO TO 80	HINPUT
C		HINPUT
C	INPUT CARD F.8.C - 5 FUNCTION NOS AND LENGTH OF EACH BELT.	HINPUT



C	READ (5,14) NF,XLONG(J)	HINPUT
14	FORMAT(5I4,F12.6)	HINPUT
	WRITE (6,15) I,J,NF,XLONG(J),UNITL	HINPUT
15	FORMAT('0 HARNESS NO.',I3,' BELT NO.',I3,' FUNCTION NOS.',5I6,	HINPUT
*	' REFERENCE SLACK = ',F9.3,1X,A4/)	HINPUT
	IF (XLONG(J).EQ.0.0) XLONG(J) = EPS(24)	HINPUT
	WRITE (6,16)	HINPUT
16	FORMAT ('0 K KS KE NT NPD NDR FUNCTION NOS.',	HINPUT
*	66X,'CARDS F.8.D' /)	CHGIII
C		HINPUT
C	SET UP POINTERS IN NTAB AND INITIAL VALUES OF TAB FOR BELT J	HINPUT
C	AS WAS DONE FOR OTHER CONTACTS IN SUBROUTINE FINPUT.	HINPUT
C		HINPUT
	NTHRNS(J) = MXNTB+1	HINPUT
	CALL FDINIT	HINPUT
	K2 = K1 + NPTSPB(J) - 1	HINPUT
	DO 70 K=K1,K2	HINPUT
C		HINPUT
C	INPUT CARD F.8.D	HINPUT
C		HINPUT
	READ (5,21) KS,KE,NPD,NDR,NF, (BAR(L,K),L=1,3)	HINPUT
21	FORMAT (9I4,3F12.0)	HINPUT
	READ (5,22) (BAR(L,K),L=7,12)	HINPUT
22	FORMAT (6F12.0)	HINPUT
	ICHEC = 0	CHGIII
	IF (K.EQ.K1.OR.K.EQ.K2) ICHEC = 1	CHGIII
	IF (ICHEC.EQ.1.AND.NPD.EQ.0) STOP 60	CHGIII
	IF (ICHEC.EQ.1.AND.NDR.EQ.0) STOP 61	CHGIII
	IF (NDR.EQ.0.AND.NPD.NE.0) STOP 62	CHGIII
	IBAR(1,K) = KS	HINPUT
	IBAR(2,K) = KE	HINPUT
	IBAR(4,K) = NPD	HINPUT
	IBAR(5,K) = NDR	HINPUT
	IBAR(3,K) = MXNTB+1	HINPUT
	CALL FDINIT	HINPUT
	SQRER = 1.0	HINPUT
	IF (KE.NE.0) SQRER = DSQRT(XDY(BAR(1,K),BD(7,KE),BAR(1,K)))	HINPUT
	DO 26 L=1,3	HINPUT
	IF (KE.NE.0) BAR(L+6,K) = BD(L+3,KE)	HINPUT
26	BAR(L+3,K) = BAR(L,K)/SQRER	HINPUT
	WRITE (6,31) K,(IBAR(L,K),L=1,5),NF	HINPUT
31	FORMAT (11I6)	HINPUT
70	CONTINUE	HINPUT
	WRITE (6,71) UNITL,UNITL,UNITL,UNITL	HINPUT
71	FORMAT ('0',12X,'BASE REFERENCE (' , A4,')',	HINPUT
*	7X,'ADJUSTED REFERENCE (' , A4,')',	HINPUT
*	11X,'OFFSET (' , A4,')',	HINPUT
*	11X,'PREFERRED DIRECTION (' ,A4,')' /	HINPUT
*	5X,'K', 4(8X,'X',8X,'Y',8X,'Z',3X) /)	HINPUT
	WRITE (6,72) (K,(BAR(L,K),L=1,12),K=K1,K2)	HINPUT
72	FORMAT (I6,3X,3F9.3,3X,3F9.3,3X,3F9.3,3X,3F9.3)	HINPUT

```
      K1 = K2+1
80 CONTINUE
      J1 = J2+1
90 CONTINUE
      DO 92 K=1,100
        BB DOT(K) = 0.0
      DO 91 J=1,2
91 PLOSS(J,K) = 0.0
      DO 92 J=1,3
92 BAR(J+12,K) = 0.0
99 RETURN
      END
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HINPUT
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	SUBROUTINE HPTURB	HPTURB
C	IMPLICIT REAL*8 (A-H,O-Z)	TWOPI
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,	HPTURB
	* NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	PAGE
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),	HPTURB
	* UNITL,UNITM,UNITT,GRAVITY(3),TWOPI	TWOPI
	COMMON/CNTRSF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)	EDGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),	HPTURB
	* SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)	HPTURB
	COMMON/RSAVE/ XSG(3,20,3),DPMI(3,3,30),LPMI(30),	ATBIII
	* NSG(9),MSG(20,9),MCG,MCGIN(24,5),KREF(20,9)	TTHKREF
	COMMON/HRNESS/ BAR(15,100),BB(100),BEDOT(100),PLOSS(2,100),	HPTURB
	* XLONG(20),HTIME(2),IBAR(5,100),NL(2,100),	HPTURB
	* NPTSPB(20),NPTPLY(20),NTHRNS(20),NBLTPH(5)	HPTURB
C	THIS COMMON/TEMPVS/ IS SHARED BY HPTURB, HBPLAY, HBELT AND HSETC.	HPTURB
	COMMON/TEMPVS/ B(3,3,3),S(3,3),T(3),R(3),V(3),T1(3),T2(3),	HPTURB
	* E(3,3,50),EDOT(3,50),FCE(3,50),FR(3,50),ZR(3,50),	HPTURB
	* TR(3,50),U(3,50),PTLOSS(2,50),BL(50),FB(50),FP(50),	HPTURB
	* OLDBB(100),RHS(3,54),C(3,3,200),IJK(54,54)	HPTURB
	* ,DMMY(29942)	80386
	DIMENSION BLOSS(2,20),HLOSS(2,5)	HPTURB
	EQUIVALENCE (BLOSS(1,1),C(1,1,1)) , (HLOSS(1,1),C(1,1,10))	HPTURB
	LOGICAL LAST	HPTURB
	DATA MAXITR/10/	HPTURB
	CALL ELTIME (1,39)	HPTURB
	CALL HBPLAY	HPTURB
	DHT = 0.0	HPTURB
	IF (TIME.NE.0.0) DHT = TIME - HTIME(1)	HPTURB
	HTIME(1) = TIME	HPTURB
	DO 11 J=1,100	HPTURB
	PTLOSS(J,1) = 0.0	HPTURB
	OLDBB(J) = BB(J)	HPTURB
	DO 11 I=1,3	HPTURB
11	BAR(I,J) = BAR(I+3,J)	HPTURB
	TSEC = 1000.0*TIME	HPTURB
	IF (NPRT(28).NE.0) WRITE (6,12) TSEC,NPG,UNITL,UNITM,UNITL,	PAGE
	* UNITL,UNITM,UNITL,UNITM	HPTURB
	IF (NPRT(28).NE.0) NPG=NPG+1	PAGE
12	FORMAT('1 HARNESS BELT RESULTS FOR TIME =',F9.3,' MSEC.',73X,	PAGE
	* 'PAGE',I5///	PAGE
	* 36X,'BELT STRAIN',6X,'(LOCAL OR ELLIPSOID)',18X,	CHGIII
	* '(INERTIAL)',14X,'PENETRATION'/	CHGIII
	* ' POINT POINT SEGMENT LENGTH ENERGY LOSS',5X,	HPTURB
	* 'REFERENCE POINT (' ,A4,')',13X,'BELT FORCES (' ,A4,')',	AFREVS
	* 9X,'ENERGY LOSS'/	HPTURB
	* ' NO. INDEX NO. (' ,A4,') (' ,2A4,')',7X,	HPTURB
	* 'X',8X,'Y',8X,'Z',13X,'X',10X,'Y',10X,'Z',8X,'(' ,2A4,')'//	HPTURB
	J1 = 1	HPTURB
	K0 = 1	HPTURB
	KNLO = 0	HPTURB
	DO 61 NH=1,NHRNSS	HPTURB

	IF (NBLTPH(NH).LE.0) GO TO 61	HPTURB
	ITER = 1	HPTURB
	KNL1 = KNLO	HPTURB
	KNLN = 0	CHGIII
C		HPTURB
C	START OF DO 59 * ITER=1,MAXITR LOOP	HPTURB
C		HPTURB
13	NJ2 = 54	HPTURB
	DO 14 I=1,NJ2	HPTURB
	DO 14 J=1,NJ2	HPTURB
14	IJK(I,J) = 0	HPTURB
	KNLO = KNL1	HPTURB
	J2 = J1 + NBLTPH(NH) - 1	HPTURB
	NTP = 0	HPTURB
	IJ = 0	HPTURB
	CALL HBELT (J1,J2,KNLO,1)	HPTURB
	KHO = 0	HPTURB
	KNLO = KNL1	HPTURB
	DO 15 NB=J1,J2	HPTURB
	IF (NPTPLY(NB).LE.0) GO TO 15	HPTURB
	NPTS = NPTPLY(NB)	HPTURB
	CALL HSETC (NPTS,KHO,KNLO,NTP,IJ)	HPTURB
	KHO = KHO + NPTS	HPTURB
	KNLO = KNLO + NPTS	HPTURB
15	CONTINUE	HPTURB
	KNLN = KNLO	CHGIII
C		HPTURB
C	SET UP C AND IJK ELEMENTS FOR TIE-POINTS.	HPTURB
C		HPTURB
	KNLO = KNL1	HPTURB
	KNLK = KNLO + 1	HPTURB
	K1 = KNLK	HPTURB
	DO 22 NB=J1,J2	HPTURB
	IF (NPTPLY(NB).LE.0) GO TO 22	HPTURB
	K2 = K1 + NPTPLY(NB) - 1	HPTURB
	DO 21 KNL=K1,K2	HPTURB
	KI = NL(1,KNL)	HPTURB
	KS = IABS(IBAR(1,KI))	HPTURB
	IF (KS.LT.100) GO TO 21	HPTURB
	KS1 = KS/100	HPTURB
	DO 16 K=KNLK,KNL	HPTURB
	KK = K	HPTURB
	KI = NL(1,K)	HPTURB
	KS = IABS(IBAR(1,KI))	HPTURB
	IF (KS.LT.100) GO TO 16	HPTURB
	KS2 = KS/100	HPTURB
	IF (KS2.EQ.KS1) GO TO 17	HPTURB
16	CONTINUE	HPTURB
17	IF (KK.EQ.KNL) GO TO 21	HPTURB
	KK1 = KK - KNLO	HPTURB
	KK2 = KNL - KNLO	HPTURB
	IQ1 = MAX0(1,KK2-1)	HPTURB

IQ2 = MIN0(KK2+1,KH0)	HPTURB
DO 18 IQ=IQ1,IQ2	HPTURB
IF (IJK(KK2,IQ).EQ.0) GO TO 18	HPTURB
IJK(KK1,IQ) = IJK(KK2,IQ)	HPTURB
IJK(KK2,IQ) = 0	HPTURB
18 CONTINUE	HPTURB
IJK(KK2,KK2) = IJ+1	HPTURB
IJK(KK2,KK1) = IJ+2	HPTURB
DO 20 J=1,3	HPTURB
DO 19 I=1,3	HPTURB
C(I,J,IJ+1) = 0.0	HPTURB
19 C(I,J,IJ+2) = 0.0	HPTURB
C(J,J,IJ+1) = 1.0	HPTURB
20 C(J,J,IJ+2) = -1.0	HPTURB
IJ = IJ + 2	HPTURB
21 CONTINUE	HPTURB
K1 = K2 + 1	HPTURB
22 CONTINUE	HPTURB
MJ2 = -(KH0+NTP)	HPTURB
IF (NPRT(28).LT.3) GO TO 29	HPTURB
NJ2 = -MJ2	HPTURB
DO 25 J=1,NJ2	HPTURB
25 WRITE (6,26) J,(RHS(I,J),I=1,3),(IJK(J,I),I=1,NJ2)	HPTURB
26 FORMAT (I6,3F12.6,20I4/(42X,20I4))	HPTURB
DO 27 KLM=1,IJ	HPTURB
27 WRITE (6,28) KLM,((C(J,I,KLM),I=1,3),J=1,3)	HPTURB
28 FORMAT (I6,9F12.6)	HPTURB
29 CALL FSMSOL (C,RHS,IJK,MJ2,IJ,54,200)	HPTURB
IF (NPRT(28).LT.3) GO TO 31	HPTURB
DO 30 J=1,NJ2	HPTURB
30 WRITE (6,26) J,(RHS(I,J),I=1,3),(IJK(J,I),I=1,NJ2)	HPTURB
31 ONE = 1.0	HPTURB
DELMAX = 0.0	HPTURB
SCALE = 1.0	HPTURB
DO 44 IT=1,2	HPTURB
K1 = K0	HPTURB
KH = 0	HPTURB
KR = NTP	HPTURB
DO 43 NB=J1,J2	HPTURB
IF (NPTPLY(NB).LE.0) GO TO 43	HPTURB
K2 = K1 + NPTPLY(NB) - 1	HPTURB
DO 42 K=K1,K2	HPTURB
KH = KH + 1	HPTURB
KR = KR + 1	HPTURB
C	HPTURB
C	HPTURB
C	HPTURB
C	HPTURB
C	HPTURB
HERE K IS INDEX OF ALL POINTS IN PLAY	HPTURB
KH IS INDEX OF ALL POINTS IN PLAY ON A SINGLE HARNESS	HPTURB
KR IS INDEX OF RHS ARRAY ELEMENTS	HPTURB
C	HPTURB
KI = NL(1,K)	HPTURB
KS = IABS(IBAR(1,KI))	HPTURB
IF (KS.GT.100) KS = MOD(KS,100)	HPTURB

	IF (IBAR(5,KI).EQ.0) GO TO 32	HPTURB
	CALL MAT31 (D(1,1,KS),RHS(1,KR),R)	HPTURB
	GO TO 37	HPTURB
C		HPTURB
C	NOTE: ENDPOINTS (K <sub>1</sub> = K1 & K2) MUST BE TYPE 5.	HPTURB
C		HPTURB
	32 CALL DOT31 (E(1,1,KH),RHS(1,KR),T1)	HPTURB
	IF (IT.EQ.2) GO TO 33	HPTURB
	DELMAX = DMAX1(DELMAX,DABS(T1(2)/DMIN1(BB(K),BB(K-1))))	HPTURB
	GO TO 34	HPTURB
	33 BB(K) = BB(K) + SCALE*T1(2)	HPTURB
	BB(K-1) = BB(K-1) - SCALE*T1(2)	HPTURB
	34 DO 35 J=1,3	HPTURB
	35 T2(J) = T1(1)*E(J,1,KH) + T1(3)*E(J,3,KH)	HPTURB
	CALL MAT31 (D(1,1,KS),T2,R)	HPTURB
	IF (NPRT(28).GE.3) WRITE (6,36) K,T1,T2,R	HPTURB
	36 FORMAT ('0',I6,3(3X,3F12.6))	HPTURB
	37 IF (IT.EQ.2) GO TO 39	HPTURB
	DO 38 J=1,3	HPTURB
	38 DELMAX = DMAX1(DELMAX,DABS(R(J)/DMAX1(EPS(1),DABS(BAR(J+3,KI)))))	HPTURB
	GO TO 42	HPTURB
	39 DO 40 J=1,3	HPTURB
	40 BAR(J+3,KI) = BAR(J+3,KI) + SCALE*R(J)	HPTURB
	KE = IBAR(2,KI)	HPTURB
	IF (KE.EQ.0) GO TO 42	HPTURB
	RER = XDY(BAR(4,KI),BD(7,KE),BAR(4,KI))	HPTURB
	IF (RER.LE.1.0) GO TO 42	HPTURB
	SQRER = 1.0/DSQRT(RER)	HPTURB
	DO 41 J=1,3	HPTURB
	41 BAR(J+3,KI) = SQRER*BAR(J+3,KI)	HPTURB
	42 CONTINUE	HPTURB
	K1 = K2 + 1	HPTURB
	43 CONTINUE	HPTURB
	IF (IT.EQ.2) GO TO 44	HPTURB
	IF (DELMAX.NE.0.0) SCALE = DMIN1(ONE,EPS(1)/DELMAX)	HPTURB
	44 CONTINUE	HPTURB
	IF (NPRT(28).GE.2) WRITE (6,45) ITER,DELMAX,SCALE	HPTURB
	45 FORMAT ('0 ITER =',I6,' DELMAX =',F15.6,' SCALE =',F15.6)	HPTURB
	LAST = DELMAX.LE.EPS(2).OR. ITER.EQ.MAXITR	HPTURB
	IF (.NOT.LAST) GO TO 52	HPTURB
	KH = 0	HPTURB
	K1 = K0	HPTURB
	HLOSS(1,NH) = 0.0	HPTURB
	HLOSS(2,NH) = 0.0	HPTURB
	DO 51 NB=J1,J2	HPTURB
	BLOSS(1,NB) = 0.0	HPTURB
	BLOSS(2,NB) = 0.0	HPTURB
	IF (NPTPLY(NB).LE.0) GO TO 51	HPTURB
	K2 = K1 + NPTPLY(NB) - 1	HPTURB
	KK1 = NL(1,K1)	HPTURB
	KK2 = NL(1,K2)	HPTURB
	DO 46 K=KK1,KK2	HPTURB

' DO 46 J=1,3	HPTURB
46 BAR(J+12,K) = 0.0	HPTURB
IF (DHT.EQ.0.0) GO TO 49	HPTURB
DO 48 K=K1,K2	HPTURB
KH = KH + 1	HPTURB
KI = NL(1,K)	HPTURB
PLOSS(2,KI) = PLOSS(2,KI) + DHT*PTLOSS(2,KH)	HPTURB
IF (K.EQ.K1) GO TO 47	HPTURB
BBDOT(K-1) = (BB(K-1)-OLDBB(K-1))/DHT	HPTURB
PLOSS(1,K-1) = PLOSS(1,K-1) + DHT*PTLOSS(1,KH-1)	HPTURB
BLOSS(1,NB) = BLOSS(1,NB) + PLOSS(1,K-1)	HPTURB
47 DO 48 J=1,3	HPTURB
48 BAR(J+12,KI) = (BAR(J+3,KI)-BAR(J,KI))/DHT	HPTURB
BBDOT(K2) = 0.0	HPTURB
PLOSS(1,K2) = 0.0	HPTURB
49 K1 = K2+1	HPTURB
DO 50 K=KK1,KK2	HPTURB
50 BLOSS(2,NB) = BLOSS(2,NB) + PLOSS(2,K)	HPTURB
HLOSS(1,NH) = HLOSS(1,NH) + BLOSS(1,NB)	HPTURB
HLOSS(2,NH) = HLOSS(2,NH) + BLOSS(2,NB)	HPTURB
51 CONTINUE	HPTURB
52 IF (NPRT(28).EQ.0) GO TO 59	HPTURB
IF (.NOT.LAST .AND. IABS(NPRT(28)).EQ.1) GO TO 59	HPTURB
K1 = K0	HPTURB
KI = 0	HPTURB
DO 57 NB=J1,J2	HPTURB
IF (NPTPLY(NB).LE.0) GO TO 57	HPTURB
WRITE (6,53) NB,NH	HPTURB
53 FORMAT ('0 BELT NO.',I4,' OF HARNESS NO.',I4)	HPTURB
K2 = K1 + NPTPLY(NB) - 1	HPTURB
DO 54 K=K1,K2	HPTURB
KH = KH + 1	HPTURB
KI = NL(1,K)	HPTURB
KS = IBAR(1,KI)	HPTURB
BK = 0.0	HPTURB
IF (K.NE.K1) BK = BB(K-1)	HPTURB
PLS = 0.0	HPTURB
IF (K.NE.K1) PLS = PLOSS(1,K-1)	HPTURB
T(1) = BAR(4,KI)	HPTURB
T(2) = BAR(5,KI)	HPTURB
T(3) = BAR(6,KI)	HPTURB
KJ = MOD(IABS(KS),100)	HPTURB
IF (LPMI(KJ).NE.0) CALL DOT 1 (DPMI(1,1,KJ),BAR(4,KI),T)	HPTURB
54 WRITE (6,55) K,KI,KS,BK,PLS,(T(J),J=1,3).	HPTURB
* (FCE(J,KH),J=1,3),PLOSS(2,KI)	HPTURB
55 FORMAT (5I8,F10.3,F12.3,2X,3F9.3,3X,3F11.3,3X,F12.3)	HPTURB
IF (LAST) WRITE (6,56) BLOSS(1,NB),BLOSS(2,NB)	HPTURB
56 FORMAT ('0 TOTAL BELT ENERGY LOSS',7X,F12.3,68X,F12.3)	HPTURB
K1 = K2 + 1	HPTURB
57 CONTINUE	HPTURB
IF (LAST) WRITE (6,58) HLOSS(1,NH),HLOSS(2,NH)	HPTURB
58 FORMAT ('0 TOTAL HARNESS ENERGY LOSS',7X,F12.3,68X,F12.3)	HPTURB

59	ITER = ITER + 1	HPTURB
C		HPTURB
C	END OF DO 59 ITER-1,MAXITR LOOP	HPTURB
C		HPTURB
	IF (.NOT.LAST) GO TO 13	HPTURB
	IF (ITER.GT.MAXITR) WRITE (6,60) MAXITR,TSEC,DELMAX,SCALE	HPTURB
60	FORMAT ('0 HPTURB ITER =',I4,' AT TIME =',F8.3,	HPTURB
	* ' MSEC. DELMAX =',F10.6,' SCALE =',F10.6)	HPTURB
	J1 = J2 + 1	HPTURB
	K0 = K1	HPTURB
	KHLO = KHLN	CHGIII
61	CONTINUE	HPTURB
	IF (NPRT(28).LT.0) NPRT(28) = 0	HPTURB
	CALL ELTIME (2,39)	HPTURB
	RETURN	HPTURB
	END	HPTURB



385-ATB:V FT2

	CNORM = 0.0	HSETC
	IF (K.NE.K2) CNORM = FB(KH)/BL(KH)	HSETC
	IF (K.NE.K1) CNORM = CNORM + FB(KH-1)/BL(KH-1)	HSETC
	KI = NL(1,KNL)	HSETC
	IF (IABS(IBAR(1,KI)).GT.100) GO TO 14	HSETC
C	IF (CNORM.NE.0.0) GO TO 14	BUTLER1
	KK = IJK(K,K)	HSETC
	DO 13 I=1,3	HSETC
13	C(I,I,KK) = ONE	HSETC
	IF (CNORM.EQ.0.0) GO TO 60	BUTLER1
14	KK = IBAR(3,KI)	HSETC
	NFD = NTAB(KK+1)	HSETC
	NFR = NTAB(KK+5)	HSETC
C		HSETC
C	SET UP B(3,3,3) AND S(3,3)	HSETC
C		HSETC
	MK(1) = KH	HSETC
	MK(2) = KH-1	HSETC
	IF (K.EQ.K2) MK(1) = 0	HSETC
	IF (K.EQ.K1) MK(2) = 0	HSETC
	DO 18 M=1,2	HSETC
	KK = MK(M)	HSETC
	IF (KK.NE.0 .AND. CNORM.NE.0.0) GO TO 16	HSETC
	DO 15 I=1,3	HSETC
	S(I,M) = 0.0	HSETC
	DO 15 J=1,3	HSETC
15	B(I,J,M) = 0.0	HSETC
	GO TO 18	HSETC
16	CALL DOT31 (E(1,1,KH),U(1,KK),T)	HSETC
	KIM = KNL + 1 - M	HSETC
	FB1 = FB(KK)/BL(KK)	HSETC
	FB2 = FP(KK)/BB(KIM) - FB1	HSETC
	FB3 = FP(KK)*BL(KK)/BB(KIM)**2	HSETC
	DO 17 I=1,3	HSETC
	SGN = ONE	HSETC
	IF (FR(I,KH).LT.0.0) SGN = -ONE	HSETC
	S(I,M) = SGN*(FB3*T(I))	HSETC
	DO 17 J=1,3	HSETC
17	B(I,J,M) = SGN*(FB1*E(J,I,KH) + FB2*T(I)*U(J,KK))	HSETC
18	CONTINUE	HSETC
	DO 19 I=1,3	HSETC
	S(I,3) = -(S(I,1) + S(I,2))	HSETC
	DO 19 J=1,3	HSETC
19	B(I,J,3) = -(B(I,J,1) + B(I,J,2))	HSETC
	IF (NFR.EQ.0) GO TO 20	HSETC
	R(1) = TAB(NFR+2)	HSETC
	R(2) = TAB(NFR+4)	HSETC
20	R(3) = 0.0	HSETC
	DO 50 M=1,3	HSETC
	RH = 0.0	HSETC
	IF (M.EQ.3) GO TO 31	HSETC
	IF (NFR.EQ.0) GO TO 48	HSETC

C		HSETC
C	CONSTRAINTS 1 AND 2	HSETC
C		HSETC
	SGN = -ONE	HSETC
	FR3 = DABS(FR(M,KH)) - R(M)*DABS(FR(3,KH))	HSETC
	IF (IBAR(1,KI).GT.0) RH = FR3	HSETC
	IF (FR3.LE.0.0) GO TO 48	HSETC
	GO TO 40	HSETC
C		HSETC
C	CONSTRAINT NO. 3	HSETC
C		HSETC
31	IF (NFD.EQ.0) GO TO 48	HSETC
	IF (IBAR(1,KI).LT.0) GO TO 40	HSETC
	SGN = ONE	HSETC
	RMAG2 = TR(1,KH)**2 + TR(2,KH)**2 + TR(3,KH)**2	HSETC
	RMAG = DSQRT(RMAG2)	HSETC
	RER2 = TR(1,KH)*E(1,3,KH) + TR(2,KH)*E(2,3,KH) + TR(3,KH)*E(3,3,KH)	HSETC
	RER2 = EDOT(3,KH)*RER2	HSETC
	RER = DSQRT(RER2)	HSETC
	PEN = RMAG/RER - RMAG	HSETC
	RRDOT = BAR(4,KI)*BAR(13,KI)	HSETC
*	+ BAR(5,KI)*BAR(14,KI)	HSETC
*	+ BAR(6,KI)*BAR(15,KI)	HSETC
	KS = IABS(IBAR(1,KI))	HSETC
	IF (KS.GT.100) KS = MOD(KS,100)	HSETC
	CALL DOT31 (D(1,1,KS),BAR(13,KI),T)	HSETC
	ERDOT = E(1,3,KH)*T(1) + E(2,3,KH)*T(2) + E(3,3,KH)*T(3)	HSETC
	C1 = PEN/RMAG2	HSETC
	C2 = RMAG*EDOT(3,KH)/(RER*RER2)	HSETC
	PDOT = C1*RRDOT - C2*ERDOT	HSETC
	NFDZ = IBAR(3,KI)	CHGIII
	CALL FRCDFL (PEN,PDOT,NFDZ,0,FDP,ELOSS)	CHGIII
	CALL FRCDFL (PEN,PDOT,NFDZ,1,FD,ELOSS)	CHGIII
	K' = FD + FR(3,KH)	HSETC
	P1LOSS(2,KH) = ELOSS	HSETC
	C1 = FDP*C1	HSETC
	C2 = FDP*C2	HSETC
	SGNB3 = -DSIGN(ONE,FR(3,KH))	HSETC
	DO 32 J=1,3	HSETC
32	B(3,J,3) = SGNB3*B(3,J,3) - C1*TR(J,KH) + C2*E(J,3,KH)	HSETC
40	DO 47 LL=1,3	HSETC
	L = 4 - LL	HSETC
	IF (KM(L).EQ.0) GO TO 47	HSETC
	DO 42 J=1,3	HSETC
42	V(J) = R(M)*B(3,J,L) + SGN*B(M,J,L)	HSETC
	KL = KM(L)	HSETC
	KML = KNL + KL - K	HSETC
	KIL = NL(1,KML)	HSETC
	IF (IBAR(5,KIL).NE.0) GO TO 43	HSETC
	KHL = KH + KL - K	HSETC
	CALL DOT31 (E(1,1,KHL),V,T)	HSETC
	T(2) = R(M)*S(3,L) + SGN*S(M,L)	HSETC

	CALL MAT31 (E(1,1,KHL),T,V)	HSETC
43	IF (LL.NE.1) GO TO 44	HSETC
	VE = V(1)*E(1,M,KH) + V(2)*E(2,M,KH) + V(3)*E(3,M,KH)	HSETC
	EV = 1.0	HSETC
	IF (IABS(IBAR(1,KI)).LT.100)	HSETC
	* EV = DSIGN(ONE,VE)/DSQRT(V(1)**2+V(2)**2+V(3)**2)	HSETC
	RH = EV*RH	HSETC
44	IF (IJK(K,KL).NE.0) GO TO 45	HSETC
	IJ = IJ+1	HSETC
	IJK(K,KL) = IJ	HSETC
45	KK = IJK(K,KL)	HSETC
	DO 46 J=1,3	HSETC
	VEV = EV*V(J)	HSETC
	DO 46 I=1,3	HSETC
46	C(I,J,KK) = C(I,J,KK) + E(I,M,KH)*VEV	HSETC
47	CONTINUE	HSETC
	DO 41 I=1,3	HSETC
41	RHS(I,K) = RHS(I,K) + RH*E(I,M,KH)	HSETC
	GO TO 50	HSETC
48	IF (IBAR(1,KI).LE.0) GO TO 50	HSETC
	KK = IJK(K,K)	HSETC
	DO 49 I=1,3	HSETC
	DO 49 J=1,3	HSETC
49	C(I,J,KK) = C(I,J,KK) + E(I,M,KH)*E(J,M,KH)	HSETC
50	CONTINUE	HSETC
60	CONTINUE	HSETC
	RETURN	HSETC
	END	HSETC

	SUBROUTINE HYABF(B,Z,A,F)		HYABF
C		REV IV	02/07/87HYABF
	IMPLICIT REAL*8(A-H,O-Z)		HYABF
C			HYABF
C	CALCULATES A, AZ, Z.AZ: OLD FORM MUST BE DIAGONAL		HYABF
C			HYABF
	DIMENSION B(24),Z(1),A(3,3)		HYABF
	P2 = 0.0		HYABF
	IF(B(1).LT.0.0)P2 = -B(1) - 2.0		HYABF
	F = 0.0		HYABF
	DO 30 I = 1,3		HYABF
	J = I		HYABF
	IF(B(1).LT.0.0)GO TO 10		HYABF
	A(I,1) = 1.0/B(I)**2		HYABF
	GO TO 15		HYABF
10	A(I,1) = B(I+16)		HYABF
	J = J + 1		HYABF
	A(I,1) = HYFCN(A(I,1),Z(I),B(J),P2)		HYABF
C	IF(P2.GT.0.0)A(I,1) = A(I,1)*DABS(Z(I)/B(J))**P2		HYABF
15	DO 20 J = 2,3		HYABF
20	A(I,J) = A(I,J-1)*Z(I)		HYABF
30	F = F + A(I,3)		HYABF
	RETURN		HYABF
	END		HYABF

	SUBROUTINE HYBND(M,Z,IV,U,C,X)		HYBND
C		REV IV	02/07/87HYBND
	IMPLICIT REAL*8(A-H,O-Z)		HYBND
C			HYBND
C	SEARCHES FOR POINT NEAREST CORNER - DIRECTION C*U		HYBND
C			HYBND
	DIMENSION Z(3,12),IV(12),U(3),X(3)		HYBND
	DO 20 I = 1,M,2		HYBND
	J = IV(I)		HYBND
	ATST = C*(U(1)*Z(1,J) + U(2)*Z(2,J) + U(3)*Z(3,J))		HYBND
	IF(I.EQ.1)GO TO 10		HYBND
	TEST = AMAX - ATST		HYBND
	COMP = DMAX1(DABS(AMAX),DABS(ATST))		HYBND
C	PRECISION TEST - TRY >1000??		HYBND
	IF(1000.*DABS(TEST).LT.COMP)TEST = 0.0		HYBND
	IF(TEST)10,15,20		HYBND
C	IF(AMAX-ATST)10,15,20		HYBND
	10 AMAX = ATST		HYBND
	J1 = J		HYBND
	15 J2 = J		HYBND
	20 CONTINUE		HYBND
	DO 25 I = 1,3		HYBND
	25 X(I) = 0.5*(Z(I,J1) + Z(I,J2))		HYBND
	RETURN		HYBND
	END		HYBND

	SUBROUTINE HYBOX(E,T,P,N,Z,IV)		HYBOX
C		REV IV 02/07/87	HYBOX
	IMPLICIT REAL*8(A-H,O-Z)		HYBOX
C			HYBOX
C	COMPUTES THE INTERSECTION OF A PLANE WITH THE EDGES OF A BOX		HYBOX
C			HYBOX
	DIMENSION T(3),E(3),TU(3),T2(3),P(3)		HYBOX
C	TO BE SAFE IV AND Z SHOULD BE DIMENSION 14 IN CALLING PROGRAM		HYBOX
	DIMENSION IV(12)		HYBOX
	DIMENSION Z(3,12)		HYBOX
	DATA ONE/1.0D0/		HYBOX
C	T - PLANE VECTOR, P POINT IN PLANE		HYBOX
	TUV = 0.0		HYBOX
	DO 10 I = 1,3		HYBOX
	TU(I) = T(I)*E(I)		HYBOX
	T2(I) = 2.0*TU(I)		HYBOX
10	TUV = TUV + T(I)*(E(I) + P(I))		HYBOX
	N = 0		HYBOX
	J = 2		HYBOX
	K = 3		HYBOX
	DO 45 I = 1,3		HYBOX
	CK = -E(K)		HYBOX
	P1 = TUV		HYBOX
	DO 40 LL = 1,2		HYBOX
	P2 = P1 - T2(I)		HYBOX
	P3 = P2 - T2(J)		HYBOX
	P4 = P1 - T2(J)		HYBOX
	M = N		HYBOX
	IF(DSIGN(ONE,P2).EQ.DSIGN(ONE,P1))GO TO 15		HYBOX
	M = M + 1		HYBOX
	Z(I,M) = (P1/TU(I) - 1.0)*E(I)		HYBOX
	Z(J,M) = -E(J)		HYBOX
	Z(K,M) = CK		HYBOX
15	IF(DSIGN(ONE,P3).EQ.DSIGN(ONE,P2))GO TO 20		HYBOX
	M = M + 1		HYBOX
	Z(I,M) = E(I)		HYBOX
	Z(J,M) = (P2/TU(J) - 1.0)*E(J)		HYBOX
	Z(K,M) = CK		HYBOX
20	IF(DSIGN(ONE,P3).EQ.DSIGN(ONE,P4))GO TO 25		HYBOX
	M = M + 1		HYBOX
	Z(I,M) = (P4/TU(I) - 1.0)*E(I)		HYBOX
	Z(J,M) = E(J)		HYBOX
	Z(K,M) = CK		HYBOX
25	IF(DSIGN(ONE,P4).EQ.DSIGN(ONE,P1))GO TO 30		HYBOX
	M = M + 1		HYBOX
	Z(I,M) = -E(I)		HYBOX
	Z(J,M) = (P1/TU(J) - 1.0)*E(J)		HYBOX
	Z(K,M) = CK		HYBOX
30	IF(M.EQ N)GO TO 35		HYBOX
	CHECK FOR PRECISION (+-+- .OR -+-+)		HYBOX
	IF(M.EQ.N+4)GO TO 35		HYBOX
C	DELETE 0 LENGTH SIDE		HYBOX

IF((Z(I,M-1).EQ.Z(I,M)).AND.(Z(J,M-1).EQ.Z(J,M)))GO TO 35	HYBOX
N = M	HYBOX
35 P1 = P1 - T2(K)	HYBOX
40 CK = -CK	HYBOX
J = K	HYBOX
45 K = I	HYBOX
C	HYBOX
IF(N.LT.6)GO TO 65	HYBOX
IV(1) = 1	HYBOX
IV(2) = 2	HYBOX
M = 2	HYBOX
DO 60 J = 3,N,4	HYBOX
D = DABS(Z(1,M)) + DABS(Z(2,M)) + DABS(Z(3,M))	HYBOX
DO 55 L = 3,N	HYBOX
DO 50 LL = 2,J	HYBOX
IF(IV(LL-1).EQ.L) GO TO 55	HYBOX
50 CONTINUE	HYBOX
F = DABS(Z(1,M)-Z(1,L))+DABS(Z(2,M)-Z(2,L))+DABS(Z(3,M)-Z(3,L))	HYBOX
IF(F.GT.D)GO TO 55	HYBOX
D = F	HYBOX
K = L	HYBOX
55 CONTINUE	HYBOX
M = K + 1	HYBOX
IF(MOD(K,2).EQ.0)M = K - 1	HYBOX
IV(J) = K	HYBOX
IV(J+1) = M	HYBOX
60 CONTINUE	HYBOX
65 RETURN	HYBOX
END	HYBOX



	SUBROUTINE HYDAD(D,A,DAD)		HYDAD
C		REV IV	02/07/87HYDAD
	IMPLICIT REAL*8(A-H,O-Z)		HYDAD
	COMPUTES D'A(*,1)D		HYDAD
	DIMENSION D(3,3),A(3),DAD(3,3)		HYDAD
	DO 10 I = 1,3		HYDAD
	DO 10 J = 1,3		HYDAD
	DAD(I,J) = 0.0		HYDAD
	DO 10 K = 1,3		HYDAD
	10 DAD(I,J) = DAD(I,J) + D(K,I)*A(K)*D(K,J)		HYDAD
	RETURN		HYDAD
	END		HYDAD

SUBROUTINE HYEST(BM,BN,TAB)	HYEST
C	REV IV 07/23/87HYEST
C LINEAR PROGRAM	HYEST
IMPLICIT REAL*8(A-H,O-Z)	HYEST
DIMENSION BM(24),BN(24),TAB(8)	HYEST
COMMON/TEMPVS/D12(3,3),A(3,3),B(3,3),XMN(3),RLN(3),XMM(3),	HYEST
* T(3),R(3),C(3,3),V(7),DMY(3055)	80386
C R GOES FROM M TO N D12 = DM*DN'	HYEST
C R = 0 CANNOT BE SOLVED WITH THIS METHOD	HYEST
BE = 1.0	HYEST
RR = R(1)**2 + R(2)**2 + R(3)**2	HYEST
IF(RR.EQ.0.0)GO TO 30	HYEST
C R.R = 0 INVALID	HYEST
M = 1	HYEST
N = 1	HYEST
IF(BM(1).LT.0.0)M = 2	HYEST
IF(BN(1).LT.0.0)N = 2	HYEST
PM = 2.	HYEST
PN = 2.	HYEST
IF(M.EQ.2)PM = -BM(1)	HYEST
IF(N.EQ.2)PN = -BN(1)	HYEST
DO 10 I = 1,3	HYEST
T(I) = R(I)	HYEST
DO 10 J = 1,3	HYEST
10 B(I,J) = D12(I,J)	HYEST
IF(N.EQ.2)CALL DOTF33(D12,BN(8),B)	HYEST
DO 15 I = 1,3	HYEST
DO 15 J = 1,3	HYEST
15 C(I,J) = B(I,J)	HYEST
IF(M.EQ.2)CALL MAT33(BM(8),B,C)	HYEST
C C WILL TRANSFORM FROM NN TO MM	HYEST
IF(M.EQ.2)CALL MAT31(BM(8),R,T)	HYEST
CALL HYLPM(BM(M),BN(N))	HYEST
BE = V(7)	HYEST
IF(V(7).LE.1.0)GO TO 30	HYEST
CALL HYABF(BM(1),V(1),A,F1)	HYEST
CALL HYABF(BN(1),V(4),B,F2)	HYEST
C ESTIMATE ALPHA	HYEST
AA = A(1,2)**2 + A(2,2)**2 + A(3,2)**2	HYEST
BB = B(1,2)**2 + B(2,2)**2 + B(3,2)**2	HYEST
ALP = DSQRT(AA/BB)	HYEST
RA = F1*(1.0/PM)	HYEST
RB = F2*(1.0/PN)	HYEST
ALP = ALP*RA*F2/(RB*F1)	HYEST
C SCALE POINTS TO ELLIPSOIDS	HYEST
DO 20 I = 1,3	HYEST
V(I) = V(I)/RA	HYEST
20 V(I+3) = V(I+3)/RB	HYEST
C ESTIMATE BETA	HYEST
CALL MAT31(C,V(4),T)	HYEST
BE = (V(1)-T(1))**2 + (V(2)-T(2))**2 + (V(3) - T(3))**2	HYEST
BE = DSQRT(BE/RR)	HYEST

C STORE VALUES IN TAB ARRAY FOR CONTACT

TAB(1) = ALP

DO 25 I = 1,6

25 TAB(I+2) = V(I)

30 TAB(2) = BE

RETURN

END

HYEST

HYEST

HYEST

HYEST

HYEST

HYEST

HYEST

C	DOUBLE PRECISION FUNCTION HYFCN(C,Z,A,P)	REV IV	02/07/87	HYFCN
	IMPLICIT REAL*8(A-H,O-Z)			HYFCN
	HYFCN = C			HYFCN
	IF(P.EQ.0.0)GO TO 10			HYFCN
	HYFCN = 0.0			HYFCN
	IF(Z.EQ.0.0)GO TO 10			HYFCN
	Q = P*(DLOG(DABS(Z)) - DLOG(A))			HYFCN
	IF(Q.GT.-88.5) HYFCN = C*DEXP(Q)			HYFCN
10	RETURN			HYFCN
	END			HYFCN

	SUBROUTINE HY LIM(A,U,B,V,C,W,Z,BD)		HY LIM
C		REV IV	12/11/87HYFIX
	IMPLICIT REAL*8(A-H,O-Z)		HY LIM
C	GIVEN Z, FIND A,B,Z: ZEZ = 1, ZEY = 0, TZ = TP		HY LIM
	DIMENSION BD(24)		HY LIM
	DIMENSION U(3),V(3),W(3),EI(3),EJ(3),T(3),TV(3)		HY LIM
	DIMENSION Z(3),Z(3),EV(3),Q(3),S(3),EZ(3)		HY LIM
	DIMENSION SM(3,3)		HY LIM
	LOGICAL PASS,USEV		HY LIM
	PASS = .FALSE.		HY LIM
	ITER = 100		HY LIM
	PP = -1./BD(1)		HY LIM
	POW = -BD(1) - 2.0		HY LIM
	P1 = -BD(1) - 1.0		HY LIM
	PO1 = 1.0/P1		HY LIM
	P2 = -BD(1)/P1		HY LIM
	DO 10 I = 1,3		HY LIM
	TV(I) = 0.0		HY LIM
10	IF(V(I).NE.0.0)TV(I) = HYFCN(1.0/V(I),V(I),BD(I+1),P2)		HYFIX
C	GET RECIPROCAL SET		HY LIM
	CALL CROSS(V,W,EI)		HY LIM
	CALL CROSS(W,U,EJ)		HY LIM
	CALL CROSS(U,V,T)		HY LIM
	EIU = EI(1)*U(1) + EI(2)*U(2) + EI(3)*U(3)		HY LIM
	G = C*EIU		HY LIM
C			HY LIM
	DO 55 IT = 1,ITER		HY LIM
	EVM = 0.0		HY LIM
	EVZ = 0.0		HY LIM
	ZEZ = 0.0		HY LIM
	USEV = .FALSE.		HY LIM
	DO 15 I = 1,3		HY LIM
	E(I) = HYFCN(BD(I+16),Z(I),BD(I+1),POW)		HY LIM
	EV(I) = E(I)*V(I)		HY LIM
	IF(EV(I).EQ.0.0)USEV = .TRUE.		HY LIM
	IF(DABS(EV(I)).GT.EVM)EVM = DABS(EV(I))		HY LIM
	EZ(I) = E(I)*Z(I)		HY LIM
	IF(DABS(EZ(I)).GT.EVZ)EVZ = DABS(EZ(I))		HY LIM
15	ZEZ = ZEZ + Z(I)*EZ(I)		HY LIM
	RHO = ZEZ**PP		HY LIM
	DO 20 I = 1,3		HY LIM
20	Z(I) = Z(I)/RHO		HY LIM
	IF(PASS)GO TO 60		HY LIM
	RHOZ = ZEZ/RHO		HY LIM
	RHOV = EVM*RHOZ/RHO		HY LIM
	RHOZ = EVZ*RHOZ		HY LIM
	IF(.NOT.USEV)GO TO 30		HY LIM
	RHOV = 1.0		HY LIM
	DO 25 I = 1,3		HY LIM
25	EV(I) = TV(I)		HY LIM
C	WHAT IF NO TV IS 0 AND EV ARE ALL 0 ?		HY LIM
	30 DO 35 I = 1,3		HY LIM

EV(I) = EV(I)/RHOV	HYLIM
35 EZ(I) = EZ(I)/RHOZ	HYLIM
C SET UP MATRIX	HYLIM
CALL CROSS(EV, T, SM(1,1))	HYLIM
CALL CROSS(T, EZ, SM(1,2))	HYLIM
CALL CROSS(EZ, EV, SM(1,3))	HYLIM
TZV = T(1)*SM(1,3) + T(2)*SM(2,3) + T(3)*SM(3,3)	HYLIM
TZ = T(1)*Z(1) + T(2)*Z(2) + T(3)*Z(3)	HYLIM
ZEV = Z(1)*EV(1) + Z(2)*EV(2) + Z(3)*EV(3)	HYLIM
IF(TZV.EQ.0.0)STOP 39	HYLIM
ZEV = ZEV/TZV	HYLIM
Q(1) = 0.0	HYLIM
Q(2) = -ZEV	HYLIM
IF(.NOT.USEV)Q(2) = Q(2)/P1	HYLIM
Q(3) = (G - TZ)/TZV	HYLIM
CALL MAT31(SM,Q,S)	HYLIM
SS = 0.0	HYLIM
ZZ = 0.0	HYLIM
DO 50 I = 1,3	HYLIM
SS = SS + DABS(S(I))	HYLIM
IF(DABS(Z(I)).LT.0.1*BD(I+1))GO TO 45	HYLIM
IF(DABS(S(I)).GT.DABS(Z(I)))S(I) = DSIGN(0.5*Z(I),S(I))	HYLIM
45 Z(I) = Z(I) + S(I)	HYLIM
IF(DABS(Z(I)).GT.BD(I+1))Z(I) = DSIGN(BD(I+1),Z(I))	HYLIM
50 ZZ = ZZ + DABS(Z(I))	HYLIM
IF(SS.LT.1.0E-10*ZZ)PASS = .TRUE.	HYLIM
55 CONTINUE	HYLIM
C	HYLIM
60 A = (EI(1)*Z(1) + EI(2)*Z(2) + EI(3)*Z(3))/EIU	HYLIM
B = (EJ(1)*Z(1) + EJ(2)*Z(2) + EJ(3)*Z(3))/EIU	HYLIM
RETURN	HYLIM
END	HYLIM



55  $S(I,M) = S(I,M) - E(I)*S(K,M)$   
60 CONTINUE  
GO TO 10  
65 RETURN  
END

HYLPR  
HYLPR  
HYLPR  
HYLPR  
HYLPR



SUBROUTINE HYLPM(BM,BN)		HYLPX
C		REV IV 02/07/87HYLPX
C	LINEAR PROGRAM EXEC	HYLPX
	IMPLICIT REAL*8(A-H,O-Z)	HYLPX
	DIMENSION BM(23),BN(23)	HYLPX
	COMMON/TEMPVS/D12(3,3),P(3,3),Q(3,3),XMN(3),RLN(3),XMM(3),	HYLPX
	* R(3),H(3),D(3,3),V(7),S(9,8),C(16),A(7),B(3),	HYLPX
	* E(9),T(7),ID(16),IP(2),DMY(34932)	80386
	CALL MAT31(D,BN,B)	HYLPX
	DO 10 I = 1,3	HYLPX
	B(I) = BM(I) - B(I) + R(I)	HYLPX
	A(I) = BM(I)	HYLPX
10	A(I+3) = BN(I)	HYLPX
	A(7) = -1.0	HYLPX
	DO 15 I = 1,16	HYLPX
	C(I) = 0.0	HYLPX
15	ID(I) = I	HYLPX
	C(7) = -1.0	HYLPX
	DO 20 I = 1,9	HYLPX
	DO 20 J = 1,8	HYLPX
20	S(I,J) = 0.0	HYLPX
C		HYLPX
COSTS	0 0 -1	HYLPX
C	I -D -R A - DB + R (>0) INF COST	HYLPX
C	I 0 0 2A	HYLPX
C	0 I 0 2B	HYLPX
C		HYLPX
	DO 25 I = 1,6	HYLPX
25	S(I+3,I) = 1.0	HYLPX
	DO 30 I = 1,3	HYLPX
	C(I+7) = 10.	HYLPX
	S(I,7) = -R(I)	HYLPX
	S(I,I) = 1.0	HYLPX
	S(I,8) = B(I)	HYLPX
	S(I+3,8) = 2.0*A(I)	HYLPX
	S(I+6,8) = 2.0*A(I+3)	HYLPX
	DO 30 J = 1,3	HYLPX
30	S(I,J+3) = -D(I,J)	HYLPX
CHECK	SIGN OF RHS	HYLPX
	DO 40 I = 1,3	HYLPX
	IF(B(I).GE.0.0)GO TO 40	HYLPX
	DO 35 J = 1,8	HYLPX
35	S(I,J) = -S(I,J)	HYLPX
40	CONTINUE	HYLPX
	J1 = 1	HYLPX
	J2 = 7	HYLPX
C		HYLPX
	CALL HYLPR(J1,J2,ID,C,S,E,T)	HYLPX
	NK = 0	HYLPX
	NZ = 0	HYLPX
COUNT	ZEROES IN SOLUTION	HYLPX
	DO 45 I = 1,7	HYLPX

C TEST SHOULD PROBABLY BE AN EPSILON TEST, DABS(T(I)).GT.EPS	HYLPX
IF((T(I).NE.0.0).OR.(C(I).EQ.10.))GO TO 45	HYLPX
NZ = NZ + 1	HYLPX
IP(NZ) = I	HYLPX
45 CONTINUE	HYLPX
C SET PASS COUNT	HYLPX
NP = 1	HYLPX
IF(NZ.GT.0)NP = 2**NZ	HYLPX
C	HYLPX
DO 55 M = 1,NP	HYLPX
NM = NK	HYLPX
NK = NK + 1	HYLPX
DO 50 I = 1,16	HYLPX
K = ID(I)	HYLPX
IF(K.GT.7)GO TO 50	HYLPX
W = 0.0	HYLPX
IF(I.GT.7)W = S(I-7,8)	HYLPX
V(K) = (W - A(K) + NM*V(K))/NK	HYLPX
50 CONTINUE	HYLPX
C LOOK FOR ALL SOLUTIONS	HYLPX
IF(M.EQ.NP)GO TO 55	HYLPX
J1 = IP(1)	HYLPX
IP(1) = IP(2)	HYLPX
IP(2) = J1	HYLPX
IF(T(J1).NE.0.0)GO TO 55	HYLPX
J2 = J1	HYLPX
CALL HYLPR(J1,J2,ID,C,S,E,T)	HYLPX
55 CONTINUE	HYLPX
RETURN	HYLPX
END	HYLPX

SUBROUTINE HYNTR(BM,BN,TAB)		HYNTR
C	IMPLICIT REAL*8(A-H,O-Z)	REV IV 02/07/87HYNTR
	CALCULATIONS IN SEGMENT M'S REFERENCE	HYNTR
	DIMENSION BM(24),BN(24),TAB(8)	HYNTR
	COMMON/TEMPVS/D12(3,3),A(3,3),B(3,3),XMN(3),RLN(3),XMM(3),	HYNTR
	* AZ(3),R(3),Z(3),DNM(3,3),DAD(3,3),DBD(3,3),	HYNTR
	* BMD(3,3),TMP(3,3),S(5,6),ZVR(3),BZV(3),V(3),	HYNTR
	* ZM(3),VN(3),F(2),BV(3),DMMY(34973)	80386
	P1 = 2.0	HYNTR
	P2 = 2.0	HYNTR
	IF(BM(1).LT.-2.0)P1 = -BM(1)	HYNTR
	IF(BN(1).LT.-2.0)P2 = -BN(1)	HYNTR
	C1 = P1 - 1.0	HYNTR
	CN = P2 - 1.0	HYNTR
C	DNM TRANSFORMS FROM M TO NN	HYNTR
	K = 8	HYNTR
	DO 15 J = 1,3	HYNTR
	DO 10 I = 1,3	HYNTR
	BMD(I,J) = 0.0	HYNTR
	IF(BM(1).LT.0.0)BMD(I,J) = BM(K)	HYNTR
	DNM(I,J) = D12(I,J)	HYNTR
	10 K = K + 1	HYNTR
	15 IF(BM(1).GT.0.0)BMD(J,J) = 1.0	HYNTR
	IF(BN(1).LT.0.0)CALL DOTT33(BN(8),D12,DNM)	HYNTR
	ALP = TAB(1)	HYNTR
	BET = TAB(2)	HYNTR
	DO 20 I = 1,3	HYNTR
	ZM(I) = TAB(I+2)	HYNTR
	20 VN(I) = TAB(I+5)	HYNTR
C	PUT VECTORS INTO M'S REFERENCE	HYNTR
	CALL DOT31(BMD,ZM,Z)	HYNTR
	CALL DOT31(DNM,VN,V)	HYNTR
	DO 25 I = 1,3	HYNTR
	25 ZVR(I) = Z(I) - V(I) - BET*R(I)	HYNTR
C		HYNTR
	DO 40 ITER = 1,100	HYNTR
	CALL HYABF(BM,ZM,A,F(1))	HYNTR
	CALL HYABF(BN,VN,B,F(2))	HYNTR
	CALL DOT31(BMD,A(1,2),AZ)	HYNTR
	CALL DOT31(DNM,B(1,2),BV)	HYNTR
	CALL HYDAD(BMD,A,DAD)	HYNTR
	CALL HYDAD(DNM,B,DBD)	HYNTR
	CALL MAT31(DBD,R,S(1,5))	HYNTR
	CALL MAT31(DBD,ZVR,BZV)	HYNTR
	C2 = CN*ALP	HYNTR
C	SET UP S MATRIX	HYNTR
	S(4,4) = 0.0	HYNTR
	S(5,5) = 0.0	HYNTR
	S(4,6) = (1.0 - F(2))/P2 - V(1)*BZV(1) - V(2)*BZV(2) - V(3)*BZV(3)	HYNTR
	S(5,6) = (1.0 - F(1))/P1	HYNTR
	S(4,5) = -BV(1)*R(1) - BV(2)*R(2) - BV(3)*R(3)	HYNTR

S(5,4) = 0.0	HYNTR
DO 30 I = 1,3	HYNTR
S(I,4) = BV(I)	HYNTR
S(4,I) = BV(I)	HYNTR
S(I,5) = -C2*S(I,5)	HYNTR
S(5,I) = AZ(I)	HYNTR
S(I,6) = -AZ(I) - ALP*BV(I) - C2*BZV(I)	HYNTR
DO 30 J = 1,3	HYNTR
30 S(I,J) = C1*DAD(I,J) + C2*DBD(I,J)	HYNTR
CALL HYSOL(S,5,5)	HYNTR
TALP = ALP + S(4,6)	HYNTR
IF(TALP.LE.0.0)TALP = ALP/2.0	HYNTR
ALP = TALP	HYNTR
TBET = BET + S(5,6)	HYNTR
IF(TBET.LE.0.0)TBET = BET/2.0	HYNTR
BET = TBET	HYNTR
SS = 0.0	HYNTR
ZZ = 0.0	HYNTR
DO 35 I = 1,3	HYNTR
SS = SS + DABS(S(I,6))	HYNTR
Z(I) = Z(I) + S(I,6)	HYNTR
ZZ = ZZ + DABS(Z(I))	HYNTR
V(I) = Z(I) - BET*R(I)	HYNTR
35 ZVR(I) = 0.0	HYNTR
CALL MAT31(BMD,Z,ZM)	HYNTR
CALL MAT31(DNM,V,VN)	HYNTR
CONVERGENCE TEST DEPENDS ON REAL*4 (1.0E-5) OR REAL*8 (??)	HYNTR
IF(SS.LT.1.0E-10*ZZ)GO TO 50	HYNTR
K = 1	HYNTR
L = 1	HYNTR
IF(BM(1).LT.0.0)K = 2	HYNTR
IF(BN(1).LT.0.0)L = 2	HYNTR
DO 37 I = 1,3	HYNTR
IF(DABS(ZM(I)).GT.BM(K)) ZM(I) = DSIGN(BM(K),ZM(I))	HYNTR
IF(DABS(VN(I)).GT.BN(L)) VN(I) = DSIGN(BN(L),VN(I))	HYNTR
K = K + 1	HYNTR
37 L = L + 1	HYNTR
CALL DOT31(BMD,ZM,Z)	HYNTR
CALL DOT31(DNM,VN,V)	HYNTR
DO 38 I = 1,3	HYNTR
38 ZVR(I) = Z(I) - V(I) - BET*R(I)	HYNTR
40 CONTINUE	HYNTR
C WRITE(6,45)	HYNTR
C 45 FORMAT(' HYNTR DID NOT CONVERGE, CONTACT IGNORED.')	HYNTR
BET = 1.0	HYNTR
50 TAB(1) = ALP	HYNTR
TAB(2) = BET	HYNTR
DO 55 I = 1,3	HYNTR
TAB(I+2) = ZM(I)	HYNTR
55 TAB(I+5) = VN(I)	HYNTR
RETURN	HYNTR
END	HYNTR

	DOUBLE PRECISION FUNCTION HYPEN(BD,E,V)		HYPEN
C		REV IV	02/07/87HYPEN
C	POINT OF MAXIMUM PENETRATION		HYPEN
C	SOLVES FOR VALUE OF ALP USED BY PLELP		HYPEN
C	POWERS OF HYPERELLIPSOID MAY BE DIFFERENT		HYPEN
	IMPLICIT REAL*8(A-H,O-Z)		HYPEN
	DIMENSION BD(24),E(3),V(3)		HYPEN
	FX(A) = A**E(1)*V(1)+A**E(2)*V(2)+A**E(3)*V(3)-1.0		HYPEN
	L = 1		HYPEN
	VM = V(1)		HYPEN
	DO 10 I = 2,3		HYPEN
	IF (V(I).LE.VM) GO TO 10		HYPEN
	L = I		HYPEN
	VM = V(I)		HYPEN
10	CONTINUE		HYPEN
	A = V(1) + V(2) + V(3)		HYPEN
	A = 1.0/A**(1.0/E(L))		HYPEN
	DEL = A/2.0		HYPEN
	AP = 0.0		HYPEN
12	F = FX(A)		HYPEN
	IF (DABS(F).LT.1.D-08) GO TO 40		HYPEN
	IF (F) 16,40,14		HYPEN
14	IF (A-DEL.LE.0.0) DEL = A/2.0		HYPEN
	AP = A		HYPEN
	FP = F		HYPEN
	A = A - DEL		HYPEN
	GO TO 12		HYPEN
16	IF (AP.NE.0.0) GO TO 18		HYPEN
	A = A + DEL		HYPEN
	GO TO 12		HYPEN
18	AM = A		HYPEN
	FM = F		HYPEN
20	IF (FP.EQ.FM) GO TO 40		HYPEN
	DEL = -FM*(AP - AM)/(FP - FM)		HYPEN
	AN = AM + DEL		HYPEN
	IF (AN.EQ.A) GO TO 40		HYPEN
	A = AN		HYPEN
	F = FX(A)		HYPEN
	IF (DABS(F).LT.1.D-08) GO TO 40		HYPEN
	IF (F) 18,40,22		HYPEN
22	FP = F		HYPEN
	AP = A		HYPEN
	GO TO 20		HYPEN
40	HYPEN = A		HYPEN
	RETURN		HYPEN
	END		HYPEN





	SUBROUTINE HYVAL(A,U,R,BD,L)		HYVAL
C		REV IV	12/11/87HYFIX
	IMPLICIT REAL*8(A-H,O-Z)		HYVAL
C	GIVEN A,U,R: COMPUTE A      Z = A*U + R		HYVAL
	DIMENSION BD(24),U(3),R(3),RM(2)		HYFIX
	ONE = 1.0		HYFIX
	POW = -BD(1) - 2.0		HYVAL
C	ARE THESE THE CORRECT TESTS??		HYFIX
	TEST = -BD(1)*0.000001		HYFIX
	TESD = 0.000001		HYFIX
	CALL HYVBX(U,R,BD(2),M,RM)		HYVAL
	A = 0.0		HYFIX
	IF (M.LT.L) GO TO 50		HYFIX
C	THIS SHOULD NEVER HAPPEN - IMPLIES R IS OUTSIDE BOX		HYFIX
	A = RM(L)		HYVAL
	IF (DABS(A).LT.TESD) GO TO 50		HYFIX
	DEL = A/5.0		HYFIX
	NSTEP = 0		HYFIX
C	ITERATION LOOP		HYFIX
10	DEL = DEL/4.0		HYFIX
	NSTEP = NSTEP + 1		HYFIX
	IF (NSTEP.LT.100) GO TO 12		HYFIX
	WRITE(6,11) M,A,DEL,F1,F2,L,RM(1),RM(2),U,R,BD		HYFIX
11	FORMAT(' HYV ',I4,4F11.6,I3,2F11.6/4X,3F11.6,4X,3F11.6/ * 4(2X,7F10.4/))		HYFIX
	STOP 102		HYFIX
12	F2 = HYVFN(A,U,R,BD,POW)		HYFIX
	IF (DABS(F2).LT.TEST) GO TO 50		HYFIX
	IF (F2) 20,50,30		HYFIX
15	F2 = HYVFN(A,U,R,BD,POW)		HYFIX
	NSTEP = NSTEP + 1		HYFIX
	IF (NSTEP.LT.100) GO TO 17		HYFIX
	WRITE(6,11) M,A,DEL,F1,F2,L,RM(1),RM(2),U,R,BD		HYFIX
	STOP 103		HYFIX
17	IF (DABS(F2).LT.TEST) GO TO 50		HYFIX
	IF (F2) 20,50,35		HYFIX
20	IF (DSIGN(ONE,A).EQ.DSIGN(ONE,A+DEL)) GO TO 22		HYFIX
	A = A/2.0		HYFIX
	DL = -A		HYFIX
	GO TO 23		HYFIX
22	DL = DEL		HYFIX
	A = A + DEL		HYFIX
23	F1 = F2		HYFIX
	GO TO 15		HYFIX
25	F2 = HYVFN(A,U,R,BD,POW)		HYFIX
	NSTEP = NSTEP + 1		HYFIX
	IF (NSTEP.LT.100) GO TO 27		HYFIX
	WRITE(6,11) M,A,DEL,F1,F2,L,RM(1),RM(2),U,R,BD		HYFIX
	STOP 104		HYFIX
27	IF (DABS(F2).LT.TEST) GO TO 50		HYFIX
	IF (F2) 35,50,30		HYFIX
30	IF (DSIGN(ONE,A).EQ.DSIGN(ONE,A-DEL)) GO TO 32		HYFIX



A = A/2.0	HYFIX
DL = -A	HYFIX
GO TO 33	HYFIX
32 DL = -DEL	HYFIX
A = A - DEL	HYFIX
33 F1 = F2	HYFIX
GO TO 25	HYFIX
35 IF (F1.EQ.F2) GO TO 50	HYFIX
A = A + F2*DL/(F1 - F2)	HYFIX
IF (DABS(DEL).GT.TESD) GO TO 10	HYFIX
C	HYVAL
50 RETURN	HYVAL
END	HYVAL

	SUBROUTINE HYVBX(Q,S,B,M,RM)		HYVBX
C	IMPLICIT REAL*8(A-H,O-Z)	REV IV	02/07/87HYVBX
	DIMENSION Q(3),S(3),B(3),RM(2)		HYVBX
C	FINDS LIMITS OF BOX IN DIRECTION Q. $Z = R*Q + S$		HYVBX
	LOGICAL VAL		HYVBX
	M = 0		HYVBX
	C = -1.0		HYVBX
	DO 30 I = 1,3		HYVBX
	IF(Q(I).EQ.0.0)GO TO 30		HYVBX
	DO 25 K = 1,2		HYVBX
	VAL = .TRUE.		HYVBX
	D = C*B(I) - S(I)		HYVBX
	DO 10 J = 1,3		HYVBX
	IF(J.EQ.I)GO TO 10		HYVBX
	IF(DABS(D*Q(J) + S(J)*Q(I)).GT.DABS(B(J)*Q(I)))VAL = .FALSE.		HYVBX
C	IF(DABS(R*Q(J) + S(J)).GT.B(J))VAL = .FALSE.		HYVBX
10	CONTINUE		HYVBX
	IF(.NOT.VAL)GO TO 25		HYVBX
	R = D/Q(I)		HYVBX
	IF(M.EQ.0)GO TO 20		HYVBX
	DO 15 L = 1,M		HYVBX
	IF(R.EQ.RM(L)) GO TO 25		HYVBX
15	CONTINUE		HYVBX
20	M = M + 1		HYVBX
	RM(M) = R		HYVBX
25	C = -C		HYVBX
30	CONTINUE		HYVBX
	IF(M.EQ.0)GO TO 35		HYVBX
	IF(RM(1).LT.RM(2))GO TO 35		HYVBX
	R = RM(1)		HYVBX
	RM(1) = RM(2)		HYVBX
	RM(2) = R		HYVBX
35	RETURN		HYVBX
	END		HYVBX

	DOUBLE PRECISION FUNCTION HYVFN(A,U,R,B,P)		HYVFN
C		REV IV	12/11/87HYVFN
	IMPLICIT REAL*8(A-H,O-Z)		HYVFN
	DIMENSION U(3),R(3),B(24)		HYVFN
	F = -1.0		HYVFN
	DO 10 I = 1,3		HYVFN
	Z = A*U(I) + R(I)		HYVFN
	C = B(I+16)		HYVFN
	IF (P.GT.0.0) C = HYFCN(C,Z,B(I+1),P)		HYVFN
10	F = F + C*Z**2		HYVFN
	HYVFN = F		HYVFN
	RETURN		HYVFN
	END		HYVFN

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C      SUBROUTINE IMPLS2(MODE,J,H)
C
C      REV IV    07/24/86SLIP
C      CALLED BY SUBROUTINE UPDATE WHEN JOINT J LOCKS TO APPLY IMPULSE
C      TO SET P.(D(M)'W(M) - D(N)'W(N)) = 0
C
C      ARGUMENTS:
C      MODE - 0: FULL LOCK      P = I
C              1: AXIS (H) FREE  P = I-HH'
C              -1: AXIS (H) LOCKED P = HH'
C
C      J      - JOINT IDENTIFICATION NUMBER
C
C      H      - AXIS VECTOR
C
C      IMPLICIT REAL*8(A-H,O-Z)
C      COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,
C      *              NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG
C      COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),
C      *              SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)
C      COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),
C      *              RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),
C      *              JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)
C      COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),
C      *              F(3,30),TQ(3,30),WJ(30),A11(3,3,30)
C      COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24),
C      *              HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12),
C      *              RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12),
C      *              KQ1(12),KQ2(12),KQTYPE(12)
C      COMMON/FLXBLE/ HF(4,12,8),B42(3,3,24),V4(3,8),NFLEX(3,8)
C      COMMON/TEMPVS/ SM(3),SN(3),TM(3,3),TN(3,3),T(3,4),TT(3,4)
C      *              ,DMMY(35065)
C      DIMENSION      TWA(3,3,30),TLA(3,3,30),H(3)
C      CALL ELTIME(1,28)
C      M = JNT(J)
C      N = J+1
C      DO 20 L=1,3
C      DO 12 K=1,NGRND
C      DO 12 I=1,3
C      U1(I,K) = 0.0
C 12 U2(I,K) = 0.0
C      DO 13 K=1,NJNT
C      DO 13 I=1,3
C      V1(I,K) = 0.0
C 13 V2(I,K) = 0.0
C      IF (NQ.LE.0) GO TO 15
C      DO 14 K=1,NQ
C      DO 14 I=1,3
C 14 V3(I,K) = 0.0
C 15 IF (NFLX.EQ.0) GO TO 18
C      DO 19 K=1,NFLX
C      DO 19 I=1,3

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19 V4(I,K) = 0.0	IMPLS2
18 DO 16 I=1,3	IMPLS2
U2(I,M) = RPHI(I,M)*D(I,L,M)	IMPLS2
16 U2(I,N) = -RPHI(I,N)*D(I,L,N)	IMPLS2
CALL DAUX(L)	IMPLS2
DO 17 K=1,NGRND	IMPLS2
DO 17 I=1,3	IMPLS2
TLA(I,L,K) = SEGLA(I,K)	IMPLS2
17 TWA(I,L,K) = WMEGD(I,K)	IMPLS2
20 CONTINUE	IMPLS2
CALL DOT33(D(1,1,M),TWA(1,1,M),TM)	IMPLS2
CALL DOT33(D(1,1,N),TWA(1,1,N),TN)	IMPLS2
CALL DOT31(D(1,1,M),WMEG(1,M),SM)	IMPLS2
CALL DOT31(D(1,1,N),WMEG(1,N),SN)	IMPLS2
DO 22 I=1,3	IMPLS2
DO 21 K=1,3	IMPLS2
T(I,K) = TM(I,K) - TN(I,K)	IMPLS2
21 TT(I,K) = T(I,K)	IMPLS2
T(I,4) = SN(I) - SM(I)	IMPLS2
22 TT(I,4) = H(I)	IMPLS2
IF (MODE.GE.0) CALL DSMSOL(T,3,3)	IMPLS2
IF (MODE.GT.0) CALL DSMSOL(TT,3,3)	IMPLS2
IF (MODE) 24,29,25	IMPLS2
24 ST = 0.0	IMPLS2
STT = XDY(H,T,H)	IMPLS2
GO TO 26	IMPLS2
25 ST = 1.0	IMPLS2
STT = -(H(1)*TT(1,4) + H(2)*TT(2,4) + H(3)*TT(3,4))	IMPLS2
26 STT = (H(1)*T(1,4) + H(2)*T(2,4) + H(3)*T(3,4))/STT	IMPLS2
DO 27 I=1,3	IMPLS2
27 T(I,4) = ST*T(I,4) + STT*TT(I,4)	IMPLS2
29 DO 30 K=1,NGRND	IMPLS2
DO 30 I=1,3	IMPLS2
DO 30 L=1,3	IMPLS2
SEGLV(I,K) = SEGLV(I,K) + T(L,4)*TLA(I,L,K)	IMPLS2
30 WMEG(I,K) = WMEG(I,K) + T(L,4)*TWA(I,L,K)	IMPLS2
IF (NPRT(3).NE.0) CALL PRINT(6HIMPLS2)	IMPLS2
CALL ELTIME(2,28)	IMPLS2
RETURN	IMPLS2
END	IMPLS2

	SUBROUTINE IMPULS(I1,I2,I3)		IMPULS
C		REV IV	07/24/86SLIP
C	ARGUMENTS: I1 - 1 - IMPULS FOR PLELP.		IMPULS
C	3 - IMPULS FOR SEGSEG.		IMPULS
C	4 - IMPULS FOR VISPR OR EJOINT		IMPULS
C	I2 - INDEX OF CONTACTING SEGMENT OR JOINT AXIS		IMPULS
C	I3 - INDEX OF PLANE, SEGMENT OR JOINT AXIS		IMPULS
C			IMPULS
C	IMPLICIT REAL*8 (A-H,O-Z)		IMPULS
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		IMPULS
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),		IMPULS
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		IMPULS
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),		SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),		IMPULS
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)		IMPULS
	COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),		IMPULS
*	F(3,30),TQ(3,30),WJ(30),A11(3,3,30)		SLIP
	COMMON/JBARTZ/ MNPL( 30),MNBLT( 8),MNSEG( 30),MNBAG( 6),		IMPULS
*	MPL(3,5,30),MBLT(3,5,8),MSEG(3,5,30),MBAG(3,10,6),		IMPULS
*	NTPL( 5,30),NTBLT( 5,8),NTSEG( 5,30)		IMPULS
	COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24),		IMPULS
*	HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12),		IMPULS
*	RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12),		IMPULS
*	KQ1(12),KQ2(12),KQTYPE(12)		IMPULS
	COMMON/FLXBLE/ HF(4,12,8),B42(3,3,24),V4(3,8),NFLEX(3,8)		IMPULS
	COMMON/TEMPVI/ CREST,TTI(3),R1I(3),R2I(3),JSTOP(4,2,30)		IMPULS
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)		DIMENB
	DIMENSION TEMP(3),DWR1(3),DWR2(3),DWR3(3),DWR4(3),VREL(3),DV(3)		IMPULS
	IF (TIME.EQ.0.0) GO TO 99		IMPULS
C			IMPULS
C	SPECIAL SETUP FOR CALL TO SUBROUTINE DAUX		IMPULS
C	REPLACE SETUP WITH U1,U2,V1,V2,V3 = 0.		IMPULS
C	ASSUME OTHER ARRAYS FROM PREVIOUS CALL TO DAUX.		IMPULS
C			IMPULS
	CALL ELTIME(1,27)		IMPULS
	CALL OUTPUT(0)		IMPULS
	KQTEST = 0		IMPULS
	NT = 0		IMPULS
	IF (I1.EQ.1) NT = NTPL (I2,I3)		IMPULS
	IF (I1.EQ.3) NT = NTSEG(I2,I3)		IMPULS
	IF (NT.EQ.0) GO TO 29		IMPULS
	KQ = -NTAB(NT+1)		IMPULS
	IF (KQ.LE.0) GO TO 29		IMPULS
	KQTYPE(KQ) = IABS(KQTYPE(KQ))		IMPULS
	CALL DAUX(0)		IMPULS
29	IF (NQ.LE.0) GO TO 31		IMPULS
	DO 30 J=1,NQ		IMPULS
	DO 30 I=1,3		IMPULS
30	V3(I,J) = 0.0		IMPULS
31	DO 32 J=1,NGRND		IMPULS

DO 32 I=1,3	IMPULS
U1(I,J) = 0.0	IMPULS
32 U2(I,J) = 0.0	IMPULS
IF (NJNT.LE.0) GO TO 21	IMPULS
DO 33 J=1,NJNT	IMPULS
DO 33 I=1,3	IMPULS
V1(I,J) = 0.0	IMPULS
33 V2(I,J) = 0.0	IMPULS
21 IF (NFLX.EQ.0) GO TO 23	IMPULS
DO 22 J=1,NFLX	IMPULS
DO 22 I=1,3	IMPULS
22 V4(I,J) = 0.0	IMPULS
C	IMPULS
C REPLACE CALLS TO CONTACT AND VISPR WITH SINGLE CALL	IMPULS
C AT FIRST CONTACT IF NOT CONSTRAINT.	IMPULS
C	IMPULS
23 IF (I1.NE.1) GO TO 34	IMPULS
NT = NTPL(I2,I3)	IMPULS
M1 = MPL(1,I2,I3)	IMPULS
M2 = MPL(2,I2,I3)	IMPULS
M3 = MPL(3,I2,I3)	IMPULS
CALL PLELP(M2,M3,M1,I3,NT)	IMPULS
IF (NTAB(NT+1).LT.0) GO TO 37	IMPULS
K1 = M2	IMPULS
K2 = M1	IMPULS
GO TO 39	IMPULS
34 IF (I1.NE.3) GO TO 35	IMPULS
NT = NTSEG(I2,I3)	IMPULS
M1 = MSEG(1,I2,I3)	IMPULS
M2 = MSEG(2,I2,I3)	IMPULS
M3 = MSEG(3,I2,I3)	IMPULS
CALL SEGSEG(I3,M1,M2,M3,NT)	IMPULS
IF (NTAB(NT+1).LT.0) GO TO 37	IMPULS
K1 = I3	IMPULS
K2 = M2	IMPULS
GO TO 39	IMPULS
35 IF (I1.NE.4) WRITE (6,36) I1,I2,I3	IMPULS
36 FORMAT('0 IMPROPER ARGUMENTS TO SUBROUTINE IMPULS'/	IMPULS
* ' ARGUMENTS = ', 3I6 /	IMPULS
* ' PROGRAM TERMINATED' )	IMPULS
IF (I1.NE.4) STOP 33	IMPULS
C	IMPULS
C RECALL VISPR FOR JOINT STOP.	IMPULS
C	IMPULS
IF (IABS(IPIN(I3)).NE.4) GO TO 25	IMPULS
CALL EJOINT(I2,I3)	IMPULS
GO TO 26	IMPULS
25 CALL VISPR(I2,I3)	IMPULS
26 K1 = IABS(JNT(I3))	IMPULS
K2 = I3+1	IMPULS
GO TO 39	IMPULS
C	IMPULS

C	SET UP SPECIAL U1,U2 FOR FIRST CONTACT OF CONSTRAINT.	IMPULS
C		IMPULS
37	KQ = -NTAB(NT+1)	IMPULS
	KQTEST = 1	IMPULS
	KQTYPE(KQ) = -IABS(KQTYPE(KQ))	IMPULS
	K1 = KQ1(KQ)	IMPULS
	K2 = KQ2(KQ)	IMPULS
	IF (K1.GT.NSEG) GO TO 38	IMPULS
	CALL MAT31(A13(1,1,2*KQ-1),QQ(1,KQ),U1(1,K1))	IMPULS
	CALL MAT31(A23(1,1,2*KQ-1),QQ(1,KQ),U2(1,K1))	IMPULS
38	IF (K2.GT.NSEG) GO TO 39	IMPULS
	CALL MAT31(A13(1,1,2*KQ ),QQ(1,KQ),U1(1,K2))	IMPULS
	CALL MAT31(A23(1,1,2*KQ ),QQ(1,KQ),U2(1,K2))	IMPULS
C		IMPULS
C	FINAL SETUP OF U1 AND U2	IMPULS
C		IMPULS
39	DO 40 J=1,NGRND	IMPULS
	DO 40 I=1,3	IMPULS
	U1(I,J) = U1(I,J)*RW(J)	IMPULS
40	U2(I,J) = U2(I,J)*RPHI(I,J)	IMPULS
	CALL DAUX(I1)	IMPULS
	IF (KQTEST.EQ.1) KQTYPE(KQ) = IABS(KQTYPE(KQ))	IMPULS
	IF (NPRT(10).NE.0) CALL PRINT(6HPREIMP)	IMPULS
	IF (I1.GT.3) GO TO 51	IMPULS
	IF (NPRT(10).NE.0) WRITE (6,42) R1I,R2I	IMPULS
42	FORMAT ('0'/(6G20.8))	IMPULS
	CALL CROSS(WMEG (1,K1),R1I(1),TEMP)	IMPULS
	CALL DOT31(D(1,1,K1),TEMP,DWR1(1))	IMPULS
	CALL CROSS(WMEG (1,K2),R2I(1),TEMP)	IMPULS
	CALL DOT31(D(1,1,K2),TEMP,DWR2(1))	IMPULS
	CALL CROSS(WMEGD(1,K1),R1I(1),TEMP)	IMPULS
	CALL DOT31(D(1,1,K1),TEMP,DWR3(1))	IMPULS
	CALL CROSS(WMEGD(1,K2),R2I(1),TEMP)	IMPULS
	CALL DOT31(D(1,1,K2),TEMP,DWR4(1))	IMPULS
	TVREL = 0.0	IMPULS
	TDV = 0.0	IMPULS
	DO 50 I=1,3	IMPULS
	VREL(I) = SEGLV(I,K1)+DWR1(I) - SEGLV(I,K2)-DWR2(I)	IMPULS
	DV (I) = SEGLA(I,K1)+DWR3(I) - SEGLA(I,K2)-DWR4(I)	IMPULS
	TVREL = TVREL + TTI(I)*VREL(I)	IMPULS
50	TDV = TDV + TTI(I)*DV (I)	IMPULS
	GO TO 53	IMPULS
51	CALL DOT31(D(1,1,K1),WMEG (1,K1),DWR1(1))	IMPULS
	CALL DOT31(D(1,1,K2),WMEG (1,K2),DWR2(1))	IMPULS
	CALL DOT31(D(1,1,K1),WMEGD(1,K1),DWR3(1))	IMPULS
	CALL DOT31(D(1,1,K2),WMEGD(1,K2),DWR4(1))	IMPULS
	TVREL = 0.0	IMPULS
	TDV = 0.0	IMPULS
	DO 52 I=1,3	IMPULS
	VREL(I) = DWR1(I) - DWR2(I)	IMPULS
	DV (I) = DWR3(I) - DWR4(I)	IMPULS
	TVREL = TVREL + TTI(I)*VREL(I)	IMPULS



52	TDV	=	TDV	+	TTI(I)*DV	(I)		IMPULS
53	ALPHA	=	0.0					IMPULS
C								IMPULS
C	NOTE:		CREST	IS	SUPPLIED	AS	(1+E)/2	WHERE E IS THE CLASSICAL
C	COEFFICIENT	OF	RESTITUTION	BUT	WITH	A	RANGE	OF -1 TO +1.
C	CREST	HAS	A	RANGE	OF	0	TO	+1 WHERE 0 (E=-1) REPRESENTS NO IMPULSE.
C								IMPULS
	IF	(TDV.NE.0.0)	ALPHA	=	-2.0*CREST*TVREL/TDV			IMPULS
	IF	(NPRT(10).NE.0)	WRITE	(6,42)	DWR1,DWR2,DWR3,DWR4,			IMPULS
	*				TTI,VREL,DV,			IMPULS
	*				TVREL,TDV,CREST,ALPHA			IMPULS
	DO	60	J=1,NGRND					IMPULS
	DO	60	I=1,3					IMP' LS
	SEGLV(I,J)	=	SEGLV(I,J)	+	ALPHA*SEGLA(I,J)			IMPULS
60	WMEG(I,J)	=	WMEG(I,J)	+	ALPHA*WMEGD(I,J)			IMPULS
	IF	(NPRT(10).NE.0)	CALL	OUTPUT(1)				IMPULS
	IF	(NPRT( 3).NE.0)	CALL	PRINT(6HIMPULS)				IMPULS
	CALL	ELTIME(2,27)						IMPULS
99	RETURN							IMPULS
	END							IMPULS

	SUBROUTINE INITIAL		INITAL
C		REV IV	07/24/86SLIP
C	PERFORMS CARD INPUT AND COMPUTATIONS FOR INITIAL		INITAL
C	POSITIONING OF THE CRASH VICTIM'S BODY SEGMENTS.		INITAL
C			INITAL
	IMPLICIT REAL*8(A-H,O-Z)		INITAL
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		INITAL
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/SGRINTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),		INITAL
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		INITAL
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),		SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),		INITAL
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)		INITAL
	COMMON/VPOSTN/ ZPLT(3),SPLT(3),AXV(3,6),VATAB(6,501,6),		VEHICL
*	VTO(6),VDT(6),TIMEV(6),OMEGV(6),NVTAB(6),INDXV(6)		INITAL
	COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),		INITAL
*	BLTTTL(5,8),PLTTTL(5,30),BAGTTL(5,6),SEG(30),		INITAL
*	JOINT(30),CGS(30),JS(30)		INITAL
	COMMON/CEULER/ IEULER(30),HIR(3,3,90),ANG(3,30),ANGD(3,30),		JDRIFT
*	FE(3,30),TQE(3,30),CONST(5,30)		JDRIFT
	REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTTL,BAGTTL,SEG,JOINT		INITAL
	LOGICAL*1 CGS,JS		INITAL
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),		INITAL
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI		TWOPI
	COMMON/TEMPVS/ TMP(140),WMGDEG(3,30),T(3),S(3),A(3,2),Z(3,3)		SLIP
*	,DMY(34862)		80386
C	NOTE : CHAIN ALSO USES TEMPVS.		INITAL
	DIMENSION YPR(3,30) , IYPR(4,30)		INITAL
C			INITAL
C	INPUT CARD G.1.A (PLOT COORDINATES OF VEHICLE REFERENCE ORIGIN)		INITAL
C			INITAL
	READ(5,22) ZPLT,I1,J1,I2,J2,I3		INITAL
22	FORMAT(3F10.0,5I4)		INITAL
	S(1) = 10.0		INITAL
	S(2) = 6.0		INITAL
	S(3) = 1.0		INITAL
C			INITAL
C	IF J1#0, INPUT CARD G.1.B (PLOT SCALING INPUT)		INITAL
C			INITAL
	IF (J1.NE.0) READ (5,22) S		INITAL
	SPLT(1) = 1.0/S(3)		INITAL
	SPLT(2) = 1.0/S(3)		INITAL
	SPLT(3) = -(S(1)/S(2))/S(3)		INITAL
	WRITE (6,23) NPG,ZPLT,I1,J1,I2,J2,I3,S		PAGE
	NPG=NPG+1		PAGE
23	FORMAT('1 SUBROUTINE INITIAL INPUT',98X,'PAGE',I5/120X,'CARD G.1'/		PAGE
*	' ZPLT(X) ZPLT(Y) ZPLT(Z) I1 J1 I2 J2 I3',		INITAL
*	' SPLT(1) SPLT(2) SPLT(3)'/3F10.0,5I6,3F10.2)		INITAL
C			INITAL
C	INPUT CARDS G.2.A - G.2.N		INITAL
C			INITAL
C	INITIAL LINEAR POSITION (IN) AND (IF I3=1) VELOCITY (IN/SEC)		INITAL

C	OF EACH BASE BODY SEGMENT. IF I3=0, VELOCITY WILL BE SET TO	INITAL
C	INITIAL VELOCITY OF VEHICLE. INPUTS IN INERTIAL REFERENCE.	INITAL
C		INITAL
	DO 37 J=1,NSEG	INITAL
	IF(J.GT.1.AND.IABS(JNT(J-1)).GT.0) GO TO 37	INITAL
	READ(5,24) (SEGLP(I,J),I=1,3),(SEGLV(I,J),I=1,3)	INITAL
24	FORMAT (6F10.0 , 4I3)	INITAL
	IF(I3.GT.0) GO TO 37	INITAL
	DO 36 I=1,3	INITAL
36	SEGLV(I,J) = SEGLV(I,NVEH)	INITAL
37	CONTINUE	INITAL
C		INITAL
C	INPUT CARDS G.3.A - G.3.N	INITAL
C		INITAL
C	FOR EACH BODY SEGMENT SUPPLY YAW, PITCH AND ROLL (DEGREES)	INITAL
C	AND (IF I3=1) THE ANGULAR VELOCITY IN LOCAL REFERENCE (DEG/SEC).	INITAL
C	IF I3=0, THE ANGULAR VELOCITY (BLANK ON INPUT CARDS) WILL BE SET	INITAL
C	EQUAL TO THE INITIAL ANGULAR VELOCITY OF THE VEHICLE.	INITAL
C		INITAL
	FIRST = 0.0	INITAL
	DO 40 J=1,NSEG	INITAL
	READ (5,24) (YPR(I,J),I=1,3),(WMGDEG(I,J),I=1,3),(IYPR(I,J),I=1,4)	INITAL
	ID1 = IYPR(1,J)	INITAL
	DO 38 I=1,3	INITAL
	IF (ID1.EQ.0) IYPR(I,J) = I	INITAL
38	WMEG(I,J) = WMGDEG(I,J)*RADIAN	INITAL
	IF (ID1.GE.0) GO TO 60	INITAL
C		INITAL
C	READ CARD G.3.J2 FOR SEGMENT NO. J WHEN IYPR(1,J) IS NEGATIVE.	INITAL
C		INITAL
	READ (5,24) A,II,IK,JJ,JK	INITAL
	IJ = II	INITAL
	LK = IK	INITAL
	DO 54 K=1,2	INITAL
	IF (IJ.GT.0) GO TO 52	INITAL
	DO 51 I=1,3	INITAL
51	Z(I,LK) = A(I,K)	INITAL
	GO TO 53	INITAL
52	DA1 = A(1,K)*RADIAN	INITAL
	DA2 = A(2,K)*RADIAN	INITAL
	SA1 = DSIN(DA1)	INITAL
	SA2 = DSIN(DA2)	INITAL
	CA1 = DCOS(DA1)	INITAL
	CA2 = DCOS(DA2)	INITAL
	IJ1 = IJ+1	INITAL
	IJ2 = IJ+2	INITAL
	IF (IJ1.GT.3) IJ1= IJ1-3	INITAL
	IF (IJ2.GT.3) IJ2= IJ2-3	INITAL
	SGN = 1.0	INITAL
	IF (SA1.LT.0.0 .AND. CA2.LT.0.0) SGN = -1.0	INITAL
	Z(IJ ,LK) = SGN*SA1*CA2	INITAL
	Z(IJ1,LK) = SGN*SA1*SA2	INITAL

Z(IJ2,LK) = SGN*CA1*CA2	INITAL
53 IJ = JJ	INITAL
54 LK = JK	INITAL
ZDOTIJ = Z(1,IK)*Z(1,JK) + Z(2,IK)*Z(2,JK) + Z(3,IK)*Z(3,JK)	INITAL
ZDOTII = Z(1,IK)*Z(1,IK) + Z(2,IK)*Z(2,IK) + Z(3,IK)*Z(3,IK)	INITAL
RATIO = ZDOTIJ/ZDOTII	INITAL
DO 55 I=1,3	INITAL
55 Z(I,JK) = Z(I,JK) - RATIO*Z(I,IK)	INITAL
LK = 6-1K-JK	INITAL
IT = MOD(JK-1K+3,3)	INITAL
IF (IT.EQ.1) CALL CROSS(Z(1,IK),Z(1,JK),Z(1,LK))	INITAL
IF (IT.EQ.2) CALL CROSS(Z(1,JK),Z(1,IK),Z(1,LK))	INITAL
DO 57 K=1,3	INITAL
IYPR(K,J) = 4-K	INITAL
SUM = 0.0	INITAL
DO 56 I=1,3	INITAL
56 SUM = SUM + Z(I,K)**2	INITAL
SQUM = DSQRT(SUM)	INITAL
DO 57 I=1,3	INITAL
57 D(K,I,J) = Z(I,K)/SQUM	INITAL
CALL YPRDEG (D(1,1,J),YPR(1,J))	INITAL
IF (FIRST.EQ.0.0) WRITE (6,58)	INITAL
58 FORMAT('0 INITIAL ANGULAR ROTATIONS COMPUTED FROM CARDS G.3.J2'//	INITAL
* ' SEGMENT',10X,'SEGMENT PRIMARY AXIS',	INITAL
* 12X,'SEGMENT SECONDARY AXIS',30X,'ANGULAR ROTATIONS (DEG)'/	INITAL
* ' NO. SEG',9X,'A1',8X,'A2',8X,'A3',11X,'B1',8X,'B2',8X,	INITAL
* 'B3',7X,'II 1K JJ JK',9X,'YAW',6X,'PITCH',5X,'ROLL'//	INITAL
FIRST = 1.0	INITAL
WRITE (6,59) J,SEG(J),A,II,1K,JJ,JK,(YPR(I,J),I=1,3)	INITAL
59 FORMAT (I4,1X,A4,3X,3F10.3,3X,3F10.3,3X,4I4,3X,3F10.3)	INITAL
60 M = IYPR(4,J)	INITAL
IF (M.EQ.0) M=NGRND	INITAL
IF (M.GE.J .AND. M.LE.NSEG) STOP 24	INITAL
IF (J.EQ.1) GO TO 80	VAXCHG
IF (M.LT.0 .AND. -M.NE.IABS(JNT(J-1))) STOP 25	INITAL
80 CALL DRCIJK (D,YPR,IYPR,HT,J)	VAXCHG
IF (I3.GT.0) GO TO 40	INITAL
CALL DOT31(D(1,1,NVEH),WMEG(1,NVEH),T)	INITAL
CALL MAT31(D(1,1,J),T,WMEG(1,J))	INITAL
DO 39 I=1,3	INITAL
39 WMGDEG(I,J) = WMEG(I,J)/RADIAN	INITAL
40 CONTINUE	INITAL
CALL VEHPOS	INITAL
IF(NJNT.EQ.0) GOTO 41	JDRIFT
CALL CHAIN(0)	JDRIFT
CALL EJGINT(1,0)	JDRIFT
DO 62 J=1,NJNT	JDRIFT
IF(IABS(IPIN(J)).NE.4) GOTO 62	JDRIFT
IF(IEULER(J).NE.2) GOTO 62	JDRIFT
DA1 = ANG(2,J) + CONST(2,J)	JDRIFT
CONST(4,J) = DCOS(DA1)	JDRIFT
CONST(5,J) = DSIN(DA1)	JDRIFT

62	CONTINUE	JDRIFT
C		INITAL
C	OUTPUT INITIAL BODY SEGMENT POSITIONS.	INITAL
C		INITAL
41	WRITE (6,42) UNITL,UNITL,UNITT	JDRIFT
42	FORMAT('O INITIAL POSITIONS (INERTIAL REFERENCE)',70X,'CARDS G.2')//INITAL	
*	/' SEGMENT',11X,'LINEAR POSITION (' ,A4,')',	INITAL
*	14X,'LINEAR VELOCITY (' ,A4,'/',A4,')'/'	AFREVS
*	' NO. SEG',2(9X,'X',11X,'Y',11X,'Z',5X) )	INITAL
	WRITE (6,43) (J,SEG(J),(SEGLP(I,J),I=1,3),(SEGLV(I,J),I=1,3)	INITAL
*	,J=1,NSEG)	INITAL
43	FORMAT(I4,1X,A4,3X,3F12.5,3X,3F12.5)	INITAL
	WRITE (6,44) UNITT	INITAL
44	FORMAT('O INITIAL ANGULAR ROTATION AND VELOCITY',71X,'CARDS G.3')//INITAL	
*	' SEGMENT',11X,'ANGULAR ROTATION (DEG)',	AFREVS
*	14X,'ANGULAR VELOCITY (DEG/',A4,')'/'	INITAL
*	' NO. SEG',8X,'YAW',8X,'PITCH',7X,'ROLL',	INITAL
*	13X,'X',11X,'Y',11X,'Z',15X,'IYPR' )	INITAL
	WRITE (6,46) (J,SEG(J),(YPR(I,J),I=1,3),(WMGDEG(I,J),I=1,3),	INITAL
*	(IYPR(I,J),I=1,4),J=1,NSEG)	INITAL
46	FORMAT(I4,1X,A4,3X,3F12.5,3X,3F12.5,3X,4I4)	INITAL
	IF (I3.EQ.0) WRITE (6,45)	INITAL
45	FORMAT('O LINEAR AND ANGULAR VELOCITIES HAVE BEEN SET EQUAL TO THEINITAL	
*	INITIAL VEHICLE VELOCITIES.')	INITAL
	IF (NHRNSS.NE.0) CALL HBPLAY	INITAL
	IF (I1.EQ.15) CALL EQUILB (YPR,IYPR)	INITAL
	CALL UNITI(0)	JDRIFT
	CALL ROTATE	INITAL
	CALL ELTIME(2,2)	INITAL
	RETURN	INITAL
	END	INITAL

	SUBROUTINE INTERS(A,B,XM,T,X,V,AX)		INTER
C		REV IV 07/23/86	TWOPI
C	DETERMINES INTERSECTION OF ELLIPSOIDS		INTER
C	X'AX = 1		INTER
C	(X'-M')B(X-M) = 1		INTER
C	WHERE A AND B ARE ELLIPSOID MATRICES		INTER
C	IF T ENTERS AS +1.0 , A IS EXTERNAL TO B AND		INTER
C	AS -1.0 , A IS INTERNAL TO B.		INTER
C			INTER
C	IF V ENTERS AS NON-ZERO, WILL USE PREVIOUS VALUE FOR START.		INTER
C	(AX) RETURNS AS (A)*(X).		INTER
C			INTER
C	RETURNS T>1 - NO INTERSECTION		INTER
C	T<1 - INTERSECTION IN WHICH CASE X WILL		INTER
C	CONTAIN COORDINATES OF CONTACT OF		INTER
C	CONTRACTED ELLIPSOIDS.		INTER
C			INTER
	IMPLICIT REAL*8 (A-H,O-Z)		INTER
	DIMENSION A(3,3),B(3,3),XM(3),X(3)		INTER
	DIMENSION C(3,4),Z(3),BM(3),AX(3),AM(3)		INTER
	EQUIVALENCE (Z(1),C(1,4))		INTER
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),		INTER
	*            UNITL,UNITM,UNITT,GRAVITY(3),TWOPI		TWOPI
C		INITIALIZATION	INTER
C		EVALUATE BM,M'AM,M'BM	INTER
C		SET N=0, V=M'BM/M'AM	INTER
	N = 0		INTER
	BMM = 0.0		INTER
	AMM = 0.0		INTER
	DO 11 I=1,3		INTER
	BM(I) = 0.0		INTER
	AM(I) = 0.0		INTER
	DO 10 J=1,3		INTER
	IF (DABS(A(I,J)).LT.EPS(20)) A(I,J) = 0.0		INTER
	AM(I) = AM(I) + A(I,J)*XM(J)		INTER
	IF (DABS(B(I,J)).LT.EPS(20)) B(I,J) = 0.0		INTER
10	BM(I) = BM(I) + B(I,J)*XM(J)		INTER
	BMM = BMM + XM(I)*BM(I)		INTER
11	AMM = AMM + XM(I)*AM(I)		INTER
	IF (V.EQ.0.0) V=T*DSQRT(BMM/AMM)		INTER
	IDONE = 0		INTER
C		NEWTON-RAPHSON ITERATION FOR	INTER
C		G(V) = FA(V)-FB(V) = 0	INTER
C		SOLVE (VA+B)X = BM FOR X	INTER
	ITER = 0		INTER
20	ITER = ITER+1		INTER
	DO 22 I=1,3		INTER
	DO 21 J=1,3		INTER
21	C(I,J) = V*A(I,J) + B(I,J)		INTER
22	Z(I) = BM(I)		INTER
	CALL DSMSOL(C,3,3)		INTER
C		EVALUATE AX	INTER

C		$FA(V) = X'AX$	INTERS
C		$FB(V) = -V(X' - M')AX$	INTERS
	FA = 0.0		INTERS
	FB = 0.0		INTERS
	CALL MAT31(A,Z,AX)		INTERS
	DO 30 I=1,3		INTERS
	X(I) = Z(I)		INTERS
	FA = FA+X(I)*AX(I)		INTERS
30	FB = FB+(X(I)-XM(I))*AX(I)		INTERS
	FB = -V*FB		INTERS
	IF (T.LT.0.0) FA = 1.0/FA		INTERS
	IF (IDONE.EQ.1) GO TO 60		INTERS
C		TEST FOR INTERSECTION	INTERS
	IF (FA-FB) 32,60,31		INTERS
C		IF FA>FB>1, NO INTERSECTION	INTERS
31	IF (T.GT.0.0.AND.FB.LT.1.0) GO TO 40		INTERS
	IF (T.LT.0.0.AND.FA.GT.1.0) GO TO 40		INTERS
	IF (N.EQ.0) GO TO 60		INTERS
	GO TO 62		INTERS
C		IF FA<FB<1, INTERSECTION	INTERS
32	IF (T.GT.0.0.AND.FB.LE.1.0) N=1		INTERS
	IF (T.LT.0.0.AND.FA.GE.1.0) N=1		INTERS
C		SOLVE (VA+B)Z = AX FOR Z	INTERS
40	DO 42 I=1,3		INTERS
	DO 41 J=1,3		INTERS
41	C(I,J) = V*A(I,J) + B(I,J)		INTERS
42	Z(I) = AX(I)		INTERS
	CALL DSMSOL(C,3,3)		INTERS
C		$F'A(V) = -2X'AZ$	INTERS
	CALL MAT31 (A,Z,AX)		INTERS
	FPA = X(1)*AX(1)		INTERS
	* + X(2)*AX(2)		INTERS
	* + X(3)*AX(3)		INTERS
	FPA = -(FPA+FPA)		INTERS
C		$DV = -G(V)/G'(V)$	INTERS
	DV = 1.0 + V		INTERS
	IF (T.LT.0.0) DV = V-FA**2		INTERS
	DV = (FB-FA)/(DV*FPA)		INTERS
	IF (ITER.GE.50) GO TO 62		INTERS
C		TEST FOR CONVERGENCE	INTERS
	IF (T*(V+DV).LE.0.0) DV = -0.5*V		INTERS
	V = V+DV		INTERS
	DV = DABS(DV/V)		INTERS
	IF (DV.LE.EPS(12)) IDONE=1		INTERS
	GO TO 20		INTERS
C		$FA(V) \rightarrow FB(B)$ , RETURN	INTERS
60	IF (T.LT.0.0) FA = 1.0/FB		INTERS
	T = DSQRT(FA)		INTERS
	IF (FA.GT.1.0) GO TO 61		INTERS
	N = 1		INTERS
	GO TO 71		INTERS
61	IF (N.EQ.0) GO TO 71		INTERS

62 WRITE (6,63)  
63 FORMAT(' INTERS ITERATION DID NOT CONVERGE')  
71 CONTINUE  
RETURN  
END

INTER  
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	SUBROUTINE KINPUT	KINPUT
C		REV IV 07/23/86TWOPI
C	PERFORMS THE FOLLOWING CARD INPUT AFTER CARDS E.1-E.4 (SUBROUTINE KINPUT	KINPUT
C	CINPUT) AND BEFORE CARDS F.1-F.5 (SUBROUTINE FINPUT).	KINPUT
C	CARD E.5 - NO LONGER REQUIRED	WINDOP
C	CARDS E.6 - DEFINITIONS OF WIND FORCE FUNCTIONS AND DRAG	WINDOP
C	COEFFICIENT FUNCTIONS	WINDOP
C	CARDS E.7 - DEFINITIONS OF JOINT RESTORING FORCE FUNCTIONS	KINPUT
C		KINPUT
	IMPLICIT REAL*8(A-H,O-Z)	KINPUT
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,	KINPUT
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	PAGE
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)	DIMENB
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),	KINPUT
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI	TWOPI
	COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),	WINDOP
*	BLTTTL(5,8),PLTTTL(5,30),BAGTTL(5,6),SEG(30),	WINDOP
*	JOINT(30),CGS(30),JS(30)	WINDOP
	REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTTL,BAGTTL,SEG,JOINT	TGMOD1
	LOGICAL*1 CGS,JS	80386
	COMMON/TEMPVS/ JTITLE(5,51),NF(5),MS(3),KTITLE(31),TH(50)	KINPUT
*	,DDMMY(34916)	80386
C	NOTE: TEMPVS IS SHARED HERE WITH SUBROUTINES CINPUT AND FINPUT.	KINPUT
	REAL BLANK,JTITLE,KTITLE	KINPUT
	DATA BLANK/4H /	KINPUT
11	FORMAT(2I6)	KINPUT
	J1 = MXTB1+1	KINPUT
	IF (NWINDF.LE.0) GO TO 31	KINPUT
	DO 30 K=1,NWINDF	KINPUT
C		KINPUT
C	INPUT CARD E.6.A - FUNCTION NO. AND TITLE	KINPUT
C		KINPUT
	READ (5,12) I,(KTITLE(J),J=1,5)	KINPUT
12	FORMAT(I4,4X,5A4)	KINPUT
	WRITE (6,13) I,(KTITLE(J),J=1,5),I,J1,NPG	PAGE
	NPG=NPG+1	PAGE
13	FORMAT('1 WIND FORCE FUNCTION NO.',I4,4X,5A4,10X,'NTI(',I2,') =',	KINPUT
*	I5,46X,'PAGE',I5/120X,'CARDS E.6'/)	PAGE
	IF (I.LE.0.OR.I.GT.50) WRITE (6,14)	KINPUT
14	FORMAT('0 IMPROPER FUNCTION NO. PROGRAM TERMINATED.')	KINPUT
	IF (I.LE.0.OR.I.GT.50) STOP 11	KINPUT
	IF (NTI(I).NE.0) WRITE (6,15) I	KINPUT
15	FORMAT('0 FUNCTION NO.',I4,' HAS ALREADY BEEN INPUTTED AND WILL BE	KINPUT
*	REPLACED BY THIS FUNCTION.')	KINPUT
	NTI(I) = J1	KINPUT
	DO 16 J=1,5	KINPUT
16	JTITLE(J,I) = KTITLE(J)	KINPUT
	J2 = J1+4	KINPUT
C		KINPUT
C	INPUT CARD E.6.B	WINDOP
C		WINDOP
	READ (5,60) (TAB(J),J=J1,J2-2),NSV,NSR	WINDOP

60	FORMAT(3F12.0,2I12)	WINDOP
	TAB(J2-1) = DFLOAT(NSV)	WINDOP
	TAB(J2) = DFLOAT(NSR)	WINDOP
	IF (TAB(J1).EQ.0.0) GOTO 22	WINDOP
	WRITE(6,23) (TAB(J),J=J1,J2-2),NSV,SEG(NSV),NSR,SEG(NSR)	WINDOP
23	FORMAT(' SPEC. HEAT RATIO      SONIC VEL.      ABS. PRESS.',7X,	WINDOP
	*      'SEGMENT      REF. SEGMENT',/3F15.4,2(I11,A4)//)	WINDOP
	J1=J2+1	WINDOP
	GOTO 30	MISC
22	WRITE (6,18) (TAB(J),J=J1,J2)	KINPUT
17	FORMAT(6F12.0)	KINPUT
18	FORMAT(10X,'D0',13X,'D1',13X,'D2',13X,'D3',8X,'REF. SEGMENT',	WINDOP
	*      /5F15.4//)	WINDOP
	J1 = J2+1	KINPUT
C		KINPUT
C	INPUT CARD E.6.C - NTMPTS	KINPUT
C		KINPUT
	READ (5,11) NTMPTS	KINPUT
	WRITE (6,19) NTMPTS	KINPUT
19	FORMAT('0 WIND FORCE TABLES FOR ',I6,' TIME POINTS.'//	KINPUT
	*      11X,'T',14X,'FX(T)',15X,'FY(T)',15X,'FZ(T)' //)	KINPUT
	TAB(J1) = NTMPTS	KINPUT
	J1 = J1+1	KINPUT
	J2 = J1+4*NTMPTS-1	KINPUT
C		KINPUT
C	INPUT CARDS E.6.D-E.6.N - NTMPTS CARDS OF T,FX(T),FY(T),FZ(T)	KINPUT
C		KINPUT
	READ (5,20) (TAB(J),J=J1,J2)	KINPUT
	WRITE (6,21) (TAB(J),J=J1,J2)	KINPUT
20	FORMAT(4F12.0)	KINPUT
21	FORMAT(3X,F12.6,3G20.6)	KINPUT
	J1 = J2+1	KINPUT
30	CONTINUE	KINPUT
31	IF (NJNTE.LE.0) GO TO 51	KINPUT
	DO 50 K=1,NJNTE	KINPUT
C		KINPUT
C	INPUT CARD E.7.A - FUNCTION NO. AND TITLE	KINPUT
C		KINPUT
	READ (5,12) I,(KTITLE(J),J=1,5)	KINPUT
	WRITE (6,32) I,(KTITLE(J),J=1,5),I,J1,NPG	PAGE
	NPG=NPG+1	PAGE
32	FORMAT('1 JOINT FORCE FUNCTION NO.',I4,4X,5A4,10X,'NTI(',I2,') =',	KINPUT
	*      I5,45X,'PAGE',I5/120X,'CARDS E.7'//)	PAGE
	IF (I.LE.0.OR.I.GT.50) WRITE (6,14)	KINPUT
	IF (I.LE.0.OR.I.GT.50) STOP 12	KINPUT
	IF (NTI(I).NE.0) WRITE (6,15) I	KINPUT
	NTI(I) = J1	KINPUT
	DO 33 J=1,5	KINPUT
33	JTITLE(J,I) = KTITLE(J)	KINPUT
C		KINPUT
C	INPUT CARD E.7.B - D0,D1,D2,D3,D4 (FOR NOW A BLANK CARD).	KINPUT
C		KINPUT

	J2 = J1+4	KINPUT
	READ (5,17) (TAB(J),J=J1,J2)	KINPUT
	WRITE (6,18) (TAB(J),J=J1,J2)	KINPUT
	J1 = J2+1	KINPUT
C		KINPUT
C	INPUT CARD E.7.C - NTHETA,NPHI	KINPUT
C		KINPUT
	READ (5,11) NTHETA,NPHI	KINPUT
	TAB(J1 ) = NTHETA	KINPUT
	TAB(J1+1) = NPHI	KINPUT
	J1 = J1+2	KINPUT
	IF (NTHETA.LT.0) GO TO 38	KINPUT
	DO 35 J=1,NTHETA	KINPUT
35	TH(J) = DFLOAT(J-1)*180.0/DFLOAT(NTHETA-1)	KINPUT
	WRITE (6,36) NTHETA,NPHI,(TH(J),J=2,NTHETA)	KINPUT
36	FORMAT('0 FUNCTION IS TABULAR FOR' ,I3,' X',I3,' VALUES OF THETA AKINPUT	
	*ND PHI'//30X,'THETA'/5X,'PHI',5X,'THETA0',F16.3,4F20.3/	KINPUT
	* (15X,5F20.3))	KINPUT
37	FORMAT(F9.2,F10.3,5G20.7/(19X,5G20.7))	KINPUT
	GO TO 40	KINPUT
38	NPOLY = -NTHETA -1	KINPUT
	WRITE (6,39) NPOLY,NPHI,(BLANK,J,J=1,NPOLY)	KINPUT
39	FORMAT('0 FUNCTION IS COEFFICIENTS OF' ,I3,' ORDER POLYNOMIALS IN KINPUT	
	*(THETA-THETA0) FOR',I3,' VALUES OF PHI.'//	KINPUT
	* 27X,'COEFFICIENTS OF (THETA-THETA0)**N'/	KINPUT
	* 5X,'PHI',5X,'THETA0',7X,5(A4,'N =',I2,11X)/(26X,A4,'N =',I2,11X,KINPUT	
	* A4,'N =',I2,11X,A4,'N =',I2,11X,A4,'N =',I2,11X,A4,'N =',I2) ) KINPUT	
40	WRITE (6,21)	KINPUT
	DO 49 I=1,NPHI	KINPUT
	PHIDEG = DFLOAT(I-1)*360.0/DFLOAT(NPHI) - 180.0	KINPUT
C		KINPUT
C	INPUT CARDS E.7.D - E.7.N NPHI SETS WITH NTHETA ITEMS PER SET.	KINPUT
C	EACH SET I IS FOR PHI(I) = -180 +(I-1)*360/NPHI DEGREES AND	KINPUT
C	ASSUMES DATA FOR PHI(NPHI+1) = 180 IS SAME AS PHI(1) = -180.	KINPUT
C		KINPUT
	J2 = J1 + IABS(NTHETA) -1	KINPUT
	READ (5,17) (TAB(J),J=J1,J2)	KINPUT
	WRITE (6,37) PHIDEG,(TAB(J),J=J1,J2)	KINPUT
	IF (NTHETA.LT.0) TAB(J1) = TAB(J1)*RADIAN	KINPUT
	IF (NTHETA.LT.0) GO TO 49	KINPUT
C		KINPUT
C	FOR TABULAR DATA, FILL IN ZERO VALUES WITH INTERPOLATED NEGATIVE KINPUT	
C	VALUES. OVERWRITE VALUE IN FIRST COLUMN (SUPPLIED AS THETA0) WITH KINPUT	
C	VALUE FOR THETA = 0 AND ALL OTHER ZERO VALUES.	KINPUT
C		KINPUT
	THETA0 = TAB(J1)	KINPUT
	IF (THETA0.EQ.0.0) GO TO 49	KINPUT
	JJ = THETA0*DFLOAT(NTHETA-1)/180.0 + 1.0 + EPS(6)	KINPUT
	JJ1 = J1+JJ	KINPUT
	IERROR = 0	KINPUT
	IF (JJ1.GT.J2) IERROR = 1	KINPUT
	IF (TAB(JJ1).LE.0.0) IERROR = 2	KINPUT

IF (IERROR.NE.0) GO TO 46	KINPUT
DO 45 J=1,JJ	KINPUT
J1J = J1+J-1	KINPUT
IF (J.NE.1.AND.TAB(J1J).GT.0.0) IERROR = 3	KINPUT
45 TAB(J1J) = TAB(JJ1)*(TH(J)-THETA0)/(TH(JJ+1)-THETA0)	KINPUT
46 IF (IERROR.NE.0) WRITE (6,47) IERROR	KINPUT
47 FORMAT('O INPUT ERROR. INCONSISTENT VALUE OF THETA0. IERROR =',I2,	KINPUT
* ' PROGRAM TERMINATED.')	KINPUT
IF (IERROR.NE.0) STOP 13	KINPUT
49 J1 = J2+1	KINPUT
50 CONTINUE	KINPUT
51 MXTB1 = J1-1	KINPUT
RETURN	KINPUT
END	KINPUT

	SUBROUTINE LINAXS(X0,Y0,THETA,NINTVS,TOTLGT)		LINAXS
C		REV 18	02/28/78LINAXS
C	PURPOSE : PREPARE A LINEAR AXIS ON A PLOT.		LINAXS
C			LINAXS
C	DESCRIPTION OF PARAMETERS:		LINAXS
C	X0,Y0 - STARTING POINT (IN INCHES, REL TO PLOTTER ORIGIN).		LINAXS
C			LINAXS
C	THETA - ANGLE OF AXIS, IN DEGREES.		LINAXS
C			LINAXS
C	NINTVS- MAGNITUDE - NO. OF INTERVALS DELINEATED BY TIC MARKS.		LINAXS
C	- SIGN DETERMINES WHETHER TIC MARKS ARE PLACED ON		LINAXS
C	POSITIVE OR NEGATIVE SIDE OF AXIS, RESPECTIVELY		LINAXS
C	(POSITIVE SIDE IS TO LEFT OF DIRECTION OF TRAVEL).		LINAXS
C			LINAXS
C	TOTLGT- TOTAL LENGTH OF AXIS, IN INCHES.		LINAXS
C			LINAXS
C	SUBROUTINES REQUIRED : SIN, COS, PLOT (NOTE: SINGLE PRECISION).		LINAXS
C			LINAXS
C	AUTHOR: W. D. FRYER, CALSPAN (MARCH 1967).		LINAXS
C			LINAXS
C	PLAGIARIZED FROM CALSPAN SUBROUTINE LIBRARY (NO. CU 0035).		LINAXS
C			LINAXS
	THR = 1.7453293E-2 * THETA		LINAXS
	SINT = SIN(THR)		LINAXS
	COST = COS(THR)		LINAXS
C			LINAXS
	DL = ABS(TOTLGT/ FLOAT(NINTVS))		LINAXS
	DX = DL*COST		LINAXS
	DY = DL*SINT		LINAXS
C			LINAXS
	TICX = -0.12* SINT		LINAXS
	TICY = 0.12* COST		LINAXS
	IF(NINTVS.GT.0) GO TO 30		LINAXS
	TICX = -TICX		LINAXS
	TICY = -TICY		LINAXS
C			LINAXS
30	X = X0		LINAXS
	Y = Y0		LINAXS
C			LINAXS
	CALL PLOT (X +TICX,Y+TICY,3)		LINAXS
	CALL PLOT (X,Y,2)		LINAXS
	NINT = IABS(NINTVS)		LINAXS
	DO 40 I=1,NINT		LINAXS
	X = X+DX		LINAXS
	Y = Y+DY		LINAXS
	CALL PLOT(X,Y,2)		LINAXS
	CALL PLOT(X+TICX,Y+TICY,2)		LINAXS
40	CALL PLOT(X,Y,2)		LINAXS
C			LINAXS
	RETURN		LINAXS
	END		LINAXS

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SUBROUTINE LOGAXS(X0,Y0,THETA,NDEC,EXTENT)
C                                     REV 19    09/18/79
C                                     LOGAXS
C PURPOSE : PREPARE LOGARITHMIC AXIS ON A PLOT.
C                                     LOGAXS
C DESCRIPTION OF PARAMETERS:
C                                     LOGAXS
C                                     LOGAXS
C     X0,Y0 - STARTING POINT (IN INCHES, REL TO PLOTTER ORIGIN).
C                                     LOGAXS
C     THETA - ANGLE OF AXIS (DEGREES).
C                                     LOGAXS
C     NDECS - MAGNITUDE OF NDECS SPECIFIES NO. OF DECADES.
C                                     LOGAXS
C     - SIGN DETERMINES WHETHER TIC MARKS ARE TO BE PLACED
C     ON POS. OR NEG. SIDE OF AXIS, RESP. (POS. SIDE IS
C     TO LEFT OF PREDOMINANT DIRECTION OF TRAVEL).
C                                     LOGAXS
C     EXTENT- MAGNITUDE OF EXTENT SETS OVER-ALL LENGTH OF AXIS
C     IN INCHES. IF EXTENT IS POSITIVE, TIC MARKS ARE
C     SPACED NORMALLY (LARGE INTERVALS FIRST). IF EXTENT
C     IS NEGATIVE, TIC MARKS ARE SPACED IN REVERSE ORDER
C     (SMALL INTERVALS FIRST).
C                                     LOGAXS
C SUBROUTINES REQUIRED : SIN, COS, PLOT (NOTE: SINGLE PRECISION).
C                                     LOGAXS
C AUTHOR: W. D. FRYER, CALSPAN (MARCH 1967).
C                                     LOGAXS
C PLAGIARIZED FROM CALSPAN SUBROUTINE LIBRARY (NO. CU 0036).
C                                     LOGAXS
C LOGICAL REVERS
C REAL XL(18),XLO(19)
C EQUIVALENCE (XLO(2),XL(1))
C DATA XLO/ 0.0 , 0.17609, 0.30103, 0.39794, 0.47712, 0.54407,
C * 0.60206, 0.65321, 0.69897, 0.74036, 0.77815, 0.81291, 0.84510,
C * 0.87506, 0.90309, 0.92942, 0.95424, 0.97772, 1.0 /
C DATA RPD /1.7453293E-2/
C                                     LOGAXS
C REVERS = .FALSE.
C IF(EXTENT.LT.0.0) REVERS = .TRUE.
C                                     LOGAXS
C NODEC = IABS(NDEC)
C SPDEC = ABS(EXTENT) / FLOAT(NODEC)
C THR = THETA*RPD
C COST = COS(THR)
C SINT = SIN(THR)
C                                     LOGAXS
C TICX1 = -0.05*SINT
C TICY1 = 0.05*COST
C TICXA = -0.12*SINT
C TICXB = -0.20*SINT
C TICYA = 0.12*COST
C TICYB = 0.20*COST
C IF(NDEC.GT.0) GO TO 50
C                                     LOGAXS

```

C		LOGAXS
	TICX1 = -TICX1	LOGAXS
	TICY1 = - TICY1	LOGAXS
	TICX2 = -TICX2	LOGAXS
	TICXA = - TICXA	LOGAXS
	TICYA = -TICYA	LOGAXS
	TICXB = -TICXB	LOGAXS
	TICYB = - TICYB	LOGAXS
C		LOGAXS
50	COST = COST*SPDEC	LOGAXS
	SINT = SINT* SPDEC	LOGAXS
	TICX2 = TICXA	LOGAXS
	TICY2 = TICYA	LOGAXS
C		LOGAXS
	XD = XO	LOGAXS
	YD = YO	LOGAXS
	ND = 1	LOGAXS
	N = 0	LOGAXS
C		LOGAXS
C	*****GO TO START POS.*****	LOGAXS
	CALL PLOT(XO+TICXB,YO+TICYB,3)	LOGAXS
	CALL PLOT(XO,YO,2)	LOGAXS
C		LOGAXS
60	N = N+1	LOGAXS
	Q = XL(N)	LOGAXS
	IF(.NOT. REVERS) GO TO 65	LOGAXS
	M = 18-N	LOGAXS
	Q = 1.0-XL(M)	LOGAXS
65	X = XD + Q*COST	LOGAXS
	Y = YD + Q*SINT	LOGAXS
	CALL PLOT(X,Y,2)	LOGAXS
	CALL PLOT(X+TICX1,Y+TICY1,2)	LOGAXS
	CALL PLOT (X,Y,2 )	LOGAXS
C		LOGAXS
	N = N+1	LOGAXS
	Q = XL(N)	LOGAXS
	IF(.NOT. REVERS) GO TO 75	LOGAXS
	M = 18-N	LOGAXS
	Q = 1.0 - XL(M)	LOGAXS
.5	X = XD + Q*COST	LOGAXS
	Y = YD + Q*SINT	LOGAXS
	CALL PLOT(X,Y,2)	LOGAXS
	CALL PLOT (X+TICX2,Y+TICY2,2)	LOGAXS
	CALL PLOT(X,Y,2)	LOGAXS
C		LOGAXS
	IF(N-16) 60,80,100	LOGAXS
C		LOGAXS
80	TICX2 = TICXB	LOGAXS
	TICY2 = TICYB	LOGAXS
	GO TO 60	LOGAXS
C		LOGAXS
100	IF(ND .EQ. NODEC) GO TO 200	LOGAXS

TICX2 = TICXA	LOGAXS
TICY2 = TICYA	LOGAXS
N = 0	LOGAXS
XD = X	LOGAXS
YD = Y	LOGAXS
ND = ND+1	LOGAXS
GO TO 60	LOGAXS
C	LOGAXS
200 RETURN	LOGAXS
END	LOGAXS



FUNCTION LTIME(N)	LTIME
	REV III.2 08/08/84REVIII
C TEMPORARY FORTRAN VERSION OF S/370 ASSEMBLER LANGUAGE ROUTINE FROM	LTIME
C CALSPAN LIBRARY THAT MEASURES ELAPSED CPU TIME IN UNITS OF 0.01	LTIME
C SECONDS. IT SHOULD BE REPLACED WITH AN EQUIVALENT ROUTINE BY THE	LTIME
C USER TO ENABLE SUBROUTINE ELTIME TO PERFORM ON HIS COMPUTER.	LTIME
C	LTIME
C ORIGINAL CALSPAN ROUTINE PERFORMS AS FOLLOWS:	LTIME
C     IT = LTIME(0) GIVES ELAPSED CPU TIME (INTEGER NUMBER OF 0.01	LTIME
C                     SECOND UNITS) SINCE SUBROUTINE REFERENCE WAS	LTIME
C                     RESET, AND RESETS THIS REFERENCE.	LTIME
C     IT = LTIME(1) SAME, EXCEPT THAT THE REFERENCE IS NOT RESET.	LTIME
C	LTIME
C	PECONV
C THIS SUBROUTINE DOESN'T WORK WITH THE P-E COMPUTER	PECONV
C BUT THE CODE IS LEFT HERE AS A DUMMY SUBROUTINE.	PECONV
C HOWEVER, THERE IS A VERSION OF THIS SUBROUTINE THAT	PECONV
C CAN BE USED, BUT IT CAN ONLY BE COMPILED WITH THE	PECONV
C P-E FORTRAN O COMPILER. THE OBJECT DECK FOR THIS	PECONV
C SUBROUTINE IS KEPT SEPARATELY AND INCLUDED IN THE	PECONV
C TASK FILE WHEN THE PROGRAM IS LINKED	PECONV
C	PECONV
DATA KTIME/0/	LTIME
KTIME = KTIME+1	LTIME
LTIME = KTIME	LTIME
IF (N.EQ.0) KTIME = 0	LTIME
RETURN	LTIME
END	LTIME

	SUBROUTINE MAT31 (A,B,C)		MAT31
C		REV 17	01/03/77MAT31
C	PERFORMS MATRIX MULTIPLICATION C = AB		MAT31
C	WHERE A IS A 3X3 MATRIX, AND B AND C ARE VECTORS OF LENGTH 3.		MAT31
C			MAT31
	IMPLICIT REAL*8 (A-H,O-Z)		MAT31
	DIMENSION A(3,3) , B(3) , C(3)		MAT31
	C(1) = A(1,1)*B(1) + A(1,2)*B(2) + A(1,3)*B(3)		MAT31
	C(2) = A(2,1)*B(1) + A(2,2)*B(2) + A(2,3)*B(3)		MAT31
	C(3) = A(3,1)*B(1) + A(3,2)*B(2) + A(3,3)*B(3)		MAT31
	RETURN		MAT31
	END		MAT31

	SUBROUTINE MAT33 (A,B,C)		MAT33
C		REV 17	01/03/77MAT33
C	PERFORMS MATRIX MULTIPLICATION C = AB		MAT33
C	WHERE A, B AND C ARE ALL 3X3 MATRICEES.		MAT33
C			MAT33
	IMPLICIT REAL*8 (A-H,O-Z)		MAT33
	DIMENSION A(3,3) , B(3,3) , C(3,3)		MAT33
	DO 10 I=1,3		MAT33
	DO 10 J=1,3		MAT33
10	C(I,J) = A(I,1)*B(1,J) + A(I,2)*B(2,J) + A(I,3)*B(3,J)		MAT33
	RETURN		MAT33
	END		MAT33

	SUBROUTINE ORTHO(P,X,L)		ORTHO
C		REV 03 05/31/73	ORTHO
C	GENERATES A SET OF RIGHT HANDED ORTHONORMAL VECTORS (P),		ORTHO
C	GIVEN ONE OF THE VECTORS (X), WHERE		ORTHO
C	P - LX3 MATRIX OF 3 ORTHONORMAL VECTORS TO BE GENERATED.		ORTHO
C	X - GIVEN VECTOR.		ORTHO
C	L - 1ST SUBSCRIPT OF P IN CALLING PROGRAM.		ORTHO
C			ORTHO
	IMPLICIT REAL*8(A-H,O-Z)		ORTHO
	DIMENSION P(L,3),X(3)		ORTHO
	M=2		ORTHO
	N=3		ORTHO
	TEST=0.		ORTHO
	DO 5 I=1,3		ORTHO
	P(I,3)=X(I)		ORTHO
	D=1.-X(I)**2		ORTHO
	IF(D.LE.TEST)GO TO 4		ORTHO
	TEST=D		ORTHO
	D=DSQRT(D)		ORTHO
	P(I,1)=D		ORTHO
	P(I,2)=0.		ORTHO
	P(M,2)=X(N)/D		ORTHO
	P(N,2)=-X(M)/D		ORTHO
	P(M,1)=X(I)*P(N,2)		ORTHO
	P(N,1)=-X(I)*P(M,2)		ORTHO
4	M=N		ORTHO
	N=I		ORTHO
5	CONTINUE		ORTHO
	RETURN		ORTHO
	END		ORTHO

	SUBROUTINE OUTPUT(IJK)		OUTPUT
		REV IV	02/01/88MISDOT
C	CONTROLS TABULATED OUTPUT ON FORTRAN UNITS (STARTING WITH NO. 21)		OUTPUT
C	OF SELECTED OPTIONAL SEGMENT LINEAR AND ANGULAR ACCELERATIONS,		OUTPUT
C	VELOCITIES AND DISPLACEMENTS, JOINT PARAMETERS AND SELECTED DATA		OUTPUT
C	FROM ALL ALLOWED CONTACT FORCE COMPUTATIONS BETWEEN BODY SEGMENTS		OUTPUT
C	AND VEHICLE COMPONENTS.		OUTPUT
C			OUTPUT
	IMPLICIT REAL*8 (A-H,O-Z)		OUTPUT
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NCRND,		OUTPUT
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),		OUTPUT
*	F(3,30),TQ(3,30),WJ(30),A11(3,3,30)		SLIP
	COMMON/SCMNTS/ D(3,3,30),WHEG(3,30),WHEGD(3,30),U1(3,30),U2(3,30),		OUTPUT
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		OUTPUT
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),		SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),		OUTPUT
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)		OUTPUT
	COMMON/JBARTZ/ MNPL( 30),MNBLT( 8),MNSEG( 30),MNBAG( 6),		OUTPUT
*	MPL(3,5,30),MBLT(3,5,8),MSEG(3,5,30),MBAG(3,10,6),		OUTPUT
*	NTPL( 5,30),NTBLT( 5,8),NTSEG( 5,30)		OUTPUT
	COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),		OUTPUT
*	BLTTTL(5,8),PLTTL(5,30),BAGTTL(5,6),SEG(30),		OUTPUT
*	JOINT(30),CGS(30),JS(30)		OUTPUT
	REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTL,BAGTTL,SEG,JOINT		OUTPUT
	LOGICAL*1 CGS,JS		OUTPUT
	COMMON/FORCES/PSF(7,70),BSF(4,20),SSF(10,40),BAGSF(3,20),		NCFORC
*	PRJNT(7,30),NPANEL(5),NPSF,NBST,NSSF,NBGSF		OUTPUT
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),		OUTPUT
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI		TWOPI
	COMMON/RSAVE/ XSG(3,20,3),DPHI(3,3,30),LPMI(30),		ATBIII
*	NSG(9),MSG(20,9),MCG,MCGIN(24,5),KREF(20,9)		TTHKREF
	COMMON/COMAIN/VAR(240),DER(240),DT,H0,HMAX,HMIN,RSTIME,		OUTPUT
*	ISTEP,NSTEPS,NDINT,NEQ_IRSIN,IRSOUT		OUTPUT
	COMMON/DAMPER/ AFSDM(3,20),APSDN(3,20),ASD(5,20),MSDM(20),MSDN(20)		OUTPUT
	COMMON/HRNESS/ BAR(15,100),BB(100),BBDOT(100),PLOSS(2,100),		OUTPUT
*	XLONG(20),HTIME(2),IBAR(5,100),NL(2,100),		OUTPUT
*	NPTSPB(20),NPTPLY(20),NTHRNS(20),NBLTPH(5)		OUTPUT
	COMMON/WINDFR/ WTIME(30),QFU(3,5),QFV(3,5),WF(3,30),IWIND(30),		WINDOP
*	MWSEG(7,30),NFVSEG(6),NFVNT(5),MOWSEG(30,30)		WINDOP
	COMMON/TEMPVS/ TDATA(14,65),ACC(7,20),T1(3),T2(3),T3(3),T4(9)		CHGIII
*	,T5(3,3),T6(3,3),T7(3),DDMY(34024)		80386
	LOGICAL LTAPES , LTHIST		OUTPUT
	DATA LINES/-1/,LPP/45/,NTMAX/65/		CHGIII
	DATA KMAX/20/,NMAX/22/,MCGMAX/5/		CHGIII
C			OUTPUT
	IF (IJK.NE.0) GO TO 13		OUTPUT
C			OUTPUT
C	SET ALL FORCE ARRAYS TO ZERO.		OUTPUT
C			OUTPUT
	DO 2 I=1,7		MISDOT
	DO 2 J=1,70		MISDOT

2	PSF(I,J) = 0.0	MISDOT
	DO 3 I=1,4	MISDOT
	DO 3 J=1,20	MISDOT
3	BSF(I,J) = 0.0	MISDOT
	DO 4 I=1,10	MISDOT
	DO 4 J=1,40	MISDOT
4	SSF(I,J) = 0.0	MISDOT
	DO 5 I=1,3	MISDOT
	DO 5 J=1,20	MISDOT
5	BAGSF(I,J) = 0.0	MISDOT
	DO 6 I=1,7	MISDOT
	DO 6 J=1,30	MISDOT
6	PRJNT(I,J) = 0.0	MISDOT
	GO TO 66	OUTPUT
C		OUTPUT
C	LTHIST = TRUE MEANS PRINT LINE OF TIME HISTORY DATA FOR THIS	OUTPUT
C	TIME POINT ON EACH OUTPUT UNIT (NT).	OUTPUT
C		OUTPUT
C	LTAPE8 = TRUE MEANS WRITE TIME HISTORY DATA ON TAPE 8.	OUTPUT
C		OUTPUT
13	NPRT4 = NPRT(4) + 4	OUTPUT
	IF (NPRT4.LE.0 .OR. NPRT4.GT.8) STOP 37	OUTPUT
	IF(NPRT(26).EQ.6) GO TO 66	TGMOD1
	GO TO (66,66,66,15,16,17,17,16) , NPRT4	OUTPUT
15	LTAPE8 = .FALSE.	OUTSTP
	LTHIST = .TRUE.	TGMOD1
	GO TO 116	TGMOD1
16	LTHIST = .TRUE.	TGMOD1
	LTAPE8 = .TRUE.	TGMOD1
	GO TO 116	TGMOD1
17	LTHIST = .FALSE.	TGMOD1
	LTAPE8 = .TRUE.	TGMOD1
	GO TO 217	TGMOD1
116	TEST = DMOD(TIME,DT)	OUTSTP
	TEST = DMIN1(TEST,DABS(DT-TEST))	OUTSTP
	IF ((NPRT(26).EQ.0.OR.NPRT(26).EQ.3).AND.TEST.GE.EPS(8))	TGMOD1
	* LTHIST=.FALSE.	TGMOD1
	IF(.NOT.LTAPE8.AND..NOT.LTHIST) GO TO 66	FIXTTH
217	CONTINUE	TGMOD1
	IF(NPRT(26).EQ.4) LTHIST=.FALSE.	TGMOD1
	IF(NPRT(26).EQ.5) LTAPE8=.FALSE.	TGMOD1
	IF(.NOT.LTAPE8.AND..NOT.LTHIST) GO TO 66	TGMOD1
	CALL ELTIME (1,8)	OUTPUT
	IF (LINES.GE.0) GO TO 21	FIXTTH
	PREVT = -999.0	OUTPUT
	LINES = 0	FIXTTH
	IF (IRSIN.NE.0) GO TO 10	OUTPUT
C		OUTPUT
C	1ST TIME IN ROUTINE, READ CARD INPUT FOR OUTPUT CONTROL.	OUTPUT
C		OUTPUT
C	1. NO. OF POINT TOTAL ACCELERATIONS ,POINT NOS. AND LOCATION	CHGIII
C	2. NO. OF POINT REL. VELOCITIES .POINT NOS. AND LOCATION	CHGIII

C	3. NO. OF POINT REL. LINEAR DISPLACEMENTS ,POINT NOS. AND LOCATI	CHGIII
C	4. NO. OF SEGMENT ANGULAR ACCELERATIONS AND SEGMENT NOS.	CHGIII
C	5. NO. OF SEGMENT REL. ANGULAR VELOCITIES AND SEGMENT NOS.	CHGIII
C	6. NO. OF SEGMENT REL. ANGULAR DISPLACEMENTS AND SEGMENT NOS.	CHGIII
C	7. NO. OF JOINT PARAMETERS AND JOINT NOS.	OUTPUT
C	8. NO. OF SEGMENT WIND FORCES AND SEGMENT NOS.	WINDOP
C	9. NO. OF JOINT FORCES AND TORQUE NOS.	WINDOP
C	10. NO. OF CENTER OF GRAVITY AND RELATED INFORMATION	WINDOP
C		OUTPUT
	WRITE(6,478)	CHGIII
478	FORMAT(1X,/,2X,'TABULAR TIME HISTORY CONTROL PARAMETERS')	CHGIII
	WRITE(6,479)	CHGIII
479	FORMAT(3X,'TYPE KSG SELECTED SEGMENTS OR JOINTS')	TTHKREF
	DO 20 K=1,9	WINDOP
C		OUTPUT
C	INPUT CARDS H.(K).(J) FOR K=1,3	OUTPUT
C		OUTPUT
	IF (K.LE.3) READ (5,18) KSG,KREF(1,K),MSG(1,K),(XSG(I,1,K),I=1,3)	TTHKREF
18	FORMAT (16,213,3F12.6)	TTHKREF
	IF (KSG.GT.KMAX) STOP 84	CHGIII
	IF (K.GT.3) GO TO 201	ATBIII
	IF (KSG.LE.1) READ(5,213) IDUMMY	ATBIII
213	FORMAT(I2)	ATBIII
	IF (KSG.LE.1) GO TO 201	ATBIII
	DO 205 J=2,KSG	ATBIII
	READ (5,210) KREF(J,K),MSG(J,K),(XSG(I,J,K),I=1,3)	TTHKREF
210	FORMAT (19,13,3F12.6)	TTHKREF
205	CONTINUE	ATBIII
201	CONTINUE	ATBIII
C		OUTPUT
C	INPUT CARDS H.(K) FOR K=4,9	WINDOP
C		OUTPUT
	IF (K.GT.3) READ (5,19) KSG,(KREF(J,K),MSG(J,K),J=1,KSG)	TTHKREF
19	FORMAT(16,22I3/(19,21I3))	TTHKREF
	IF (KSG.GT.KMAX) STOP 85	CHGIII
	WRITE (6,78) K,KSG,(MSG(J,K),J=1,KSG)	TTHKREF
	WRITE (6,81) (KREF(J,K),J=1,KSG)	TTHKREF
78	FORMAT(' H. ',11,1X,13,3X,20I3)	TTHKREF
81	FORMAT(' REF ',20I3)	TTHKREF
	DO 80 J=1,KSG	TTHKREF
	IF(KREF(J,K).GT.NGRND.OR.KREF(J,K).LT.0) STOP 55	TTHKREF
80	CONTINUE	TTHKREF
	IF (K.NE.7 .OR. KSG.EQ.0) GO TO 20	OUTPUT
	DO 12 J=1,KSG	OUTPUT
	L = MSG(J,K)	OUTPUT
	IF (IABS(IPIN(L)).EQ.4) MSG(J,K) = -L	OUTPUT
12	CONTINUE	OUTPUT
20	NSG(K) = KSG	OUTPUT
C		ATBIII
C	READ INPUT CARDS H.10	WINDOP
C		ATBIII
	READ (5,111) MCG	ATBIII

111	FORMAT(I6)	ATBIII
	IF (MCG.GT.MCGMAX) STOP 86	CHGIII
	IF (MCG.EQ.0) GO TO 114	ATBIII
	DO 113 K=1,MCG	ATBIII
	READ (5,112) M,N,(MCGIN(I+2,K),I=1,N)	ATBIII
112	FORMAT (24I3)	ATBIII
	IF (N.GT.NMAX) STOP 87	CHGIII
	WRITE (6,117) N,(MCGIN(I+2,K),I=1,N)	TTHKREF
117	FORMAT(' H.10',I3,3X,22I3)	TTHKREF
	WRITE (6,81) M	TTHKREF
	MCGIN(1,K) = M	ATBIII
113	MCGIN(2,K) = N	ATBIII
114	CONTINUE	ATBIII
10	IF (.NOT.LTAPE8) GO TO 21	OUTPUT
	WRITE (8) NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,NPANEL,	OUTPUT
*	MNPL,MNBLT,MNSEG,MNBAG,MPL,MBLT,MSEG,MBAG	OUTPUT
	WRITE (8) DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTTL,BAGTTL,	OUTPUT
*	SEG,JOINT,UNITL,UNITM,UNITT,NSG,MSG,XSG,MCG,	ATBIII
*	MCGIN,KREF,NHRNSS,NBLTPH,NPTSPB,NSD,MSDM,MSDN	CHGIII
21	IF(LTHIST) LINES= LINES + 1	FIXTTH
	IF (MOD(LINES,LPP).EQ.1 .AND. LTHIST) CALL HEDING (LINES,LPP)	OUTPUT
	NT = 20	OUTPUT
	USEC = 1000.0*TIME	OUTPUT
C		OUTPUT
C	COMPUTE AND PRINT DATA FOR 9 TYPES OF OUTPUT ABOVE	WINDOP
C		OUTPUT
	DO 44 K=1,9	WINDOP
	IF (NSG(K).LE.0) GO TO 44	OUTPUT
	KSG = NSG(K)	OUTPUT
	IF (K.GT.8) GO TO 440	WINDOP
	J3 = 3	OUTPUT
	IF (K.EQ.7) J3 = 2	OUTPUT
	DO 43 J1=1,KSG,J3	OUTPUT
	J2 = MIN0(J1+J3-1,KSG)	OUTPUT
	NT =NT + 1	OUTPUT
C	SETUP LOGICAL UNIT CONTROL (FOR PRINTER) FOR PERKIN & ELMER	PECONV
C	CALL CARCON(NT,1)	80386
	DO 38 J=J1,J2	OUTPUT
	L = IABS(MSG(J,K))	OUTPUT
	GO TO (22,24,26,29,31,34,35,601),K	WINDOP
C		OUTPUT
C	1. POIN" TOTAL ACCELERATION IN KREF(1) REFERENCE	CHGIII
C		OUTPUT
22	IF(LPMI(L).EQ.0) GO TO 521	CHGIII
	CALL MAT31(LPMI(1,1,L),XSG(1,J,K),T7)	CHGIII
	GO TO 523	CHGIII
521	DO 522 JL=1,3	CHGIII
522	T7(JL) = XSG(JL,J,K)	CHGIII
523	CALL CROSS (WMEC(1,L),T7,T1)	CHGIII
	CALL CROSS (WMEG(1,L),T1,T2)	OUTPUT
	CALL CROSS (WMEGD(1,L),T7,T3)	CHGIII
	CALL MAT31(D(1,1,L),GRAVITY,T7)	ACCEL



CALL MAT31(D(1,1,L),SEGLA(1,L),T4)	OUTPUT
DO 23 I=1,3	OUTPUT
IF(MSG(J,K).LT.0) T4(I)=T4(I)+T7(I)	ACCEL
ACC(I,J) = (T4(I)+T3(I)+T2(I))/G	OUTPUT
23 T1(I) = ACC(I,J)	OUTPUT
IF(MSG(J,K).GE.0) GO TO 405	ACCEL
KRF=L	ACCEL
IF(LPMI(KRF).NE.0) CALL DOT31(DPMI(1,1,KRF),T1,ACC(1,J))	ACCEL
IF(KREF(J,K).EQ.1) GOTO 33	ACCEL
DO 600 II=1,3	ACCEL
600 ACC(II,J)=ACC(II,J)-GRAVITY(II)/G	ACCEL
GOTO 33	ACCEL
C	OUTPUT
C 2. POINT REL. VELOCITY IN KREF(2) REFERENCE	CHGIII
C	OUTPUT
24 IF(KREF(J,2).EQ.0) KRF = NVEH	TTHKREF
IF(KREF(J,2).NE.0) KRF = KREF(J,2)	TTHKREF
IF(LPMI(L).EQ.0) GO TO 524	CHGIII
CALL MAT31(DPMI(1,1,L),XSG(1,J,K),T7)	CHGIII
GO TO 525	CHGIII
524 DO 526 JL=1,3	CHGIII
526 T7(JL) = XSG(JL,J,K)	CHGIII
525 CALL CROSS (WMEG(1,L),T7,T1)	CHGIII
CALL DOT31(D(1,1,L),T1,T2)	OUTPUT
DO 25 I=1,3	OUTPUT
25 T3(I) = T2(I) + SEGLV(I,L) - SEGLV(I,KRF)	CHGIII
GO TO 28	OUTPUT
C	OUTPUT
C 3. POINT REL. LINEAR DISPLACEMENT IN KREF(3) REFERENCE	CHGIII
C	OUTPUT
26 IF(KREF(J,3).EQ.0) KRF = NVEH	TTHKREF
IF(KREF(J,3).NE.0) KRF = KREF(J,3)	TTHKREF
IF (LPMI(L).EQ.0) GO TO 76	CHGIII
CALL DOT33 (DPMI(1,1,L),D(1,1,L),T4)	OUTPUT
CALL DOT31 (T4,XSG(1,J,K),T1)	OUTPUT
GO TO 77	OUTPUT
76 CALL DOT31 (D(1,1,L),XSG(1,J,K),T1)	OUTPUT
77 DO 27 I=1,3	OUTPUT
27 T3(I) = T1(I) + SEGLP(I,L) - SEGLP(I,KRF)	CHGIII
28 IF (LPMI(KRF).EQ.0) GO TO 403	CHGIII
CALL DOT33(DPMI(1,1,KRF),D(1,1,KRF),T5)	CHGIII
CALL MAT31(T5,T3,ACC(1,J))	CHGIII
GO TO 33	OUTPUT
403 CALL MAT31(D(1,1,KRF),T3,ACC(1,J))	CHGIII
33 ACC(4,J) = DSQRT(ACC(1,J)**2+ACC(2,J)**2+ACC(3,J)**2)	CHGIII
GO TO 38	CHGIII
C	OUTPUT
C 4. SEGMENT ANGULAR ACCELERATION IN KREF(4) REFERENCE	CHGIII
C	OUTPUT
29 DO 30 I=1,3	OUTPUT
ACC(I,J) = WMEGD(I,L)/(2.0*PI)	OUTPUT
30 T1(I) = ACC(I,J)	OUTPUT

405	CONTINUE	CHGIII
	IF(KREF(J,K).EQ.0) GO TO 401	TTHKREF
	KRF = KREF(J,K)	TTHKREF
	IF(LPMI(KRF).EQ.0) GO TO 402	CHGIII
	CALL DOT33(DPMI(1,1,KRF),D(1,1,KRF),T5)	CHGIII
	CALL DOTT33(T5,D(1,1,L),T6)	CHGIII
	CALL MAT31(T6,T1,ACC(1,J))	CHGIII
	GO TO 33	CHGIII
402	CALL DOTT33(D(1,1,KRF),D(1,1,L),T6)	CHGIII
	CALL MAT31(T6,T1,ACC(1,J))	CHGIII
	GO TO 33	CHGIII
401	KRF = L	CHGIII
	IF(LPMI(KRF).NE.0) CALL DOT31(DPMI(1,1,KRF),T1,ACC(1,J))	CHGIII
	GO TO 33	OUTPUT
C		OUTPUT
C	5. SEGMENT REL. ANGULAR VELOCITY IN KREF(5) REFERENCE	CHGIII
C		OUTPUT
31	IF(KREF(J,5).EQ.0) KRF = NVEH	TTHKREF
	IF(KREF(J,5).NE.0) KRF = KREF(J,5)	TTHKREF
	CALL DOT31 (D(1,1,L),WMEG(1,L),T1)	CHGIII
	CALL MAT31 (D(1,1,KRF),T1,T2)	CHGIII
	DO 32 I=1,3	OUTPUT
	IF (KRF.NE.L) T2(I)=T2(I)-WMEG(I,KRF)	PLTINC
32	T3(I) = T2(I)/(2.0*PI)	PLTINC
	IF(LPMI(KRF).EQ.0) GO TO 449	CHGIII
	CALL DOT31(DPMI(1,1,KRF),T3,ACC(1,J))	CHGIII
	GO TO 483	CHGIII
449	CONTINUE	CHGIII
	DO 457 KJL=1,3	CHGIII
457	ACC(KJL,J) = T3(KJL)	CHGIII
483	ACC(4,J) = DSQRT(ACC(1,J)**2+ACC(2,J)**2+ACC(3,J)**2)	CHGIII
	GO TO 38	OUTPUT
C		OUTPUT
C	6. SEGMENT REL. ANGULAR DISPLACEMENT IN KREF(6) REFERENCE	CHGIII
C		OUTPUT
34	IF(KREF(J,6).EQ.0) KRF = NVEH	TTHKREF
	IF(KREF(J,6).NE.0) KRF = KREF(J,6)	TTHKREF
	IF (LPMI(KRF).EQ.0.AND.LPMI(L).EQ.0) GO TO 36	CHGIII
	IF (LPMI(L).EQ.0) GO TO 435	CHGIII
	CALL DOT33(DPMI(1,1,L),D(1,1,L),T4)	CHGIII
435	IF (LPMI(KRF).EQ.0) GO TO 436	CHGIII
	CALL DOT33(DPMI(1,1,KRF),D(1,1,KRF),T5)	CHGIII
436	IF (LPMI(L).NE.0) GO TO 438	CHGIII
	CALL DOTT33(D(1,1,L),T5,T1)	CHGIII
	GO TO 37	CHGIII
438	IF (LPMI(KRF).NE.0) GO TO 439	CHGIII
	CALL DOTT33(T4,D(1,1,KRF),T1)	CHGIII
	GO TO 37	CHGIII
439	CALL DOTT33(T4,T5,T1)	CHGIII
	GO TO 37	CHGIII
36	CALL DOTT33(D(1,1,L),D(1,1,KRF),T1)	CHGIII
37	CALL YPRDEG(T1,ACC(1,J))	OUTPUT

	TRACE = 0.5*(T1(1)+T2(2)+T3(3)-1.0)	OUTPUT
	IF (TRACE.GT. 1.0) TRACE = 1.0	OUTPUT
	IF (TRACE.LT.-1.0) TRACE = -1.0	OUTPUT
	ACC(4,J) = DACOS(TRACE)/RADIAN	OUTPUT
	GO TO 38	OUTPUT
C		OUTPUT
C	7. JOINT PARAMETERS	OUTPUT
C		OUTPUT
	35 ACC(1,J) = PRJNT(1,L)	OUTPUT
	ACC(2,J) = PRJNT(2,L)/RADIAN	OUTPUT
	ACC(3,J) = PRJNT(3,L)/RADIAN	OUTPUT
	ACC(4,J) = PRJNT(4,L)/RADIAN	OUTPUT
	ACC(5,J) = DSQRT(PRJNT(5,L))	OUTPUT
	ACC(6,J) = DSQRT(PRJNT(6,L))	OUTPUT
	ACC(7,J) = DSQRT(PRJNT(7,L))	OUTPUT
	GOTO 38	WINDOP
C		WINDOP
C	8. SEGMENT WIND FORCE IN KREF(8) REFERENCE	WINDOP
C		WINDOP
	601 IF(KREF(J,8).EQ.0) KRF = NGRND	TTHKREF
	IF(KREF(J,8).NE.0) KRF = KREF(J,8)	TTHKREF
	CALL MAT31 (D(1,1,KRF),WF(1,L),T2)	WINDOP
	IF(LPMI(KRF).EQ.0) GO TO 602	WINDOP
	CALL DOT31(DPMI(1,1,KRF),T2,ACC(1,J))	WINDOP
	GO TO 604	WINDOP
	602 CONTINUE	WINDOP
	DO 603 KJL=1,3	WINDOP
	603 ACC(KJL,J) = T2(KJL)	WINDOP
	604 ACC(4,J) = DSQRT(ACC(1,J)**2+ACC(2,J)**2+ACC(3,J)**2)	WINDOP
	38 CONTINUE	OUTPUT
	IF (.NOT.LTAPE8) GO TO 40	OUTPUT
	KK = 0	OUTPUT
	I2 = 4	OUTPUT
	IF (K.EQ.7) I2 = 7	OUTPUT
	DO 39 J=J1,J2	OUTPUT
	DO 39 I=1,I2	OUTPUT
	KK = KK+1	OUTPUT
	39 TDATA(KK,NT-20) = ACC(I,J)	OUTPUT
	40 IF (.NOT.LTHIST) GO TO 43	OUTPUT
	IF (K.LE.6) WRITE (NT,41) USEC,((ACC(I,J),I=1,4),J=J1,J2)	OUTPUT
	IF (K.EQ.8) WRITE (NT,41) USEC,((ACC(I,J),I=1,4),J=J1,J2)	WINDOP
	41 FORMAT(F9.3,3(3X,4F9.3) )	OUTPUT
	IF (K.EQ.7) WRITE (NT,42) USEC,((ACC(I,J),I=1,7),J=J1,J2)	OUTPUT
	42 FORMAT(F9.3,2(F5.0,3F9.3,2X,3F9.3))	OUTPUT
	43 CONTINUE	OUTPUT
	GO TO 44	CHGIII
C		ATBIII
C	9. JOINT FORCES & TORQUES IN KREF(9) GEOMETRIC COORDINATE SYSTEM	WINDOP
C		CHGIII
	440 DO 860 L=1,KSG	PLTINC
	KRF = NVEH	PLTINC
	IF(KREF(L,9).NE.0) KRF = KREF(L,9)	PLTINC

LL=MSG(L,K)	CHGIII
IF (LPMI(KRF).EQ.0) GO TO 851	CHGIII
CALL DOT33 (DPMI(1,1,KRF),D(1,1,KRF),T5)	CHGIII
CALL MAT31 (T5,F(1,LL),T1)	CHGIII
CALL MAT31 (T5,TQ(1,LL),T2)	CHGIII
DO 852 JJ=1,3	CHGIII
T1(JJ) = T1(JJ)/100.0	CHGIII
852 T2(JJ) = -T2(JJ)/100.0	OUT385
GO TO 859	CHGIII
851 CONTINUE	CHGIII
CALL MAT31 (D(1,1,KRF),F(1,LL),T1)	CHGIII
CALL MAT31 (D(1,1,KRF),TQ(1,LL),T2)	CHGIII
DO 853 JJ=1,3	CHGIII
T1(JJ) = T1(JJ)/100.0	CHGIII
853 T2(JJ) = -T2(JJ)/100.0	OUT385
859 NT = NT + 1	CHGIII
C P & E CARRIAGE CONTROL	PECONV
C CALL CARCON(NT,1)	80386
IF (.NOT.LTAPE8) GO TO 855	CHGIII
DO 854 JL=1,3	CHGIII
TDATA (JL ,NT-20) = T1(JL)	CHGIII
854 TDATA (JL+3,NT-20) = T2(JL)	CHGIII
855 CONTINUE	CHGIII
IF (LTHIST) WRITE (NT,857) USEC,T1,T2	CHGIII
857 FORMAT(F9.3,3X,3F9.3,3X,3(2X,D10.3))	CHGIII
860 CONTINUE	CHGIII
44 CONTINUE	CHGIII
C	ATBIII
C 10. PRINT BODY PROPERTIES	WINDOP
C	ATBIII
IF (MCG.EQ.0) GO TO 131	ATBIII
DO 130 NCG=1,MCG	ATBIII
M = MCGIN(1,NCG)	ATBIII
N = MCGIN(2,NCG)	ATBIII
DO 120 J=1,9	ATBIII
120 T4(J) = 0.0	ATBIII
SUMW = 0.0	ATBIII
T7(1)=0.0	KINETIC
T7(2)=0.0	KINETIC
DO 123 I=1,N	ATBIII
K = MCGIN(I+2,NCG)	ATBIII
WG = W(K)/G	ATBIII
V=(SEGLV(1,K)-SEGLV(1,M))*2	KINETIC
* +(SEGLV(2,K)-SEGLV(2,M))*2	KINETIC
* +(SEGLV(3,K)-SEGLV(3,M))*2	KINETIC
T7(1)=T7(1)+0.5*WG*V	KINETIC
SUMW = SUMW + WG	ATBIII
DO 121 J=1,3	ATBIII
T7(2)=T7(2)+0.5*PHI(J,K)*(WMEG(J,K)-WMEG(J,M))*2	KINETIC
121 T1(J) = PHI(J,K)*WMEG(J,K)	ATBIII
CALL DOT31 (D(1,1,K),T1,T2)	ATBIII
CALL CROSS (SEGLP(1,K),SEGLV(1,K),T1)	ATBIII

DO 122 J=1,3	ATBIII
T4(J ) = T4(J ) + WG*SEGLP(J,K)	ATBIII
T4(J+3) = T4(J+3) + WG*SEGLV(J,K)	ATBIII
122 T4(J+6) = T4(J+6) + WG*T1(J) + T2(J)	ATBIII
123 CONTINUE	ATBIII
T7(3)=T7(1)+T7(2)	KINETIC
DO 124 J=1,3	ATBIII
124 T4(J) = T4(J)/SUMW - SEGLP(J,M)	ATBIII
C	ATBIII
C TRANSFORM FROM PRINCIPAL AXES TO LOCAL AXES	TGMOD1
C	ATBIII
IF (LPMI(M).EQ.0) GO TO 330	ATBIII
CALL DOT33(DPMI(1,1,M),D(1,1,M),T5)	ATBIII
CALL MAT31(T5,T4(1),T1)	ATBIII
CALL MAT31(T5,T4(4),T2)	ATBIII
CALL MAT31(T5,T4(7),T3)	ATBIII
GO TO 333	ATBIII
330 CONTINUE	ATBIII
CALL MAT31 (D(1,1,M),T4(1),T1)	ATBIII
CALL MAT31 (D(1,1,M),T4(4),T2)	ATBIII
CALL MAT31 (D(1,1,M),T4(7),T3)	ATBIII
333 CONTINUE	ATBIII
NT = NT + 1	ATBIII
IF (.NOT.LTAPE8) GO TO 126	ATBIII
DO 125 J=1,3	ATBIII
TDATA (J ,NT-20) = T1(J)	ATBIII
TDATA (J+3,NT-20) = T2(J)	ATBIII
TDATA(J+9,NT-20) = T7(J)	KINETIC
125 TDATA(J+6,NT-20) = T3(J)	ATBIII
126 IF (LTHIST) WRITE (NT,127) USEC,T1,T2,T3,T7	KINETIC
127 FORMAT (F9.3,3F8.3,9(1X,D10.3))	KINETIC
130 CONTINUE	ATBIII
131 CONTINUE	ATBIII
C	OUTPUT
C PRINT PLANE FORCES	OUTPUT
C	OUTPUT
MPSF = 0	OUTPUT
IF (NPL.EQ.0) GO TO 49	OUTPUT
IF (NPRT(18).EQ.1.OR.NPRT(18).EQ.7) GO TO 49	VARTTH
IF (NPRT(18).EQ.10.OR.NPRT(18).EQ.11) GO TO 49	VARTTH
IF (NPRT(18).GE.14) GO TO 49	VARTTH
DO 45 J=1,NPL	OUTPUT
45 MPSF = MPSF + MNPL(J)	OUTPUT
IF (MPSF.EQ.0) GO TO 49	OUTPUT
DO 47 J1=1,MPSF,2	OUTPUT
J2 = MINO(J1+1,MPSF)	OUTPUT
NT = NT+1	OUTPUT
C SETUP LOGICAL UNIT CONTROL (PRINTER CONTROL) FOR P & E	PECONV
C CALL CARCON(NT,1)	80386
IF (.NOT.LTAPE8) GO TO 47	OUTPUT
KK = 0	OUTPUT
DO 46 J=J1,J2	OUTPUT

DO 46 I=1,7	OUTPUT
KK = KK+1	OUTPUT
46 TDATA(KK,NT-20) = PSF(I,J)	OUTPUT
47 IF (LTHIST) WRITE (NT,48) USEC,((PSF(I,J),I=1,7),J=J1,J2)	OUTPUT
48 FORMAT(F9.3,2(F9.3,3F9.2,3F8.3) )	OUTPUT
C	OUTPUT
C PRINT BELT FORCES	OUTPUT
C	OUTPUT
49 MBSF = 0	OUTPUT
IF (NBLT.EQ.0) GO TO 67	OUTPUT
IF (NPRT(18).EQ.2.OR.NPRT(18).GE.13) GO TO 67	VARTTH
IF (NPRT(18).GE.7.AND.NPRT(18).LE.9) GO TO 67	VARTTH
DO 50 J=1,NBLT	OUTPUT
50 MBSF = MBSF + MNBTL(J)	OUTPUT
IF (MBSF.EQ.0) GO TO 67	OUTPUT
DO 52 J1=1,MBSF,2	OUTPUT
J2 = MINO(J1+1,MBSF)	OUTPUT
NT = NT+1	OUTPUT
C LOGICAL UNIT (PRINTER CONTROL) FOR P & E	PECONV
C CALL CARCON(NT,1)	80386
IF (.NOT.LTAPE8) GO TO 52	OUTPUT
KK = 0	OUTPUT
DO 51 J=J1,J2	OUTPUT
DO 51 I=1,4	OUTPUT
KK = KK+1	OUTPUT
51 TDATA(KK,NT-20) = BSF(I,J)	OUTPUT
52 IF (LTHIST) WRITE (NT,53) USEC,((BSF(I,J),I=1,4),J=J1,J2)	OUTPUT
53 FORMAT(F9.3,4(F15.6,F12.2,3X) )	OUTPUT
C	OUTPUT
C PRINT HARNESS-BELT ENDPOINT FORCES (STORED IN BSF ARRAY).	OUTPUT
C	OUTPUT
67 IF (NHRNSS.LE.0) GO TO 71	OUTPUT
IF (NPRT(18).EQ.3.OR.NPRT(18).EQ.11) GO TO 71	VARTTH
IF (NPRT(18).EQ.9.OR.NPRT(18).EQ.8) GO TO 71	VARTTH
IF (NPRT(18).EQ.13.OR.NPRT(18).EQ.14) GO TO 71	VARTTH
IF (NPRT(18).GE.16) GO TO 71	VARTTH
MBSF1 = MBSF + 1	OUTPUT
DO 68 I=1,NHRNSS	OUTPUT
68 MBSF = MBSF + NBLTPH(I)	OUTPUT
DO 70 J1=MBSF1,MBSF,2	OUTPUT
J2 = MINO(J1+1,MBSF)	OUTPUT
NT = NT+1	OUTPUT
C LOGICAL UNIT (PRINTER CONTROL) FOR P & E	PECONV
C CALL CARCON(NT,1)	80386
IF (.NOT.LTAPE8) GO TO 70	OUTPUT
KK = 0	OUTPUT
DO 69 J=J1,J2	OUTPUT
DO 69 I=1,4	OUTPUT
KK = KK+1	OUTPUT
69 TDATA(KK,NT-20) = BSF(I,J)	OUTPUT
70 IF (LTHIST) WRITE (NT,53) USEC,((BSF(I,J),I=1,4),J=J1,J2)	OUTPUT
C	OUTPUT

C	PRINT SPRING DAMPER FORCES (STORED IN BSF ARRAY).	OUTPUT
C		OUTPUT
	71 IF (NSD.LE.0) GO TO 54	OUTPUT
	IF (NPRT(18).EQ.4.OR.NPRT(18).EQ.9) GO TO 54	VARTTH
	IF (NPRT(18).GE.12) GO TO 54	VARTTH
	MBSF1 = MBSF + 1	OUTPUT
	MBSF = MBSF + (NSD: )/2	OUTPUT
	DO 73 J1=MBSF1,MBSF,2	OUTPUT
	J2 = MINO(J1+1,MBSF)	OUTPUT
	NT = NT+1	OUTPUT
C	LOGICAL UNIT (PRINTER CONTROL) FOR P & E	PECONV
C	CALL CARCON(NT,1)	80386
	IF (.NOT.LTAPE8) GO TO 73	OUTPUT
	KK = 0	OUTPUT
	DO 72 J=J1,J2	OUTPUT
	DO 72 I=1,4	OUTPUT
	KK = KK+1	OUTPUT
	72 TDATA(KK,NT-20) = BSF(I,J)	OUTPUT
	73 IF (LTHIST) WRITE (NT,74) USEC,((BSF(I,J),I=1,4),J=J1,J2)	OUTPUT
	74 FORMAT (F9.3,4(F14.3,F12.2,4X))	OUTPUT
C		OUTPUT
C	PRINT SEGMENT CONTACT FORCES	OUTPUT
C		OUTPUT
	54 MSSF = 0	OUTPUT
	IF (NPRT(18).EQ.5.OR.NPRT(18).EQ.13) GO TO 161	VARTTH
	IF (NPRT(18).EQ.10.OR.NPRT(18).EQ.11) GO TO 161	VARTTH
	IF (NPRT(18).GE.15) GO TO 161	VARTTH
	DO 55 J=1,NSEG	OUTPUT
	55 MSSF = MSSF + MNSEG(J)	OUTPUT
	IF (MSSF.EQ.0) GO TO 59	OUTPUT
	DO 57 J=1,MSSF	OUTPUT
	NT = NT+1	OUTPUT
C	LOGICAL UNIT (PRINTER CONTROL) FOR P & E	PECONV
C	CALL CARCON(NT,1)	80386
	IF (.NOT.LTAPE8) GO TO 57	OUTPUT
	DO 56 I=1,10	OUTPUT
	56 TDATA(I,NT-20) = SSF(I,J)	OUTPUT
	57 IF (LTHIST) WRITE (NT,58) USEC,(SSF(I,J),I=1,10)	OUTPUT
	58 FORMAT(2F9.3,3F9.2,3F8.3,2X,3F8.3)	OUTPUT
	161 CONTINUE	VARTTH
C		OUTPUT
C	PRINT AIRBAG FORCES	OUTPUT
C		OUTPUT
	59 IF (NBAG.EQ.0) GO TO 65	OUTPUT
	IF (NPRT(18).EQ.6.OR.NPRT(18).EQ.9) GO TO 65	VARTTH
	IF (NPRT(18).GE.12) GO TO 65	VARTTH
	K1 = 1	OUTPUT
	DO 64 J=1,NBAG	OUTPUT
	IF (MNBAG(J).EQ.0) GO TO 64	OUTPUT
	KBAG = MNBAG(J)+NPANEL(J)+5	OUTPUT
	DO 63 J1=1,KBAG,4	OUTPUT
	J2 = MINO(J1+3,KBAG)	OUTPUT

	K2 = K1+J2-J1	OUTPUT
	NT = NT+1	OUTPUT
C	LOGICAL UNIT (PRINTER CONTROL) FOR P & E	PECONV
C	CALL CARCON(NT,1)	30386
	IF (.NOT.LTAPE8) GO TO 61	OUTPUT
	KK = 0	OUTPUT
	DO 60 K=K1,K2	OUTPUT
	DO 60 I=1,3	OUTPUT
	KK = KK+1	OUTPUT
60	TDATA(KK,NT-20) = BAGSF(I,K)	OUTPUT
61	IF (.NOT.LTHIST) GO TO 63	OUTPUT
	IF (J1.EQ.1) WRITE (NT,75) USEC,((BAGSF(I,K),I=1,3),K=K1,K2)	OUTPUT
	IF (J1.NE.1) WRITE (NT,62) USEC,((BAGSF(I,K),I=1,3),K=K1,K2)	OUTPUT
75	FORMAT (F9.3,3X,3F9.2,2(3X,3F9.3),3X,3F9.2)	OUTPUT
62	FORMAT(F9.3,4(3X,3F9.2))	OUTPUT
63	K1 = K2+1	OUTPUT
64	CONTINUE	OUTPUT
65	NT = NT-20	OUTPUT
	IF(NT.GT.NTMAX) STOP 56	CHGIII
	IF (LTAPE8) WRITE (8) NT,USEC,((TDATA(I,J),I=1,14),J=1,NT)	OUTPUT
	PREVT = TIME	OUTPUT
	CALL ELTIME(2,8)	OUTPUT
66	RETURN	OUTPUT
	END	OUTPUT



	SUBROUTINE PANEL (DRR,ZR,JB)	PANEL
		REV III.2 08/08/84REVIII
C	COMPUTES AIRBAG PARAMETERS DURING INFLATION OF BAG.	PANEL
C		PANEL
C	GIVEN: DRR - DC MATRIX RELATIVE TO VEHICLE	PANEL
C	ZR - CG LOCATION IN VEHICLE REFERENCE	PANEL
C		PANEL
C	COMPUTE: SEGLP,SEGLV,SEGLA,D,WMEG & WMEGD FOR SEGMENT JB.	PANEL
C		PANEL
	IMPLICIT REAL*8 (A-H,O-Z)	PANEL
	DIMENSION DRR(3,3),ZR(3),T1(3),T2(3)	PANEL
	COMMON/CONTROL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,	PANEL
	*          NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),	PANEL
	*          SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)	PANEL
	CALL MAT33 (DRR,D(1,1,NVEH),D(1,1,JB))	PANEL
	CALL MAT31 (DRR,WMEG(1,NVEH),WMEG(1,JB))	PANEL
	CALL DOT31 (D(1,1,NVEH),ZR,SEGLP(1,JB))	PANEL
	CALL CROSS (WMEG(1,NVEH),ZR,T1)	PANEL
	CALL DOT31 (D(1,1,NVEH),T1,SEGLV(1,JB))	PANEL
	CALL CROSS (WMEG(1,NVEH),T1,T2)	PANEL
	CALL DOT31 (D(1,1,NVEH),T2,SEGLA(1,JB))	PANEL
	DO 10 I=1,3	PANEL
	SEGLP(I,JB) = SEGLP(I,JB) + SEGLP(I,NVEH)	PANEL
	SEGLV(I,JB) = SEGLV(I,JB) + SEGLV(I,NVEH)	PANEL
	SEGLA(I,JB) = SEGLA(I,JB) + SEGLA(I,NVEH)	PANEL
10	WMEGD(I,JB) = WMEGD(I,NVEH)	PANEL
	RETURN	PANEL
	END	PANEL

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SUBROUTINE PDAUX (VAR,DER,NEQ,KDINT)                                PDAUX
C                                                                    REV IV    07/24/86SLIP
C    PURPOSE IS TO ACT AS INTERFACE BETWEEN INTEGRATOR AND DAUX TO  PDAUX
C    ACCOMODATE VARIABLE NUMBER OF FUNCTIONS TO BE INTEGRATED.    PDAUX
C                                                                    PDAUX
C    ARGUMENTS:                                                    PDAUX
C        VAR - ARRAY OF NEQ STATE VARIABLES UPDATED BY DINT.      PDAUX
C        DER - ARRAY OF NEQ DERIVATIVES TO BE SUPPLIED BY DAUX.   PDAUX
C        NEQ - NUMBER OF STATE VARIABLES AND DERIVATIVES.         PDAUX
C        KDINT - INTEGRATION STEP NUMBER IN DINT.                 PDAUX
C                                                                    PDAUX
C    IMPLICIT REAL*8 (A-H,O-Z)                                     PDAUX
C    DIMENSION VAR(3,1),DER(3,1)                                   PDAUX
C    COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,       PDAUX
C    * NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG            PAGE
C    COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30), PDAUX
C    * SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)              PDAUX
C    COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60), SLIP
C    * RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),           PDAUX
C    * JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)          PDAUX
C    COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),      PDAUX
C    * BLTTTL(5,8),PLTTTL(5,30),BAGTTL(5,6),SEG(30),            PDAUX
C    * JCINT(30),CGS(30),JS(30)                                   PDAUX
C    REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,FLTTTL,BAGTTL,SEG,JOINT PDAUX
C    LOGICAL*1 CGS,JS                                             PDAUX
C    COMMON/INTEST/ SGTEST(3,4,30),XTEST(3,120),SEGT(120),REGT(120) PDAUX
C    REAL SEGT                                                    PDAUX
C    COMMON/FLXBLE/ HF(4,12,8),B42(3,3,24),V4(3,8),NFLEX(3,8)    PDAUX
C    COMMON/CEULER/ IEULER(30),HIR(3,3,90),ANG(3,30),ANGD(3,30),  SLIP
C    * FE(3,30),TQE(3,30),CONST(5,30)                            SLIP
C    COMMON/TEMPVS/ T(3,30),VXT(3),DDMY(35020)                    80386
C    DIMENSION SD(3,3,30) , E1(30) , NTST(30) , LSEG(30) , RGTTL(4) PDAUX
C    LOGICAL LSEG                                                 PDAUX
C    DATA NTST/30*0/                                             PDAUX
C    DATA RGTTL/8HANG VEL ,8HLIN VEL ,8HANG ACC ,8HLIN ACC /    PDAUX
C    CALL ELTIME(1,6)                                             PDAUX
C    MBAG = NGRND                                                 PDAUX
C    IF (NTST(1).NE.0) GO TO 10                                    PDAUX
C    LSEG(1) = .FALSE.                                           VAXCHG
C    NTST(1) = 1                                                  ATBIII
C    DO 5 M=2,MBAG                                               ATBIII
C    LSEG(M) = ISING(M).GE.0 .AND. JNT(M-1).NE.0                ATBIII
C    IF (IABS(IPIN(M-1)).GE.5.AND.IEULER(M-1).GE.0) LSEG(M)=.FALSE. SLIP
C    5 NTST(M) = M                                               PDAUX
C    NTST(NGRND) = -NGRND                                         PDAUX
C    LSEG(NGRND) = .TRUE.                                         PDAUX
C    IF (NFLX.EQ.0) GO TO 10                                       PDAUX
C    DO 6 J=1,NFLX                                               PDAUX
C    M = NFLEX(2,J)                                               PDAUX
C    6 NTST(M) = -M                                               PDAUX
C    10 IF (KDINT.EQ.4) GO TO 48                                   PDAUX
C    IF (KDINT.GT.0) GO TO 20                                     PDAUX

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C		PDAUX
C	KDINT=0 IMPLIES INITIAL CALL FROM DINT. PDAUX TO SUPPLY INITIAL	PDAUX
C	VALUES TO STATE VARIABLES AND COMPUTE VALUE OF NEQ.	PDAUX
C		PDAUX
C		PDAUX
C	(A) SET Q TO IDENTITY QUATERNION	PDAUX
C		PDAUX
	N = 0	PDAUX
	DO 12 M=1,MBAG	PDAUX
	IF (NTST(M).LT.0) GO TO 12	PDAUX
	N = N+1	PDAUX
	REGT(N) = RGTTL(1)	PDAUX
	SEGT(N) = SEG(M)	PDAUX
	E1(N) = 1.0	PDAUX
	DO 11 I=1,3	PDAUX
	XTEST(I,N) = SGTEST(I,1,M)**2	PDAUX
	11 VAR(I,N) = 0.0	PDAUX
	12 CONTINUE	PDAUX
C		PDAUX
C	(B) SEGLP OF REFERENCE SEGMENTS	PDAUX
C		PDAUX
	DO 14 M=1,MBAG	PDAUX
	IF (LSEG(M)) GO TO 14	PDAUX
	N = N+1	PDAUX
	REGT(N) = RGTTL(2)	PDAUX
	SEGT(N) = SEG(M)	PDAUX
	DO 13 I=1,3	PDAUX
	XTEST(I,N) = SGTEST(I,2,M)**2	PDAUX
	13 VAR(I,N) = SEGLP(I,M)	PDAUX
	14 CONTINUE	PDAUX
C		PDAUX
C	(C) WMEG	PDAUX
C		PDAUX
	DO 16 M=1,MBAG	PDAUX
	IF (NTST(M).LT.0) GO TO 16	PDAUX
	N = N+1	PDAUX
	REGT(N) = RGTTL(3)	PDAUX
	SEGT(N) = SEG(M)	PDAUX
	DO 15 I=1,3	PDAUX
	XTEST(I,N) = SGTEST(I,3,M)**2	PDAUX
	15 VAR(I,N) = WMEG(I,M)	PDAUX
	16 CONTINUE	PDAUX
C		PDAUX
C	(D) SEGLV OF REFERENCE SEGMENTS	PDAUX
C		PDAUX
	DO 18 M=1,MBAG	PDAUX
	IF (LSEG(M)) GO TO 18	PDAUX
	N = N+1	PDAUX
	REGT(N) = RGTTL(4)	PDAUX
	SEGT(N) = SEG(M)	PDAUX
	DO 17 I=1,3	PDAUX
	XTEST(I,N) = SGTEST(I,4,M)**2	PDAUX

17	VAR(I,N) = SEGLV(I,M)	PDAUX
18	CONTINUE	PDAUX
	NEQ = 3*N	PDAUX
	GO TO 40	PDAUX
20	IF (KDINT.NE.1) GO TO 30	PDAUX
C		PDAUX
C	KDINT = 1, 1ST STEP IN ADVANCING INTEGRATING INTERVAL,	PDAUX
C	SAVE DC MATRICES IF TIME HAS ADVANCED.	PDAUX
C		PDAUX
	N = 0	PDAUX
	DO 22 M=1,MBAG	PDAUX
	IF (NTST(M).LT.0) GO TO 22	PDAUX
	N = N+1	PDAUX
	DO 21 J=1,3	PDAUX
	DO 21 I=1,3	PDAUX
21	SD(I,J,N) = D(I,J,M)	PDAUX
22	CONTINUE	PDAUX
C		PDAUX
C	KDINT > 0,1 - FETCH SAVED DC MATRICES AND UPDATE BY CURRENT THETA.	PDAUX
C		PDAUX
C	(A) UPDATE D BY Q	PDAUX
C		PDAUX
30	N = 0	PDAUX
	DO 32 M=1,MBAG	PDAUX
	IF (NTST(M).LT.0) GO TO 32	PDAUX
	N = N+1	PDAUX
	EDOTE = VAR(1,N)**2 + VAR(2,N)**2 + VAR(3,N)**2	PDAUX
	IF (EDOTE.GE.1.0) KDINT = -KDINT	PDAUX
	IF (KDINT.LE.0) GO TO 99	PDAUX
	E1(N) = DSQRT(1.0-EDOTE)	PDAUX
	CALL DSETQ(SD(1,1,N),VAR(1,N),EDOTE,E1(N),D(1,1,M))	PDAUX
32	CONTINUE	PDAUX
C		PDAUX
C	KDINT > 6 - STORE STATE VARIABLES INTO PROGRAM ARRAYS.	PDAUX
C		PDAUX
C	(B) SEGLP OF REFERENCE SEGMENTS	PDAUX
C		PDAUX
	DO 35 M=1,MBAG	PDAUX
	IF (LSEG(M)) GO TO 35	PDAUX
	N = N+1	PDAUX
	DO 34 I=1,3	PDAUX
34	SEGLP(I,M) = VAR(I,N)	PDAUX
35	CONTINUE	PDAUX
C		PDAUX
C	(C) WMEG	PDAUX
C		PDAUX
	DO 31 M=1,MBAG	PDAUX
	IF (NTST(M).LT.0) GO TO 31	PDAUX
	N = N+1	PDAUX
	DO 36 I=1,3	PDAUX
36	WMEG(I,M) = VAR(I,N)	PDAUX
31	CONTINUE	PDAUX

C		PDAUX
C	(D) SEGLV OF REFERENCE SEGMENTS	PDAUX
C		PDAUX
	DO 38 M=1,MBAG	PDAUX
	IF (LSEG(M)) GO TO 38	PDAUX
	N = N+1	PDAUX
	DO 37 I=1,3	PDAUX
	37 SEGLV(I,M) = VAR(I,N)	PDAUX
	38 CONTINUE	PDAUX
C		PDAUX
C	CALL DAUX ROUTINE TO COMPUTE DERIVATIVES	PDAUX
C		PDAUX
	40 CALL DAUX(0)	PDAUX
C		PDAUX
C	STORE DERIVATIVES FOR INTEGRATING SUBROUTINE.	PDAUX
C		PDAUX
C	(A) DERIVATIVE OF Q	PDAUX
C		PDAUX
	N = 0	PDAUX
	DO 39 M=1,MBAG	PDAUX
	IF (NTST(M).LT.0) GO TO 39	PDAUX
	N = N+1	PDAUX
	CALL CROSS(VAR(1,N),WMEG(1,M),VXT)	PDAUX
	DO 41 I=1,3	PDAUX
	41 DER(I,N) = 0.5*(E1(N)*WMEG(I,M) + VXT(I) )	PDAUX
	39 CONTINUE	PDAUX
	NQUAT = N	PDAUX
C		PDAUX
C	(B) SEGLV OF REFERENCE SEGMENTS	PDAUX
C		PDAUX
	DO 43 M=1,MBAG	PDAUX
	IF (LSEG(M)) GO TO 43	PDAUX
	N = N+1	PDAUX
	DO 42 I=1,3	PDAUX
	42 DER(I,N) = SEGLV(I,M)	PDAUX
	43 CONTINUE	PDAUX
C		PDAUX
C	(C) WMEGD	PDAUX
C		PDAUX
	DO 47 M=1,MBAG	PDAUX
	IF (NTST(M).LT.0) GO TO 47	PDAUX
	N = N+1	PDAUX
	DO 44 I=1,3	PDAUX
	44 DER(I,N) = WMEGD(I,M)	PDAUX
	47 CONTINUE	PDAUX
C		PDAUX
C	(D) SEGLA OF REFERENCE SEGMENTS	PDAUX
C		PDAUX
	DO 46 M=1,MBAG	PDAUX
	IF (LSEG(M)) GO TO 46	PDAUX
	N = N+1	PDAUX
	DO 45 I=1,3	PDAUX

45 DER(I,N) = SEGLA(I,M)	PDAUX
46 CONTINUE	PDAUX
IF (KDINT.NE.4) GO TO 99	PDAUX
48 N = 0	PDAUX
DO 51 M=1,MBAG	PDAUX
IF (NTST(M).LT.0) GO TO 51	PDAUX
N = N+1	PDAUX
E1(N) = 1.0	PDAUX
DO 50 I=1,3	PDAUX
DER(I,N) = 0.5*WMEG(I,M)	PDAUX
50 VAR(I,N) = 0.0	PDAUX
51 CONTINUE	PDAUX
99 IF (KDINT.EQ.2) KDINT = NQUAT	PDAUX
CALL ELTIME(2,6)	PDAUX
RETURN	PDAUX
END	PDAUX

	SUBROUTINE PLEDG(AREAL,BD,PL)		PLEDG
C		REV IV 12/11/87	HYFIX
	IMPLICIT REAL*8(A-H,O-Z)		PLEDG
	LOGICAL AREAL		PLEDG
	DIMENSION BD(24),PL(24)		HYFIX
	DIMENSION HAREA(2,2,5),ZC(3,14),X(3),UV(3,2),IV(14)		HYFIX
C	SHARED WITH PLELP-PLSEGF		HYFIX
	COMMON/TEMPVS/DMNT(3,3),DHNT(3,3),DUM1(18),TM(3),R(3),RM(3),		HYFIX
X	DUM2(9),UP(3),VP(3),U(3),V(3),EU(3),EV(3),ET(3),		HYFIX
X	A(2),B(2),CC(2),DUM4(12),TH(3),XH(3),RMD(3),RND(3),		HYFIX
X	APT(2,2,2),AC(2,2),BC(2,2),AFP,E(2,2),DELT,AREA,		HYFIX
X	AB,BB,BT(2),XNC(3),UH(3),P,AMR,FM,T4(3),ALIM(2,2)		HYFIX
*	,DMY(34965)		80386
	EQUIVALENCE (UV(1,1),U(1))		HYFIX
	EQUIVALENCE (ALIM(1,1),BMIN),(ALIM(1,2),AMIN)		HYFIX
	EQUIVALENCE (ALIM(2,1),BMAX),(ALIM(2,2),AMAX)		HYFIX
	EQUIVALENCE (AC(1,1),BB1),(AC(1,2),AA1)		HYFIX
	EQUIVALENCE (AC(2,1),BB2),(AC(2,2),AA2)		HYFIX
	EQUIVALENCE (BC(1,1),AB1),(BC(1,2),BA1)		HYFIX
	EQUIVALENCE (BC(2,1),AB2),(BC(2,2),BA2)		HYFIX
C			HYFIX
	AREA = 0.0		PLEDG
	AREAL = .FALSE.		PLEDG
	CALCULATE CENTER OF ELLIPSE IN PLANE		PLEDG
C	T4 IS VECTOR FROM CENTER OF ELLIPSOID TO CENTER OF ELLIPSE		PLEDG
	DO 10 I = 1,3		PLEDG
	T4(I) = FM*XH(I)		HYFIX
	10 XNC(I) = XNC(I) + T4(I)		PLEDG
C	XNC P1 TO CENTER OF ELLIPSE		PLEDG
C	PUT PLANE VECTORS IN ELLIPSE SYSTEM TH IS PLANE VECTOR		PLEDG
	IF (BD(1).LT.0.0) CALL MAT33(BD(8),DMNT,DHNT)		HYPER
	IF (BD(1).LT.0.0) GO TO 20		HYPER
	DO 15 I = 1,3		HYPER
	DO 15 J = 1,3		HYPER
	15 DHNT(I,J) = DMNT(I,J)		HYPER
	20 CALL MAT31(DHNT,PL( 8),UP)		HYPER
	CALL MAT31(DHNT,PL(13),VP)		HYPER
	CALL MAT31(DHNT,PL(18), U)		HYPER
	CALL MAT31(DHNT,PL(21), V)		HYPER
C	U IS P2 - P1, V IS P3 - P1, PLANE VECTOR IS TM		PLEDG
	CALCULATE CENTER FROM P1 IN U, V COORDINATES		PLEDG
	B(1) = (UP(1)*XNC(1) + UP(2)*XNC(2) + UP(3)*XNC(3))/PL(12)		PLEDG
	B(2) = (VP(1)*XNC(1) + VP(2)*XNC(2) + VP(3)*XNC(3))/PL(17)		PLEDG
	AMIN = -B(1)		HYFIX
	AMAX = 1.0 - B(1)		HYFIX
	BMIN = -B(2)		HYFIX
	BMAX = 1.0 - B(2)		HYFIX
C	GET ELLIPSE EQUATION		PLEDG
	DO 25 I = 1,2		HYPER
	DO 25 J = 1,2		HYPER
	25 E(I,J) = 0.0		HYPER
	IF (BD(1).GT.0.0) GO TO 35		HYPER

C TREAT HYPER AS ELLIPSE FOR FIRST GUESS	HYPER
DO 30 I = 1,3	HYPER
EU(I) = U(I)*BD(I+16)	HYPER
30 EV(I) = V(I)*BD(I+16)	HYPER
C GET INTERSECTION OF PLANE WITH BOX	HYFIX
CALL HYBOX(BD(2),TH,T4,MB,ZC,IV)	HYPER
IF (MB.LT.6) GO TO 140	HYPER
GO TO 40	HYPER
35 CALL MAT31(BD(7),U,EU)	HYPER
CALL MAT31(BD(7),V,EV)	HYPER
40 DO 45 K = 1,3	HYPER
E(1,1) = E(1,1) + U(K)*EU(K)	HYPER
E(1,2) = E(1,2) + V(K)*EU(K)	HYPER
45 E(2,2) = E(2,2) + V(K)*EV(K)	HYPER
DELT = E(1,1)*E(2,2) - E(1,2)**2	PLEDGE
C WHAT ABOUT AMR FOR HYPER?? 1 - FM**P ?	HYFIX
R2D = AMR/DELT	HYFIX
COMPUTE BOUNDS OF ELLIPSOID LOCATION OF MAX AND MIN ALPHA	HYFIX
AA2 = DSQRT(E(2,2)*R2D)	HYFIX
AA1 = -AA2	HYFIX
C BA IS VALUE OF BETA AT AT ALPHA MAX	HYFIX
BA1 = E(1,2)*AA2/E(2,2)	HYFIX
BA2 = -BA1	HYFIX
IF (BD(1).GE.-2.0) GO TO 50	HYPER
CALL HYBND(MB,ZC,IV,UP,-1.,X)	HYPER
CALL HYLIM(AA1,U,BA1,V,FM,XH,X,BD)	HYFIX
50 AMIN = DMAX1(AA1,AMIN)	HYFIX
IF (AMIN.GE.AMAX) GO TO 140	HYFIX
IF (BD(1).GE.-2.0) GO TO 55	HYPER
CALL HYBND(MB,ZC,IV,UP,1.,X)	HYPER
CALL HYLIM(AA2,U,BA2,V,FM,XH,X,BD)	HYFIX
55 AMAX = DMIN1(AA2,AMAX)	HYFIX
IF (AMIN.GE.AMAX) GO TO 140	HYPER
COMPUTE BOUNDS OF ELLIPSOID LOCATION OF MAX AND MIN BETA	HYFIX
BB2 = DSQRT(E(1,1)*R2D)	HYFIX
BB1 = -BB2	HYFIX
C AB IS VALUE OF ALPHA AT AT BETA MAX	HYFIX
AB1 = E(1,2)*BB2/E(1,1)	HYFIX
AB2 = -AB1	HYFIX
IF (BD(1).GE.-2.0) GO TO 60	HYPER
CALL HYBND(MB,ZC,IV,VP,-1.,X)	HYPER
CALL HYLIM(BB1,V,AB1,U,FM,XH,X,BD)	HYFIX
60 BMIN = LMAX1(BB1,BMIN)	HYFIX
IF (BMIN.GE.BMAX) GO TO 140	HYFIX
IF (BD(1).GE.-2.0) GO TO 65	HYPER
CALL HYBND(MB,ZC,IV,VP,1.,X)	HYPER
CALL HYLIM(BB2,V,AB2,U,FM,XH,X,BD)	HYFIX
65 BMAX = DMIN1(BB2,BMAX)	HYFIX
IF (BMIN.GE.BMAX) GO TO 140	HYPER
COMPUTE ALPHA'S AT BMIN AND BMAX; BETA'S AT AMIN AND AMAX IF NOT ON	HYFIX
C ELLIPSOID	HYFIX
IF (BD(1).LT.-2.0) GO TO 80	HYPER



DO 76 L = 1,2	HYFIX
K = 3 - L	HYFIX
DO 75 J = 1,2	HYPER
DIS = 0.0	HYFIX
AFP = BC(J,L)	HYFIX
IF (ALIM(J,L).EQ.AC(J,L)) GO TO 74	HYFIX
AFP = ALIM(J,L)/E(L,L)	HYFIX
DISC = AMR/E(L,L) - DELT*AFP**2	HYFIX
DIS = 0.0	HYFIX
IF (DISC.GT.0.0) DIS = DSQRT(DISC)	HYFIX
AFP = -AFP*E(1,2)	HYFIX
74 APT(1,J,L) = DMAX1 (AFP-DIS,ALIM(1,K))	HYFIX
APT(2,J,L) = DMIN1 (AFP+DIS,ALIM(2,K))	HYFIX
75 CONTINUE	HYPER
76 CONTINUE	HYFIX
GO TO 95	HYPER
80 DO 90 L = 1,2	HYPER
K = 3 - L	HYFIX
DO 89 J = 1,2	HYFIX
DIS = 0.0	HYFIX
BT(1) = BC(J,L)	HYFIX
BT(2) = BC(J,L)	HYFIX
IF (ALIM(J,L).EQ.AC(J,L)) GO TO 88	HYFIX
M = 2	HYFIX
IF (ALIM(J,L).LT.0.0) M = 1	HYFIX
CM = BC(M,L)/AC(M,L)	HYFIX
CL = ALIM(J,L)*CM	HYFIX
DO 82 I = 1,3	HYFIX
82 RM(I) = T4(I) + ALIM(J,L)*(UV(I,K) + CM*UV(I,L))	HYFIX
DO 85 I = 1,2	HYFIX
CALL HYVAL(BT(I),UV(1,L),RM,BD,I)	HYFIX
85 BT(I) = BT(I) + CL	HYFIX
88 APT(1,J,L) = DMAX1 (BT(1),ALIM(1,K))	HYFIX
APT(2,J,L) = DMIN1 (BT(2),ALIM(2,K))	HYFIX
89 CONTINUE	HYFIX
90 CONTINUE	HYPER
C SET UP LEGAL BOUNDARIES	HYFIX
C APT            L = 1                            L = 2	HYFIX
C            A-(BMIN)    A-(BMAX)            B-(AMIN)    B-(AMAX)	HYFIX
C            A+(BMIN)    A+(BMAX)            B+(AMIN)    B+(AMAX)	HYFIX
C SET UP HAREA (LINE SEGMENTS) CLOCKWISE STARTING WITH AMIN	HYFIX
95 L = 0	HYFIX
HAREA(1,1,L+1) = AMIN	HYFIX
HAREA(2,1,L+1) = APT(2,1,2)	HYFIX
HAREA(1,2,L+1) = AMIN	HYFIX
HAREA(2,2,L+1) = APT(1,1,2)	HYFIX
IF (APT(2,1,2).GE.APT(1,1,2)) L = L + 1	HYFIX
HAREA(1,1,L+1) = APT(1,1,1)	HYFIX
HAREA(2,1,L+1) = BMIN	HYFIX
HAREA(1,2,L+1) = APT(2,1,1)	HYFIX
HAREA(2,2,L+1) = BMIN	HYFIX
IF (APT(2,1,1).GE.APT(1,1,1)) L = L + 1	HYFIX

HAREA(1,1,L+1) = AMAX	HYFIX
HAREA(2,1,L+1) = APT(1,2,2)	HYFIX
HAREA(1,2,L+1) = AMAX	HYFIX
HAREA(2,2,L+1) = APT(2,2,2)	HYFIX
IF (APT(2,2,2).GE.APT(1,2,2)) L = L + 1	HYFIX
HAREA(1,1,L+1) = APT(2,2,1)	HYFIX
HAREA(2,1,L+1) = BMAX	HYFIX
HAREA(1,2,L+1) = APT(1,2,1)	HYFIX
HAREA(2,2,L+1) = BMAX	HYFIX
IF (APT(2,2,1).GE.APT(1,2,1)) L = L + 1	HYFIX
IF (L.LE.1) GO TO 140	HYFIX
HAREA(1,1,L+1) = HAREA(1,1,1)	HYFIX
HAREA(2,1,L+1) = HAREA(2,1,1)	HYFIX
IF (BD(1).GE.-2) CALL PLREA(L,HAREA,AREA,AB,BB,E,DELT,AMR)	HYFIX
IF (BD(1).LT.-2) CALL HYREA(L,HAREA,AREA,AB,BB)	HYFIX
AREAL = AREA.GT.0.0	HYFIX
IF (.NOT.AREAL) GO TO 140	HYPER
C	HYPER
DO 120 I = 1,3	HYPER
RM(I) = AB*U(I) + BB*V(I) + T4(I)	HYPER
120 RMD(I) = RM(I)	HYPER
COMPUTE POINT ON ELLIPSOID BELOW CENTROID (CONTACT POINT?)	PLEDG
CONVERT PLANE VECTOR, ET = E*TM	PLEDG
C TRY TO USE OTHER LOGIC	HYFIX
IF(BD(1).LT.0.0)GO TO 130	HYPER
CALL MAT31(BD(7),TM,ET)	PLEDG
A2 = TM(1)*ET(1) + TM(2)*ET(2) + TM(3)*ET(3)	PLEDG
A1 = AB*(TM(1)*EU(1)+TM(2)*EU(2)+TM(3)*EU(3))	HYFIX
1+FM+ BB*(TM(1)*EV(1)+TM(2)*EV(2)+TM(3)*EV(3))	HYFIX
A1 = A1/A2	HYFIX
A0 = (AB**2*E(1,1) + 2.*AB*BB*E(1,2) + BB**2*E(2,2) - AMR)/A2	HYFIX
DISC = A1**2 - A0	PLEDG
IF(DISC.LT.0.0)DISC = 0.0	PLEDG
P = A1 + DSQRT(DISC)	PLEDG
GO TO 140	HYPER
COMPUTE FOR HYPER	HYPER
130 CALL HYVAL(CA,TH,RM,BD,1)	HYFIX
P = -CA	HYFIX
CALL DOT31(BD(8),RMD,RM)	HYPER
140 RETURN	HYPER
END	PLEDG

	SUBROUTINE PLELP(M,MM,N,NN,NT)	PLELP
C	IMPLICIT REAL*8(A-H,O-Z)	PLELP
	LOGICAL AREAL	EDGE
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)	PLELP
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),	PLELP
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)	PLELP
	COMMON/FORCES/PSF(7,70),BSF(4,20),SSF(10,40),BAGSF(3,20),	NCFORC
*	PRJNT(7,30),NPANEL(5),NPSF,NBSF,NSSF,NBGSF	PLELP
	COMMON/CNTRSF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)	EDGE
	COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24),	PLELP
*	HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12),	PLELP
*	RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12),	PLELP
*	KQ1(12),KQ2(12),KQTYPE(12)	PLELP
	COMMON/RSAGE/ XSG(3,20,3),DPMI(3,3,30),LPMI(30),	TGMOD7
*	NSG(9),MSG(20,9),MCG,MCGIN(24,5),KREF(20,9)	TGMOD7
	COMMON/TEMPVS/DMNT(3,3),TEMP(3,3),B(3,3),XMN(3),RLN(3),XMM(3),	PLELP
*	TM(3),R(3),RM(3),DMNWN(3),RLM(3),RN(3),VMN(3),VR(3),	PLELP
*	WNM(3),WCM(3),WCN(3),VREL(3),FFM(3),FR(3),TQM(3),	PLELP
*	TQN(3),TQNT(3),T(3),H(3),TH(3),XH(3),RMD(3),RND(3),	EDGE
*	TD(3),TT4(3,4),TT5(3,4),XNC(3),UH(3),P,AMR,FM,CF,	EDGE
*	VRM,VRT,VRTS,VRTST,TF,ELCROSS,MCF,NCF,DMHY(34964)	80386
	CALL ELTIME(1,21)	PLELP
	CALL DOT33(D(1,1,M),D(1,1,N),DMNT)	PLELP
	DO 10 I = 1,3	PLELP
10	XMN(I) = SEGLP(I,M) - SEGLP(I,N)	PLELP
	CALL MAT31(D(1,1,M),XMN,XMM)	PLELP
	CALL MAT31(DMNT,PL(1,NN),TM)	PLELP
	CALL MAT31(DMNT,PL(5,NN),TD)	EDGE
	BET = 0.0	EDGE
	J = 3	HYPER
	IF(BD(1,MM).LT.0.0) J = 4	HYPER
	DO 15 I=1,3	EDGE
	J = J + 1	HYPER
	XNC(I) = XMM(I) + BD(J,MM) - TD(I)	HYPER
15	BET = BET - TM(I)*XNC(I)	EDGE
C		EDGE
C	BET IS FROM CENTER OF FIGURE TO PLANE	EDGE
	IF(BD(1,MM).GT.0.0)GO TO 30	HYPER
C	PUT PLANE VECTOR INTO HYPER	HYPER
	CALL MAT31(BD(8,MM),TM,TH)	HYPER
	CALL MAT31(BD(8,MM),XNC,UH)	HYPER
	DO 20 I = 1,3	HYPER
	XNC(I) = UH(I)	HYPER
	UH(I) = DABS(TH(I))*BD(I+1,MM)/BD(I+19,MM)	HYPER
	R(I) = BD(I+19,MM)/(BD(I+19,MM) - 1.0)	HYPER
20	RND(I)= UH(I)**R(I)	HYPER
	ALP = HYPEN(BD(1,MM),R,RND)	HYPER
	DO 25 I = 1,3	HYPER
	POW = 1.0/(BD(I+19,MM) - 1.0)	HYPER
	XH(I) = -DSIGN(BD(I+1,MM)*(UH(I)*ALP)**POW,TH(I))	HYPER
25	RND(I) = XH(I)	HYPER

	BTE = TH(1)*XH(1) + TH(2)*XH(2) + TH(3)*XH(3)	HYPER
	FM = BET/BTE	HYPER
	AMR = 1.0 - DABS(FM)**(-BD(1,MM))	HYPER
	GO TO 35	HYPER
C	CODE FOR ELLIPSE	EDGE
	XH = E'T	EDGE
C		HYPER
	30 CALL MAT31(BD(16,MM),TM,XH)	EDGE
	BTS = TM(1)*XH(1) + TM(2)*XH(2) + TM(3)*XH(3)	PLELP
	BTE = - DSQRT(BTS)	EDGE
	FM = BET/BTS	EDGE
	AMR = 1.0 -BET*FM	EDGE
C		HYPER
	35 P = BET - BTE	PLELP
	PSF(1,NPSF) = P	PLELP
	MCF = NTAB(NT+1)	PLELP
	NCF = -MCF	PLELP
	IF(NCF.GT.0)CFQQ(NCF) = -999.	HYPER
	IF(P.LE.0.0) GO TO 85	EDGE
C		EDGE
C	CALL EDGE ROUTINE TO FIND IF ELLIPSOID INTERSECTS FINITE PLANE	EDGE
C	IF IT DOES; AREAL WILL BE TRUE, P WILL BE PENETRATION AT CENTROID	EDGE
C	AND RM WILL BE LOCATION OF CENTROID	EDGE
C	RM IS REFERENCED TO CENTER OF ELLIPSOID	EDGE
C	USE OLD FORMULA FOR ROLL-SLIDE?, I.E. ROLL-SLIDE SHOULDN'T	EDGE
C	CALL PLEDG	EDGE
C		EDGE
	LT = NTAB(NT)	HYPER
	IF(TAB(LT+22).LE.0.0)GO TO 40	EDGE
C		HYPER
	IF (AMR.LE.0.0) GO TO 85	HYPER
	IF (BD(1,MM).LT.0.0.AND.BD(23,MM).NE.0.0) STOP 22	EDGE
	CALL PLEDG(AREAL,BD(1,MM),PL(1,NN))	HYPER
	IF(.NOT.AREAL)GO TO 85	EDGE
	PSF(1,NPSF) = P	EDGE
C		HYPER
	40 IF (TAB(LT+22).GT.-2.0.AND.AMR.LE.0.0) GO TO 85	HYPER
	RHO = 0.0	PLELP
	IF(MCF.GT.0)RHO = TAB(MCF+4)	HYPER
	BETE = 1.0 + RHO*P/BTE	HYPER
	IF(BD(1,MM).GT.0.0)BETE = BETE/BTE	HYPER
	IF(BD(1,MM).LT.0.0)CALL DOT31(BD(8,MM),RND,XH)	EDGE
	TRT = P*(1.0 - RHO)	HYPER
	J = 3	HYPER
	IF(BD(1,MM).LT.0.0)J = 4	HYPER
	DO 45 I = 1,3	HYPER
	J = J + 1	EDGE
	IF(TAB(LT+22).LE.0.0)RM(I) = BETE*XH(I)	EDGE
	IF(TAB(LT+22).GT.0.0)RM(I) = RM(I) - TRT*TM(I)	HYPER
	RLM(I) = RM(I) + BD(J,MM)	HYPER
	45 RN(I) = RLM(I) + XMM(I)	PLELP
	CALL DOT31(DMNT,RN,RLN)	HYPER
	IF (TAB(LT+22).GT.0.0) GO TO 55	

	IF (TAB(LT+22).GT.-3.0.AND.TAB(LT+22).LT.0.0) GO TO 55	HYPER
C		EDGE
C	CHECK BOUNDARY USING OLD METHOD	EDGE
	DO 50 I = 8,13,5	HYPER
	IF(PL(I+4,NN).LE.0.0)GO TO 50	HYPER
	DIST = RLN(1)*PL(I,NN)	PLELP
	* + RLN(2)*PL(I+1,NN)	PLELP
	* + RLN(3)*PL(I+2,NN) - PL(I+3,NN)	PLELP
	IF((DIST.LE.0.0).OR.(DIST.GT.PL(I+4,NN))) GO TO 85	HYPER
50	CONTINUE	HYPER
C		EDGE
55	CALL PLSEGF(M,N,NT)	HYPER
C	DMNWN,VMN,VR,WNM,WCM,WCN,VREL,FFM,FR,TQM,TQN,TQNT,T	EDGE
C	FM,CF,VRM,VRT,VRTS,VRTEST,TF,ELOSS	EDGE
C		EDGE
C	STORE RESULTS	EDGE
	DO 60 I = 1,3	HYPER
60	PSF(I+4,NPSF) = RLN(I)	HYPER
	IF(LPMI(N).NE.0) CALL DOT31(DPMI(1,1,N),RLN,PSF(5,NPSF))	EDGE
	IF(MCF.LT.0)GO TO 65	HYPER
	PSF(2,NPSF) = FM	PLELP
	PSF(3,NPSF) = 0.0	PLELP
	TRT = TF**2 - FM**2	PLELP
	IF(TRT.GT.0.0) PSF(3,NPSF) = DSQRT(TRT)	PLELP
	PSF(4,NPSF) = TF	PLELP
	GO TO 85	HYPER
C		PLELP
C	ROLL-SLIDE	PLELP
	REVISED	8/18/85
65	DO 70 I = 1,3	HYPER
70	PSF(I+1,NPSF) = T(I)	HYPER
	IF(BD(1,MM).LT.0.0) STOP 28	HYPER
	CALL CROSS(TM,WNM,TH)	EDGE
	CALL MAT31(BD(16,MM),TH,UH)	EDGE
	TRT = (TM(1)*UH(1) + TM(2)*UH(2) + TM(3)*UH(3))/BTS	EDGE
	DO 75 I = 1,3	HYPER
75	RMD(I) = DABS(BETE)*(UH(I) - TRT*XH(I))	HYPER
	CALL CROSS(DMNWN,TM,TH)	EDGE
	CALL CROSS(WNM,RMD,XNC)	EDGE
	SQQ(NCF) = 0.0	PLELP
	DO 80 I = 1,3	HYPER
80	SQQ(NCF) = SQQ(NCF) + TM(I)*XNC(I) - 2.0*TH(I)*VR(I)	HYPER
	CALL DOT31(D(1,1,M),XNC,RQQ(1,NCF))	EDGE
85	CALL ELTIME(2,21)	HYPER
	RETURN	PLELP
	END	PLELP

	SUBROUTINE PLREA(L,H,AREA,AB,BB,E,D,R)	HYFIX
C		REV IV 12/11/87HYFIX
	IMPLICIT REAL*8(A-H,O-Z)	PLREA
	COMPUTES AREA AND CENTROID (TRUE AREA = AREA* UxV /6)	HYFIX
	C  UxV  IS NEVER COMPUTED  UxV  = UxV.T = AREA OF PARALLELOGRAM	PLREA
	C THIS ROUTINE WILL ONLY BE CALLED IF THERE IS AN INTERSECTION	PLREA
	DIMENSION H(2,2,5),E(2,2)	HYFIX
	AREA = 0.0	PLREA
	AB = 0.0	PLREA
	BB = 0.0	PLREA
	IF (L.LE.1) GO TO 15	HYFIX
	C = R/DSQRT(D)	HYFIX
	C12 = 2.0*R/D	HYFIX
	C11 = C12*E(1,1)	HYFIX
	C22 = C12*E(2,2)	HYFIX
	C12 = C12*E(1,2)	HYFIX
	DO 10 I = 1,L	HYFIX
	COMPUTE FOR STRAIGHT LINE SEGMENTS	HYFIX
	AR = H(1,1,I)*H(2,2,I) - H(1,2,I)*H(2,1,I)	HYFIX
	IF (AR.EQ.0.0) GO TO 5	HYFIX
	AB = AB + AR*(H(1,1,I) + H(1,2,I))	HYFIX
	BB = BB + AR*(H(2,1,I) + H(2,2,I))	HYFIX
	AREA = AREA + AR	HYFIX
	COMPUTE FOR ELLIPSE	HYFIX
	5 AR = H(1,2,I)*H(2,1,I+1) - H(1,1,I+1)*H(2,2,I)	HYFIX
	IF (AR.EQ.0.0) GO TO 10	HYFIX
	ARC = AR/C	HYFIX
	IF (DABS(ARC).GT.1.0) ARC = DSIGN(1.0D0,ARC)	HYFIX
	AR = C*DASIN(ARC)	HYFIX
	X21 = H(1,1,I+1) - H(1,2,I)	HYFIX
	Y21 = H(2,1,I+1) - H(2,2,I)	HYFIX
	AB = AB + C12*X21 + C22*Y21	HYFIX
	BB = BB - C11*X21 - C12*Y21	HYFIX
	AREA = AREA + AR	HYFIX
	10 CONTINUE	HYFIX
	IF (AREA.LE.0.0) GO TO 15	HYFIX
	AREA = 3.0*AREA	HYFIX
	AB = AB/AREA	PLREA
	BB = BB/AREA	PLREA
C	AREA = AREA/6.0	HYFIX
	15 RETURN	PLREA
	END	PLREA



DO 18 I=1,3	PLSEGF
L = L+1	PLSEGF
FFM(I) = FM*TM(I) + FF*VREL(I) + FS*TAB(L)	PLSEGF
TF = TF + FFM(I)**2	PLSEGF
TTI(I) = T(I)	PLSEGF
R1I(I) = RLM(I)	PLSEGF
18 R2I(I) = RLN(I)	PLSEGF
TF = DSQRT(TF)	PLSEGF
MT = NTAB(NT+5)	PLSEGF
CREST = TAB(MT+3)	PLSEGF
CALL DOT31 (D(1,1,M),FFM,FR)	PLSEGF
IF (MCF.LE.0) GO TO 21	PLSEGF
CALL CROSS (RLM,FFM,TQM)	PLSEGF
CALL CROSS (RN,FFM,TQNT)	PLSEGF
CALL DOT31 (DMNT,TQNT,TQN)	PLSEGF
DO 19 I=1,3	PLSEGF
U1(I,M) = U1(I,M) + FR(I)	PLSEGF
U1(I,N) = U1(I,N) - FR(I)	PLSEGF
U2(I,M) = U2(I,M) + TQM(I)	PLSEGF
19 U2(I,N) = U2(I,N) - TQN(I)	PLSEGF
IF (NCF.LE.0) GO TO 23	PLSEGF
21 DO 22 I=1,3	PLSEGF
HQQ(I,NCF) = FR(I)/TF	PLSEGF
TQQ(I,NCF) = T(I)	PLSEGF
RK1(I,NCF) = RLM(I)	PLSEGF
22 RK2(I,NCF) = RLN(I)	PLSEGF
CFQQ(NCF) = CF	PLSEGF
MT = NTAB(NT+5)	PLSEGF
IF (KQTYPE(NCF).EQ.3) CFQQ(NCF) = TAB(MT+4)	PLSEGF
23 RETURN	PLSEGF
END	PLSEGF



	SUBROUTINE PLTXYZ(P,C)	PLTXYZ
C		REV III.5 05/30/85VEHICL
C	STORES PLOT CHARACTER (C) INTO PLOTYZ, PLOTXZ AND PLOTXY ARRAYS	PLTXYZ
C	IN VEHICLE REFERENCE FOR POINT (P) GIVEN IN INERTIAL REFERENCE.	PLTXYZ
C		PLTXYZ
	IMPLICIT REAL*8 (A-H,O-Z)	PLTXYZ
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,	PLTXYZ
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),	PLTXYZ
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)	PLTXYZ
	COMMON/VPOSTN/ ZPLT(3),SPLT(3),AXV(3,6),VATAB(6,501,6),	VEHICL
*	VT0(6),VDT(6),TIMEV(6),OMEGV(6),NVTAB(6),INDXV(6)	PLTXYZ
	COMMON/TEMPVS/ DUM(101),PLOTYZ(96,55),PLOTXZ(96,55),PLOTXY(96,55)	PLTXYZ
*	,DMY(33032)	80386
	LOGICAL*1 C,PLOTYZ,PLOTXZ,PLOTXY	PLTXYZ
	DIMENSION P(3),TMP(3),XYZ(3)	PLTXYZ
	DATA NPLTZ/96/ , NPLTX/55/	PLTXYZ
C		PLTXYZ
C	CONVERT P FROM INERTIAL TO VEHICLE REFERENCE BY	PLTXYZ
C	XYZ = DVEH(P-XCOMP)	PLTXYZ
C		PLTXYZ
	DO 10 I=1,3	PLTXYZ
10	TMP(I) = P(I) - SEGLP(I,NVEH)	PLTXYZ
	CALL MAT31(D(1,1,NVEH),TMP,XYZ)	PLTXYZ
C		PLTXYZ
C	CONVERT XYZ INTO PLOT CORDINATES IX,IY,IZ AND	PLTXYZ
C	IF WITHIN PLOT LIMITS, STORE C IN PLOTYZ, PLOTXZ AND PLOTXY.	PLTXYZ
C		PLTXYZ
	IX = SPLT(1)*XYZ(1) + ZPLT(1) + 0.5	PLTXYZ
	IZ = SPLT(3)*XYZ(3) + ZPLT(3) + 0.5	PLTXYZ
	IF (IZ.LT.1 .OR. IZ.GT.NPLTZ) GO TO 11	PLTXYZ
	IY = SPLT(2)*XYZ(2) + ZPLT(2) + 0.5	PLTXYZ
	IF (IY.GE.1 .AND. IY.LE.NPLTX) PLOTYZ(IZ,IY) = C	PLTXYZ
	IF (IX.GE.1 .AND. IX.LE.NPLTX) PLOTXZ(IZ,IX) = C	PLTXYZ
11	IY = -SPLT(3)*XYZ(2) + ZPLT(2) + 0.5	PLTXYZ
	IF (IY.LT.1 .OR. IY.GT.NPLTZ) GO TO 99	PLTXYZ
	IF (IX.GE.1 .AND. IX.LE.NPLTX) PLOTXY(IY,IX) = C	PLTXYZ
99	RETURN	PLTXYZ
	END	PLTXYZ

	SUBROUTINE POSTPR(PRDT)	REV IV	02/01/88	POSTPR
C	CONTROLS GENERATION OF PRINTED TABULAR TIME HISTORIES			POSTPR
C	AND PLOTS BY THE VALUE OF NPRT(4) AS FOLLOWS:			POSTPR
C				POSTPR
C	VALUE OF	TIME		POSTPR
C	NPRT(4)	HISTORIES	PLOTS	POSTPR
C				POSTPR
C	+4	**	NO	POSTPR
C	+3	YES	YES	POSTPR
C	+2	YES	NO	POSTPR
C	+1	**	YES	POSTPR
C	0	**	NO	POSTPR
C	-1	NO	YES	POSTPR
C	-2	YES	NO	POSTPR
C	-3	YES	YES	POSTPR
C				POSTPR
C	** TIME HISTORIES WERE PRINTED BY SUBROUTINE OUTPUT.			POSTPR
C	COMMON/CDINT/ JDTPTS(18),ZZ(1000,3),DMY(8068)			80386
C	NOTE: THIS OVERWRITES COMMON /CDINT/.			POSTPR
C	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,			POSTPR
C	* NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG			PAGE
C	REAL*8 TIME			POSTPR
C	COMMON/FORCES/PSF(7,70),BSF(4,20),SSF(10,40),BAGSF(3,20),			NCFORC
C	* PRJNT(7,30),NPANEL(5),NPSF,NBSF,NSSF,NBGSF			POSTPR
C	REAL*8 PSF,BSF,SSF,BAGSF,PRJNT			POSTPR
C	COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),			POSTPR
C	* BLTTTL(5,8),PLTTTL(5,30),BAGTTL(5,6),SEG(30),			POSTPR
C	* JOINT(30),CGS(30),JS(30)			POSTPR
C	REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTTL,BAGTTL,SEG,JOINT			POSTPR
C	LOGICAL*1 CGS,JS			POSTPR
C	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),			POSTPR
C	* UNITL,UNITM,UNITT,GRAVITY(3),TWOPI			TWOPI
C	REAL*8 PI,RADIAN,G,THIRD,EPS,UNITL,UNITM,UNITT,GRAVITY,TWOPI			80386
C	COMMON/JBARTZ/ MNPL( 30),MNBLT( 8),MNSEG( 30),MNBAG( 6),			POSTPR
C	* MPL(3,5,30),MBLT(3,5,8),MSEG(3,5,30),MBAG(3,10,6),			POSTPR
C	* NTPL( 5,30),NTBLT( 5,8),NTSEG( 5,30)			POSTPR
C	COMMON / / APSDM(3,20),APSDN(3,20),ASD(5,20),MSDM(20),MSDN(20)			POSTPR
C	REAL*8 .. 1,APSDN,ASD			POSTPR
C	COMMON/HRNESS/ BAR(15,100),BB(100),BBDOT(100),PLOSS(2,100),			POSTPR
C	* XLONG(20),HTIME(2),IBAR(5,100),NL(2,100),			POSTPR
C	* NPTSPB(20),NPTPLY(20),NTHRNS(20),NBLTPH(5)			POSTPR
C	REAL*8 BAR,BB,BBDOT,PLOSS,XLONG,HTIME			POSTPR
C	COMMON/RSAVE/ XSG(3,20,3),DPMI(3,3,30),LPMI(30),			ATBIII
C	* NSG(9),MSG(20,9),MCG,MCGIN(24,5),KREF(20,9)			TTHKREF
C	REAL*8 XSG,DPMI,TDATA,UMSEC,PRDT,TEST1,TEST2,VDT1			TGMOD1
C	REAL*8 VDT2,R30,R26			TGMOD1
C	NOTE: SUBROUTINES POSTPR & HEDING SHARE THIS COMMON/TEMPVS/.			POSTPR
C	THE FIRST DIMENSION OF XLAB,YLAB,PLB1 AND PLB2 SHOULD BE THE SAME			POSTPR
C	AS THE VALUE ASSIGNED TO NW60 WHICH IS THE NUMBER OF WORDS THAT			POSTPR
C	IS NECESSARY TO CONTAIN 60 CONSECUTIVE CHARACTERS DEPENDING ON THE			POSTPR

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C      COMPUTER SYSTEM THIS PROGRAM IS OPERATING ON. THE VALUE OF NW60      POSTPR
C      SHOULD BE 15 ON IBM 360 AND 370, 10 ON UNIVAC 1108, 6 ON CDC 6600. POSTPR
C      THE LAST TERM IN FORMAT 13 BELOW SHOULD BE 15A4(IBM), 10A6(UNIVAC) POSTPR
C      OR 6A10(CDC). ALSO, THE FIRST DIMENSION OF PLDATA IN SUBROUTINE      POSTPR
C      HEDING SHOULD BE 97(IBM), 77(UNIVAC) OR 61(CDC).                      REDIM2
C                                                                              POSTPR
      COMMON/TEMPVS/ TDATA(14,65),HEDATA(470),                          POSTPR
*          XO(20),XN(20),XL(20),XS(20),XLAB(15,20),PLB1(15,20), POSTPR
*          YO(20),YN(20),YL(20),YS(20),YLAB(15,20),PLB2(15,20), POSTPR
*          NYP(20),MX(2,20),MY(2,10,20),NX(20),NY(20),          POSTPR
*          NXLAB(20),NYLAB(20),NPLB1(20),NPLB2(20),          POSTPR
*          USEC(45),Z(1000,25),ZTTH(14,45,65),IDMMY          80386
      CHARACTER*4 XLAB,YLAB,PLB1,PLB2          80386
      COMMON/DEVICE/ IDEF,IOPORT,MODEL          80386
      LOGICAL LTABH,LPLOT          POSTPR
      DATA LPP/45/, NZD1/1000/, NZD2/25/          PLTINC
      DATA NW60/15/          POSTPR
      LTABH = .FALSE.          POSTPR
      LPLOT = .FALSE.          POSTPR
      NPRT4 = IABS(NPRT(4))          POSTPR
      LPLOT = NPRT4.EQ.1 .OR. NPRT4.EQ.3          POSTPR
      LTABH = NPRT4.EQ.2 .OR. NPRT4.EQ.3          POSTPR
      IF(NPRT(26).EQ.4) LTABH = .FALSE.          TGMOD1
      IF(NPRT(26).GE.5) GO TO 99          TGMOD1
C                                                                              POSTPR
C      READ INPUT CARD H.11 TO CONTROL COMPUTATION OF HIC, HSI & CSI.      WINDOP
C                                                                              POSTPR
      READ (5,11) JDTPTS          POSTPR
      WRITE(6,700) NPG          PAGE
      NPG=NPG+1          PAGE
700 FORMAT(1H1,122X,'PAGE',15/,2X,          PAGE
*      'POSTPROCESSOR CONTROL PARAMETERS',/)          PAGE
      WRITE(6,701)          CHGIII
701 FORMAT(13X,'HIC & HSI POINT',7X,'CSI POINT')          CHGIII
      WRITE(6,702) JDTPTS(1),JDTPTS(2)          CHGIII
702 FORMAT(5X,'H.11',10X,I2,17X,I2,/)          WINDOP
      NDPT = 0          POSTPR
      IHIC = 0          TGMOD1
      I26 = 0          TGMOD1
      ITST1 = 0          TGMOD1
      ITST2 = 0          TGMOD1
      IF(NPRT(26).LT.0) I26 = IABS(NPRT(26))          TGMOD1
      IF(JDTPTS(1).GT.0.OR.JDTPTS(2).GT.0) IHIC = 1          TGMOD1
      IF(NPRT(30).EQ.0.AND.NPRT(26).EQ.3) ITST1 = 1          TGMOD1
      IF(NPRT(30).LT.I26) ITST2 = 1          TGMOD1
      IF(IHIC.EQ.1.AND.ITST1.EQ.1) WRITE(6,751)          TGMOD1
      IF(IHIC.EQ.1.AND.ITST2.EQ.1) WRITE(6,752) NPRT(30),I26          TGMOD1
751 FORMAT(3X,'WARNING! LOGIC OF INPUT INDICATES USER ANTICIPATES HICTGMOD1
*, HSI AND CSI TO BE COMPUTED BASED ON DATA FOR EVERY SUCCESSFUL', TGMOD1
*/,10X,'INTEGRATION STEP. YET DATA WAS STORED (WRITTEN TO TAPE8) EVTGMOD1
*ERY DT. ')          TGMOD1
752 FORMAT(3X,'WARNING! LOGIC OF INPUT INDICATES USER ANTICIPATES HICTGMOD1

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*, HSI AND CSI TO BE COMPUTED BASED ON DATA FOR EVERY ',I2,/,10X,' TGMOD1
*INTEGER MULTIPLE OF DT, YET DATA WAS STORED (WRITTEN TO TAPE8) EVETGMOD1
*RY ',I2,' INTEGER MULTIPLE OF DT.') TGMOD1
IF(JDTPTS(1).GT.0.AND.NPRT(26).EQ.2.AND.NPRT(30).LT.1) STOP 91 TGMOD1
IF(JDTPTS(2).GT.0.AND.NPRT(26).EQ.2.AND.NPRT(30).LT.1) STOP 92 TGMOD1
IF (JDTPTS(1).NE.0) NDPT = NDPT + 1 POSTPR
IF (JDTPTS(2).NE.0) NDPT = NDPT + 1 POSTPR
IF (.NOT.LPLOT .AND. .NOT.LTABH .AND. NDPT.EQ.0) GO TO 99 POSTPR
CALL ELTIME (1,36) POSTPR
IF (.NOT.LPLOT) GO TO 20 POSTPR
C POSTPR
C READ INDICES OF VARIABLES TO BE PLOTTED AND POSTPR
C ARGUMENTS TO SUBROUTINE SLPLOT ON CARDS I. POSTPR
C POSTPR
C INPUT CARD I.1 POSTPR
C POSTPR
READ (5,11) NPLT , (NYP(K),K=1,NPLT) POSTPR
11 FORMAT (18I4) POSTPR
IF(NPLT.GT.0.AND.ITST1.EQ.1) WRITE(6,753) TGMOD1
IF(NPLT.GT.0.AND.ITST2.EQ.1) WRITE(6,754) NPRT(30),I26 TGMOD1
753 FORMAT(3X,'WARNING! LOGIC OF INPUT INDICATES USER ANTICIPATES PLOTGMOD1
*TS TO BE COMPUTED BASED ON DATA FOR EVERY SUCCESSFUL INTEGRATION STGMOD1
*TEP',/,10X,'YET DATA WAS STORED (WRITTEN TO TAPE8) EVERY DT.') TGMOD1
754 FORMAT(3X,'WARNING! LOGIC OF INPUT INDICATES USER ANTICIPATES PLOTGMOD1
*TS TO BE COMPUTED BASED ON DATA FOR EVERY ',I2,/,10X,'INTEGER MULTITGMOD1
*PLE OF DT, YET DATA WAS STORED (WRITTEN TO TAPE8) EVERY ',I2, TGMOD1
* ' INTEGER MULTIPLE OF DT.') TGMOD1
IF (NPLT.LE.0) LPLOT = .FALSE. POSTPR
IF (.NOT.LPLOT) GO TO 20 POSTPR
DO 15 K=1,NPLT POSTPR
NYPLT = NYP(K) POSTPR
C POSTPR
C INPUT CARD I.2.K POSTPR
C POSTPR
READ (5,11) MX(1,K), MX(2,K), (MY(1,J,K), MY(2,J,K), J=1,NYPLT) POSTPR
C POSTPR
C INPUT CARD I.3.K POSTPR
C POSTPR
READ (5,12) NX(K), X0(K), XN(K), XL(K), XS(K) POSTPR
12 FORMAT (I4 , 4X , 4F8.0 ) POSTPR
C POSTPR
C INPUT CARD I.4.K POSTPR
C POSTPR
READ (5,12) NY(K), Y0(K), YN(K), YL(K), YS(K) POSTPR
C POSTPR
C INPUT CARD I.5.K POSTPR
C POSTPR
READ (5,13) NXLAB(K), (XLAB(I,K),I=1,NW60) POSTPR
13 FORMAT (I4 , 4X , 15A4) POSTPR
C POSTPR
C NOTE - ABOVE FORMAT ASSUMES 4 ALPHANUMERIC CHARACTERS FOR SINGLE POSTPR
C PRECISION WORDS ON IBM 360 AND 370 COMPUTERS THE 15A4 TERM IN THEPOSTPR

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C	FORMAT WILL HAVE TO BE CHANGED ON NON-IBM COMPUTERS TO PRODUCE A	POSTPR
C	CONTINUOUS STRING OF 60 CHARACTERS IN CORE MEMORY.	POSTPR
C		POSTPR
C	INPUT CARD I.6.K	POSTPR
C		POSTPR
	READ (5,13) NYLAB(K), (YLAB(I,K), I=1, NW60)	POSTPR
C		POSTPR
C	INPUT CARD I.7.K	POSTPR
C		POSTPR
	READ (5,13) NPLB1(K), (PLB1(I,K), I=1, NW60)	POSTPR
C		POSTPR
C	INPUT CARD I.8.K	POSTPR
C		POSTPR
15	READ (5,13) NPLB2(K), (PLB2(I,K), I=1, NW60)	POSTPR
C		CHGIII
C	WRITE OUT PLOTTING CONTROL DATA	CHGIII
C		CHGIII
	WRITE(6,703)	CHGIII
703	FORMAT(4X, 'PLOTTING CONTROLS', /)	CHGIII
	WRITE(6,704)	CHGIII
704	FORMAT(12X, 'NO. PLOTS', 11X, 'NO. OF Y VARIABLES PER PLOT')	CHGIII
	WRITE(6,705) NPLT, (NYP(JK), JK=1, NPLT)	CHGIII
705	FORMAT(5X, 'I.1', 7X, I2, 7X, 20(I2, 2X))	CHGIII
	WRITE(6,706)	CHGIII
706	FORMAT(12X, 'MX1 MX2 MY1A MY2A MY1B MY2B MY1C MY2C MY1D MY2D MY1E MCHGIII	
	*Y2E MY1F MY2F MY1G MY2G MY1H MY2H MY1I MY2I MY1J MY2J')	CHGIII
	DO 730 IJ=1, NPLT	CHGIII
	WRITE(6,707) IJ, MX(1, IJ), MX(2, IJ).	CHGIII
	* (MY(1, L, IJ), MY(2, L, IJ), L=1, NYP(IJ))	CHGIII
707	FORMAT(5X, 'I.2.', I2, 2X, I2, 2X, I2, 2X, 20(I2, 3X))	CHGIII
730	CONTINUE	CHGIII
	WRITE(6,708)	CHGIII
708	FORMAT(14X, 'NX', 8X, 'X0', 9X, 'XN', 8X, 'XL', 9X, 'XS')	CHGIII
	DO 731 IJ=1, NPLT	CHGIII
	WRITE(6,709) IJ, NX(IJ), X0(IJ), XN(IJ), XL(IJ), XS(IJ)	CHGIII
709	FORMAT(5X, 'I.3.', I2, 2X, I3, 4X, 4(F8.3, 2X))	CHGIII
731	CONTINUE	CHGIII
	WRITE(6,710)	CHGIII
710	FORMAT(14X, 'NY', 8X, 'Y0', 9X, 'YN', 8X, 'YL', 9X, 'YS')	CHGIII
	DO 732 IJ=1, NPLT	CHGIII
	WRITE(6,711) IJ, NY(IJ), Y0(IJ), YN(IJ), YL(IJ), YS(IJ)	CHGIII
711	FORMAT(5X, 'I.4.', I2, 2X, I3, 4X, 4(F8.3, 2X))	CHGIII
732	CONTINUE	CHGIII
	WRITE(6,712)	CHGIII
712	FORMAT(12X, 'NXLAB', 15X, 'XLAB')	CHGIII
	DO 733 IJ=1, NPLT	CHGIII
	WRITE(6,713) IJ, NXLAB(IJ), (XLAB(L, IJ), L=1, NW60)	CHGIII
713	FORMAT(5X, 'I.5.', I2, 2X, I3, 5X, 15A4)	CHGIII
733	CONTINUE	CHGIII
	WRITE(6,714)	CHGIII
714	FORMAT(12X, 'NYLAB', 15X, 'YLAB')	CHGIII
	DO 734 IJ=1, NPLT	CHGIII

WRITE(6,715) IJ,NYLAB(IJ),(YLAB(L,IJ),L=1,NW60)	CHGIII
715 FORMAT(5X,'I.6.',I2,2X,I3,5X,15A4)	CHGIII
734 CONTINUE	CHGIII
WRITE(6,716)	CHGIII
716 FORMAT(12X,'NPLB1',15X,'PLB1')	CHGIII
DO 735 IJ=1,NPLT	CHGIII
WRITE(6,717) IJ,NPLB1(IJ),(PLB1(L,IJ),L=1,NW60)	CHGIII
717 FORMAT(5X,'I.7.',I2,2X,I3,5X,15A4)	CHGIII
735 CONTINUE	CHGIII
WRITE(6,718)	CHGIII
718 FORMAT(12X,'NPLB2',15X,'PLB2')	CHGIII
DO 736 IJ=1,NPLT	CHGIII
WRITE(6,719) IJ,NPLB2(IJ),(PLB2(L,IJ),L=1,NW60)	CHGIII
719 FORMAT(5X,'I.8.',I2,2X,I3,5X,15A4)	CHGIII
736 CONTINUE	CHGIII
C	POSTPR
C READ TIME HISTORY DATA FROM TAPE 8.	POSTPR
C	POSTPR
20 NPTS = 0	POSTPR
LINES = 0	POSTPR
IF (NPRT(4).GT.0) REWIND 8	POSTPR
READ (8,END=29) NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,NPANEL,	POSTPR
* MNPL,MNBLT,MNSEG,MNBAG,MPL,MBLT,MSEG,MBAG	POSTPR
READ (8,END=29) DATE,COMENT,VPSTTL,BDYTTTL,BLTTL,PLTTL,BAGTTL,	POSTPR
* SEG,JOINT,UNITL,UNITM,UNITT,NSG,MSG,XSG,MCG,	ATBIII
* MCGIN,KREF,NHRNSS,NBLTPH,NPTSPB,NSD,MSDM,MSDN	CHGIII
21 READ (8,END=29) NT, UMSEC, ((TDATA(I,J),I=1,14),J=1,NT)	POSTPR
R30 = 1.0D0	TGMOD1
IF(NPRT(30).GT.0) R30 = NPRT(30)	TGMOD1
VDT1 = R30*PRDT	TGMOD1
TEST1 = DMOD(UMSEC,VDT1)	TGMOD1
TEST1 = DMIN1(TEST1,DABS(VDT1 - TEST1))	TGMOD1
IF(NPRT(30).GT.0.AND.TEST1.GT.EPS(4)) GO TO 25	TGMOD1
NPTS = NPTS + 1	POSTPR
IF (NPTS.GT.NZD1 .AND. (NDPT.NE.0 .OR. LPLOT) ) STOP 52	ATBIII
ZZ(NPTS,1) = UMSEC	PLTINC
Z(NPTS,1) = UMSEC	PLTINC
IF (NDPT.EQ.0) GO TO 22	POSTPR
C	POSTPR
C STORE DATA FOR HIC, HSI AND CSI.	POSTPR
C	POSTPR
JJ = 1	POSTPR
DO 61 I=1,2	POSTPR
IF (JDTPTS(I).EQ.0) GO TO 61	POSTPR
JJ = JJ + 1	POSTPR
JD = JDTPTS(I) - 1	POSTPR
JE = 4*MOD(JD,3) + 4	POSTPR
JP = JD/3 + 1	POSTPR
ZZ(NPTS,JJ) = TDATA(JE,JP)	PLTINC
61 CONTINUE	POSTPR
22 IF (.NOT.LPLOT) GO TO 25	POSTPR
C	POSTPR

C	STORE DATA FOR PLOTTING	POSTPR
C		POSTPR
	JY = 1	PLTINC
	DO 24 K=1,NPLT	POSTPR
	JE = IABS(MX(2,K))	POSTPR
	IF (JE.EQ.0) GO TO 23	POSTPR
	JY = JY + 1	POSTPR
	IF (JY.GT.NZD2) STOP 53	ATBIII
	JP = MX(1,K) - 20	POSTPR
	Z(NPTS,JY) = TDATA(JE,JP)	POSTPR
23	NYPLT = NYP(K)	POSTPR
	DO 24 J=1,NYPLT	POSTPR
	JY = JY + 1	POSTPR
	JP = MY(1,J,K) - 20	POSTPR
	IF (JY.GT.NZD2) STOP 54	ATBIII
	JE = IABS(MY(2,J,K))	POSTPR
	Z(NPTS,JY) = UMSEC	POSTPR
24	IF (JE.NE.0) Z(NPTS,JY) = TDATA(JE,JP)	POSTPR
25	IF (.NOT.LTABH) GO TO 21	POSTPR
C		POSTPR
C	STORE DATA TO PRINT TABULAR TIME HISTORIES	POSTPR
C		POSTPR
	R26 = 1.0D0	TGMOD1
	IF(NPRT(26).LT.0) IFLG = 1	TGMOD1
	IF(IFLG.EQ.1) N26 = IABS(NPRT(26))	TGMOD1
	IF(IFLG.EQ.1) R26 = N26	TGMOD1
	VDT2 = R26*PRDT	TGMOD1
	TEST2 = DMOD(UMSEC,VDT2)	TGMOD1
	TEST2 = DMIN1(TEST2,DABS(VDT2 - TEST2))	TGMOD1
	IF (NPRT(26).LE.0 .AND. TEST2.GT.EPS(4)) GO TO 21	TGMOD1
	LINES = LINES + 1	POSTPR
	NTTH = MOD(LINES-1,LPP) + 1	POSTPR
	USEC(NTTH) = UMSEC	POSTPR
	DO 26 J=1,NT	POSTPR
	DO 26 I=1,14	POSTPR
26	ZTTH(I,NTTH,J) = TDATA(I,J)	POSTPR
	IF (NTTH.EQ.LPP) CALL HEDING (LINES,LPP)	POSTPR
	GO TO 21	POSTPR
29	IF (.NOT.LTABH .OR. LINES.EQ.0) GO TO 30	POSTPR
	IF (NTTH.NE.LPP) CALL HEDING (LINES,LPP)	POSTPR
30	IF (NDPT.NE.0) CALL HICCSI(NPTS)	POSTPR
	IF (.NOT.LPLOT) GO TO 98	POSTPR
C		POSTPR
C	PLOT DATA VIA SUBROUTINE SLPLOT.	POSTPR
C		POSTPR
C	INCLUDE ANY PROGRAM STATEMENTS HERE REQUIRED BY YOUR COMPUTER AND	POSTPR
C	PLOTTING SYSTEMS FOR PLOT INITIALIZATION (E.G., CALL PLOTS).	POSTPR
C		POSTPR
	CALL PLOTS (IDEF,IOPORT,MODEL)	80386
	JZ = 1	PLTINC
	DO 50 K=1,NPLT	POSTPR
	JX = 1	POSTPR

IF (MX(2,K).EQ.0) GO TO 42	POSTPR
JZ = JZ + 1	POSTPR
JX = JZ	POSTPR
IF (Z(1,JX).EQ.0.0 .OR. MX(2,K).GE.0) GO TO 42	POSTPR
DO 41 I=2,NPTS	POSTPR
41 Z(I,JX) = Z(I,JX) - Z(1,JX)	POSTPR
Z(1,JX) = 0.0	POSTPR
42 NYPLT = NYP(K)	POSTPR
DO 44 J=1,NYPLT	POSTPR
JY = JZ + J	POSTPR
IF (Z(1,JY).EQ.0.0 .OR. MY(2,J,K).GE.0) GO TO 44	POSTPR
DO 43 I=2,NPTS	POSTPR
43 Z(I,JY) = Z(I,JY) - Z(1,JY)	POSTPR
Z(1,JY) = 0.0	POSTPR
44 CONTINUE	POSTPR
NXK = NX(K)	POSTPR
NYK = NY(K)	POSTPR
XOK = XO(K)	POSTPR
YOK = YO(K)	POSTPR
XNK = XN(K)	POSTPR
YNK = YN(K)	POSTPR
XLK = XL(K)	POSTPR
YLK = YL(K)	POSTPR
XSK = XS(K)	POSTPR
YSK = YS(K)	POSTPR
NXLABK = NXLAB(K)	POSTPR
NYLABK = NYLAB(K)	POSTPR
NPLB1K = NPLB1(K)	POSTPR
NPLB2K = NPLB2(K)	POSTPR
CALL SLPLOT(Z(1,JX ), NXK, XOK, XNK, XLK, XSK, XLAB(1,K), NXLABK,	POSTPR
* Z(1,JZ+1), NYK, YOK, YNK, YLK, YSK, YLAB(1,K), NYLABK,	POSTPR
* NPTS,NYPLT,NZD1,PLB1(1,K),NPLB1K,PLB2(1,K),NPLB2K)	POSTPR
C	POSTPR
C INSERT ANY CODE REQUIRED BY YOUR SYSTEM TO ADVANCE PLOT PAGES HERE	POSTPR
C	POSTPR
IF(NPRT(31).EQ.1) GO TO 444	CHGIII
X00 = -0.5*(XSK-(XLK-0.5)) + XLK + 3.0	FXPLOT
Y00 = -0.5*(YSK-(YLK-1.0))	FXPLOT
CALL PLOT (X00,Y00,-3)	FXPLOT
50 JZ = JZ + NYPLT	POSTPR
444 CONTINUE	CHGIII
C	POSTPR
C INSERT ANY PLOT TERMINATION CODE REQUIRED BY YOUR SYSTEM HERE.	POSTPR
C	POSTPR
CALL PLOT(12.0,0.0,999)	PECONV
98 CALL ELTIME (2,36)	POSTPR
99 RETURN	POSTPR
END	POSTPR





IF (LPMI(I).EQ.0) GO TO 19	PRINT
CALL DOT33 (DPMI(1,1,I),D(1,1,I),T3)	PRINT
CALL DOT31(DPMI(1,1,I),WMEG(1,I),T1)	FIXPRT
CALL DOT31(DPMI(1,1,I),WMEGD(1,I),T2)	FIXPRT
CALL YPRDEG (T3,YPR)	PRINT
WRITE (6,31) I,SEG(I),YPR,(T1(K),K=1,3),(T2(K),K=1,3)	FIXPRT
GO TO 20	PRINT
19 CALL YPRDEG (D(1,1,I),YPR)	PRINT
WRITE (6,31) I,SEG(I),YPR,(WMEG(K,I),K=1,3),(WMEGD(K,I),K=1,3)	FIXPRT
20 CONTINUE	FIXPRT
WRITE(6,770)	CHGIII
770 FORMAT(//,1X,23X,'(INERTIAL)',27X,'(INERTIAL)',32X,'(INERTIAL)')	CHGIII
WRITE (6,22) UNITL,UNITL,UNITT	PRINT
22 FORMAT(18X,'LINEAR POSITION (' ,A4,')',	CHGIII
* 13X,'LINEAR VELOCITY (' ,A4,'/' ,A4,')',	PRINT
* 16X,'LINEAR ACCELERATIONS (G''S)'/	PRINT
* ' SEGMENT',10X,'X',10X,'Y',10X,'Z',	PRINT
* 13X,'X',11X,'Y',11X,'Z',15X,'X',13X,'Y',13X,'Z'//)	PRINT
DO 30 I=1,MBAG	PRINT
DO 29 K=1,3	PRINT
29 T1(K) = SEGLA(K,I)/G	PRINT
30 WRITE (6,31) I,SEG(I),(SEGLP(K,I),K=1,3),(SEGLV(K,I),K=1,3),T1	PRINT
31 FORMAT(13,1X,A4,3X,3F11.4,3X,3F12.5,3X,3F14.6)	PRINT
IF (NSEG.GT.6) WRITE (6,32) NPG	PAGE
IF (NSEG.GT.6) NPG=NPG+1	PAGE
32 FORMAT('1',122X,'PAGE',I5)	PAGE
WRITE(6,775)	CHGIII
775 FORMAT(//,1X,23X,'(INERTIAL)',29X,'(LOCAL)')	CHGIII
WRITE (6,33) UNITL,UNITT,UNITT,UNITM,UNITL	KINETIC
33 FORMAT(18X,'U1 ARRAY (' ,A4,'/' ,A4,'**2)',	KINETIC
* 14X,'U2 ARRAY (RAD/' ,A4,'**2)',	KINETIC
* 25X,'KINETIC ENERGY'/	KINETIC
* 15X,'EXTERNAL LINEAR ACCELERATIONS',	KINETIC
* 8X,'EXTERNAL ANGULAR ACCELERATIONS',	KINETIC
* 22X,'(' ,A4,'-' ,A4,')'/	KINETIC
* ' SEGMENT',10X,'X',10X,'Y',10X,'Z',13X,'X',11X,'Y',11X,'Z',	KINETIC
* 14X,'LINEAR',7X,'ANGULAR',7X,'TOTAL'//)	KINETIC
DO 80 J=1,3	KINETIC
80 TKE(J)=0.0	KINETIC
DO 34 I=1,NSEG	PRINT
V=SEGLV(1,I)**2+SEGLV(2,I)**2+SEGLV(3,I)**2	KINETIC
SKE(1)=0.5*W(I)*V/G	KINETIC
SKE(2)=0.0	KINETIC
DO 81 J=1,3	KINETIC
81 SKE(2)=SKE(2)+0.5*PHI(J,I)*WMEG(J,I)**2	KINETIC
SKE(3)=SKE(1)+SKE(2)	KINETIC
DO 82 J=1,3	KINETIC
82 TKE(J)=TKE(J)+SKE(J)	KINETIC
IF (LPMI(I).EQ.0) GO TO 73	FIXPRT
CALL DOT31 (DPMI(1,1,I),U2(1,I),T1)	FIXPRT
WRITE (6,61) I,SEG(I),(U1(K,I),K=1,3),	KINETIC
* (T1(K),K=1,3),(SKE(K),K=1,3)	KINETIC

GO TO 34	PRINT
73 CONTINUE	PRINT
WRITE (6,61) I,SEG(I),(U1(K,I),K=1,3),	KINETIC
* (U2(K,I),K=1,3),(SKE(K),K=1,3)	KINETIC
61 FORMAT(I3,1X,A4,3X,3(D11.4,1X),3X,3(D12.5,1X),3X,3(D12.5,1X))	KINETIC
34 CONTINUE	FIXPRT
WRITE(6,83) (TKE(K),K=1,3)	KINETIC
83 FORMAT(1X,98X,'TOTAL BODY KINETIC ENERGY'/	KINETIC
* 1X,90X,3(1X,D12.5))	KINETIC
IF (NJNT.LE.0) GO TO 39	PRINT
WRITE(6,776)	CHGIII
776 FORMAT(/,1X,27X,'(INERTIAL)',27X,'(INERTIAL)')	CHGIII
WRITE (6,35) UNITM,UNITL,UNITM,UNITL	PRINT
35 FORMAT(24X,'JOINT FORCES (' ,A4,')',	CHGIII
* 15X,'JOINT TORQUES (' ,2A4,')',	PRINT
* 9X,'RELATIVE ANGULAR'/	PRINT
* ' JOINT IPIN',9X,'X',10X,'Y',10X,'Z',13X,'X',11X,'Y',11X,'Z',	PRINT
* 7X,'VELOCITY (RAD/' ,A4,')' /)	PRINT
DO 36 J=1,NJNT	PRINT
IPINJ = IPIN(J)	PRINT
IF (IABS(IPIN(J)).EQ.4) IPINJ = IEULER(J)	PRINT
DO 137 II=1,3	MISC
137 T1(II)=-TQ(II,J)	MISC
WRITE (6,37) J,JOINT(J),IPINJ,(F(K,J),K=1,3),(T1(K),K=1,3),WJ(J)	MISC
37 FORMAT(I3,1X,A4,I4,7X,3(D10.3,1X),3X,3(D11.4,1X),3X,F13.3)	FIXPRT
36 CONTINUE	FIXPRT
39 IF (NQ.LE.0) GO TO 99	PRINT
WRITE (6,41)	CHGIII
WRITE (6,47)	CHGIII
47 FORMAT(1X,45X,'(INERTIAL)')	CHGIII
WRITE (6,49) UNITM,UNITL	CHGIII
41 FORMAT(///' OTHER CONSTRAINT FORCES',/)	CHGIII
49 FORMAT(1X,' NO. TYPE SEG1 SEG2',	CHGIII
* 15X,'CONSTRAINT FORCE (' ,A4,')',	PRINT
* 16X,'DISTANCE (' ,A4,')' /)	PRINT
ICH = 0	FIXPRT
DO 50 J=1,NQ	PRINT
IF (KQTYPE(J).NE.5) ICH = 0	FIXPRT
IF (KQTYPE(J).LT.0) GO TO 50	PRINT
IF (KQTYPE(J).EQ.5) ICH = ICH + 1	FIXPRT
IF (ICH.EQ.2) GO TO 50	FIXPRT
M = KQ1(J)	PRINT
N = KQ2(J)	PRINT
CALL DOT31(D(1,1,M),RK1(1,J),T1)	PRINT
CALL DOT31(D(1,1,N),RK2(1,J),T2)	PRINT
S1 = 0.0	PRINT
DO 42 I=1,3	PRINT
HH(I) = SEGLP(I,M)+T1(I) - SEGLP(I,N)-T2(I)	PRINT
42 S1 = S1 + HH(I)**2	PRINT
SQS1 = DSQRT(S1)	PRINT
WRITE (6,43) J,KQTYPE(J),SEG(M),SEG(N),(QQ(I,J),I=1,3),SQS1	PRINT
43 FORMAT(I4,I6,4X,A4,2X,A4,3X,3G15.7,6X,G15.7)	PRINT

```
50 CONTINUE
99 IF (NPRT(28).LE.0) NPRT(28) = -1
   RETURN
   END
```

```
PRINT
PRINT
PRINT
PRINT
```

	SUBROUTINE PRIPLT	PRIPLT
C		REV IV 07/24/86SLIP
C	PRODUCES PRINTER PLOT OF Y-Z PLANE VIEW AND X-Z PLANE VIEW OF	PRIPLT
C	BODY SEGMENT CGS, JOINTS AND SELECTED POINTS OF VEHICLE COMPONENTS	PRIPLT
C		PRIPLT
	IMPLICIT REAL*8 (A-H,O-Z)	PRIPLT
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,	PRIPLT
	* NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),	PRIPLT
	* SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)	PRIPLT
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),	SLIP
	* RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),	PRIPLT
	* JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)	PRIPLT
	COMMON/JBARTZ/ MNPL( 30),MNBLT( 8),MNSEG( 30),MNBAG( 6),	PRIPLT
	* MPL(3,5,30),MBLT(3,5,8),MSEG(3,5,30),MBAG(3,10,6),	PRIPLT
	* NTPL( 5,30),NTBLT( 5,8),NTSEG( 5,30)	PRIPLT
	COMMON/CNTRF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)	EDGE
	COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),	PRIPLT
	* BLTTTL(5,8),PLTTTL(5,30),BAGTTL(5,6),SEG(30),	PRIPLT
	* JOINT(30),CGS(30),JS(30)	PRIPLT
	COMMON/HRNESS/ BAR(15,100),BB(100),BBDOT(100),PLOSS(2,100),	PRIPLT
	* XLONG(20),HTIME(2),IBAR(5,100),NL(2,100),	PRIPLT
	* NPTSPB(20),NPTPLY(20),NTHRNS(20),NBLTPH(5)	PRIPLT
	REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTTL,BAGTTL,SEG,JOINT	PRIPLT
	LOGICAL*1 CGS,JS	PRIPLT
	COMMON/TEMPVS/ TEMP1(3),TEMP(3),TEMP2(3),CJOINT(3,30),BSN(2),	PRIPLT
	* PLOTYZ(96,55),PLOTXZ(96,55),PLOTXY(96,55)	PRIPLT
	* ,DDMY(33032)	80386
	LOGICAL*1 PLOTYZ,PLOTXZ,PLOTXY,CHARS(7),BLANK,BCHAR	PRIPLT
	LOGICAL NPRT5,NPRT6,NPRT7	PRIPLT
	DATA CHARS/' ','+', '@', '!', ' ', '-', '.', '*', '/', BLANK/' ' /	PRIPLT
	DATA ISTEP/0/ , NPLTI/96/ , NPLTJ/55/	PRIPLT
C		PRIPLT
C	DETERMINE IF PLOTTING IS TO BE DONE FOR THIS TIME STEP.	PRIPLT
C		PRIPLT
	ISTEP = ISTEP+1	PRIPLT
	NPRT5 = (NPRT(5)).EQ.1)	PRIPLT
	IF (NPRT(5).GT.1) NPRT5 = (MOD(ISTEP,NPRT(5))).EQ.1)	PRIPLT
	NPRT6 = (NPRT(6)).EQ.1)	PRIPLT
	IF (NPRT(6).GT.1) NPRT6 = (MOD(ISTEP,NPRT(6))).EQ.1)	PRIPLT
	NPRT7 = (NPRT(7)).EQ.1)	PRIPLT
	IF (NPRT(7).GT.1) NPRT7 = (MOD(ISTEP,NPRT(7))) EQ 1)	PRIPLT
	IF (.NOT.NPRT5 .AND. .NOT.NPRT6 .AND. NOT.NPRT7) GO TO 99	PRIPLT
	CALL ELTIME(1, 4)	PRIPLT
C		PRIPLT
C	BLANK OUT PLOT ARRAYS.	PRIPLT
C		PRIPLT
	DO 10 J=1,NPLTJ	PRIPLT
	PLOTYZ(1,J) = CHARS(6)	PRIPLT
	PLOTXZ(1,J) = CHARS(6)	PRIPLT
	PLOTXY(1,J) = CHARS(6)	PRIPLT
	DO 10 I=2,NPLTI	PRIPLT

	PLOTYZ(I,J) = BLANK	PRIPLT
	PLOTXZ(I,J) = BLANK	PRIPLT
10	PLOTXY(I,J) = BLANK	PRIPLT
C		PRIPLT
C	PLOT VEHICLE REFERENCE ORIGIN USING SYMBOL(*).	PRIPLT
C		PRIPLT
	CALL PLTXYZ (SEGLP(1,NVEH),CHARS(7))	PRIPLT
C		PRIPLT
C	PLOT CG OF BODY SEGMENTS USING SEGMENT SYMBOLS.	PRIPLT
C		PRIPLT
	DO 20 I=1,NSEG	PRIPLT
20	CALL PLTXYZ(SEGLP(1,I),CGS(I))	PRIPLT
C		PRIPLT
C	COMPUTE AND PLOT JOINT LOCATIONS USING JOINT SYMBOLS.	PRIPLT
C		PRIPLT
	IF (NJNT.EQ.0) GO TO 40	PRIPLT
	DO 31 J=1,NJNT	PRIPLT
	I = IABS(JNT(J))	PRIPLT
	IF (I.LE.0) GO TO 31	PRIPLT
	CALL DOT31(D(1,1,I),SR(1,2*J-1),TEMP)	PRIPLT
	DO 30 L=1,3	PRIPLT
30	CJOINT(L,J) = TEMP(L)+SEGLP(L,I)	PRIPLT
	CALL PLTXYZ (CJOINT(1,J),JS(J))	PRIPLT
31	CONTINUE	PRIPLT
	IF (NPRT(13).NE.0) WRITE (6,32) ((CJOINT(I,J),I=1,3),J=1,NJNT)	PRIPLT
32	FORMAT ('O JOINT POSITIONS'/(1X,9F14.4))	PRIPLT
C		PRIPLT
C	PLOT BELT ANCHOR, FIXED AND TANGENT POINTS USING SYMBOL(.).	PRIPLT
C		PRIPLT
40	IF (NBLT.LE.0) GO TO 50	PRIPLT
	DO 43 J=1,NBLT	PRIPLT
	IF (MNBLT(J).LE.0) GO TO 43	PRIPLT
	M1 = MBLT(1,1,J)	PRIPLT
	M2 = MBLT(2,1,J)	PRIPLT
	M3 = MBLT(3,1,J)	PRIPLT
	DO 41 I=1,3	PRIPLT
41	TEMP1(I) = BELT(I+6,J) + BD(I+3,M3)	PRIPLT
	CALL DOT31 (D(1,1,M2),TEMP1,TEMP)	PRIPLT
	CALL DOT31 (D(1,1,M1),BELT(1,J),TEMP1)	PRIPLT
	CALL DOT31 (D(1,1,M1),BELT(4,J),TEMP2)	PRIPLT
	DO 42 I=1,3	PRIPLT
	TEMP1(I) = TEMP1(I) + SEGLP(I,M1)	PRIPLT
	TEMP2(I) = TEMP2(I) + SEGLP(I,M1)	PRIPLT
42	TEMP (I) = TEMP (I) + SEGLP(I,M2)	PRIPLT
	CALL PLTXYZ (TEMP1,CHARS(1))	PRIPLT
	CALL PLTXYZ (TEMP2,CHARS(1))	PRIPLT
	CALL PLTXYZ (TEMP,CHARS(1))	PRIPLT
	CALL PLTXYZ (TPTS(1,J),CHARS(1))	PRIPLT
	CALL PLTXYZ (TPTS(4,J),CHARS(1))	PRIPLT
43	CONTINUE	PRIPLT
C		PRIPLT
C	PLOT POINTS IN PLAY ON HARNESS-BELT SYSTEMS USING SYMBOL(.).	PRIPLT

C		PRIPLT
	50 IF (NHRNSS.LE.0) GO TO 60	PRIPLT
	J1 = 1	PRIPLT
	K1 = 1	PRIPLT
	DO 54 NH=1,NHRNSS	PRIPLT
	IF (NBLTPH(NH).LE.J) GO TO 54	PRIPLT
	J2 = J1 + NBLTPH(NH) - 1	PRIPLT
	DO 53 NB=J1,J2	PRIPLT
	IF (NPTPLY(NB).LE.0) GO TO 53	PRIPLT
	K2 = K1 + NPTPLY(NB) - 1	PRIPLT
	DO 52 K=K1,K2	PRIPLT
	KI = NL(1,K)	PRIPLT
	KS = IABS(IBAR(1,KI))	PRIPLT
	IF (KS.GT.100) KS = MOD(KS,100)	PRIPLT
	CALL DOT31 (D(1,1,KS),BAR(4,KI),TEMP1)	PRIPLT
	CALL DOT31 (D(1,1,KS),BAR(7,KI),TEMP2)	PRIPLT
	DO 51 I=1,3	PRIPLT
	51 TEMP(I) = SEGLP(I,KS) + TEMP1(I) + TEMP2(I)	PRIPLT
	52 CALL PLTXYZ (TEMP,CHARS(1))	PRIPLT
	K1 = K2+1	PRIPLT
	53 CONTINUE	PRIPLT
	J1 = J2+1	PRIPLT
	54 CONTINUE	PRIPLT
C		PRIPLT
C	PLOT CENTER AND END OF AXES OF ELLIPSOIDAL TARGET USING SYMBOLS	PRIPLT
C	(@) FOR CENTER, (-) FOR ENDS OF Z AXIS,(!) FOR ENDS OF X,Y AXES.	PRIPLT
C		PRIPLT
	60 IF (NBAG.EQ.0) GO TO 80	PRIPLT
	BSN(1) = 1.0	PRIPLT
	BSN(2) = -1.0	PRIPLT
	DO 68 J=1,NBAG	PRIPLT
	IF (MNBAG(J).EQ.0) GO TO 68	PRIPLT
	JB = NVEH+J	PRIPLT
	BCHAR = CHARS(5)	PRIPLT
	L2 = 2	PRIPLT
	DO 67 I=1,4	PRIPLT
	IF (I.EQ.3) BCHAR = CHARS(4)	PRIPLT
	IF (I.EQ.4) BCHAR = CHARS(3)	PRIPLT
	IF (I.EQ.4) L2 = 1	PRIPLT
	DO 67 L=1,L2	PRIPLT
	DO 64 K=1,3	PRIPLT
	64 TEMP1(K) = BD(K,3,B)	PRIPLT
	IF (I.EQ.4) GO TO 65	PRIPLT
	TEMP1(I) = TEMP1(I) + BSN(L)*BD(I,JB)	PRIPLT
	65 CALL DOT31 (D(1,1,JB),TEMP1,TEMP2)	PRIPLT
	DO 66 K=1,3	PRIPLT
	66 TEMP2(K) = TEMP2(K) + SEGLP(K,JB)	PRIPLT
	67 CALL PLTXYZ (TEMP2,BCHAR)	PRIPLT
	68 CONTINUE	PRIPLT
C		PRIPLT
C	PRINT Y-Z , X-Z AND X-Y PLANE VIEW PLOTS.	PRIPLT
C		PRIPLT

83	TMSC = 1000.0*TIME	PRIPLT
	IF (.NOT.NPRT5) GO TO 83	PRIPLT
	WRITE (2,81) TMSC,SEGLP(2,NVEH),SEGLP(3,NVEH)	PRIPLT
81	FORMAT ('1 T=',F10.3,' Y0=',F10.5,' Z0=',F10.5,' Y-Z PLANE')	PRIPLT
	WRITE (2,82) PLOTYZ	PRIPLT
82	FORMAT (2X,96A1)	PRIPLT
83	IF (.NOT.NPRT6) GO TO 85	PRIPLT
	WRITE (2,84) TMSC,SEGLP(1,NVEH),SEGLP(3,NVEH)	PRIPLT
84	FORMAT ('1 T=',F10.3,' X0=',F10.5,' Z0=',F10.5,' X-Z PLANE')	PRIPLT
	WRITE (2,82) PLOTXZ	PRIPLT
85	IF (.NOT.NPRT7) GO TO 87	PRIPLT
	WRITE (2,86) TMSC,SEGLP(1,NVEH),SEGLP(2,NVEH)	PRIPLT
86	FORMAT ('1 T=',F10.3,' X0=',F10.5,' Y0=',F10.5,' X-Y PLANE')	PRIPLT
	WRITE (2,82) PLOTXY	PRIPLT
87	CALL ELTIME(2, 4)	PRIPLT
99	RETURN	PRIPLT
	END	PRIPLT



	SUBROUTINE QSET(F,Y,X,DER,N)	QSET
C		REV III.3 10/01/84REVIII
	IMPLICIT REAL*8(A-H,O-Z)	QSET
	DIMENSION F(5,3,80),Y(5,3,80),X(3,80),DER(3,80)	QSET
	DIMENSION T1(3),T2(3),T3(3),T4(3)	QSET
	DO 20 I=1,N	QSET
	E1=DSQRT(1.D0 -X(1,I)**2-X(2,I)**2-X(3,I)**2)	QSET
	E1D=-(X(1,I)*DER(1,I)+X(2,I)*DER(2,I)+X(3,I)*DER(3,I))/E1	QSET
	E2=DSQRT(1.D0-Y(1,1,I)**2-Y(1,2,I)**2-Y(1,3,I)**2)	QSET
	E2D=-(Y(1,1,I)*Y(2,1,I)+Y(1,2,I)*Y(2,2,I)+Y(1,3,I)*Y(2,3,I))/E2	QSET
	UHB=X(1,I)*F(3,1,I)+X(2,I)*F(3,2,I)+X(3,I)*F(3,3,I)	QSET
	UHC=X(1,I)*F(4,1,I)+X(2,I)*F(4,2,I)+X(3,I)*F(4,3,I)	QSET
	UDB=DER(1,I)*F(3,1,I)+DER(2,I)*F(3,2,I)+DER(3,I)*F(3,3,I)	QSET
	UDD=DER(1,I)**2+DER(2,I)**2+DER(3,I)**2	QSET
	EB=(E1D**2+UDD+UHB)/E1	QSET
	EC = (1.5*(UDB-E1D*EB)+UHC+F(5,1,I)*(E1D**2+UDD))/E1	QSET
	T1(1)=X(2,I)*F(3,3,I)-X(3,I)*F(3,2,I)	QSET
	T2(1)=X(2,I)*F(4,3,I)-X(3,I)*F(4,2,I)	QSET
	T3(1)=X(2,I)*Y(1,3,I)-X(3,I)*Y(1,2,I)	QSET
	T4(1)=X(2,I)*Y(2,3,I)-X(3,I)*Y(2,2,I)	QSET
	T1(2)=X(3,I)*F(3,1,I)-X(1,I)*F(3,3,I)	QSET
	T2(2)=X(3,I)*F(4,1,I)-X(1,I)*F(4,3,I)	QSET
	T3(2)=X(3,I)*Y(1,1,I)-X(1,I)*Y(1,3,I)	QSET
	T4(2)=X(3,I)*Y(2,1,I)-X(1,I)*Y(2,3,I)	QSET
	T1(3)=X(1,I)*F(3,2,I)-X(2,I)*F(3,1,I)	QSET
	T2(3)=X(1,I)*F(4,2,I)-X(2,I)*F(4,1,I)	QSET
	T3(3)=X(1,I)*Y(1,2,I)-X(2,I)*Y(1,1,I)	QSET
	T4(3)=X(1,I)*Y(2,2,I)-X(2,I)*Y(2,1,I)	QSET
	DO 20 J=1,3	QSET
	F(3,J,I)=E1*F(3,J,I)-T1(J)+EB*X(J,I)	JTF984
	F(4,J,I)=E1*F(4,J,I)-T2(J)+EC*X(J,I)	JTF984
	Y(3,J,I)=E1*Y(1,J,I)-T3(J)-E2*X(J,I)	JTF984
20	Y(4,J,I)=E1*Y(2,J,I)-T4(J)-E2D*X(J,I)	JTF984
	RETURN	QSET
	END	QSET

	SUBROUTINE QUAT(ANG,Q)		QUAT
		REV IV 07/23/86	TWOPI
C	COMPUTES QUATERNIONS FROM YAW, PITCH, ROLL ANGLES IN DEGREES		QUAT
C	IMPLICIT REAL *8(A-H,O-Z)		QUAT
	DIMENSION ANG(3),Q(4),R(4),T(3)		QUAT
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),		QUAT
	* UNITL,UNITM,UNITT,GRAVITY(3),TWOPI		TWOPI
	A = 0.5*ANG(1)*RADIAN		QUAT
	Q(1) = DCOS(A)		QUAT
	Q(2) = 0.0		QUAT
	Q(3) = 0.0		QUAT
	Q(4) = DSIN(A)		QUAT
	K = 3		QUAT
	DO 10 I = 2,3		QUAT
	A = 0.5*ANG(I)*RADIAN		QUAT
	R(1) = DCOS(A)		QUAT
	R(2) = 0.0		QUAT
	R(3) = 0.0		QUAT
	R(4) = 0.0		QUAT
	R(K) = DSIN(A)		QUAT
	DOT = Q(2)*R(2) + Q(3)*R(3) + Q(4)*R(4)		QUAT
	CALL CROSS(Q(2),R(2),T)		QUAT
	DO 5 J = 2,4		QUAT
5	Q(J) = Q(1)*R(J) + R(1)*Q(J) + T(J-1)		QUAT
	Q(1) = Q(1)*R(1) - DOT		QUAT
10	K = 2		QUAT
	SUM = DSQRT(Q(1)**2 + Q(2)**2 + Q(3)**2 + Q(4)**2)		QUAT
	DO 12 I = 1,4		QUAT
12	Q(I) = Q(I)/SUM		QUAT
	RETURN		QUAT
	END		QUAT

	DOUBLE PRECISION FUNCTION RCRT(A,PL,Z,IP)		REV 03	07/19/73	RCRT
C					RCRT
C	COMPUTES THE RADIUS OF CURVATURE AT POINT Z OF ELLIPSOID A				RCRT
C	IN THE PLANE PL(I,IP) WHERE				RCRT
C					RCRT
C	A: 3X3 MATRIX DEFINING ELLIPSOID.				RCRT
C	PL: 4X3 MATRIX CONTAINING THREE ORTHONORMAL VECTORS.				RCRT
C	Z: 3 COORDINATES OF POINT ON THE ELLIPSOID				RCRT
C	AS MEASURED FROM CENTER OF ELLIPSOID				RCRT
C	IP: IDENTIFIES THE NORMAL VECTOR OF PLANE IN WHICH THE				RCRT
C	RADIUS OF CURVATURE IS DESIRED.				RCRT
C					RCRT
	IMPLICIT REAL*8 (A-H,O-Z)				RCRT
	DIMENSION A(3,3),PL(4,3),Z(3),T(5)				RCRT
	DO 10 I=1,5				RCRT
10	T(I) = 0.0				RCRT
	M = IP+1				RCRT
	N = IP+2				RCRT
	IF(M.GT.3) M = M-3				RCRT
	IF(N.GT.3) N = N-3				RCRT
	DO 30 I=1,3				RCRT
	S1 = 0.				RCRT
	S2 = 0.				RCRT
	DO 20 J=1,3				RCRT
	S1 = S1+A(I,J)*PL(J,M)				RCRT
20	S2 = S2+A(I,J)*PL(J,N)				RCRT
	T(1) = T(1)+S1*Z(I)				RCRT
	T(2) = T(2)+S2*Z(I)				RCRT
	T(3) = T(3)+S1*PL(I,M)				RCRT
	T(4) = T(4)+S2*PL(I,N)				RCRT
30	T(5) = T(5)+S1*PL(I,N)				RCRT
	W = DSQRT(T(1)**2+T(2)**2)				RCRT
	T(1) = T(1)/W				RCRT
	T(2) = T(2)/W				RCRT
	RCRT = W/(T(3)*T(2)**2-2.0*T(1)*T(2)*T(5)+T(4)*T(1)**2)				RCRT
	IF(RCRT.LT.0.0) RCRT = -RCRT				RCRT
	RETURN				RCRT
	END				RCRT

C	SUBROUTINE ROT (A,L,TH)	REV IV	07/23/86	TWOPI	ROT
C	COMPUTES ROTATION MATRIX A FOR ANGLE TH				ROT
C	ABOUT X,Y OR Z AXIS AS L = 1, 2, OR 3.				ROT
C					ROT
C	ARGUMENTS:				ROT
C	A: 3X3 ROTATION MATRIX TO BE COMPUTED.				ROT
C	L: 1,2 OR 3 TO ROTATE ABOUT X,Y OR Z AXIS.				ROT
C	TH: ANGLE OF ROTATION IN RADIAN.				ROT
C					ROT
	IMPLICIT REAL*8 (A-H,O-Z)				ROT
	DIMENSION A(3,3)				ROT
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),				ROT
	* UNITL,UNITM,UNITT,GRAVITY(3),TWOPI				TWOPI
	C=DCOS(TH)				ROT
	S=DSIN(TH)				ROT
	IF (DABS(C) .LT.EPS(8)) C=0.0				CONVER
	IF (DABS(S) .LT.EPS(8)) S=0.0				CONVER
	ONE = 1.0				ROT
	IF (1.0-DABS(C) .LT.EPS(8)) C = DSIGN(ONE,C)				CONVER
	IF (1.0-DABS(S) .LT.EPS(8)) S = DSIGN(ONE,S)				CONVER
	IF (L.EQ.2) S = -S				ROT
	DO 30 I=1,3				ROT
	IF(I.EQ.3)GO TO 20				ROT
	DO 10 J=1,2				ROT
	A(I,J+1)=0.0				ROT
	A(J+1,I)=0.0				ROT
	IF(I+J+L.NE.5)GO TO 10				ROT
	A(I,J+1)=S				ROT
	A(J+1,I)=-S				ROT
	10 CONTINUE				ROT
	20 A(I,I)= C				ROT
	IF(I.EQ.L)A(I,I)=1.0				ROT
	30 CONTINUE				ROT
	RETURN				ROT
	END				ROT

	SUBROUTINE ROTATE	REV IV 02/20/87	ROTATE
C			HYPER
C	THE PURPOSE OF THIS ROUTINE IS TO TRANSFORM THOSE VARIABLES THAT		ROTATE
C	HAVE BEEN SUPPLIED IN LOCAL GEOMETRIC COORDINATES TO PRINCIPAL		ROTATE
C	AXES COORDINATES AS INDICATED BY LPMI(I) # 0 FOR I = 1 TO NSEG.		ROTATE
C			ROTATE
	IMPLICIT REAL*8 (A-H,O-Z)		ROTATE
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		ROTATE
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/RSAVE/ XSG(3,20,3),DPMI(3,3,30),LPMI(30),		ATBIII
*	NSG(9),MSG(20,9),MCG,MCGIN(24,5),KREF(20,9)		TTHKREF
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),		SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),		ROTATE
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)		ROTATE
	COMMON/CNTRSF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)		EDGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),		ROTATE
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		ROTATE
	COMMON/JBARTZ/ MNPL( 30),MNBLT( 8),MNSEG( 30),MNBAG( 6),		ROTATE
*	MPL(3,5,30),MBLT(3,5,8),MSEG(3,5,30),MBAG(3,10,6),		ROTATE
*	NTPL( 5,30),NTBLT( 5,8),NTSEG( 5,30)		ROTATE
	COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24),		ROTATE
*	HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12),		ROTATE
*	RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12),		ROTATE
*	KQ1(12),KQ2(12),KQTYPE(12)		ROTATE
	COMMON/DAMPER/ APSDM(3,20),APSDN(3,20),ASD(5,20),MSDM(20),MSDN(20)		ROTATE
	COMMON/WINDFR/ WTIME(30),QFU(3,5),QFV(3,5),WF(3,30),IWIND(30),		WINDOP
*	MWSEG(7,30),NFVSEG(6),NFVNT(5),MOWSEG(30,30)		WINDOP
	COMMON/HRNESS/ BAR(15,100),BB(100),BBDOT(100),PLOSS(2,100),		ROTATE
*	XLONG(20),HTIME(2),IBAR(5,100),NL(2,100),		ROTATE
*	NPTSPB(20),NPTPLY(20),NTHRNS(20),NBLTPH(5)		ROTATE
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)		WINDROT
	COMMON/CEULER/ IEULER(30),HIR(3,3,90),ANG(3,30),ANGD(3,30),		FXHROT
*	FE(3,30),TQE(3,30),CONST(5,30)		FXHROT
	COMMON/TEMPVS/ T1(3),T3(3,3),LBD(40),T2(3),T4(3,3),DMY(35069)		80386
C			ROTATE
C	TRANSFORM DIRECTION COSINE MATRICEES D FROM INPUT CARDS G.3.		ROTATE
C			ROTATE
	LTEST = 0		ROTATE
	DO 20 J=1,30		ROTATE
	IF (J.GT.NSEG) LPMI(J) = 0		ROTATE
	IF (LPMI(J).EQ.0) GO TO 20		ROTATE
	LTEST = 1		ROTATE
	DO 12 I=1,3		ROTATE
	T1(I) = WMEG(I,J)		ROTATE
	DO 12 K=1,3		ROTATE
12	T3(I,K) = D(I,K,J)		ROTATE
	CALL MAT33 (DPMI(1,1,J),T3,D(1,1,J))		ROTATE
	CALL MAT31 (DPMI(1,1,J),T1,WMEG(1,J))		ROTATE
20	CONTINUE		ROTATE
	IF (LTEST.EQ.0) GO TO 99		ROTATE
C			ROTATE
C	TRANSFORM SR,HT AND HB FROM INPUT CARDS B.3.		ROTATE



DO 45 I=1,3	ROTATE
45 T1(I) = APSDN(I,J)	ROTATE
CALL MAT31 (DPMI(1,1,KSEG),T1,APSDN(1,J))	ROTATE
50 CONTINUE	ROTATE
C	FIXROT
C TRANSFORM QFU AND QFV FROM INPUT CARDS D.9.	FIXROT
C	FIXROT
151 NFORCE = NFVSEG(6)	FIXROT
IF (NFORCE.LE.0) GO TO 100	WINDROT
DO 152 J=1,NFORCE	FIXROT
KSEG = IABS(NFVSEG(J))	FIXROT
IF (LPMI(KSEG).EQ.0) GO TO 152	FIXROT
DO 143 I=1,3	FIXROT
T1(I) = QFU(I,J)	FIXROT
143 T2(I) = QFV(I,J)	FIXROT
CALL MAT31 (DPMI(1,1,KSEG),T1,QFU(1,J))	FIXROT
CALL MAT31 (DPMI(1,1,KSEG),T2,QFV(1,J))	FIXROT
152 CONTINUE	FIXROT
C	WINDROT
C ROTATE WIND FORCE FUNCTIONS	WINDROT
C	WINDROT
100 IF (NWINDF.EQ.0) GOTO 51	WINDROT
DO 101 I=1,NSEG	WINDROT
IF (MWSEG(1,I).EQ.0) GOTO 101	WINDROT
NT = MWSEG(5,I)	WINDROT
DO 102 J=1,I-1	WINDROT
IF (NT.EQ.MWSEG(5,J)) GOTO 101	WINDROT
102 CONTINUE	WINDROT
KT = NTI(NT)	WINDROT
RK = TAB(KT)	WINDROT
IF (RK.NE.0) GOTO 101	WINDROT
NSR = IDINT(TAB(KT+4))	WINDROT
IF (NSR.EQ.0 .OR. LPMI(NSR).EQ.0) GOTO 101	WINDROT
NENTRY = TAB(KT+5)	WINDROT
K1 = KT+6	WINDROT
K2 = 4*NENTRY+KT+2	WINDROT
DO 103 K=K1,K2,4	WINDROT
DO 104 J=1,3	WINDROT
104 T1(J) = TAB(K+J)	WINDROT
103 CALL MAT31(DPMI(1,1,NSR),T1,TAB(K+1))	WINDROT
101 CONTINUE	WINDROT
C	ROTATE
C CHECK PLANE AND ELLIPSOID ASSIGNMENTS ON INPUT CARDS F.1.	ROTATE
C TRANSFORM PLANE ARRAYS SET UP FROM INPUT CARD D.1.	ROTATE
C	ROTATE
51 DO 52 J=1,40	ROTATE
LBD(J) = 0	ROTATE
52 IF (J.LE.NSEG) LBD(J) = J	ROTATE
IF (NPL.LE.0) GO TO 61	ROTATE
DO 60 J=1,NPL	ROTATE
IF (MNPL(J).EQ.0) GO TO 60	ROTATE
LPL = 0	ROTATE

KPL = MNPL(J)	ROTATE
DO 56 I=1,KPL	ROTATE
M1 = MPL (1,I,J)	ROTATE
M2 = MPL (2,I,J)	ROTATE
M3 = MPL (3,I,J)	ROTATE
IF (LPL.EQ.M1 .OR. LPL.EQ.0) GO TO 54	ROTATE
WRITE (6,53) J,M1,LPL	ROTATE
53 FORMAT('O INPUT ERROR HAS BEEN DETECTED IN SUBROUTINE ROTATE.'/	ROTATE
* ' PLANE NO.',I3,' HAS BEEN ASSIGNED TO BOTH SEGMENTS NO.',	ROTATE
* I3,' AND NO.',I3,'.'/ PROGRAM IS BEING TERMINATED.')	ROTATE
STOP 43	ROTATE
54 LPL = M1	ROTATE
IF (LBD(M3).EQ.M2 .OR. LBD(M3).EQ.0) GO TO 55	ROTATE
WRITE (6,68) M3,M2,LBD(M3)	ROTATE
STOP 44	ROTATE
55 LBD(M3) = M2	ROTATE
56 CONTINUE	ROTATE
IF (LPMI(LPL).EQ.0) GO TO 60	ROTATE
L = 1	EDGE
DO 59 K=1,6	EDGE
IF((K.EQ.3).OR.(K.EQ.6)) L = L-1	EDGE
IF((K.EQ.4).OR.(K.EQ.5)) L = L+1	EDGE
DO 58 I=1,3	ROTATE
T1(I) = PL(L,J)	EDGE
58 L=L+1	EDGE
CALL MAT31 (DPMI(1,1,LPL),T1,PL(L-3,J))	EDGE
59 L=L+1	EDGE
60 CONTINUE	ROTATE
C	ROTATE
C CHECK ELLIPSOID ASSIGNMENTS ON INPUT CARDS F.2.	ROTATE
C TRANSFORM BELT(L,J) FOR L=1,9 FROM INPUT CARDS D.3.	ROTATE
C	ROTATE
61 IF (NBLT.LE.0) GO TO 66	ROTATE
DO 65 J=1,NBLT	ROTATE
IF (MNBLT(J).EQ.0) GO TO 65	ROTATE
KBLT = MNBLT(J)	ROTATE
DO 62 I=1,KBLT	ROTATE
M1 = MBLT(1,I,J)	ROTATE
M2 = MBLT(2,I,J)	ROTATE
M3 = MBLT(3,I,J)	ROTATE
IF (LBD(M3).EQ.M2 .OR. LBD(M3).EQ.0) GO TO 62	ROTATE
WRITE (6,68) M3,M2,LBD(M3)	ROTATE
STOP 45	ROTATE
62 LBD(M3) = M2	ROTATE
IF (LPMI(M1).EQ.0) GO TO 63	ROTATE
DO 57 I=1,3	ROTATE
T3(I,1) = BELT(I ,J)	ROTATE
57 T3(I,2) = BELT(I+3,J)	ROTATE
CALL MAT31 (DPMI(1,1,M1),T3(1,1),BELT(1,J))	ROTATE
CALL MAT31 (DPMI(1,1,M1),T3(1,2),BELT(4,J))	ROTATE
63 IF (LPMI(M2).EQ.0) GO TO 65	ROTATE
DO 64 I=1,3	ROTATE



64	T3(I,3) = BELT(I+6,J)	ROTATE
	CALL MAT31 (DPMI(1,1,M2),T3(1,3),BELT(7,J))	ROTATE
65	CONTINUE	ROTATE
C		ROTATE
C	CHECK ELLIPSOID ASSIGNMENTS ON INPUT CARDS F.3.	ROTATE
C		ROTATE
66	DO 70 J=1,NSEG	ROTATE
	IF (MNSEG(J).EQ.0) GO TO 70	ROTATE
	KSEG = MNSEG(J)	ROTATE
	DO 69 I=1,KSEG	ROTATE
	M1 = MSEG(1,I,J)	ROTATE
	M2 = MSEG(2,I,J)	ROTATE
	M3 = MSEG(3,I,J)	ROTATE
	IF (LBD(M1).EQ.J .OR. LBD(M1).EQ.0) GO TO 67	ROTATE
	WRITE (6,68) M1,J,LBD(M1)	ROTATE
	STOP 46	ROTATE
67	LBD(M1) = J	ROTATE
	IF (LBD(M3).EQ.M2 .OR. LBD(M3).EQ.0) GO TO 69	ROTATE
	WRITE (6,68) M3,M2,LBD(M3)	ROTATE
68	FORMAT('0 INPUT ERROR HAS BEEN DETECTED IN SUBROUTINE ROTATE.'/	ROTATE
	* ' ELLIPSOID NO.',I3,' HAS BEEN ASSIGNED TO BOTH SEGMENTS NO.',	ROTATE
	* I3,' AND NO.',I3,'.'/ PROGRAM IS BEING TERMINATED.')	ROTATE
	STOP 47	ROTATE
69	LBD(M3) = M2	ROTATE
70	CONTINUE	ROTATE
C		ROTATE
C	CHECK ELLIPSOID ASSIGNMENTS ON INPUT CARDS F.6.	ROTATE
C		ROTATE
	IF (NBAG.EQ.0) GO TO 174	TGMOD8
	DO 73 J=1,NBAG	ROTATE
	IF (MNBAG(J).EQ.0) GO TO 73	ROTATE
	KBAG = MNBAG(J)	ROTATE
	DO 72 I=1,KBAG	ROTATE
	M2 = MBAG(2,I,J)	ROTATE
	M3 = MBAG(3,I,J)	ROTATE
	IF (LBD(M3).EQ.M2 .OR. LBD(M3).EQ.0) GO TO 72	ROTATE
	WRITE (6,68) M3,M2,LBD(M3)	ROTATE
	STOP 50	ROTATE
72	LBD(M3) = M2	ROTATE
73	CONTINUE	ROTATE
C		TGMOD8
C	CHECK ELLIPSOID ASSIGNMENTS ON INPUT CARDS F.7.	TGMOD8
C		TGMOD8
174	IF(NWINDF.EQ.0) GO TO 74	TGMOD8
	DO 175 J=1,NSEG	TGMOD8
	M1 = IABS(MWSEG(1,J))	TGMOD8
	IF(M1.EQ.0) GO TO 175	TGMOD8
	M2 = MWSEG(2,J)	TGMOD8
	IF(LBD(M2).EQ.M1 .OR. LBD(M2).EQ.0) GO TO 172	TGMOD8
	WRITE(6,68) M2,M1,LBD(M2)	TGMOD8
	STOP 48	TGMOD8
172	LBD(M2) = M1	TGMOD8

175	CONTINUE	TGMOD8
C		ROTATE
C	CHECK ELLIPSOID ASSIGNMENTS ON INPUT CARDS F.8.	ROTATE
C	TRANSFORM BAR(L,K) FOR L=4,12 FROM INPUT CARDS F.8.D.	ROTATE
C		ROTATE
74	IF (NHRNSS.EQ.0) GO TO 81	ROTATE
	J1 = 1	ROTATE
	K1 = 1	ROTATE
	DO 80 II=1,NHRNSS	ROTATE
	IF (NBLTPH(II).LE.0) GO TO 80	ROTATE
	J2 = J1 + NBLTPH(II) - 1	ROTATE
	DO 79 JJ=J1,J2	ROTATE
	IF (NPTSPB(JJ).LE.0) GO TO 79	ROTATE
	K2 = K1 + NPTSPB(JJ) - 1	ROTATE
	DO 78 K=K1,K2	ROTATE
	M2 = MOD(IBAR(1,K),100)	ROTATE
	M3 = IBAR(2,K)	ROTATE
	IF (M3.EQ.0) GO TO 88	BUTLER1
	IF (LBD(M3).EQ.M2 .OR. LBD(M3).EQ.0) GO TO 75	ROTATE
	WRITE (6,68) M3,M2,LBD(M3)	ROTATE
	STOP 51	ROTATE
75	LBD(M3) = M2	ROTATE
88	IF (LPMI(M2).EQ.0) GO TO 78	BUTLER1
	DO 77 J=3,9,3	ROTATE
	DO 76 I=1,3	ROTATE
	IJ = I+J	ROTATE
76	T1(I) = BAR(IJ,K)	ROTATE
77	CALL MAT31 (DPMI(1,1,M2),T1,BAR(J+1,K))	ROTATE
73	CONTINUE	ROTATE
	K1 = K2+1	ROTATE
79	CONTINUE	ROTATE
	J1 = J2+1	ROTATE
80	CONTINUE	ROTATE
C		ROTATE
C	TRANSFORM DATA IN BD ARRAYS FOR ELLIPSOIDS THAT HAVE BEEN ASSIGNED	ROTATE
C		ROTATE
81	DO 90 J=1,40	ROTATE
	IF (LBD(J).EQ.0) GO TO 90	ROTATE
	KSEG = LBD(J)	ROTATE
	IF (LPMI(KSEG).EQ.0) GO TO 90	ROTATE
	L = 4	HYPER
	IF (BD(1,J).LT.0.0) L = 5	HYPER
	M = 8	HYPER
	DO 82 I=1,3	ROTATE
	T1(I) = BD(L,J)	HYPER
	L = L + 1	HYPER
	DO 82 K = 1,3	HYPER
	T3(K,I) = BD(M,J)	HYPER
82	M = M + 1	HYPER
	CALL MAT31 (DPMI(1,1,KSEG),T1,BD(L-3,J))	HYPER
	IF (BD(1,J).GT.0.0) GO TO 84	HYPER
	CALL MAT33 (DPMI(1,1,KSEG),T3,BD(8,J))	HYPER

GO TO 90  
84 CALL DOTT33 (BD( 7,J),DPMI(1,1,KSEG),T3)  
CALL MAT33 (DPMI(1,1,KSEG),T3,BD( 7,J))  
CALL DOTT33 (BD(16,J),DPMI(1.1,KSEG),T3)  
CALL MAT33 (DPMI(1,1,KSEG),T3,BD(16,J))  
90 CONTINUE  
99 RETURN  
END

HYPER  
HYPER  
ROTATE  
ROTATE  
ROTATE  
ROTATE  
ROTATE  
ROTATE

	SUBROUTINE RSTART(IF,IT)		RSTART
		REV IV 07/24/86	SLIP
C	THE FIVE FUNCTIONS OF SUBROUTINE RSTART ARE:		RSTART
C	1. READ INPUT & INITIALIZATION RECORD FROM OLD RESTART TAPE.		RSTART
C	2. WRITE INPUT & INITIALIZATION RECORD ONTO NEW RESTART TAPE.		RSTART
C	3. READ TIME POINT RECORD FROM OLD RESTART TAPE.		RSTART
C	4. READ NEW INPUT DATA FROM INPUT STREAM FOR RESTART.		RSTART
C	5. WRITE TIME POINT RECORD ONTO NEW RESTART TAPE.		RSTART
C	IMPLICIT REAL*8(A-H,O-Z)		RSTART
C	ALL LABELED COMMON BLOCKS ARE INCLUDED HERE		RSTART
C	TO GIVE A COMPLETE SET FOR REFERENCE		RSTART
C 1	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		RSTART
	* NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	DIMENSION IC1(51)		PAGE
	EQUIVALENCE (IC1(1),NSEG)		RSTART
C 2	COMMON/CNTRSF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)		RSTART
	DIMENSION RC2(1888)		EDGE
	EQUIVALENCE (RC2(1),PL(1,1))		EDGE
C 3	COMMON/VPOSTN/ ZPLT(3),SPLT(3),AXV(3,6),VATAB(6,501,6),		RSTART
	* VTO(6),VDI(6),TIMEV(6),OMEGV(6),NVTAB(6),INDXV(6)		VEHICL
	DIMENSION RC3(18084),IC3(12)		RSTART
	EQUIVALENCE (RC3(1),ZPLT(1)),(IC3(1),NVTAB(1))		VEHICL
C 4	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),		RSTART
	* SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		RSTART
	DIMENSION RC4(900)		RSTART
	EQUIVALENCE (RC4(1),D(1,1,1))		RSTART
C 5	COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),		RSTART
	* F(3,30),TQ(3,30),WJ(30),A11(3,3,30)		SLIP
	DIMENSION RC5A(1296),RC5B(480)		SLIP
	EQUIVALENCE (RC5A(1),V1(1,1)),(RC5B(1),F(1,1))		RSTART
C 6	COMMON/ABDATA/ ZDEF(3,5),DBR(3,3,5),DPVCTR(3,5),DEPLOY(3,5),		RSTART
	* AB(3,5),B(9,4,5),ZR(3,4,5),BFB(3,4,5),DRR(9,4,5),		RSTART
	* VBAGG(5),VSCS(5),SPRK(5),CK(5),CMASS(5),CYMIN(5),		RSTART
	* CYMOUT(5),BAGPV(5),PD(5),VBAG(5),VOLBP(5),		RSTART
	* PCYV(5),PCYMIN(5),PVBAG(5),TV1(3,4,5),TV2(3,10,5),		RSTART
	* SWITCH(5),PYMOUT(5),SCALE(5),PREVT,IFULL(6)		RSTART
	DIMENSION RC6A(610),RC6B(271)		RSTART
	EQUIVALENCE (RC6A(1),ZDEP(1,1)),(RC6B(1),CYMIN(1))		RSTART
C 7	COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),		RSTART
	* BLTTTL(5,8),PLTTTL(5,30),BAGTTL(5,6),SEG(30),		RSTART
	* JOINT(30),CGS(30),JS(30)		RSTART
	REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTTL,BAGTTL,SEG,JOINT		RSTART
	LOGICAL*1 CGS,JS		RSTART

	REAL RC7,RC7A,XDTE,XCMENT	RSTART
	DIMENSION RC7(305),RC7A(348),XDTE(3),XCMENT(40)	RSTART
	EQUIVALENCE (RC7(1),VPSTTL(1)),(RC7A(1),DATE(1))	RSTART
C 8	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),	RSTART
	* UNITL,UNITM,UNITT,GRAVITY(3),TWOPI	TWOPI
	DIMENSION RC8(35)	TWOPI
	EQUIVALENCE (RC8(1),PI)	RSTART
C 9	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),	SLIP
	* RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),	RSTART
	* JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)	RSTART
	DIMENSION RC9(2460),IC9(150)	SLIP
	EQUIVALENCE (RC9(1),PHI(1,1)),(IC9(1),JNT(1))	RSTART
C 10	COMMON/JBARTZ/ MNPL( 30),MNBLT( 8),MNSEG( 30),MNBAG( 6),	RSTART
	* MPL(3,5,30),MBLT(3,5,8),MSEG(3,5,30),MBAG(3,10,6),	RSTART
	* NTPL( 5,30),NTBLT( 5,8),NTSEG( 5,30)	RSTART
	DIMENSION IC10(1614)	RSTART
	EQUIVALENCE (IC10(1),MNPL(1))	RSTART
C 11	COMMON/FORCES/PSF(7,70),BSF(4,20),SSF(10,40),BAGSF(3,20),	NCFORC
	* PRJNT(7,30),NPANEL(5),NPSF,NBSF,NSSF,NBGSF	RSTART
	DIMENSION RC11(1240),IC11(9)	NCFORC
	EQUIVALENCE (RC11(1),PSF(1,1)),(IC11(1),NPANEL(1))	RSTART
C 12	COMMON/INTEST/ SGTEST(3.4,30),XTEST(3,120),SEGT(120),REGT(120)	RSTART
	REAL SEGT	RSTART
	DIMENSION RC12(720)	RSTART
	EQUIVALENCE (RC12(1),SGTEST(1,1,1))	RSTART
C 13	COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24),	RSTART
	* HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12),	RSTART
	* RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12),	RSTART
	* KQ1(12),KQ2(12),KQTYPE(12)	RSTART
	DIMENSION RC13(72),IC13(36),RC13A(1212),RC13H(348)	RSTART
	EQUIVALENCE (RC13(1),RK1(1,1)),(IC13(1),KQ1(1)),	RSTART
	* (RC13A(1),A13(1,1,1)),(RC13H(1),HHT(1,1,1))	RSTART
C 14	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)	DIMENB
	DIMENSION IC14(1304)	BUTLER2
	EQUIVALENCE (IC14(1),MXNTI)	RSTART
C 15	COMMON/COMAIN/VAR(240),DER(240),DT,H0,HMAX,HMIN,RSTIME,	RSTART
	* ISTEP,NSTEPS,NDINT,NEQ,IRSIN,IRSOUT	RSTART
	DIMENSION RC15(485),IC15(6)	RSTART
	EQUIVALENCE (RC15(1),VAR(1)),(IC15(1),ISTEP)	RSTART
C 16	COMMON/CDINT/ UU(4),GH(3,4),	RSTART
	* E(3,240),FF(5,240),GG(5,240),Y(5,240),U(5,240),	RSTART
	* H,HPRINT,HS,TPRINT,TSTART,ICNT,IDBL,IFLAG,IDMMY	80386
C	NOTE: FF REPLACES F FROM SUBROUTINE DINT.	RSTART

	DIMENSION RC16(5541),IC16(3)	RSTART
	EQUIVALENCE (RC16(1),UU(1)),(IC16(1),ICNT)	RSTART
C 17	COMMON/DAMPER/ APSDM(3,20),APSDN(3,20),ASD(5,20),MSDM(20),MSDN(20)	RSTART
	DIMENSION RC17(220),IC17(40)	RSTART
	EQUIVALENCE (RC17(1),APSDM(1,1)),(IC17(1),MSDM(1))	RSTART
C 18	COMMON/CEULER/ IEULER(30),HIR(3,3,90),ANG(3,30),ANGD(3,30),	RSTART
	* FE(3,30),TQE(3,30),CONST(5,30)	JDRIFT
	DIMENSION RC18(1320)	JDRIFT
	EQUIVALENCE (RC18(1),HIR(1,1,1))	RSTART
C 19	COMMON/TEMPVI/ CREST,TTI(3),RII(3),R2I(3),JSTOP(4,2,30)	RSTART
	DIMENSION RC19(10),IC19(180)	RSTART
	EQUIVALENCE (RC19(1),CREST),(IC19(1),JSTOP(1,1,1))	RSTART
C 20	COMMON/CYDATA/ CYTD(5),CYPA(5),CYSP(5),CYT0(5),CYV0(5),CYCD(5),	RSTART
	* CYK(5),CYR(5),CYAT(5),CYPV(5),CYCD0(5),CYA0(5),	RSTART
	* CYP0(5),CYSS(5),CYL0(5),CYC(5),CYRH00(5),CYVMAX(5),	RSTART
	* CYORFC(5),CYRHO(5),CYT(5),CYP(5),CYV(5)	RSTART
	DIMENSION RC20A(95),RC20B(20)	RSTART
	EQUIVALENCE (RC20A(1),CYTD(1)),(RC20B(1),CYRHO(1))	RSTART
C 21	COMMON/RSAGE/ XSG(3,20,3),DPMI(3,3,30),LPMI(30),	RSTART
	* NSG(9),MSG(20,9),MCG,MCGIN(24,5),KREF(20,9)	ATBIII
	DIMENSION RC21(450),IC21(520)	TTHKREF
	EQUIVALENCE (RC21(1),XSG(1,1,1)),(IC21(1),LPMI(1))	RSTART
C 22	COMMON/FLXBLE/ HF(4,12,8),B42(3,3,24),V4(3,8),NFLEX(3,8)	RSTART
	DIMENSION RC22(624),IC22(24)	RSTART
	EQUIVALENCE (RC22(1),HF(1,1,1)),(IC22(1),NFLEX(1,1))	RSTART
C 23	COMMON/HRNESS/ BAR(15,100),BB(100),BBDOT(100),PLOSS(2,100),	RSTART
	* XLONG(20),HTIME(2),IBAR(5,100),NL(2,100),	RSTART
	* NPTSPB(20),NPTPLY(20),NTHRNS(20),NBLTPH(5)	RSTART
	DIMENSION RC23(1922),IC23(765)	RSTART
	EQUIVALENCE (RC23(1),BAR(1,1)),(IC23(1),IBAR(1,1))	RSTART
C 24	COMMON/WINDFR/ WTIME(30),QFU(3,5),QFV(3,5),WF(3,30),IWIND(30),	RSTART
	* MWSEG(7,30),NFVSEG(6),NFVNT(5),MOWSEG(30,30)	WINDOP
	DIMENSION RC24(150),IC24(1151)	WINDOP
	EQUIVALENCE (RC24(1),WTIME(1)),(IC24(1),IWIND(1))	WINDOP
C	REAL AOLD4,AAOLD4	RSTART
	DIMENSION COMMON(24),INDEX(3)	RSTART
	DATA COMMON /8HCONTRL ,8HCNTRSF ,8HVPOSTN ,8HSGMNTS ,	RSTART
	* 8HCMATRX ,8HABDATA ,8HTITLES ,8HCNSNTS ,	RSTART
	* 8HDESCRP ,8HJBARTZ ,8HFORCES ,8HINTEST ,	RSTART
	* 8HCSTRNT ,8HTABLES ,8HCOMAIN ,8HCDINT ,	RSTART
	* 8HDAMPER ,8HCEULER ,8HTEMPVI ,8HCYDATA ,	RSTART
	* 8HRSAGE ,8HFLXBLE ,8HHRNESS ,8HWINDFR /	RSTART
	DATA BLANK/8H /	RSTART

	CALL ELTIME(1,25)	RSTART
	GO TO (100,200,300,400,500),IF	RSTART
C		RSTART
C	1. READ INPUT & INITIALIZATION RECORD FROM OLD RESTART TAPE.	RSTART
C		RSTART
	100 READ (IT) IC1, PL, RC3, IC3, NSYM, RC6A, IFULL, XDTE, XCMENI,	RSTART
	* RC7, CGS, JS, RC8, RC9, IC9, IC10, NPANEL, SGTEST,	RSTART
	* RC13, IC13, IC14, DT, H0, HMAX, HMIN, NSTEPS, NDINT,	RSTART
	* RC17, IC17, IEULER, IC19, RC20A, RC21, IC21, HF, IC22,	RSTART
	* RC23, IC23, RC24, IC24	RSTART
	WRITE (6,101) IT,XDTE,XCMENI	RSTART
	101 FORMAT('O INPUT DATA HAS BEEN READ IN FROM UNIT NO.',I4//	RSTART
	* 10X,3A4//10X,20A4/10X,20A4)	RSTART
	GO TO 999	RSTART
C		RSTART
C	2. WRITE INPUT & INITIALIZATION RECORD ONTO NEW RESTART TAPE.	RSTART
C		RSTART
	200 WRITE (IT) IC1, PL, RC3, IC3, NSYM, RC6A, IFULL, DATE, COMENI,	RSTART
	* RC7, CGS, JS, RC8, RC9, IC9, IC10, NPANEL, SGTEST,	RSTART
	* RC13, IC13, IC14, DT, H0, HMAX, HMIN, NSTEPS, NDINT,	RSTART
	* RC17, IC17, IEULER, IC19, RC20A, RC21, IC21, HF, IC22,	RSTART
	* RC23, IC23, RC24, IC24	RSTART
	GO TO 999	RSTART
C		RSTART
C	3. READ TIME POINT RECORD FROM OLD RESTART TAPE.	RSTART
C		RSTART
	300 READ (IT) TIME, BELT, TPTS, BD, RC4, RC5B, RC6B, IFULL, IPIN,	RSTART
	* RC11, IC11, XTEST, SEGT, REGT, RC13H, KQTYPE, TAB,	RSTART
	* VAR, DER, NEQ, RC16, IC16, IEULER, RC18, IC19, RC20B,	RSTART
	* RC21, IC21, V4, RC23, NL, NPTPLY, WTIME, IWIND	RSTART
	CALL OUTPUT(1)	RSTART
	GO TO 999	RSTART
C		RSTART
C	5. WRITE TIME POINT RECORD ONTO NEW RESTART TAPE.	RSTART
C		RSTART
	500 WRITE (IT) TIME, BELT, TPTS, BD, RC4, RC5B, RC6B, IFULL, IPIN,	RSTART
	* RC11, IC11, XTEST, SEGT, REGT, RC13H, KQTYPE, TAB,	RSTART
	* VAR, DER, NEQ, RC16, IC16, IEULER, RC18, IC19, RC20B,	RSTART
	* RC21, IC21, V4, RC23, NL, NPTPLY, WTIME, IWIND	RSTART
	GO TO 999	RSTART
C		RSTART
C	4. READ NEW INPUT DATA FROM INPUT STREAM FOR RESTART.	RSTART
C		RSTART
	400 READ (5,399) AVAR,INDEX,ITYPE,RR,II,AA,RROLD,IIOLD,AAOLD	RSTART
	399 FORMAT(A8,4I4,2(F8.0,I8,A8))	RSTART
	CALL SEARCH(AVAR,INDEX,NCOM,ITEM)	RSTART
	IF (NCOM.LE.0) GO TO 490	RSTART
	IF (NCOM.GT.24) GO TO 999	RSTART
	IF (ITYPE.GT.3) GO TO 490	RSTART
	GO TO ( 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12,	RSTART
	* 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, 24) , NCOM	RSTART
C	COMMON /CONTRL/	RSTART

1	IF (ITEM.GT.1)	GO TO 401	RSTART
	IF (ITYPE.NE.1)	GO TO 490	RSTART
	ROLD - TIME		RSTART
	TIME - RR		RSTART
	GO TO 492		RSTART
401	IF (ITEM.GT.52)	GO TO 490	PAGE
	IF (ITYPE.NE.2)	GO TO 490	RSTART
	IOLD - IC1(ITEM-1)		RSTART
	IC1(ITEM-1) - II		RSTART
	GO TO 494		RSTART
C	COMMON /CNTSRF/		RSTART
2	IF (ITEM.GT.1888)	GO TO 490	EDGE
	IF (ITYPE.NE.1)	GO TO 490	RSTART
	ROLD - RC2(ITEM)		RSTART
	RC2(ITEM) - RR		RSTART
	GO TO 492		RSTART
C	COMMON /VPOSTN/		RSTART
3	IF (ITEM.GT.18084)	GO TO 403	VEHICL
	IF (ITYPE.NE.1)	GO TO 490	RSTART
	ROLD - RC3(ITEM)		RSTART
	RC3(ITEM) - RR		RSTART
	GO TO 492		RSTART
403	IF (ITEM.GT.18096)	GO TO 490	VEHICL
	IF (ITYPE.NE.2)	GO TO 490	RSTART
	IOLD - IC3(ITEM-18084)		VEHICL
	IC3(ITEM-18084) - II		VEHICL
	GO TO 494		RSTART
C	COMMON /SGMNTS/		RSTART
4	IF (ITEM.GT.900 )	GO TO 404	RSTART
	IF (ITYPE.NE.1)	GO TO 490	RSTART
	ROLD - RC4(ITEM)		RSTART
	RC4(ITEM) - RR		RSTART
	GO TO 492		RSTART
404	IF (ITEM.GT.930 )	GO TO 490	RSTART
	IF (ITYPE.NE.2)	GO TO 490	RSTART
	IOLD - NSYM(ITEM-900)		RSTART
	NSYM(ITEM-900) - II		RSTART
	GO TO 494		RSTART
C	COMMON /CMATRX/		RSTART
5	IF (ITEM.GT.1776)	GO TO 490	SLIP
	IF (ITYPE.NE.1)	GO TO 490	RSTART
	ROLD - RC5A(ITEM)		RSTART
	RC5A(ITEM) - RR		RSTART
	GO TO 492		RSTART
C	COMMON /ABDATA/		RSTART
6	IF (ITEM.GT.881 )	GO TO 406	RSTART
	IF (ITYPE.NE.1)	GO TO 490	RSTART
	ROLD - RC6A(ITEM)		RSTART
	RC6A(ITEM) - RR		RSTART
	GO TO 492		RSTART
406	IF (ITEM.GT.887 )	GO TO 490	RSTART
	IF (ITYPE.NE.2)	GO TO 490	RSTART



	IOLD = IFULL(ITEM-881)	RSTART
	IFULL(ITEM-881) = II	RSTART
	GO TO 494	RSTART
C	COMMON /TITLES/ NOTE: NO PROVISION FOR CGS OR JS.	RSTART
7	IF (ITEM.GT.348 ) GO TO 490	RSTART
	IF (ITYPE.NE.3) GO TO 490	RSTART
	AOLD = RC7A(ITEM)	RSTART
	RC7A(ITEM) = AA	RSTART
	GO TO 496	RSTART
C	COMMON /CNSNTS/	RSTART
8	IF (ITEM.GT.35 ) GO TO 490	TWOPI
	IF (ITEM.GT.31 ) GO TO 408	RSTART
	IF (ITEM.LE.28 ) GO TO 408	RSTART
	IF (ITYPE.NE.3) GO TO 490	RSTART
	AOLD = RC8(ITEM)	RSTART
	RC8(ITEM) = AA	RSTART
	GO TO 496	RSTART
408	IF (ITYPE.NE.1) GO TO 490	RSTART
	ROLD = RC8(ITEM)	RSTART
	RC8(ITEM) = RR	RSTART
	GO TO 492	RSTART
C	COMMON /DESCRP/	RSTART
9	IF (ITEM.GT.2460) GO TO 409	SLIP
	IF (ITYPE.NE.1) GO TO 490	RSTART
	ROLD = RC9(ITEM)	RSTART
	RC9(ITEM) = RR	RSTART
	GO TO 492	RSTART
409	IF (ITEM.GT.2610) GO TO 490	SLIP
	IF (ITYPE.NE.2) GO TO 490	RSTART
	IOLD = IC9(ITEM-2460)	SLIP
	IC9(ITEM-2460) = II	SLIPRT
	GO TO 494	RSTART
C	COMMON /JBARTZ/	RSTART
10	IF (ITEM.GT.1614) GO TO 490	RSTART
	IF (ITYPE.NE.2) GO TO 490	RSTART
	IOLD = IC10(ITEM)	RSTART
	IC10(ITEM) = II	RSTART
	GO TO 494	RSTART
C	COMMON /FORCES/	RSTART
11	IF (ITEM.GT.1240) GO TO 411	NCFORC
	IF (ITYPE.NE.1) GO TO 490	RSTART
	ROLD = RC11(ITEM)	RSTART
	RC11(ITEM) = RR	RSTART
	GO TO 492	RSTART
411	IF (ITEM.GT.1249) GO TO 490	NCFORC
	IF (ITYPE.NE.2) GO TO 490	RSTART
	IOLD = IC11(ITEM-1240)	NCFORC
	IC11(ITEM-1240) = II	NCFORC
	GO TO 494	RSTART
C	COMMON /INTEST/	RSTART
12	IF (ITEM.GT.720 ) GO TO 412	RSTART
	IF (ITYPE.NE.1) GO TO 490	RSTART

ROLD = RC12(ITEM)	RSTART
RC12(ITEM) = RR	RSTART
GO TO 492	RSTART
412 IF (ITEM.GT.840 ) GO TO 512	RSTART
IF (ITYPE.NE.3) GO TO 490	RSTART
AOLD = SEGT(ITEM-720)	RSTART
SEGT(ITEM-720) = AA	RSTART
GO TO 496	RSTART
512 IF (ITEM.GT.960 ) GO TO 490	RSTART
IF (ITYPE.NE.3) GO TO 490	RSTART
AOLD = REGT(ITEM-840)	RSTART
REGT(ITEM-840) = AA	RSTART
GO TO 496	RSTART
C COMMON /CSTRNT/	RSTART
13 IF (ITEM.GT.1212) GO TO 413	RSTART
IF (ITYPE.NE.1) GO TO 490	RSTART
ROLD = RC13A(ITEM)	RSTART
RC13A(ITEM) = RR	RSTART
GO TO 492	RSTART
413 IF (ITEM.GT.1248) GO TO 490	RSTART
IF (ITYPE.NE.2) GO TO 490	RSTART
IOLD = IC13(ITEM-1212)	RSTART
IC13(ITEM-1212) = II	RSTART
GO TO 494	RSTART
C COMMON /TABLES/	RSTART
14 IF (ITEM.GT.1304 ) GO TO 414	RSTART
IF (ITYPE.NE.2) GO TO 490	BUTLER2
IOLD = IC14(ITEM)	RSTART
IC14(ITEM) = II	RSTART
GO TO 494	RSTART
414 IF (ITEM.GT.5804) GO TO 490	RSTART
IF (ITYPE.NE.1) GO TO 490	MISC
ROLD = TAB(ITEM-1304)	RSTART
TAB(ITEM-1304) = RR	BUTLER2
GO TO 492	BUTLER2
C COMMON /COMAIN/	RSTART
15 IF (ITEM.GT.485 ) GO TO 415	RSTART
IF (ITYPE.NE.1) GO TO 490	RSTART
ROLD = RC15(ITEM)	RSTART
RC15(ITEM) = RR	RSTART
GO TO 492	RSTART
415 IF (ITEM.GT.491 ) GO TO 490	RSTART
IF (ITYPE.NE.2) GO TO 490	RSTART
IOLD = IC15(ITEM-485)	RSTART
IC15(ITEM-485) = II	RSTART
GO TO 494	RSTART
C COMMON /CDINT /	RSTART
16 IF (ITEM.GT.5541) GO TO 416	RSTART
IF (ITYPE.NE.1) GO TO 490	RSTART
ROLD = RC16(ITEM)	RSTART
RC16(ITEM) = RR	RSTART
GO TO 492	RSTART

416	IF (ITEM.GT.5544) GO TO 490	RSTART
	IF (ITYPE.NE.2) GO TO 490	RSTART
	IOLD = IC16(ITEM-5541)	RSTART
	IC16(ITEM-5541) = II	RSTART
	GO TO 494	RSTART
C	COMMON /DAMPER/	RSTART
17	IF (ITEM.GT.220 ) GO TO 417	RSTART
	IF (ITYPE.NE.1) GO TO 490	RSTART
	ROLD = RC17(ITEM)	RSTART
	RC17(ITEM) = RR	RSTART
	GO TO 492	RSTART
417	IF (ITEM.GT.260 ) GO TO 490	RSTART
	IF (ITYPE.NE.2) GO TO 490	RSTART
	IOLD = IC17(ITEM-220)	RSTART
	IC17(ITEM-220) = II	RSTART
	GO TO 494	RSTART
C	COMMON /CEULER/	RSTART
18	IF (ITEM.GT.30 ) GO TO 418	RSTART
	IF (ITYPE.NE.2) GO TO 490	RSTART
	IOLD = IEULER(ITEM)	RSTART
	IEULER(ITEM) = II	RSTART
	GO TO 494	RSTART
418	IF (ITEM.GT.1350) GO TO 490	JDRIFT
	IF (ITYPE.NE.1) GO TO 490	RSTART
	ROLD = RC18(ITEM-30)	RSTART
	RC18(ITEM-30) = RR	RSTART
	GO TO 492	RSTART
C	COMMON /TEMPVI/	RSTART
19	IF (ITEM.GT.10 ) GO TO 419	RSTART
	IF (ITYPE.NE.1) GO TO 490	RSTART
	ROLD = RC19(ITEM)	RSTART
	RC19(ITEM) = RR	RSTART
	GO TO 492	RSTART
419	IF (ITEM.GT.190 ) GO TO 490	RSTART
	IF (ITYPE.NE.2) GO TO 490	RSTART
	IOLD = IC19(ITEM-10)	RSTART
	IC19(ITEM-10) = II	RSTART
	GO TO 494	RSTART
C	COMMON /CYDATA/	RSTART
20	IF (ITEM.GT.115 ) GO TO 490	RSTART
	IF (ITYPE.NE.1) GO TO 490	RSTART
	ROLD = RC20A(ITEM)	RSTART
	RC20A(ITEM) = RR	RSTART
	GO TO 492	RSTART
C	COMMON /RSAGE/	RSTART
21	IF (ITEM.GT.450 ) GO TO 421	RSTART
	IF (ITYPE.NE.1 ) GO TO 490	RSTART
	ROLD = RC21(ITEM)	RSTART
	RC21(ITEM) = RR	RSTART
	GO TO 492	RSTART
421	IF (ITEM.GT.970 ) GO TO 490	TTHKREF
	IF (ITYPE.NE.2 ) GO TO 490	RSTART

IOLD = IC21(ITEM-450)	RSTART
IC21(ITEM-450) = II	RSTART
GO TO 494	RSTART
C COMMON /FLXBLE/	RSTART
22 IF (ITEM.GT.624 ) GO TO 422	RSTART
IF (ITYPE.NE.1 ) GO TO 490	RSTART
ROLD = RC22(ITEM)	RSTART
RC22(ITEM) = RR	RSTART
GO TO 492	RSTART
422 IF (ITEM.GT.648 ) GO TO 490	RSTART
IF (ITYPE.NE.2 ) GO TO 490	RSTART
IOLD = IC22(ITEM-624)	RSTART
IC22(ITEM-624) = II	RSTART
GO TO 494	RSTART
C COMMON /HRNESS/	RSTART
23 IF (ITEM.GT.1922) GO TO 423	RSTART
IF (ITYPE.NE.1) GO TO 490	RSTART
ROLD = RC23(ITEM)	RSTART
RC23(ITEM) = RR	RSTART
GO TO 492	RSTART
423 IF (ITEM.GT.2687) GO TO 490	RSTART
IF (ITYPE.NE.2) GO TO 490	RSTART
IOLD = IC23(ITEM-1922)	RSTART
IC23(ITEM-1922) = II	RSTART
GO TO 494	RSTART
C COMMON /WINDFR/	RSTART
24 IF (ITEM.GT.150 ) GO TO 424	WINDOP
IF (ITYPE.NE.1) GO TO 490	RSTART
ROLD = RC24(ITEM)	RSTART
RC24(ITEM) = RR	RSTART
GO TO 492	RSTART
424 IF (ITEM.GT.1301) GO TO 490	WINDOP
IF (ITYPE.NE.2) GO TO 490	RSTART
IOLD = IC24(ITEM-150)	WINDOP
IC24(ITEM-150) = II	WINDOP
GO TO 494	RSTAi
C	RSTART
C ERROR MESSAGE - TERMINATE PROGRAM.	RSTART
C	RSTART
490 WRITE (6,491) AVAR,INDEX,NCOM,ITEM,ITYPE,RR,II,AA	RSTART
491 FORMAT('0 SUBROUTINE RSTART INPUT ERROR'//	RSTART
* ' AVAR= ',A8,' INDEX= ',3I6,' NCOM= ',I6,' ITEM= ',I6,	RSTART
* ' ITYPE= ',I6,' RR= ',G15.8,' II= ',I8,' AA= ',A8//	RSTART
* ' PROGRAM IS BEING TERMINATED.')	RSTART
STOP 2	RSTART
C	RSTART
C PRINT MESSAGE FOR REAL VARIABLES.	RSTART
C	RSTART
492 WRITE (6,493) AVAR,INDEX,COMMON(NCOM),ROLD,RR	RSTART
493 FORMAT('0',A6,'(',I4,',',I4,',',I4,') OF COMMON/',A6,'/',	RSTART
* ' HAS BEEN CHANGED FROM ',G15.8,' TO ',G15.8)	RSTART
IF (RROLD.EQ.0.0) GO TO 400	RSTART

IF (DABS(RROLD-ROLD).LE.0.00001*RROLD) GO TO 400	RSTART
WRITE (6,383) RROLD	RSTART
383 FORMAT(' INPUT VALUE FOR RROLD WAS ',G15.8//)	RSTART
GO TO 490	RSTART
C	RSTART
C PRINT MESSAGE FOR INTEGER VARIABLES.	RSTART
C	RSTART
494 WRITE (6,495) AVAR,INDEX,COMMON(NCOM),IOLD,II	RSTART
495 FORMAT('0',A6,'(',I4,',',I4,',',I4,') OF COMMON',A6,'/',	RSTART
* ' HAS BEEN CHANGED FROM ', I8,' TO ', I8)	RSTART
IF (IIOLD.EQ.0) GO TO 400	RSTART
IF (IOLD.EQ.IIOLD) GO TO 400	RSTART
WRITE (6,385) IIOLD	RSTART
385 FORMAT(' INPUT VALUE FOR IIOLD WAS ',I8//)	RSTART
GO TO 490	RSTART
C	RSTART
C PRINT MESSAGE FOR ALPHANUMERIC VARIABLES.	RSTART
C	RSTART
496 WRITE (6,497) AVAR,INDEX,COMMON(NCOM),AOLD,AA	RSTART
497 FORMAT('0',A6,'(',I4,',',I4,',',I4,') OF COMMON',A6,'/',	RSTART
* ' HAS BEEN CHANGED FROM ', A8,' TO ', A8)	RSTART
IF (AAOLD.EQ.BLANK) GO TO 400	RSTART
AAOLD4 = AAOLD	RSTART
AOLD4 = AOLD	RSTART
IF (AOLD4.EQ.AAOLD4) GO TO 400	RSTART
WRITE (6,387) AAOLD	RSTART
387 FORMAT(' INPUT VALUE FOR AAOLD WAS ',A8//)	RSTART
GO TO 490	RSTART
999 CALL ELTIME(2,25)	RSTART
RETURN	RSTART
END	RSTART

	SUBROUTINE SEARCH(AVAR,INDEX,NCOM,ITEM)		SEARCH
		REV IV 07/24/86	SLIP
C	CALL BY SUBROUTINE RSTART TO COMPUTE NCOM & ITEM FROM AVAR &		SEARCH
C	INDEX. RETURNS NCOM=0 FOR ERROR AND NCOM=50 FOR BLANK.		SEARCH
C			SEARCH
	IMPLICIT REAL*8(A-H,O-Z)		SEARCH
	DIMENSION BVAR(264),KOUNT(25),NDIM(3,264),NJ(3),NK(3),INDEX(3)		SLIP
	DIMENSION C1 ( 17) , NC1 ( 51)		PAGE
	DIMENSION C2 ( 4) , NC2 ( 12)		SEARCH
	DIMENSION C3 ( 10) , NC3 ( 30)		SEARCH
	DIMENSION C4 ( 9) , NC4 ( 27)		SEARCH
	DIMENSION C5 ( 9) , NC5 ( 27)		SLIP
	DIMENSION C6 ( 30) , NC6 ( 90)		SEARCH
	DIMENSION C7 ( 11) , NC7 ( 33)		SEARCH
	DIMENSION C8 ( 10) , NC8 ( 30)		TWOPI
	DIMENSION C9 ( 15) , NC9 ( 45)		SEARCH
	DIMENSION C10( 11) , NC10( 33)		SEARCH
	DIMENSION C11( 10) , NC11( 30)		SEARCH
	DIMENSION C12( 4) , NC12( 12)		SEARCH
	DIMENSION C13( 16) , NC13( 48)		SEARCH
	DIMENSION C14( 7) , NC14( 21)		SEARCH
	DIMENSION C15( 13) , NC15( 39)		SEARCH
	DIMENSION C16( 15) , NC16( 45)		SEARCH
	DIMENSION C17( 5) , NC17( 15)		SEARCH
	DIMENSION C18( 7) , NC18( 21)		SEARCH
	DIMENSION C19( 5) , NC19( 15)		SEARCH
	DIMENSION C20( 23) , NC20( 69)		SEARCH
	DIMENSION C21( 8) , NC21( 24)		CHGIII
	DIMENSION C22( 4) , NC22( 12)		SEARCH
	DIMENSION C23( 12) , NC23( 36)		SEARCH
	DIMENSION C24( 9) , NC24( 27)		WINDOP
C			SEARCH
	EQUIVALENCE (C1 (1),BVAR( 1)) , (NC1 (1),NDIM(1, 1))		SEARCH
	EQUIVALENCE (C2 (1),BVAR( 18)) , (NC2 (1),NDIM(1, 18))		PAGE
	EQUIVALENCE (C3 (1),BVAR( 22)) , (NC3 (1),NDIM(1, 22))		PAGE
	EQUIVALENCE (C4 (1),BVAR( 32)) , (NC4 (1),NDIM(1, 32))		PAGE
	EQUIVALENCE (C5 (1),BVAR( 41)) , (NC5 (1),NDIM(1, 41))		PAGE
	EQUIVALENCE (C6 (1),BVAR( 50)) , (NC6 (1),NDIM(1, 50))		SLIP
	EQUIVALENCE (C7 (1),BVAR( 80)) , (NC7 (1),NDIM(1, 80))		SLIP
	EQUIVALENCE (C8 (1),BVAR( 91)) , (NC8 (1),NDIM(1, 91))		SLIP
	EQUIVALENCE (C9 (1),BVAR(101)) , (NC9 (1),NDIM(1,101))		SLIP
	EQUIVALENCE (C10(1),BVAR(116)) , (NC10(1),NDIM(1,116))		SLIP
	EQUIVALENCE (C11(1),BVAR(127)) , (NC11(1),NDIM(1,127))		SLIP
	EQUIVALENCE (C12(1),BVAR(137)) , (NC12(1),NDIM(1,137))		SLIP
	EQUIVALENCE (C13(1),BVAR(141)) , (NC13(1),NDIM(1,141))		SLIP
	EQUIVALENCE (C14(1),BVAR(157)) , (NC14(1),NDIM(1,157))		SLIP
	EQUIVALENCE (C15(1),BVAR(164)) , (NC15(1),NDIM(1,164))		SLIP
	EQUIVALENCE (C16(1),BVAR(177)) , (NC16(1),NDIM(1,177))		SLIP
	EQUIVALENCE (C17(1),BVAR(192)) , (NC17(1),NDIM(1,192))		SLIP
	EQUIVALENCE (C18(1),BVAR(197)) , (NC18(1),NDIM(1,197))		SLIP
	EQUIVALENCE (C19(1),BVAR(204)) , (NC19(1),NDIM(1,204))		SLIP
	EQUIVALENCE (C20(1),BVAR(209)) , (NC20(1),NDIM(1,209))		SLIP

	EQUIVALENCE (C21(1),BVAR(232)) , (NC21(1),NDIM(1,232))	SLIP
	EQUIVALENCE (C22(1),BVAR(240)) , (NC22(1),NDIM(1,240))	SLIP
	EQUIVALENCE (C23(1),BVAR(244)) , (NC23(1),NDIM(1,244))	SLIP
	EQUIVALENCE (C24(1),BVAR(256)) , (NC24(1),NDIM(1,256))	SLIP
C		SEARCH
	DATA NVAR/264/ , KOM/24/ , BLANK/8H /	SLIP
	DATA KOUNT/1,18,22,32,41,50,80,91,101,116,127,137,141,157,	SLIP
	* 164,177,192,197,204,209,232,240,244,256,265/	SLIP
C		SEARCH
C	1 COMMON/CONTRL/	SEARCH
C		SEARCH
	DATA C1 / 8HTIME ,8HNSEG ,8HNJNT ,8HNPL ,8HNBLT ,	SEARCH
	* 8HNBAG ,8HNVEH ,8HNGRND ,8HNS ,8HNQ ,	SEARCH
	* 8HNSD ,8HNFLX ,8HNNRNS ,8HNWINDF ,8HNJNTF ,	SEARCH
	* 8HNPRT ,8HNPG /	PAGE
	DATA NC1 / 0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 ,	SEARCH
	* 0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 ,	SEARCH
	* 0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 ,	SEARCH
	* 36,0,0 , 0,0,0 /	PAGE
C		SEARCH
C	2 COMMON/CNTRSF/	SEARCH
C		SEARCH
	DATA C2 / 8HPL ,8HBELT ,8HTPTS ,8HBD /	SEARCH
	DATA NC2 / 24,30,0 , 20,8,0 , 6,8,0 , 24,40,0 /	EDGE
C		SEARCH
C	3 COMMON/VPOSTN/	SEARCH
C		SEARCH
	DATA C3 / 8HZPLT ,8HSPLT ,8HAXV ,8HVATAB ,8HVTO ,	SEARCH
	* 8HVDI ,8HTIMEV ,8HOMEGV ,8HNVTAB ,8HINDXV /	SEARCH
	DATA NC3 / 3,0,0 , 3,0,0 , 3,6,0 , 6,501,6 , 6,0,0 ,	VEHICL
	* 6,0,0 , 6,0,0 , 6,0,0 , 6,0,0 , 6,0,0 /	SEARCH
C		SEARCH
C	4 COMMON/SGMNTS/	SEARCH
C		SEARCH
	DATA C4 / 8HD ,8HWMEG ,8HWMEGD ,8HU1 ,8HU2 ,	SEARCH
	* 8HSEGLP ,8HSEGLV ,8HSEGLA ,8HNSYM /	SEARCH
	DATA NC4 / 3,3,30 , 3,30,0 , 3,30,0 , 3,30,0 , 3,30,0 ,	SEARCH
	* 3,30,0 , 3,30,0 , 3,30,0 , 30,0,0 /	SEARCH
C		SEARCH
C	5 COMMON/CMATRX/	SEARCH
C		SEARCH
	DATA C5 / 8HV1 ,8HV2 ,8HV3 ,8HB12 ,8HA22 ,	SEARCH
	* 8HF ,8HTQ ,8HWJ ,8HA11 /	SLIP
	DATA NC5 / 3,30,0 , 3,30,0 , 3,12,0 , 3,3,60 , 3,3,60 ,	SEARCH
	* 3,30,0 , 3,30,0 , 30,0,0 , 3,3,60 /	SLIP
C		SEARCH
C	6 COMMON/ABDATA/	SEARCH
C		SEARCH
	DATA C6 / 8HZDEP ,8HDBR ,8HDPVCTR ,8HDEPLOY ,8HAB ,	SEARCH
	* 8HB ,8HZR ,8HBF ,8HDBR ,8HVBAGG ,	SEARCH
	* 8HVSCS ,8HSPRK ,8HCK ,8HCMASS ,8HCYMIN ,	SEARCH
	* 8HCYMOUT ,8HBAGPV ,8HPD ,8HVBAG ,8HVOLBP ,	SEARCH

	*	8HPCYV	,8HPCYMIN	,8HPVBAG	,8HTV1	,8HTV2	, SEARCH
	*	8H SWITCH	,8HPYMOUT	,8HSCALE	,8HPREVT	,8HIFULL	/ SEARCH
	DATA NC6 /	3,5,0	, 3,3,5	, 3,5,0	, 3,5,0	, 3,5,0	, SEARCH
	*	9,4,5	, 3,4,5	, 3,4,5	, 9,4,5	, 5,0,0	, SEARCH
	*	5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	, SEARCH
	*	5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	, SEARCH
	*	5,0,0	, 5,0,0	, 5,0,0	, 3,4,5	, 3,10,5	, SEARCH
	*	5,0,0	, 5,0,0	, 5,0,0	, 0,0,0	, 6,0,0	/ SEARCH
C							SEARCH
C	7	COMMON/TITLES/					
C							SEARCH
	DATA C7 /	8HDATE	,8HCOMMENT	,8HVPSTTL	,8HBDYTTL	,8HBLTTTL	, SEARCH
	*	8HPLTTL	,8HBAGTTL	,8HSEG	,8HJOINT	,8HCGS	, SEARCH
	*	8HJS	/				SEARCH
	DATA NC7 /	3,0,0	, 40,0,0	, 20,0,0	, 5,0,0	, 5,8,0	, SEARCH
	*	5,30,0	, 5,6,0	, 30,0,0	, 30,0,0	, 30,0,0	, SEARCH
	*	30,0,0	/				SEARCH
C							SEARCH
C	8	COMMON/CNSNTS/					
C							SEARCH
	DATA C8 /	8HPI	,8HRADIAN	,8HG	,8HTHIRD	,8HEPS	, SEARCH
	*	8HUNITL	,8HUNITM	,8HUNITT	,8HGRAVITY	,8HTWOPI	/ TWOPI
	DATA NC8 /	0,0,0	, 0,0,0	, 0,0,0	, 0,0,0	, 24,0,0	, SEARCH
	*	0,0,0	, 0,0,0	, 0,0,0	, 3,0,0	, 0,0,0	/ TWOPI
C							SEARCH
C	9	COMMON/DESCRP/					
C							SEARCH
	DATA C9 /	8HPI	,8HW	,8HRW	,8HSR	,8HHA	, SEARCH
	*	8HNB	,8HRPHI	,8HHT	,8HSPRING	,8HVISC	, SEARCH
	*	8HJNT	,8HJPIN	,8HJSING	,8HJGLOB	,8HJOINTF	/ SEARCH
	DATA NC9 /	3,30,0	, 30,0,0	, 30,0,0	, 4,60,0	, 3,60,0	, SLIP
	*	3,60,0	, 3,30,0	, 3,3,60	, 5,90,0	, 7,90,0	, SEARCH
	*	30,0,0	, 30,0,0	, 30,0,0	, 30,0,0	, 30,0,0	/ SEARCH
C							SEARCH
C	10	COMMON/JBARTZ/					
C							SEARCH
	DATA C10/	8HMNPL	,8HMNBTL	,8HMNSEG	,8HMNBAG	,8HMPL	, SEARCH
	*	8HMBLT	,8HMSEG	,8HMBAG	,8HNTPL	,8HNTBLT	, SEARCH
	*	8HNTSEG	/				SEARCH
	DATA NC10/	30,0,0	, 8,0,0	, 30,0,0	, 6,0,0	, 3,5,30	, SEARCH
	*	3,5,8	, 3,5,30	, 3,10,6	, 5,30,0	, 5,8,0	, SEARCH
	*	5,30,0	/				SEARCH
C							SEARCH
C	11	COMMON/FORCES/					
C							SEARCH
	DATA C11/	8HPSF	,8HBSF	,8HSSF	,8HBAGSF	,8HPRJNT	, SEARCH
	*	8HNPANEL	,8HNPSF	,8HNBFSF	,8HNSSF	,8HNBGSF	/ SEARCH
	DATA NC11/	7,70,0	, 4,20,0	, 10,40,0	, 3,20,0	, 7,30,0	, NCFORC
	*	5,0,0	, 0,0,0	, 0,0,0	, 0,0,0	, 0,0,0	/ SEARCH
C							SEARCH
C	12	COMMON/INTEST/					
C							SEARCH



	DATA C12/ 8HSGTEST	,8HXTST	,8HSEGT	,8HRECT	/	SEARCH
	DATA NC12/ 3,4,30	, 3,120,0	, 120,0,0	, 120,0,0	/	SEARCH
C						SEARCH
C 13	COMMON/CSTRNT/					SEARCH
C						SEARCH
	DATA C13/ 8HA13	,8HA23	,8HB31	,8HB32	,8HHHT	SEARCH
*	8HRK1	,8HRK2	,8HQ	,8HTQQ	,8HRQQ	SEARCH
*	8HHQQ	,8HSQQ	,8HCFQQ	,8HKQ1	,8HKQ2	SEARCH
*	8HKQTYPE	/				SEARCH
	DATA NC13/ 3,3,24	, 3,3,24	, 3,3,24	, 3,3,24	, 3,3,12	SEARCH
*	3,12,0	, 3,12,0	, 3,12,0	, 3,12,0	, 3,12,0	SEARCH
*	3,12,0	, 12,0,0	, 12,0,0	, 12,0,0	, 12,0,0	SEARCH
*	12,0,0	/				SEARCH
C						SEARCH
C 14	COMMON/TABLES/					SEARCH
C						SEARCH
	DATA C14/ 8HMXNTI	,8HMXNTB	,8HMXTB1	,8HMXTB2	,8HNTI	SEARCH
*	8HNTAB	,8HTAB	/			SEARCH
	DATA NC14/ 0,0,0	, 0,0,0	, 0,0,0	, 0,0,0	, 50,0,0	SEARCH
*	1250,0,0	, 4500,0,0/				BUTLER2
C						SEARCH
C 15	COMMON/COMAIN/					SEARCH
C						SEARCH
	DATA C15/ 8HVAR	,8HDER	,8HDT	,8HHO	,8HHMAX	SEARCH
*	8HHMIN	,8HRSTIME	,8HISTEP	,8HNSTEPS	,8HNDINT	SEARCH
*	8HNEQ	,8HIRSIN	,8HIRSOUT	/		SEARCH
	DATA NC15/ 240,0,0	, 240,0,0	, 0,0,0	, 0,0,0	, 0,0,0	SEARCH
*	0,0,0	, 0,0,0	, 0,0,0	, 0,0,0	, 0,0,0	SEARCH
*	0,0,0	, 0,0,0	, 0,0,0	/		SEARCH
C						SEARCH
C 16	COMMON/CDINT /					SEARCH
C						SEARCH
	DATA C16/ 8HUU	,8HGH	,8HE	,8HFF	,8HGG	SEARCH
*	8HY	,8HU	,8HH	,8HHPRINT	,8HHS	SEARCH
*	8HTPRINT	,8HTSTART	,8HICNT	,8HIDBL	,8HIFLAG	SEARCH
	DATA NC16/ 4,0,0	, 3,4,0	, 3,240,0	, 5,240,0	, 5,240,0	SEARCH
*	5,240,0	, 5,240,0	, 0,0,0	, 0,0,0	, 0,0,0	SEARCH
*	0,0,0	, 0,0,0	, 0,0,0	, 0,0,0	, 0,0,0	SEARCH
C						SEARCH
C 17	COMMON/DAMPER/					SEARCH
C						SEARCH
	DATA C17/ 8HAPSDM	,8HAPSDN	,8HASD	,8HMSDM	,8HMSDN	SEARCH
	DATA NC17/ 3,20,0	, 3,20,0	, 5,20,0	, 20,0,0	, 20,0,0	SEARCH
C						SEARCH
C 18	COMMON/CEULER/					SEARCH
C						SEARCH
	DATA C18/ 8HIEULER	,8HHIR	,8HANG	,8HANGD	,8HFE	SEARCH
*	8HTQE	,8HCONST	/			SEARCH
	DATA NC18/ 30,0,0	, 3,3,90	, 3,30,0	, 3,30,0	, 3,30,0	JDRIFT
*	3,30,0	, 5,30,0	/			JDRIFT
C						SEARCH
C 19	COMMON/TEMPVI/					SEARCH

C	DATA C19/ 8HCREST	,8HTTI	,8HR1I	,8HR2I	,8HJSTOP	SEARCH
	DATA NC19/ 0,0,0	, 3,0,0	, 3,0,0	, 3,0,0	, 4,2,30	/ SEARCH
C						SEARCH
C 20	COMMON/CYDATA/					SEARCH
C	DATA C20/ 8HCYTD	,8HCYPA	,8HCYSP	,8HCYTO	,8HCYVO	SEARCH
*	8HCYCD	,8HCYK	,8HCYR	,8HCYAT	,8HCYPV	SEARCH
*	8HCYCD0	,8HCYAO	,8HCYPO	,8HCYSS	,8HCYLO	SEARCH
*	8HCYC	,8HCYRHO0	,8HCYVMAX	,8HCYORFC	,8HCYRHO	SEARCH
*	8HCYT	,8HCYRHP	,8HCYV	/		SEARCH
	DATA NC20/ 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	SEARCH
*	5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	SEARCH
*	5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	SEARCH
*	5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	SEARCH
±	5,0,0	, 5,0,0	, 5,0,0	/		SEARCH
C						SEARCH
C 21	COMMON/RSAGE/					SEARCH
C	DATA C21/ 8HXSG	,8HDPMI	,8HLPMI	,8HNSG	,8HMSG	SEARCH
*	8HMC	,8HMCIN	,8HKREF	/		CHGIII
	DATA NC21/ 3,20,3	, 3,3,30	, 30,0,0	, 9,0,0	, 20,9,0	WINDOP
*	1,0,0	, 24,5,0	, 20,9,0	/		TTHKREF
C						SEARCH
C 22	COMMON/FLXBLE/					SEARCH
C	DATA C22/ 8HHF	,8HB42	,8HV4	,8HNFLEX	/	SEARCH
	DATA NC22/ 4,12,8	, 3,3,24	, 3,8,0	, 3,8,0	/	SEARCH
C						SEARCH
C 23	COMMON/HRNESS/					SEARCH
C	DATA C23/ 8HBBAR	,8HBB	,8HBBDO	,8HPLOSS	,8HXLONG	SEARCH
*	8HHTIME	,8HIBAR	,8HNL	,8HNPTSPB	,8HNPTPLY	SEARCH
*	8HNTHRNS	,8HNBTPH	/			SEARCH
	DATA NC23/ 15,100,0	, 100,0,0	, 100,0,0	, 2,100,0	, 20,0,0	SEARCH
*	2,0,0	, 5,100,0	, 2,100,0	, 20,0,0	, 20,0,0	SEARCH
*	20,0,0	, 5,0,0	/			SEARCH
C						SEARCH
C 24	COMMON/WINDFR/					SEARCH
	DATA C24/ 8HWTIME	,8HQFU	,8HQFV	,8HWF	,8HIWIND	WINDOP
*	8HMWSEG	,8HNFVSEG	,8HNFVNT	,8HMOWSEG	/	WINDOP
	DATA NC24/ 30,0,0	, 3, 5,0	, 3, 5,0	, 3,30,0	, 30,0,0	WINDOP
*	7,30,0	, 6,0,0	, 5,0,0	, 30,30,0	/	WINDOP
	NCOM = 50					SEARCH
	IF (AVAR.EQ.BLANK) GO TO 99					SEARCH
C						SEARCH
C	SEARCH FOR VARIABLE NO. IV.					SEARCH
C						SEARCH
	NCOM = 0					SEARCH
	DO 10 IV=1,NVAR					SEARCH
	IF (AVAR.EQ.BVAR(IV)) GO TO 12					SEARCH
	10 CONTINUE					SEARCH

	GO TO 99	
C		SEARCH
C	SEARCH FOR COMMON NO. IC.	SEARCH
C		SEARCH
	12 DO 20 IC=1,KOM	SEARCH
	IF (IV.GE.KOUNT(IC).AND.IV.LT.KOUNT(IC+1)) GO TO 22	SEARCH
	20 CONTINUE	SEARCH
	GO TO 99	SEARCH
C		SEARCH
C	COMPUTE ITEM NO. FOR VARIABLE IV IN COMMON IC.	SEARCH
C		SEARCH
	22 K1 = KOUNT(IC)	SEARCH
	K2 = IV-1	SEARCH
	ITEM = 1	SEARCH
	IF (K1.EQ.IV) GO TO 25	SEARCH
	DO 24 K=K1,K2	SEARCH
	NI = 1	SEARCH
	DO 23 I=1,3	SEARCH
	IF (NDIM(I,K).NE.0) NI=NI*NDIM(I,K)	SEARCH
	23 CONTINUE	SEARCH
	24 ITEM = ITEM+NI	SEARCH
	25 DO 26 I=1,3	SEARCH
	IF (INDEX(I).EQ.0 .AND. NDIM(I,IV).NE.0) GO TO 99	SEARCH
	IF (NDIM(I,IV).EQ.0 .AND. INDEX(I).GT.1) GO TO 99	SEARCH
	NJ(I) = MAX0(INDEX(I)-1,0)	SEARCH
	NK(I) = MAX0(NDIM(I,IV),1)	SEARCH
	IF (NJ(I).GE.NK(I)) GO TO 99	SEARCH
	26 CONTINUE	SEARCH
	ITEM = ITEM+NJ(1)+NJ(2)*NK(1)+NJ(3)*NK(2)*NK(1)	SEARCH
	NCOM = IC	SEARCH
	99 RETURN	SEARCH
	END	SEARCH

	SUBROUTINE SEGSEG(M,MM,N,NS,NT)		SEGSEG
C	IMPLICIT REAL*8(A-H,O-Z)	REV IV 02/07/87HYPER	
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)		SEGSEG
	COMMON/CNTRSF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)		EDGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),		SEGSEG
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		SEGSEG
	COMMON/FORCES/PSF(7,70),BSF(4,20),SSF(10,40),BAGSF(3,20),		NCFORC
*	PRJNT(7,30),NPANEL(5),NPSF,NBSF,NSSF,NBGSF		SEGSEG
	COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24),		SEGSEG
*	HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12),		SEGSEG
*	RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12),		SEGSEG
*	KQ1(12),KQ2(12),KQTYPE(12)		SEGSEG
	COMMON/RSAGE/ XSG(3,20,3),DPMI(3,3,30),LPMI(30),		TGMOD7
*	NSG(9),MSG(20,9),MCG,MCGIN(24,5),KREF(20,9)		TGMOD7
	COMMON/TEMPVS/DMNT(3,3),TEMP(3,3),B(3,3),XMN(3),RLN(3),XMM(3),		SEGSEG
*	TM(3),R(3),RM(3),DMNWN(3),RLM(3),RN(3),VMN(3),VR(3),		SEGSEG
*	WNM(3),WCM(3),WCN(3),VREL(3),FFM(3),FR(3),TQM(3),		SEGSEG
*	TQN(3),TQNT(3),T(3),H(3),T1(3),T2(3),RMD(3),RND(3),		SEGSEG
*	TD(3),TT4(3,4),TT5(3,4),T3(3),T4(3),P,AMR,FM,CF,		SEGSEG
*	VRM,VRT,VRTS,VRTST,TF,ELOSS,MCF,NCF,T5(3),T6(3)		TGMOD7
*	,DDMY(34958)		80386
	CALL ELTIME(1,23)		SEGSEG
C			EDGE
C	COMPUTATIONS ARE DONE IN M'S REFERENCE SYSTEM		EDGE
	NN = IABS(NS)		SEGSEG
	CALL DOT33(D(1,1,M),D(1,1,N),DMNT)		SEGSEG
	DO 10 I = 1,3		SEGSEG
10	XMN(I) = SEGLP(I,M) - SEGLP(I,N)		SEGSEG
	CALL MAT31(D(1,1,M),XMN,XMM)		SEGSEG
	J = 3		HYPER
	IF(BD(1,NN).LT.0.0)J = 4		HYPER
	CALL MAT31(DMNT,BD(J+1,NN),RLN)		HYPER
	J = 3		HYPER
	IF(BD(1,MM).LT.0.0)J = 4		HYPER
	DO 15 I = 1,3		EDGE
	J = J + 1		HYPER
15	R(I) = RLN(I) - XMM(I) - BD(J,MM)		HYPER
	LT = NTAB(NT)		SEGSEG
	TB = 1.0		EDGE
	IF((BD(1,MM).GT.0.0).AND.(BD(1,NN).GT.0.0))GO TO 20		HYPER
C NEW	HYPERELLIPSOID - AT LEAST ONE SURFACE IS A HYPERELLIPSOID		HYPER
	IF (BD(1,MM).LT.0.0.AND.BD(23,MM).NE.0.0) STOP 23		HYPER
	IF (BD(1,NN).LT.0.0.AND.BD(23,NN).NE.0.0) STOP 23		HYPER
C A	HYPERELLIPSOID MUST HAVE IDENTICAL POWERS.		HYPER
C	IF(NS.LT.0) STOP - INTERIOR INTERSECTION NOT OPERATIONAL		HYPER
	IF(NS.LT.0) STOP 38		HYPER
	IF(TAB(LT+23).LE.1.0) CALL HYEST(BD(1,MM),BD(1,NN),TAB(LT+22))		HYPER
	IF(TAB(LT+23).GT.1.0) CALL HYNTR(BD(1,MM),BD(1,NN),TAB(LT+22))		HYPER
	BET = TAB(LT+23)		HYPER
	IF(BET.GT.1.0)TB = 1.0/BET		HYPER
	GO TO 25		HYPER

C	OLD ELLIPSOIDS	HYPER
	20 IF(NS.LT.0.0)TB = -TB	HYPER
	CALL DOTT33(BD(7,NN),DMNT,TEMP)	EDGE
	CALL MAT33(DMNT,TEMP,B)	EDGE
	CALL INTERS(BD(7,MM),B,R,TB,RM,TAB(LT+22),TM)	SEGSEG
C	A B R Z C AZ	EDGE
C	INTERS SOLVES (CA + B)Z = BR, TB = SQRT(Z.AZ)	EDGE
C		EDGE
	25 MCF = NTAB(NT+1)	HYPER
	NCF = -MCF	SEGSEG
	IF(NCF.GT.0)CFQQ(NCF) = -999.	SEGSEG
C		EDGE
C	CHECK FOR INTERSECTION	EDGE
C		EDGE
	IF(TB.GE.1.0)GO TO 75	HYPER
	S1 = 0.0	SEGSEG
	S2 = 0.0	SEGSEG
	DO 30 I = 1,3	HYPER
	RI = R(I)	SEGSEG
	IF(NS.LT.0)RI = RM(I) + TB*(RM(I) - R(I))	SEGSEG
	S1 = S1 + RI**2	SEGSEG
30	S2 = S2 + TM(I)**2	HYPER
	AMR = DSQRT(S2)	SEGSEG
	P = (1.0/TB - 1.0)*DSQRT(S1)	SEGSEG
	J = 3	HYPER
	IF(BD(1,MM).LT.0.0)J = 4	HYPER
	DO 35 I = 1,3	HYPER
	J = J + 1	HYPER
	IF((BD(1,MM).LT.0.0).OR.(BD(1,NN).LT.0.0))RM(I) = TB*RM(I)	HYPER
	TM(I) = -TM(I)/AMR	SEGSEG
	T2(I) = RM(I) - R(I)	SEGSEG
	RN(I) = T2(I) + RLN(I)	SEGSEG
35	RLM(I) = RM(I) + BD(J,MM)	HYPER
	CALL DOT31(DMNT,RN,RLN)	SEGSEG
	CALL PLSEGF(M,N,NT)	SEGSEG
C		EDGE
C	STORE PRINT DATA	EDGE
C		EDGE
	SSF(1,NSSF) = P	SEGSEG
	DO 40 I = 1,3	HYPER
	SSF(I+4,NSSF) = RLM(I)	EDGE
40	SSF(I+7,NSSF) = RLN(I)	HYPER
	IF(LPMI(M).NE.0) CALL DOT31(DPMI(1,1,M),RLM,SSF(5,NSSF))	EDGE
	IF(LPMI(N).NE.0) CALL DOT31(DPMI(1,1,N),RLN,SSF(8,NSSF))	EDGE
	IF(MCF.LT.0)GO TO 45	HYPER
	SSF(2,NSSF) = FM	SEGSEG
	TF2FM2 = TF**2 - FM**2	SEGSEG
	IF(TF2FM2.LT.0.0)TF2FM2 = 0.0	SEGSEG
	SSF(3,NSSF) = DSQRT(TF2FM2)	SEGSEG
	SSF(4,NSSF) = TF	SEGSEG
	GO TO 75	HYPER
C		EDGE

C	ROLL-SLIDE	
45	DO 50 I = 1,3	EDGE
50	SSF(I+1,NSSF) = T(I)	HYPER
	IF((BD(1,MM).LT.0.0).OR.(BD(1,NN).LT.0.0)) STOP 29	HYPER
	ANR = XDY(TM,B,T2)	HYPER
	CALL CROSS(TM,WNM,T2)	SEGSEG
	CALL MAT31(B,VR,T1)	SEGSEG
	TB = TM(1)*T1(1) + TM(2)*T1(2) + TM(3)*T1(3)	SEGSEG
	DO 60 I = 1,3	EDGE
	DO 55 J = 1,3	HYPER
	K = I + 3*(J+1)	HYPER
	TT4(I,J) = BD(K,MM)/AMR + B(I,J)/ANR	SEGSEG
55	TT5(I,J) = TT4(I,J)	SEGSEG
	TT4(I,4) = T2(I) - (T1(I) - TB*TM(I))/ANR	HYPER
60	TT5(I,4) = TM(I)	EDGE
	CALL DSMSOL(TT4,3,3)	HYPER
	CALL DSMSOL(TT5,3,3)	SEGSEG
	S1 = TM(1)*TT4(1,4) + TM(2)*TT4(2,4) + TM(3)*TT4(3,4)	SEGSEG
	S2 = (TM(1)*TT5(1,4) + TM(2)*TT5(2,4) + TM(3)*TT5(3,4))/S1	EDGE
	DO 65 I = 1,3	EDGE
	RMD(I) = TT4(I,4) - S2*TT5(I,4)	HYPER
65	RND(I) = RND(I) + VR(I)	EDGE
	CALL CROSS(DMNWN,RND,T1)	HYPER
	CALL CROSS(WMEG(1,MM),RMD,T2)	EDGE
	CALL MAT31(B,RND,T3)	EDGE
	CALL CROSS(DMNWN,TM,T4)	EDGE
	S1 = TM(1)*T3(1) + TM(2)*T3(2) + TM(3)*T3(3)	EDGE
	SQQ(NCF) = 0.0	EDGE
	DO 70 I = 1,3	SEGSEG
	T1(I) = T1(I) - T2(I)	HYPER
70	SQQ(NCF)=SQQ(NCF)+TM(I)*T1(I)-VR(I)*(T4(I)+(T3(I)-S1*TM(I))/ANR)	EDGE
	CALL DOT31(D(1,1,M),T1,RQQ(1,NCF))	HYPER
75	CALL ELTIME(2,23)	EDGE
	RETURN	HYPER
	END	SEGSEG
		SEGSEG

	SUBROUTINE SETUP1	REV IV 07/24/86	SETUP1
C			SLIP
C	FOR KK=1 (BEFORE CONTACT ROUTINE IN DAUX)		SETUP1
C	SET UP INITIAL VALUES OF A2 AND B2 ARRAYS FOR THIS TIME POINT.		SETUP1
C	SET UP INITIAL VALUES OF ARRAYS U1,U2 AND V1.		SETUP1
C			SETUP1
	IMPLICIT REAL*8(A-H,O-Z)		SETUP1
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		SETUP1
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),		SETUP1
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		SETUP1
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),		SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),		SETUP1
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)		SETUP1
	COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),		SETUP1
*	F(3,30),TQ(3,30),WJ(30),A11(3,3,30)		SLIP
	COMMON/CEULER/ IEULER(30),HIR(3,3,90),ANG(3,30),ANGD(3,30),		SLIP
*	FE(3,30),TOE(3,30),CONST(5,30)		SLIP
	COMMON/TEMPVS/T(3),S(3),T1(3),T2(3),T3(3),T4(3),T5(3),T6(3),		SETUP1
*	T7(3),T8(3),T9(3),T10(3),T11(3),T12(3),HH(3),		SETUP1
*	TT1(3,3),TT2(3,3),S1,SQS1,S2,S3,S4,V1T,SR2		SLIP
*	,DDMY(35043)		80386
	DATA IFIRST/1/		SLIP
C			SETUP1
	CALL ELTIME(1,10)		SETUP1
	IF (IFIRST.EQ.0) GO TO 15		SLIP
	IF (NJNT.EQ.0) GO TO 15		SLIP
	DO 10 I = 1,NJNT		SLIP
	DO 10 J = 1,3		SLIP
	DO 8 K = 1,3		SLIP
	8 A11(J,K,I) = 0.0		SLIP
	10 A11(J,J,I) = 1.0		SLIP
	IFIRST = 0		SLIP
	15 DO 20 I=1,NGRND		SLIP
C			SETUP1
C	SET EACH U1N = 0		SETUP1
C			SETUP1
	U1(1,I) = 0.0		SETUP1
	U1(2,I) = 0.0		SETUP1
	U1(3,I) = 0.0		SETUP1
C			SETUP1
C	SET EACH U2N = WNX(PHIN*WN)		SETUP1
C			SETUP1
	U2(1,I) = WMEG(2,I)*WMEG(3,I) * (PHI(2,I)-PHI(3,I))		SETUP1
	U2(2,I) = WMEG(1,I)*WMEG(3,I) * (PHI(3,I)-PHI(1,I))		SETUP1
20	U2(3,I) = WMEG(1,I)*WMEG(2,I) * (PHI(1,I)-PHI(2,I))		SETUP1
	IF (NPRT(11).NE.0) WRITE (6,21) ((U2(I,J),I=1,3),J=1,NSEG)		SETUP1
21	FORMAT(' U2 ARRAY'/(1X,1P9D14.4))		SETUP1
	IF (NJNT.LE.0) GO TO 98		SETUP1
	DO 40 J=1,NJNT		SETUP1
	DO 31 K=1,3		SETUP1
	T1(K) = SR(K,2*J-1)		SLIP

	T2(K) = SR(K,2*J )	SLIP
	IF (IABS(IPIN(J)).LT.5) GO TO 31	SLIP
	IF (IEULER(J).EQ.-1) GO TO 31	SLIP
	T1(K) = T1(K) + SR(4,2*J-1)*HT(K,3,2*J-1)	SLIP
31	V1(K,J) = 0.0	SLIP
	I = IABS(JNT(J))	SETUP1
	IF (I.LE.0) GO TO 40	SETUP1
C		SETUP1
C	FOR EACH JOINT SET	SETUP1
C	B12(2J-1) = B12(J,I ) = -D(I)' * SR(2J-1) X	SETUP1
C	B12(2J ) = B12(J,J+1) = D(J+1)' * SR(2J) X	SETUP1
C		SETUP1
	B12(1,1,2*J-1) = D(3,1,I)*T1(2) - D(2,1,I)*T1(3)	SLIP
	B12(2,1,2*J-1) = D(3,2,I)*T1(2) - D(2,2,I)*T1(3)	SLIP
	B12(3,1,2*J-1) = D(3,3,I)*T1(2) - D(2,3,I)*T1(3)	SLIP
	B12(1,2,2*J-1) = D(1,1,I)*T1(3) - D(3,1,I)*T1(1)	SLIP
	B12(2,2,2*J-1) = D(1,2,I)*T1(3) - D(3,2,I)*T1(1)	SLIP
	B12(3,2,2*J-1) = D(1,3,I)*T1(3) - D(3,3,I)*T1(1)	SLIP
	B12(1,3,2*J-1) = D(2,1,I)*T1(1) - D(1,1,I)*T1(2)	SLIP
	B12(2,3,2*J-1) = D(2,2,I)*T1(1) - D(1,2,I)*T1(2)	SLIP
	B12(3,3,2*J-1) = D(2,3,I)*T1(1) - D(1,3,I)*T1(2)	SLIP
C		SETUP1
	B12(1,1,2*J ) = D(2,1,J+1)*T2(3) - D(3,1,J+1)*T2(2)	SLIP
	B12(2,1,2*J ) = D(2,2,J+1)*T2(3) - D(3,2,J+1)*T2(2)	SLIP
	B12(3,1,2*J ) = D(2,3,J+1)*T2(3) - D(3,3,J+1)*T2(2)	SLIP
	B12(1,2,2*J ) = D(3,1,J+1)*T2(1) - D(1,1,J+1)*T2(3)	SLIP
	B12(2,2,2*J ) = D(3,2,J+1)*T2(1) - D(1,2,J+1)*T2(3)	SLIP
	B12(3,2,2*J ) = D(3,3,J+1)*T2(1) - D(1,3,J+1)*T2(3)	SLIP
	B12(1,3,2*J ) = D(1,1,J+1)*T2(2) - D(2,1,J+1)*T2(1)	SLIP
	B12(2,3,2*J ) = D(1,2,J+1)*T2(2) - D(2,2,J+1)*T2(1)	SLIP
	B12(3,3,2*J ) = D(1,3,J+1)*T2(2) - D(2,3,J+1)*T2(1)	SLIP
C		SETUP1
C	NOTE THAT FOR EACH JOINT	SETUP1
C	A21(M,N) = B12(N,M)	SETUP1
C		SETUP1
C	FOR EACH JOINT SET	SETUP1
C	V1(J) = -D(I)'*W(I)X( W(I)XSR(2J-1) )	SETUP1
C	+D(J+1)'*W(J+1)X( W(J+1)XSR(2J) )	SETUP1
C		SETUP1
	CALL CROSS(WMEG(1,I),T1,T)	SLIP
	CALL CROSS(WMEG(1,I),T,S)	SETUP1
	CALL DOT31(D(1,1,I),S,V1(1,J))	SETUP1
	CALL CROSS(WMEG(1,J+1),T2,T)	SLIP
	CALL CROSS(WMEG(1,J+1),T,S)	SETUP1
	CALL DOT31(D(1,1,J+1),S,T)	SETUP1
	DO 32 K=1,3	SLIP
32	V1(K,J) = T(K) - V1(K,J)	SLIP
	IF (IABS(IPIN(J)).LT.5) GO TO 40	SLIP
	IF (IEULER(J).EQ.-1) GO TO 40	SLIP
	CALL DOT31(D(1,1,I),HT(1,3,2*J-1),T4)	SLIP
	CALL CROSS(WMEG(1,I),HT(1,3,2*J-1),T5)	SLIP
	CALL DOT31(D(1,1,I),T5,T6)	SLIP



V1T = V1(1,J)*T4(1) + V1(2,J)*T4(2) + V1(3,J)*T4(3)	SLIP
SR2 = 2.0*SR(4,2*J)	SLIP
DO 34 K = 1,3	SLIP
V1(K,J) = V1(K,J) - V1T*T4(K) - SR2*T6(K)	SLIP
S1=T4(1)*B12(1,K,2*J-1)+T4(2)*B12(2,K,2*J-1)+T4(3)*B12(3,K,2*J-1)	SLIP
S2=T4(1)*B12(1,K,2*J )+T4(2)*B12(2,K,2*J )+T4(3)*B12(3,K,2*J )	SLIP
DO 33 L = 1,3	SLIP
A11(K,L,J) = -T4(K)*T4(L)	SLIP
B12(L,K,2*J-1) = B12(L,K,2*J-1) - S1*T4(L)	SLIP
33 B12(L,K,2*J ) = B12(L,K,2*J ) - S2*T4(L)	SLIP
34 A11(K,K,J) = 1.0 + A11(K,K,J)	SLIP
40 CONTINUE	SLIP
IF (NPRT(11).NE.0) WRITE (6,41) ((V1(I,J),I=1,3),J=1,NJNT)	SETUP1
41 FORMAT(' V1 ARRAY'/(1X,1P9D14.4))	SETUP1
C	SETUP1
C IF IPIN(M)=1, SET V2(M)=(WN.HN-WM.HM)DN'WNXHN	SETUP1
C	SETUP1
DO 50 J=1,NJNT	SETUP1
DO 43 K=1,3	SETUP1
43 V2(K,J) = 0.0	SETUP1
IF (IPIN(J).LT.1) GO TO 50	SETUP1
IF (IPIN(J).GT.1.AND.IPIN(J).LT.6) GOTO 50	SLIP
I = IABS(JNT(J))	SLIP
CALL CROSS (WMEG(1,I ),HB(1,2*J-1),T)	SETUP1
CALL DOT31 (D(1,1,I ),T,T1)	SETUP1
C CALL CROSS (WMEG(1,J+1),HB(1,2*J ),T)	SETUP1
C CALL DOT31 (D(1,1,J+1),T,T2)	SETUP1
S1 = WMEG(1,I)*HB(1,2*J-1)	SETUP1
* + WMEG(2,I)*HB(2,2*J-1)	SETUP1
* + WMEG(3,I)*HB(3,2*J-1)	SETUP1
S2 = WMEG(1,J+1)*HB(1,2*J)	SETUP1
* + WMEG(2,J+1)*HB(2,2*J)	SETUP1
* + WMEG(3,J+1)*HB(3,2*J)	SETUP1
DO 44 K=1,3	SETUP1
C 44 V2(K,J) = S1*T1(K) - S2*T2(K)	SETUP1
44 V2(K,J) = (S1-S2)*T1(K)	SETUP1
50 CONTINUE	SETUP1
98 CALL ELTIME(2,10)	SETUP1
RETURN	SETUP1
END	SETUP1

	SUBROUTINE SETUP2	REV IV 07/24/86	SLIP
C			SETUP2
C	CALL BY DAUX AFTER CONTACT ROUTINES AND BY UPDATE PRIOR TO		SETUP2
C	DAUX TO SET UP A2 ARRAY AND (FOR NQ#0) THE A13,A23 AND V3 ARRAYS.		SETUP2
C			SETUP2
	IMPLICIT REAL*8(A-H,O-Z)		SETUP2
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		SETUP2
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),		SETUP2
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		SETUP2
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),		SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),		SETUP2
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)		SETUP2
	COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),		SETUP2
*	F(3,30),TQ(3,30),WJ(30),A11(3,3,30)		SLIP
	COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24),		SETUP2
*	HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12),		SETUP2
*	RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12),		SETUP2
*	KQ1(12),KQ2(12),KQTYPE(12)		SETUP2
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),		SETUP2
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI		TWOPI
	LOGICAL*1 FREE,LDDMY		80386
	COMMON/TEMPVS/T(3),S(3),T1(3),T2(3),T3(3),T4(3),T5(3),T6(3),		SETUP2
*	T7(3),T8(3),T9(3),T10(3),T11(3),T12(3),HH(3),		SETUP2
*	TT1(3,3),TT2(3,3),S1,SQS1,S2,S3,S4		SETUP2
*	,WCRM(3),RM(3),WCM(3),WWCM(3),WWM(3),RBA(3),BA		SETUP2
*	,WCRN(3),RN(3),WCN(3),WWCN(3),WWN(3),RBAD(3)		SETUP2
*	,IDUM(14290),FREE(30),LDDMY(2),DDMY(27859)		80386
C			SETUP2
	CALL ELTIME(1,26)		SETUP2
C			SETUP2
C	COMPUTE A22 ARRAY VIA DHHPIN FOR DAUX2 ROUTINES.		SETUP2
C			SETUP2
	IF (NJNT.EQ.0) GO TO 50		SETUP2
	DO 49 M=1,NJNT		SETUP2
	FREE(M) = .TRUE.		SLIP
	N = IABS(JNT(M))		SETUP2
	IF (N.EQ.0) GO TO 49		SETUP2
	IF (IPIN(M).EQ.0) GOTO 49		SLIP
	IF (IPIN(M).GE.2.AND. IPIN(M).LE.5) GO TO 49		SLIP
	FREE(M) = .FALSE.		SLIP
	CALL DHHPIN(A22(1,1,2*M-1),T,N,M,2*M-1)		SETUP2
	CALL DHHPIN(A22(1,1,2*M),T,M+1,M,2*M)		SETUP2
49	CONTINUE		SETUP2
C			PECONV
C	THIS STATEMENT IS NECESSARY FOR THE PROGRAM TO RUN ON THE		PECONV
C	P&E FORTRAN VII O (REV 4) COMPILER		PECONV
C			PECONV
	NNNET = IPIN(M)		PECONV
C			SETUP2
C	SET UP A13,A23 AND V3 ARRAYS FOR DAUX33.		SETUP2
C			SETUP2

50 IF (NQ.EQ.0) GO TO 98	SETUP2
DO 70 K=1,NQ	SETUP2
IF (KQTYPE(K).LT.0) GO TO 70	SETUP2
IF (KQTYPE(K).EQ.5) GO TO 70	SETUP2
M = KQ1(K)	SETUP2
N = KQ2(K)	SETUP2
IF (KQTYPE(K).EQ.2 .OR. KQTYPE(K).EQ.4) GO TO 53	SETUP2
C	SETUP2
C FOR KQTYPE = 1 OR 3, SET HHT = I	SETUP2
C	SETUP2
DO 52 J=1,3	SETUP2
DO 51 I=1,3	SETUP2
51 HHT(I,J,K) = 0.0	SETUP2
52 HHT(J,J,K) = 1.0	SETUP2
IF (KQTYPE(K).NE.6) GO TO 61	SETUP2
C	SETUP2
C FOR KQTYPE=6, SET HHT= I-TT'	SETUP2
C	SETUP2
DO 60 J=1,3	SETUP2
DO 60 I=1,3	SETUP2
60 HHT(I,J,K) = HHT(I,J,K) - TQQ(I,K)*TQQ(J,K)	SETUP2
GO TO 61	SETUP2
53 IF (KQTYPE(K).NE.2) GO TO 56	SETUP2
C	SETUP2
C FOR KQTYPE=2, COMPUTE HH AND HHT.	SETUP2
C	SETUP2
CALL DOT31(D(1,1,M),RK1(1,K),T1)	SETUP2
CALL DOT31(D(1,1,N),RK2(1,K),T2)	SETUP2
S1 = 0.0	SETUP2
DO 54 I=1,3	SETUP2
HH(I) = SEGLP(I,M)+T1(I) - SEGLP(I,N)-T2(I)	SETUP2
54 S1 = S1 + HH(I)**2	SETUP2
SQS1 = DSQRT(S1)	SETUP2
DO 55 I=1,3	SETUP2
HH(I) = HH(I)/SQS1	SETUP2
55 IF (DABS(HH(I)).LE.EPS(12)) HH(I) = 0.0	SETUP2
CALL DOT31(HH,HH,HHT(1,1,K))	SETUP2
56 IF (KQTYPE(K).NE.4) GO TO 61	SETUP2
C	SETUP2
C FOR KQTYPE = 4, SET HHT = HHT	SETUP2
C	SETUP2
CALL DOT31(HQQ(1,K),HQQ(1,K),HHT(1,1,K))	SETUP2
C	SETUP2
C SET A13(2K-1) = HHT	SETUP2
C AND A13(2K) = -HHT	SETUP2
C	SETUP2
61 DO 62 J=1,3	SETUP2
DO 62 I=1,3	SETUP2
A13(I,J,2*K-1) = HHT(I,J,K)	SETUP2
62 A13(I,J,2*K) = -HHT(I,J,K)	SETUP2
C	SETUP2
C SET A23(2K-1) = (R1X)(D1)A13(2K-1)	SETUP2

C	AND A23(2K) = (R2X)(D2)A13(2K)	SETUP2
C		SETUP2
	CALL MAT33(D(1,1,M),A13(1,1,2*K-1),TT1)	SETUP2
	CALL MAT33(D(1,1,N),A13(1,1,2*K ),TT2)	SETUP2
	DO 63 J=1,3	SETUP2
	CALL CROSS(RK1(1,K),TT1(1,J),A23(1,J,2*K-1) )	SETUP2
63	CALL CROSS(RK2(1,K),TT2(1,J),A23(1,J,2*K ) )	SETUP2
	IF (KQTYPE(K).EQ.4) GO TO 72	SETUP2
C		SETUP2
C	FOR KQTYPE = 1,2 OR 3, SET B31 = A13' AND B32 = A23'	SETUP2
C		SETUP2
	DO 71 I=1,3	SETUP2
	DO 71 J=1,3	SETUP2
	B31(I,J,2*K-1) = A13(J,I,2*K-1)	SETUP2
	B31(I,J,2*K ) = A13(J,I,2*K )	SETUP2
	B32(I,J,2*K-1) = A23(J,I,2*K-1)	SETUP2
71	B32(I,J,2*K ) = A23(J,I,2*K )	SETUP2
	GO TO 76	SETUP2
C		SETUP2
C	FOR KQTYPE = 4, SET B31(2K-1) = HTT	SETUP2
C	B31(2K ) = -HTT	SETUP2
C	B32 = (B31)(D')(RX)'	SETUP2
C		SETUP2
	72 CALL DOTT31(HQQ(1,K),TQQ(1,K),B31(1,1,2*K-1))	SETUP2
	DO 73 I=1,3	SETUP2
	DO 73 J=1,3	SETUP2
73	B31(I,J,2*K) = -B31(I,J,2*K-1)	SETUP2
	CALL DOTT33(D(1,1,M),B31(1,1,2*K-1),B32(1,1,2*K-1))	SETUP2
	CALL DOTT33(D(1,1,N),B31(1,1,2*K ),B32(1,1,2*K ))	SETUP2
	DO 74 J=1,3	SETUP2
	CALL CROSS(RK1(1,K),B32(1,J,2*K-1),TT1(1,J))	SETUP2
74	CALL CROSS(RK2(1,K),B32(1,J,2*K ),TT2(1,J))	SETUP2
	DO 75 I=1,3	SETUP2
	DO 75 J=1,3	SETUP2
	B32(I,J,2*K-1) = TT1(J,I)	SETUP2
75	B32(I,J,2*K ) = TT2(J,I)	SETUP2
C		SETUP2
C	COMPUTE V3 = D2'(W2X(W2XR2)) - D1'(W1X(W1XR1))	SETUP2
C		SETUP2
	76 CALL CROSS(WMEG(1,M),RK1(1,K),T3)	SETUP2
	CALL CROSS (WMEG(1,M),T3,T4)	SETUP2
	CALL DOT31 (D(1,1,M),T4,T5)	SETUP2
	CALL CROSS (WMEG(1,N),RK2(1,K),T6)	SETUP2
	CALL CROSS (WMEG(1,N),T6,T7)	SETUP2
	CALL DOT31 (D(1,1,N),T7,T8)	SETUP2
	DO 64 I=1,3	SETUP2
64	V3(I,K) = T8(I) - T5(I)	SETUP2
	IF (KQTYPE(K).NE.2) GO TO 67	SETUP2
C		SETUP2
C	RECOMPUTE V3 FOR KQTYPE=2.	SETUP2
C		SETUP2
	CALL DOT31 (D(1,1,M),T3,T9 )	SETUP2

CALL DOT31 (D(1,1,N),T6,T10)	SETUP2
S2 = 0.0	SETUP2
DO 65 I=1,3	SETUP2
T11(I) = SEGLV(I,M)+T9(I) - SEGLV(I,N)-T10(I)	SETUP2
65 S2 = S2 + T11(I)**2	SETUP2
S3 = HH(1)*V3(1,K) + HH(2)*V3(2,K) + HH(3)*V3(3,K)	SETUP2
S4 = S3-S2/SQS1	SETUP2
DO 66 I=1,3	SETUP2
66 V3(I,K) = S4*HH(I)	SETUP2
67 IF (KQTYPE(K).NE.3.AND.KQTYPE(K).NE.6) GO TO 77	SETUP2
C FOR KQTYPE=3 OR 6, ADD R DOT TERM FROM PLELP OR SEGSEG TO V3.	SETUP2
C	SETUP2
C	SETUP2
DO 68 I=1,3	SETUP2
68 V3(I,K) = V3(I,K) + RQQ(I,K)	SETUP2
IF (KQTYPE(K).NE.6) GO TO 70	SETUP2
C FOR KQTYPE=6, SET V3 = (I-TT')(V3+RQQ)	SETUP2
C	SETUP2
C	SETUP2
VQQ = V3(1,K)*TQQ(1,K) + V3(2,K)*TQQ(2,K) + V3(3,K)*TQQ(3,K)	SETUP2
DO 69 I=1,3	SETUP2
69 V3(I,K) = V3(I,K) - VQQ*TQQ(I,K)	SETUP2
77 IF (KQTYPE(K).NE.4) GO TO 70	SETUP2
C FOR KQTYPE = 4, ADD R TERM FROM PLELP OR SEGSEG TO V3.	SETUP2
C	SETUP2
C	SETUP2
S3 = TQQ(1,K)*V3(1,K) + TQQ(2,K)*V3(2,K) + TQQ(3,K)*V3(3,K)	SETUP2
S4 = S3+SQQ(K)	SETUP2
DO 78 I=1,3	SETUP2
78 V3(I,K) = S4*HQQ(I,K)	SETUP2
70 CONTINUE	SETUP2
C SPECIAL SETUP FOR TENSION ELEMENTS (KQTYPE = 5).	SETUP2
C	SETUP2
C	SETUP2
N = 0	SETUP2
79 N = N+1	SETUP2
IF (N.GE.NQ) GO TO 98	SETUP2
IF (KQTYPE(N).NE.5) GO TO 79	SETUP2
DO 81 I=1,3	SETUP2
DO 80 J=1,3	SETUP2
A13(I,J,2*N-1) = 0.0	SETUP2
A13(I,J,2*N ) = 0.0	SETUP2
A23(I,J,2*N ) = 0.0	SETUP2
B31(I,J,2*N-1) = 0.0	SETUP2
B31(I,J,2*N ) = 0.0	SETUP2
A13(I,J,2*N+1) = 0.0	SETUP2
A13(I,J,2*N+2) = 0.0	SETUP2
A23(I,J,2*N+1) = 0.0	SETUP2
B31(I,J,2*N+1) = 0.0	SETUP2
B31(I,J,2*N+2) = 0.0	SETUP2
HHT(I,J,N ) = 0.0	SETUP2
80 HHT(I,J,N+1 ) = 0.0	SETUP2

A13(I,I,2*N-1) = 1.0	SETUP2
B31(I,I,2*N-1) = RK1(1,N+1)	SETUP2
B31(I,I,2*N ) = RK1(3,N+1)	SETUP2
A13(I,I,2*N+2) = 1.0	SETUP2
B31(I,I,2*N+1) = RK1(3,N+1)	SETUP2
81 B31(I,I,2*N+2) = RK1(2,N+1)	SETUP2
N1 = KQ1(N)	SETUP2
N2 = KQ2(N)	SETUP2
DO 82 K=1,3	SETUP2
CALL CROSS(RK1(1,N),D(1,K,N1),A23(1,K,2*N-1))	SETUP2
82 CALL CROSS(RK2(1,N),D(1,K,N2),A23(1,K,2*N+2))	SETUP2
DO 83 I=1,3	SETUP2
DO 83 J=1,3	SETUP2
B32(I,J,2*N-1) = RK1(1,N+1)*A23(J,I,2*N-1)	SETUP2
B32(I,J,2*N ) = RK1(3,N+1)*A23(J,I,2*N+2)	SETUP2
B32(I,J,2*N+1) = RK1(3,N+1)*A23(J,I,2*N-1)	SETUP2
83 B32(I,J,2*N+2) = RK1(2,N+1)*A23(J,I,2*N+2)	SETUP2
CALL CROSS(WMEG(1,N1),RK1(1,N),WCRM)	SETUP2
CALL CROSS(WMEG(1,N2),RK2(1,N),WCRN)	SETUP2
CALL DOT31(D(1,1,N1),RK1(1,N),RM)	SETUP2
CALL DOT31(D(1,1,N2),RK2(1,N),RN)	SETUP2
CALL DOT31(D(1,1,N1),WCRM,WCM)	SETUP2
CALL DOT31(D(1,1,N2),WCRN,WCN)	SETUP2
BA = 0.0	SETUP2
DO 84 I=1,3	SETUP2
RBA (I) = SEGLP(I,N2) + RN (I) - SEGLP(I,N1) - RM (I)	SETUP2
RBAD(I) = SEGLV(I,N2) + WCN(I) - SEGLV(I,N1) - WCM(I)	SETUP2
84 BA = BA + RBA(I)**2	SETUP2
BA = DSQRT(BA)	SETUP2
FORCE = 0.0	SETUP2
IF (BA.GT.RK2(3,N+1)) FORCE = RK2(1,N+1)*(1.0-RK2(3,N+1)/BA)	SETUP2
DO 85 I=1,3	SETUP2
V3(I,N) = RK2(2,N+1)*RBAD(I) + FORCE*RBA(I)	SETUP2
85 V3(I,N+1) = -V3(I,N)	SETUP2
CALL CROSS(WMEG(1,N1),WCRM,WWCM)	SETUP2
CALL CROSS(WMEG(1,N2),WCRN,WWCN)	SETUP2
CALL DOT31(D(1,1,N1),WWCM,WWM)	SETUP2
CALL DOT31(D(1,1,N2),WWCN,WWN)	SETUP2
DO 86 I=1,3	SETUP2
V3(I,N ) = V3(I,N ) - RK1(1,N+1)*WWM(I) - RK1(3,N+1)*WWN(I)	SETUP2
86 V3(I,N+1) = V3(I,N+1) - RK1(3,N+1)*WWM(I) - RK1(2,N+1)*WWN(I)	SETUP2
N = N+1	SETUP2
GO TO 79	SETUP2
98 CALL ELTIME(2,26)	SETUP2
RETURN	SETUP2
END	SETUP2

	SUBROUTINE SINPUT		SINPUT
C		REV IV 02/20/87	HYPER
C	READS AND PRINTS THE INPUT CARDS THAT DESCRIBE THE PHYSICAL		SINPUT
C	DIMENSIONS OF THE PLANES REPRESENTING THE VEHICLE PANELS AND OF		SINPUT
C	THE RESTRAINT BELTS. ALSO PROCESSES THOSE DATA CARDS THAT DESCRIBES		SINPUT
C	ADDITIONAL CONTACT ELLIPSOIDS, CONSTRAINTS, BODY SEGMENT SYMMETRY		SINPUT
C	OPTIONS AND SPRING DAMPER FUNCTIONS.		SINPUT
C			SINPUT
	IMPLICIT REAL*8 (A-H,O-Z)		SINPUT
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,XGRND,		SINPUT
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/CNTRF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)		EDGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),		SINPUT
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		SINPUT
	COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24),		SINPUT
*	HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12),		SINPUT
*	RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12),		SINPUT
*	KQ1(12),KQ2(12),KQTYPE(12)		SINPUT
	COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),		SINPUT
*	BLTTTL(5,8),PLTTL(5,30),BAGTTL(5,6),SEG(30),		SINPUT
*	JOINT(30),CGS(30),JS(30)		SINPUT
	REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTL,BAGTTL,SEG,JOINT		SINPUT
	LOGICAL*1 CGS,JS,LP4		HYPER
	COMMON/DAMPER/ APSDM(3,20),APSDN(3,20),ASD(5,20),MSDM(20),MSDN(20)		SINPUT
	COMMON/WINDFR/ WTIME(30),QFU(3,5),QFV(3,5),WF(3,30),IWIND(30),		WINDOP
*	MWSEG(7,30),NFVSEG(6),NFVNT(5),MOWSEG(30,30)		WINDOP
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),		SINPUT
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI		TWOPI
	COMMON/TEMPVS/ P1(3),P2(3),P3(3),P4(3),DE(3,3),DMY(35092)		80386
	DIMENSION IDYPR(3)		SINPUT
	DATA IDYPR/3,2,1/		SINPUT
	DATA MAXBD/40/		CHGIII
	DATA NPLMAX/30/,NBLTMX/8/,NBAGMX/5/,NELPMX/40/,NQMAX/12/,		MISC
*	NSDMAX/20/,NHRNSM/5/,NWINDM/50/,NJNTFM/50/,NFORCM/5/		MISC
C			SINPUT
C	INPUT CARD D.1		SINPUT
C			SINPUT
	READ (5,11) NPL,NBLT,NBAG,NELP,NQ,NSD,NHRNSS,NWINDF,NJNTF,NFORCES		SINPUT
11	FORMAT(12I6)		SINPUT
	WRITE (6,16) NPG,NPL,NBLT,NBAG,NELP,NQ,NSD,NHRNSS,NWINDF,NJNTF,		PAGE
*	NFORCE		PAGE
	NPG=NPG+1		PAGE
16	FORMAT('1 NPL NBLT NBAG NELP NQ NSD NHRNSS',		PAGE
*	' NWINDF NJNTF NFORCE',43X,'PAGE',15/1018,40X,'CARD D.1')		PAGE
	IF (NPL.GT.NPLMAX) STOP 65		CHGIII
	IF (NBLT.GT.NBLTMX) STOP 66		MISC
	IF (NBAG.GT.NBAGMX) STOP 67		MISC
	IF (NELP.GT.NELPMX) STOP 68		MISC
	IF (NQ.GT.NQMAX) STOP 69		CHGIII
	IF (NSD.GT.NSDMAX) STOP 70		CHGIII
	IF (NHRNSS.GT.NHRNSM) STOP 71		MISC
	IF (NWINDF.GT.NWINDM) STOP 72		MISC

	IF (MINTF.GT.NJNTFM) STOP 73	MISC
	IF (NFORCE.GT.NFORCM) STOP 74	MISC
	IF (NPL.EQ.0) GO TO 15	SINPUT
	IPAGE = 0	SINPUT
	DO 20 J=1,NPL	SINPUT
C		SINPUT
C	READ AND PRINT CARDS D.2.A,D.2.B AND D.2.C FOR THE JTH PLANE.	SINPUT
C		SINPUT
	READ (5,23) JJ,(PLTTL(I,J),I = 1,5),P1,P2,P3	SINPUT
	23 FORMAT (I4,4X,5A4/(3F12.0))	SINPUT
	IF (JJ.NE.J) WRITE (6,24) JJ,J	SINPUT
	24 FORMAT (' PLANE INDEX INPUT ERROR,',2I4)	SINPUT
	IF (JJ.NE.J) STOP 10	SINPUT
	IF (MOD(J,7).EQ.1.AND.IPAGE.EQ.0) WRITE (6,12) IPAGE	PAGE
	IF (MOD(J,7).EQ.1.AND.IPAGE.EQ.1) WRITE (6,112) IPAGE,NPG	PAGE
	IF (MOD(J,7).EQ.1.AND.IPAGE.EQ.1) NPG=NPG+1	PAGE
	112 FORMAT(I1,' PLANE INPUTS',109X,'PAGE',I5/120X,'CARDS D.2')	PAGE
	12 FORMAT(I1,' PLANE INPUTS',106X,'CARDS D.2')	SINPUT
	IPAGE = 1	SINPUT
	WRITE (6,25) J, (PLTTL(I,J),I = 1,5),P1,P2,P3	SINPUT
	25 FORMAT('0 PLANE NO.',I4,4X,5A4//17X,'X',11X,'Y',11X,'Z'/	SINPUT
	* ' POINT 1 ' ,3F12.4/	SINPUT
	* ' POINT 2 ' ,3F12.4/	SINPUT
	* ' POINT 3 ' ,3F12.4)	SINPUT
C		SINPUT
C	PROGRAM NOW ASSUMES THE FINITE PLANE IS A PARALLELOGRAM IN SHAPE	SINPUT
C	WHERE THE INPUT POINTS P1,P2,P3 ARE 3 OF THE CORNERS SUCH THAT	SINPUT
C	EDGE P1-P2 IS LESS THAN 180 DEGREES CLOCKWISE (AS VIEWED BY THE	SINPUT
C	OCCUPANT) FROM THE EDGE P1-P3.	SINPUT
C		SINPUT
C	SET UP PL ARRAY AS REQUIRED BY SUBROUTINE PLELP	SINPUT
C		SINPUT
C	PL(1,J) = A0 NORMAL EQUATION OF JTH PLACE	SINPUT
C	PL(2,J) = B0 A0*X + B0*Y + C0*Z = D0	SINPUT
C	PL(3,J) = C0	SINPUT
C	PL(4,J) = D0	SINPUT
C		SINPUT
C	PL(5,J)	SINPUT
C	PL(6,J) POINT 1	EDGE
C	PL(7,J)	SINPUT
C		SINPUT
C	PL(8,J) =A1	SINPUT
C	PL(9,J) =B1 NORMAL EQUATION OF 1ST BOUNDARY PLANE	SINPUT
C	PL(10,J)=C1 A1*X + B1*Y + C1*Z = D1	SINPUT
C	PL(11,J)=D1 AND E1 IS LENGTH OF PLANE FROM BOUNDARY.	SINPUT
C	PL(12,J)=E1	SINPUT
C		SINPUT
C	PL(13,J)=A2	SINPUT
C	PL(14,J)=B2 NORMAL EQUATION OF 2ND BOUNDARY PLANE	SINPUT
C	PL(15,J)=C2 A2*X + B2*Y + C2*Z = D2	SINPUT
C	PL(16,J)=D2 AND E2 IS LENGTH OF PLANE FROM BOUNDARY.	SINPUT
C	PL(17,J)=E2	SINPUT



C			SINPUT
C	PL(18,J)		EDGE
C	PL(19,J)	POINT 2 - POINT 1	EDGE
C	PL(20,J)		EDGE
C			EDGE
C	PL(21,J)		EDGE
C	PL(22,J)	POINT 3 - POINT 1	EDGE
C	PL(23,J)		EDGE
C			EDGE
C	PL(24,J)	NOT CURRENTLY USED	EDGE
	S22 = 0.0		SINPUT
	S23 = 0.0		SINPUT
	S33 = 0.0		SINPUT
	DO 26 I =1,3		SINPUT
	P2(I) = P2(I)-P1(I)		SINPUT
	P3(I) = P3(I)-P1(I)		SINPUT
	PL(I+ 4,J) = P1(I)		EDGE
	PL(I+17,J) = P2(I)		EDGE
	PL(I+20,J) = P3(I)		EDGE
	S22 = S22 + P2(I)*P2(I)		SINPUT
	S23 = S23 + P2(I)*P3(I)		SINPUT
26	S33 = S33 + P3(I)*P3(I)		SINPUT
	S2 = DSQRT(S22)		SINPUT
	S3 = DSQRT(S33)		SINPUT
	CALL CROSS(P2,P3,PL(1,J))		SINPUT
	S1 = 0.0		SINPUT
	DO 27 I=1,3		SINPUT
27	S1 = S1 + PL(I,J)**2		SINPUT
	S1 = DSQRT(S1)		SINPUT
	DO 28 I=1,3		SINPUT
	PL(I,J) = PL(I,J)/S1		SINPUT
	PL(I+7 ,J) = (S33*P2(I) - S23*P3(I)) / (S1*S3)		SINPUT
28	PL(I+12,J) = (S22*P3(I) - S23*P2(I)) / (S1*S2)		SINPUT
	PL( 4,J) = P1(1)*PL( 1,J) + P1(2)*PL( 2,J) + P1(3)*PL( 3,J)		SINPUT
	PL(11,J) = P1(1)*PL( 8,J) + P1(2)*PL( 9,J) + P1(3)*PL(10,J)		SINPUT
	PL(12,J) = P2(1)*PL( 8,J) + P2(2)*PL( 9,J) + P2(3)*PL(10,J)		SINPUT
	PL(16,J) = P1(1)*PL(13,J) + P1(2)*PL(14,J) + P1(3)*PL(15,J)		SINPUT
20	PL(17,J) = P3(1)*PL(13,J) + P3(2)*PL(14,J) + P3(3)*PL(15,J)		SINPUT
15	IF (NBLT.EQ.0) GO TO 35		SINPUT
	DO 30 J=1,NBLT		SINPUT
C			SINPUT
C	READ AND PRINT CARDS D.3.A, D.3.B AND D.3.C FOR THE JTH BELT.		SINPUT
C			SINPUT
	READ (5,13) (BLTTTL(I,J),I = 1,5),(BELT(I,J),I = 1,11)		SINPUT
13	FORMAT (5A4/(6F12.0))		SINPUT
	IF (MOD(J,5).EQ.1) WRITE (6,21) NPG		PAGE
	IF (MOD(J,5).EQ.1) NPG=NPG+1		PAGE
21	FORMAT('1 BELT INPUTS',110X,'PAGE',I5/120X,'CARDS D.3')		PAGE
30	WRITE (6,14) J,(BLTTTL(I,J),I = 1,5),(BELT(I,J),I = 1,11)		SINPUT
14	FORMAT('0 BELT NO.',I4,4X,5A4//		SINPUT
	* 30X,'ANCHOR POINT A',46X,'ANCHOR POINT B'//		SINPUT
	* 2(16X,'X',19X,'Y',19X,'Z',3X)/6F20.3//		SINPUT

	* 26X, 'FIXED POINT ON SEGMENT', 45X, 'SLACK(+)'/	SINPUT
	* 16X, 'X', 19X, 'Y', 19X, 'Z', 17X, 'BLANK', 13X, 'LENGTH(-)'/5F20.3)	SINPUT
C		SINPUT
C	CALL AIRBG1 ROUTINE IF REQUIRED FOR AIRBAG INPUT	SINPUT
C		SINPUT
	35 IF (NBAG.NE.0) CALL AIRBG1	SINPUT
	IF (NELP.LE.0) GO TO 51	SINPUT
C		SINPUT
C	READ AND PRINT CARDS D.5 FOR ELLIPSOID INPUT, IF ANY.	SINPUT
C	NOTE: NELP IS THE NO. OF ELLIPSOIDS TO BE SUPPLIED HERE, NOT THE	SINPUT
C	NO. OF ELLIPSOIDS IN THE PROGRAM, SINCE THE FIRST NSEG	SINPUT
C	ELLIPSOIDS WERE SUPPLIED ON CARDS B.2.A - B.2.1. HOWEVER	SINPUT
C	THEY MAY BE REPLACED HERE IF DESIRED.	SINPUT
C		SINPUT
	WRITE (6,41) NPG,UNITL,UNITL	PAGE
	NPG=NPG+1	PAGE
	41 FORMAT('1 ADDITIONAL ELLIPSOID INPUT',95X,'PAGE',I5/120X,	PAGE
	* 'CARDS D.5'/17X,'SEMIAXES (' ,A4,')',18X,'OFFSET (' ,A4,')',	PAGE
	* 20X,'ROTATION (DEG)',15X,'POWER'/	HYPER
	* 3X,'NO.',2(8X,'X',8X,'Y',8X,'Z',6X),7X,'YAW',7X,'PITCH',5X,	SINPUT
	* 'ROLL'//)	SINPUT
	DO 50 MM=1,NELP	SINPUT
	READ (5,42) M,P1,P2,P3,P4	HYPER
	42 FORMAT(I6,9F6.0,3F4.0)	HYPER
	IF (M.GT.MAXBD) STOP 63	CHGIII
C		CHGIII
C	PREVENT EXTRA ELLIPSOIDS FROM CHANGING AIRBAG ELLIPSOIDS	CHGIII
C		CHGIII
	IF (M.GT.NVEH.AND.M.LT.NGRND) WRITE (6,330)	CHGIII
	330 FORMAT(3X,'THE EXTRA CONTACT ELLIPSOID NUMBER IS THE SAME AS AN A	CHGIII
	*RBAG ELLIPSOID')	CHGIII
	IF (M.GT.NVEH.AND.M.LT.NGRND) STOP 64	CHGIII
	WRITE (6,43) M,P1,P2,P3,P4	HYPER
	43 FORMAT(I6,3(3X,3F9.3,3X),3F6.0)	HYPER
	CALL DRCYPR (DE,P3,IDYPR)	SINPUT
	N = 1	HYPER
	LP4 = .FALSE.	HYPER
	DO 39 J = 1,3	HYPER
	39 IF (P4(J).GT.2.0) LP4 = .TRUE.	HYPER
	IF (LP4) N = 2	HYPER
	DO 46 I = 1,3	HYPER
	BD(N ,M) = P1(I)	HYPER
	BD(N+3,M) = P2(I)	HYPER
	IF (LP4) GO TO 46	HYPER
	DO 45 J=1,3	SINPUT
	SUM1 = 0.0	SINPUT
	SUM2 = 0.0	SINPUT
	DO 44 L=1,3	SINPUT
	SUM1 = SUM1 + DE(L,I)/P1(L)**2*DE(I,J)	SINPUT
	44 SUM2 = SUM2 + DE(L,I)*P1(L)**2*DE(L,J)	SINPUT
	K = 3*I +J +3	SINPUT
	BD(K ,M) = SUM1	SINPUT

45	BD(K+9,M) = SUM2	SINPUT
46	N = N + 1	HYPER
	IF (.NOT.LP4) GO TO 50	HYPER
	BD(1,M) = -P4(1)	HYPER
	N = 8	HYPER
	DO 48 J = 1,3	HYPER
	BD(J+19,M) = P4(J)	HYPER
	IF (BD(J+19,M).EQ.0.0) BD(J+19,M) = BD(20,M)	HYPER
	BD(J+16,M) = 1.0/BD(J+1,M)**2	HYPER
	DO 48 I = 1,3	HYPER
	BD(N,M) = DE(I,J)	HYPER
48	N = N + 1	HYPER
	BD(23,M) = 0.0	HYPER
	IF (BD(20,M).NE.BD(21,M)) BD(23,M) = 1.0	HYPER
	IF (BD(21,M).NE.BD(22,M)) BD(23,M) = 1.0	HYPER
	IF (BD(22,M).NE.BD(20,M)) BD(23,M) = 1.0	HYPER
50	CONTINUE	SINPUT
C		SINPUT
C	READ AND PRINT CARDS D.6 FOR CONSTRAINT INPUT, IF ANY.	SINPUT
C		SINPUT
51	IF (NQ.LE.0) GO TO 70	SINPUT
	DO 60 K=1,NQ	SINPUT
	READ (5,52) KQTYPE(K),KQ1(K),KQ2(K),(RK1(I,K),I=1,3)	SINPUT
	* , (RK2(I,K),I=1,3)	SINPUT
52	FORMAT(3I6,6F6.0)	SINPUT
	IF (K.EQ.1) WRITE (6,53) NPG,UNITL,UNITL	PAGE
	IF (K.EQ.1) NPG=NPG+1	PAGE
53	FORMAT('1 CONSTRAINT INPUT',105X,'PAGE',15/120X,'CARDS D.6'/	PAGE
	* ' TYPE SEGMENT SEGMENT POINT ON 1ST SEGMENT ('	SINPUT
	* A4,')', ' POINT ON 2ND SEGMENT (' ,A4,')'/'	SINPUT
	* ' NO. NO. 1 NO. 2 X Y Z	SINPUT
	* X Y Z'//)	SINPUT
	WRITE (6,54) KQTYPE(K),KQ1(K),KQ2(K),(RK1(I,K),I=1,3)	SINPUT
	* , (RK2(I,K),I=1,3)	SINPUT
54	FORMAT(I6,2I9,2(6X,3F9.3) )	SINPUT
60	CONTINUE	SINPUT
C		SINPUT
C	CARD D.7 BODY SEGMENT SYMMETRY INPUT	SINPUT
C		SINPUT
70	READ (5,71) (NSYM(J),J=1,NSEG)	SINPUT
71	FORMAT(18I4)	SINPUT
	DO 103 J=1,NSEG	TGMOD2
	LJ = NSYM(J)	TGMOD2
	IF(IABS(LJ).GT.NSEG) GO TO 107	TGMOD2
	IF(LJ) 104,103,105	TGMOD2
105	LK = NSYM(LJ)	TGMOD2
	IF(IABS(LK).GT.NSEG) GO TO 107	TGMOD2
	IF(LK.NE.J) GO TO 106	TGMOD2
	GO TO 103	TGMOD2
104	JJ = -J	TGMOD2
	LJ = -LJ	TGMOD2
	LK = NSYM(LJ)	TGMOD2

IF(IABS(LK).GT.NSEG) GO TO 107	TGMOD2
IF((LK.NE.JJ).OR.(NSYM(J).EQ.JJ)) GO TO 106	TGMOD2
GO TO 103	TGMOD2
106 STOP 96	TGMOD2
107 STOP 97	TGMOD2
103 CONTINUE	TGMOD2
WRITE(6,72) (J,J-1,NSEG)	SINPUT
WRITE(6,73) (NSYM(J),J-1,NSEG)	SINPUT
72 FORMAT('0 BODY SEGMENT SYMMETRY INPUT',91X,'CARD D.7'//	SINPUT
* ' SEG NO.',30I4)	SINPUT
73 FORMAT('0 NSYM(J)',30I4)	SINPUT
NSEG1 = NSEG+1	SINPUT
DO 74 J=NSEG1,NGRND	SINPUT
74 NSYM(J) = 0	SINPUT
IF (NSD.LE.0) GO TO 90	SINPUT
C	SINPUT
C CARD D.8 SPRING DAMPERS FUNCTION INPUT.	SINPUT
C	SINPUT
DO 79 J=1,NSD	SINPUT
79 READ (5,80) MSDM(J),MSDN(J),(APSDM(I,J),I=1,3),	SINPUT
* (APSDN(I,J),I=1,3),(ASD(I,J),I=1,5)	SINPUT
80 FORMAT(2I3,11F6.0)	SINPUT
WRITE (6,81) UNITL	SINPUT
81 FORMAT('0',5X,'SPRING DAMPERS FUNCTION INPUT',82X,'CARDS D.8'//	SINPUT
* 18X,'COORDINATES OF ATTACHMENT POINTS ('A4,')'//	SINPUT
* 5X,'SEGMENT',9X,'SEGMENT M',16X,'SEGMENT N',15X,	SINPUT
* 'SPRING FORCE FUNCTION',12X,'DAMPING FORCE FUNCTION'//	AFREVS
* ' NO. M N',2(6X,'X',7X,'Y',7X,'Z',2X),7X,'DO',9X,'A1',11X,	SINPUT
* 'A2',13X,'B1',10X,'B2' // )	SINPUT
DO 82 J=1,NSD	SINPUT
82 WRITE (6,83) J,MSDM(J),MSDN(J),(APSDM(I,J),I=1,3),	SINPUT
* (APSDN(I,J),I=1,3),(ASD(I,J),I=1,5)	SINPUT
83 FORMAT(I3,2I4,2(1X,3F8.2),F11.2,2F12.3,F15.3,F12.3)	SINPUT
C	SINPUT
C CARDS D.9 FORCE AND/OR TORQUE FUNCTIONS.	CHGIII
C	SINPUT
90 NFVSEG(6)= NFORCE	SINPUT
IF (NFORCE.LE.0) GO TO 99	SINPUT
WRITE (6,91)	SINPUT
91 FORMAT ('0',6X,'FORCE AND/OR TORQUE FUNCTION INPUTS',78X,'CARDS D.	CHGIII
*9'//, 5X,'NO.', 5X,'SEG', 5X,'FCN', 13X,'X', 9X,'Y', 9X,'Z',	CHGIII
* 13X,'YAW', 6X,'PITCH', 6X,'ROLL' //)	SINPUT
DO 95 J=1,NFORCE	SINPUT
READ (5,92) NFVSEG(J),NFVNT(J),P1,P2	SINPUT
92 FORMAT (2I6,6F10.0)	SINPUT
WRITE (6,93) J,NFVSEG(J),NFVNT(J),P1,P2	SINPUT
93 FORMAT (3I8,6X,3F10.3,6X,3F10.3)	SINPUT
CALL DRCYPR (DE,P2,IDYPR)	SINPUT
DO 94 I=1,3	SINPUT
94 QFU(I,J) = DE(1,I)	FIXSPT
95 CALL CROSS (P1,QFU(1,J),QFV(1,J))	SINPUT
99 RETURN	SINPUT

END

SINPUT

```

SUBROUTINE SLPLOT (X, NX, XO, XN, XL, XSIZE, XLAB, NXLB,      SLPLOT
*                Y, NY, YO, YN, YL, YSIZE, YLAB, NYLB,      SLPLOT
*                NPTS, NYY, NDY, PLAB1, NPLB1, PLAB2, NPLB2) SLPLOT
REV III.2 08/08/84REVIII
C
C
C ARGUMENTS:
C   X(NPTS)      - ARRAY OF NPTS ABSCISSAS TO BE PLOTTED.      SLPLOT
C   Y(NDY,NYY)   - ARRAY OF NPTS*NY Y ORDINATES TO BE PLOTTED. SLPLOT
C   NX,NY        - POSITIVE - NO. OF LINEAR SUBDIVISIONS.      SLPLOT
C                 NEGATIVE - NO. OF LOGARITHMIC DECADES.      SLPLOT
C   XO,YO        - AXES ORIGINS (POWER OF TEN IF NX,NY NEGATIVE). SLPLOT
C   XN,YN        - AXES END VALUES (REQUIRED IF NX,NY POSITIVE). SLPLOT
C   XL,YL        - LENGTH (INCHES) OF X,Y AXES.                SLPLOT
C   XSIZE,YSIZE  - PAPER SIZE (INCHES) IN X,Y DIRECTIONS.      SLPLOT
C   XLAB,YLAB    - X,Y AXES LABELS (ALPHANUMERIC ARRAYS).      SLPLOT
C   NXLB,NYLB    - NO. OF CHARACTERS IN X,Y LABELS.            SLPLOT
C   NPTS         - NO. OF POINTS IN X ARRAY AND EACH Y ARRAY.  SLPLOT
C   NYY          - NO. OF Y ARRAYS TO BE PLOTTED VS. X ARRAY.  SLPLOT
C   NDY          - FIRST DIMENSION OF Y ARRAY IN CALLING ROUTINE. SLPLOT
C                 (NDY MUST BE .GE. NPTS)                      SLPLOT
C   PLAB1,PLAB2  - 1ST & 2ND LINES OF PLOT ID LABELS (ALPHANUMERIC). SLPLOT
C   NPLB1,NPLB2  - NO. OF CHARACTERS IN PLOT ID LABELS.        SLPLOT
C
C NOTE: PLOTS WILL BE TRUNCATED AS FOLLOWS:
C   NX,NY POSITIVE - XO,YO .LE. X,Y .LE. XN,YN
C   NX,NY NEGATIVE - XO,YO .LE. X,Y .LE. XN*10**(-NX),YO*10**(-NY)
C
C DIMENSION X(NPTS),Y(NDY,NYY)
C CHARACTER*4 XLAB(1),YLAB(1),PLAB1(1),PLAB2(1)
C
C NOTE: THIS ROUTINE HAS BEEN WRITTEN FOR THE PLOTTING FACILITIES
C AT CALSPAN. THE FOLLOWING ITEMS ARE KNOWN TO BE CONTRARY TO THE
C NORMAL CALCOMP PROCEDURES AND SHOULD BE EXAMINED BY USERS AT OTHERS
C COMPUTER SYSTEMS AND CHANGES MADE ACCORDINGLY.
C
C 1. AT CALSPAN THE PLOTTED CHARACTERS GENERATED BY SUBROUTINE
C SYMBOL HAVE A WIDTH OF 6/7 TIMES THE HEIGHT. FOR THE CALCOMP
C ROUTINES THE WIDTH IS EQUAL TO THE HEIGHT. THE STATEMENT
C 'WIDTHF = 6.0/7.0' SHOULD BE CHANGED TO 'WIDTHF = 1.0'.
C
C 2. THE ONLY INITIALIZATION REQUIRED AT CALSPAN IS THE STATEMENT
C 'CALL PLOT (0.0,0.0,0)' TO ESTABLISH A NEW PAGE, INCLUDING
C THE FIRST PAGE. THIS IS FOLLOWED BY 'CALL PLOT (XO,YO,-3)' TO
C SET THE PLOT ORIGIN ON THE PAGE. PROPER PLOT INITIALIZATION
C SHOULD BE DONE HERE AND IN SUBROUTINE POSTPR (AFTER STATEMENTS
C NO. 30) AS REQUIRED BY THE USER'S PLOTTING FACILITY.
C
C 3. THE STATEMENT 'CALL NEWPEN(2)' SHOULD BE EXAMINED OR DELETED.
C
C 4. THE STATEMENT 'CALL EFLOT' AFTER STATEMENT NO. 50 IN POSTPR
C IS REQUIRED AT CALSPAN TO CLOSE OUT THE PLOT FILES. THIS
C SHOULD BE CHANGED TO CONFORM TO THE REQUIREMENTS OF THE

```

C	USER'S PLOTTING FACILITIES.	SLPLOT
C		SLPLOT
C	5. THE NECESSARY JOB CONTROL LANGUAGE FOR PLOTTING IS NECESSARY.	SLPLOT
C		SLPLOT
C	6. THE ONLY CALCOMP ROUTINES NEEDED ARE SYMBOL, NUMBER AND PLOT.	SLPLOT
C		SLPLOT
	LOGICAL NXPOS,NXNEG,NYPOS,NYNEG	SLPLOT
	DATA HN/0.07/, HL/0.105/	SLPLOT
	WIDTHF = 1.0	SLPLOT
	WN = WIDTHF*HN	REDIMN
	WL = WIDTHF*HL	SLPLOT
C	** PLOT PAGE INITIALIZATION **	SLPLOT
	CALL PLOT (0.0,0.0,-3)	SLPLOT
	XP = 0.5*(XSIZE-(XL-0.5))	CHANGE
	YP = 0.5*(YSIZE-(YL-1.0))	SLPLOT
	CALL PLOT (XP,YP,-3)	SLPLOT
	NXPOS = NX.GT.0	SLPLOT
	NXNEG = NX.LT.0	SLPLOT
	NYPOS = NY.GT.0	SLPLOT
	NYNEG = NY.LT.0	SLPLOT
C	** PLOT AXES AND ID LABELS. **	SLPLOT
	XP = 0.0	SLPLOT
	YP = 0.0	SLPLOT
	IF (.NOT.NXPOS) GO TO 12	SLPLOT
C	** LINEAR X AXIS **	SLPLOT
	CALL LINAXS (XP, YP, 0.0, NX, XL)	SLPLOT
	XB = XL/(XN-XO)	SLPLOT
C	** LINEAR X AXIS NUMERICS **	SLPLOT
	DX = XL/FLOAT(NX)	SLPLOT
	EX = XO	SLPLOT
	DD = (XN-XO)/FLOAT(NX)	SLPLOT
	ND = 0.99 - ALOG10(ABS(DD))	SLPLOT
	IF (ND.LE.0) ND = -1	SLPLOT
	IX = 0	SLPLOT
	YC = YP - 2.0*HN	SLPLOT
11	AX = ABS(EX)	SLPLOT
	NF = 0	SLPLOT
	IF (AX.GE.10.0) NF = ALOG10(AX)	SLPLOT
	NS = 0	SLPLOT
	IF (EX.LT.0.0) NS = 1	SLPLOT
	SP = NS+NF+2+ND	SLPLOT
	XC = XP - 0.5*SP*WN	SLPLOT
	CALL NUMBER (XC, YC, HN, EX, 0.0, ND)	SLPLOT
	XP = XP + DX	SLPLOT
	EX = EX + DD	SLPLOT
	IX = IX + 1	SLPLOT
	IF (ABS(EX).GT.ABS(0.1*DD)) GO TO 18	SLPLOT
	IF (IX.GT.NX) GO TO 12	SLPLOT
	CALL PLOT (XP, YP+YL,3)	SLPLOT
	CALL PLOT (XP, YP,2)	SLPLOT
18	IF (IX.LE.NX) GO TO 11	SLPLOT
12	IF (.NOT.NXNEG) GO TO 14	SLPLOT

C	**	LOG X AXIS	**	SLPLOT
		CALL LOGAXS (XP, YP, 0.0, -NX, XL)		SLPLOT
		XB = XL/ALOG(10.0**(-NX))		SLPLOT
		XA = -XB*ALOG(X0)		SLPLOT
C	**	LOG X AXIS NUMERICS	**	SLPLOT
		DX = XL/FLOAT(-NX)		SLPLOT
		EX = ALOG10(X0)		SLPLOT
		IX = 0		SLPLOT
13		CALL NUMBER (XP-1.0*WN, YP-2.5*HN, HN, 10.0, 0.0, -1)		SLPLOT
		CALL NUMBER (XP+1.0*WN, YP-2.0*HN, HN, EX, 0.0, -1)		SLPLOT
		XP = XP + DX		SLPLOT
		EX = EX + 1.0		SLPLOT
		IX = IX - 1		SLPLOT
		IF (IX.GE.NX) GO TO 13		SLPLOT
14		IF (NXLB.LE.0) GO TO 15		SLPLOT
C	**	X AXIS LABEL	**	SLPLOT
		XPX = (XL-FLOAT(NXLB)*WL)/2.0		SLPLOT
		YPX = YP-4.0*HN-HL		SLPLOT
		CALL SYMBOL(XPX, YPX, HL, XLAB, 0.0, NXLB)		SLPLOT
15		IF (NPLB1.LE.0) GO TO 16		SLPLOT
C	**	PLOT LABEL - 1ST LINE	**	SLPLOT
		XP1 = (XL-FLOAT(NPLB1)*WL)/2.0		SLPLOT
		YP1 = YP-4.0*HN-4.0*HL		SLPLOT
		CALL SYMBOL(XP1, YP1, HL, PLAB1, 0.0, NPLB1)		SLPLOT
16		IF (NPLB2.LE.0) GO TO 20		SLPLOT
C	**	PLOT LABEL - 2ND LINE	**	SLPLOT
		XP2 = (XL-FLOAT(NPLB2)*WL)/2.0		SLPLOT
		YP2 = YP-4.0*HN-6.0*HL		SLPLOT
		CALL SYMBOL(XP2, YP2, HL, PLAB2, 0.0, NPLB2)		SLPLOT
20		XP = 0.0		SLPLOT
C	**	COMPLETE AXIS GRID	**	SLPLOT
		IF (NYPOS) CALL LINAXS (XL, YP, 90.0, NY, YL)		SLPLOT
		IF (NYNEG) CALL LOGAXS (XL, YP, 90.0, -NY, YL)		SLPLOT
		IF (NXPOS) CALL LINAXS (XL, YL, 180.0, NX, XL)		SLPLOT
		IF (NXNEG) CALL LOGAXS (XL, YL, 180.0, -NX, -XL)		SLPLOT
		IF (.NOT.NYPOS) GO TO 22		SLPLOT
C	**	LINEAR Y AXIS	**	SLPLOT
		CALL LINAXS (XP, YL, -90.0, NY, YL)		SLPLOT
		YB = YL/(YN-Y0)		SLPLOT
C	**	LINEAR Y AXIS NUMERICS	**	SLPLOT
		DY = YL/FLOAT(NY)		SLPLOT
		EY = Y0		SLPLOT
		DD = (YN-Y0)/FLOAT(NY)		SLPLOT
		ND = 0.99 - ALOG10(ABS(DD))		SLPLOT
		IF (ND.LE.0) ND = -1		SLPLOT
		IY = 0		SLPLOT
		XC = XP - 1.0*HN		SLPLOT
21		AY = ABS(EY)		SLPLOT
		NF = 0		SLPLOT
		IF (AY.GE.10.0) NF = ALOG10(AY)		SLPLOT
		NS = 0		SLPLOT
		IF (EY.LT.0.0) NS = 1		SLPLOT



SP = NS+NF+2+ND	SLPLOT
YC = YP - 0.5*SP*WN	SLPLOT
CALL NUMBER (XC, YC, HN, EY, 90.0, ND)	SLPLOT
YP = YP + DY	SLPLOT
EY = EY + DD	SLPLOT
IY = IY + 1	SLPLOT
IF (ABS(EY).GT.ABS(0.1*DD)) GO TO 19	SLPLOT
IF (IY.GT.NY) GO TO 22	SLPLOT
CALL PLOT (XP+XL, YP, 3)	SLPLOT
CALL PLOT (XP, YP, 2)	SLPLOT
19 IF (IY.LE.NY) GO TO 21	SLPLOT
22 IF (.NOT.NYNEG) GO TO 24	SLPLOT
C       **       LOG Y AXIS       **	SLPLOT
CALL LOGAXS (XP, YL, -90.0, -NY, -YL)	SLPLOT
YB = YL/ALOG(10.0**(-NY))	SLPLOT
YA = -YB*ALOG(YO)	SLPLOT
C       **       LOG Y AXIS NUMERICS       **	SLPLOT
DY = YL/FLOAT(-NY)	SLPLOT
EY = ALOG10(YO)	SLPLOT
IY = 0	SLPLOT
23 CALL NUMBER (XP-1.0*HN, YP-1.0*WN, HN, 10.0, 90.0, -1)	SLPLOT
CALL NUMBER (XP-1.5*HN, YP+1.0*WN, HN, EY, 90.0, -1)	SLPLOT
YP = YP + DY	SLPLOT
EY = EY + 1.0	SLPLOT
IY = IY - 1	SLPLOT
IF (IY.GE.NY) GO TO 23	SLPLOT
24 IF (NYLB.LE.0) GO TO 25	SLPLOT
C       **       Y AXIS LABEL       **	SLPLOT
XPY = XP-4.0*HN	SLPLOT
YPY = (YL-FLOAT(NYLB)*WL)/2.0	SLPLOT
CALL SYMBOL(XPY, YPY, HL, YLAB, 90.0, NYLB)	SLPLOT
25 CONTINUE	SLPLOT
C       **       PLOT DATA ARRAYS       **	SLPLOT
NSYM = 24	SLPLOT
IS = NPTS/NSYM	SLPLOT
IF (IS.EQ.0) IS = 1	VARTTH
XOMIN = XO/1000.0	SLPLOT
YOMIN = YO/1000.0	SLPLOT
DO 40 J=1, NYY	SLPLOT
IPEN = 3	SLPLOT
DO 39 I=1, NPTS	SLPLOT
X1 = X2	SLPLOT
Y1 = Y2	SLPLOT
IF (NXPOS) X2 = XB*(X(I) -XO)	SLPLOT
IF (NYPOS) Y2 = YB*(Y(I,J)-YO)	SLPLOT
IF (NXNEG) X2 = XA + XB*ALOG(AMAX1(X(I), XOMIN))	SLPLOT
IF (NYNEG) Y2 = YA + YB*ALOG(AMAX1(Y(I,J), YOMIN,))	SLPLOT
IF (Y2.LT.0.0 .OR. Y2.GT.YL) GO TO 33	SLPLOT
IF (X2.LT.0.0 .OR. X2.GT.XL) GO TO 33	SLPLOT
IF (IPEN.EQ.3) GO TO 33	SLPLOT
CALL PLOT (X2,Y2,IPEN)	SLPLOT
C       **       PLOT NYSM SYMBOLS       **	SLPLOT

IF (NYY.EQ.1 .OR. MOD(I,IS).NE.0) GO TO 39	SLPLOT
IF (MOD((I/IS)-1,NYY)+1.EQ.J)	80386
* CALL SYMBOL (X2,Y2,0.14,CHAR(J),0.0,-2)	80386
GO TO 39	SLPLOT
33 IF (I.EQ.1) GO TO 39	SLPLOT
DX = X2 - X1	SLPLOT
IF (DX.NE.0.0) GO TO 34	SLPLOT
AX0 = 1.0	SLPLOT
AXL = 0.0	SLPLOT
IF (X1.GE.0.0) AX0 = 0.0	SLPLOT
IF (X1.LE.XL ) AXL = 1.0	SLPLOT
GO TO 35	SLPLOT
34 AX0 = -X1 /DX	SLPLOT
AXL = (XL-X1)/DX	SLPLOT
35 AX1 = AMIN1(AX0,AXL)	SLPLOT
AX2 = AMAX1(AX0,AXL)	SLPLOT
DY = Y2 - Y1	SLPLOT
IF (DY.NE.0.0) GO TO 36	SLPLOT
AY0 = 1.0	SLPLOT
AYL = 0.0	SLPLOT
IF (Y1.GE.0.0) AY0 = 0.0	SLPLOT
IF (Y1.LE.YL ) AYL = 1.0	SLPLOT
GO TO 37	SLPLOT
36 AY0 = -Y1 /DY	SLPLOT
AYL = (YL-Y1)/DY	SLPLOT
37 AY1 = AMIN1(AY0,AYL)	SLPLOT
AY2 = AMAX1(AY0,AYL)	SLPLOT
A1 = AMAX1(AX1,AY1,0.0)	SLPLOT
A2 = AMIN1(AX2,AY2,1.0)	SLPLOT
IF (A1.GE.A2 ) GO TO 39	SLPLOT
XP = X1 + A1*DX	SLPLOT
YP = Y1 + A1*DY	SLPLOT
CALL PLOT(XP,YP,IPEN)	SLPLOT
IPEN = 2	SLPLOT
XP = X1 + A2*DX	SLPLOT
YP = Y1 + A2*DY	SLPLOT
CALL PLOT(XP,YP,IPEN)	SLPLOT
IF (A2.NE.1.0) IPEN = 3	SLPLOT
39 CONTINUE	SLPLOT
40 CONTINUE	SLPLOT
RETURN	SLPLOT
END	SLPLOT

C

SUBROUTINE SOLVA(R,AA11,AA22,AA12)

REV III.2 08/08/84REVIII

IMPLICIT REAL\*8 (A-H,O-Z)

DIMENSION R(2,3)

A11=R(1,1)\*\*2

A12=2.0\*R(2,1)\*R(1,1)

A13=R(2,1)\*\*2

A21=R(1,2)\*\*2

A22=2.0\*R(2,2)\*R(1,2)

A23=R(2,2)\*\*2

A31=R(1,3)\*\*2

A32=2.0\*R(2,3)\*R(1,3)

A33=R(2,3)\*\*2

DEL=A11\*(A22\*A33-A23\*A32)-A12\*(A21\*A33-A23\*A31)+

\* A13\*(A21\*A32-A22\*A31)

AA11=((A22-A12)\*(A33-A23)-(A23-A13)\*(A32-A22))/DEL

AA12=((A23-A13)\*(A31-A21)-(A21-A11)\*(A33-A23))/DEL

AA22=((A21-A11)\*(A32-A22)-(A22-A12)\*(A31-A21))/DEL

RETURN

END

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	SUBROUTINE SOLVR(A1,A2,A3,A4,A5,A6,A7,A8,P,RX,RZ)	SOLVR
C		REV III.2 08/08/84REVIII
	IMPLICIT REAL*8 (A-H,O-Z)	SOLVR
C		SOLVR
C	*****	SOLVR
C		SOLVR
C	THIS SUBROUTINE WILL SOLVE A SET OF SIMULTANEOUS EQUATIONS	SOLVR
C	TO FIND COMPONENTS OF VECTOR R THAT SATISFY THE PROPERTIES NEEDED	SOLVR
C	TO DETERMINE THE EQUATION OF THE PROJECTED ELLIPSE.	SOLVR
C		SOLVR
C	SEE WRITEUP.	SOLVR
C		SOLVR
C	*****	SOLVR
	DIMENSION P(3)	SOLVR
	B=A1*P(1)+A2*P(2)+A3*P(3)	SOLVR
	D=A4*P(1)+A5*P(2)+A6*P(3)	SOLVR
	T1=A7*(D/B)**2+A6-2.0*A8*D/B	SOLVR
	T2=2.0*A7*D/(B)**2-2.0*A8/B	SOLVR
	T3=A7*(1/B)**2-1	SOLVR
	RZ=(-T2+DSQRT(T2**2-4.0*T1*T3))/(2.0*T1)	SOLVR
	RX=-D*RZ/B-1.0/B	SOLVR
	RETURN	SOLVR
	END	SOLVR



DDO = DEL-ASD(1,I)	SPDAMP
IF (DDO.LE.0.0 .AND. ASD(2,I).LE.0.0) GO TO 41	SPDAMP
FS = DDO*(DABS(ASD(2,I)) + DABS(DDO)*ASD(3,I))	SPDAMP
FD = DMV*(ASD(4,I)+DABS(DMV)*ASD(5,I))	SPDAMP
GO TO 29	SPDAMP
21 DDO = DEL+ASD(1,I)	SPDAMP
JF1 = ASD(2,I)	SPDAMP
IF (JF1.EQ.0) GO TO 22	SPDAMP
JF2 = NTI(JF1)	SPDAMP
IF (DDO.GT.0.0 .OR. ASD(3,I).EQ.0.0) FS = EVALFD(DDO,JF2,1)	SPDAMP
22 JF3 = ASD(4,I)	SPDAMP
IF (JF3.EQ.0) GO TO 29	SPDAMP
JF4 = NTI(JF3)	SPDAMP
IF (DDO.GT.0.0 .OR. ASD(3,I).EQ.0.0) FD = EVALFD(DMV,JF4,1)	SLIP
29 DO 30 K=1,3	SPDAMP
30 TOTF(K) = (FS+FD)*DUNIT(K)	SPDAMP
C	SPDAMP
C AND ADD THE RESULTING FORCE AND TORQUE TO THE U1 AND U2 ARRAYS.	SPDAMP
C	SPDAMP
CALL MAT31(D(1,1,M),TOTF,T5)	SPDAMP
CALL MAT31(D(1,1,N),TOTF,T6)	SPDAMP
CALL CROSS(APSDM(1,I),T5,T7)	SPDAMP
CALL CROSS(APSDN(1,I),T6,T8)	SPDAMP
DO 40 K=1,3	SPDAMP
U1(K,M) = U1(K,M) - TOTF(K)	SPDAMP
U1(K,N) = U1(K,N) + TOTF(K)	SPDAMP
U2(K,M) = U2(K,M) - T7(K)	SPDAMP
40 U2(K,N) = U2(K,N) + T8(K)	SPDAMP
41 IBSF = 3-2*MOD(I,2)	SPDAMP
NBSF = NBSFO + (I+1)/2	SPDAMP
BSF(IBSF ,NBSF) = DEL	SPDAMP
BSF(IBSF+1,NBSF) = FD + FS	SPDAMP
90 CONTINUE	SPDAMP
CALL ELTIME(2,32)	SPDAMP
RETURN	SPDAMP
END	SPDAMP

```

C      SUBROUTINE SPLINE (X,Y,F,N,L)
C
C      REV 19      05/14/79
C
C      ROUTINE TO FIT A SET OF POLYNOMIALS OF DEGREE L
C      TO A SET OF GIVEN DATA POINTS (X(I),Y(I),I=1,N)
C
C      FUNCTION IS OF FORM:
C
C      Y = F(2,K) + F(3,K)*DX + F(4,K)*DX**2 + F(5,K)*DX**3
C
C      WHERE: DX = XX - F(1,K)
C      F(1,K) .LE. XX .LT. F(1,K+1) ; (SETS K)
C      IF (XX.GT.F(1,N)) ; USE K=N, CONSTANT FIT TO Y(N)
C      IF (XX.LT.F(1,1)) ; EXTRAPOLATED FIT FOR K=1
C
C      F(1,I) = X(I) ,      I=1,N
C      F(2,I) = Y(I) ,      I=1,N
C
C      DEGREE L      CONTINUITY
C      0  F(3,I) = F(4,I) = F(5,I) = 0 , I=1,N      NONE
C      1  F(4,I) = F(5,I) = 0 ,      I=1,N      Y
C      2  F(5,I) = 0 ,      I=1,N      Y,Y'
C      3  CUBIC SPLINE      Y,Y',Y''
C
C      F(K,N)=0 FOR K=3,5 IN ALL CASES
C
C      FOR L=2 AND L=3 THE CHANGES IN THE L'TH DERIVATIVES ARE MINIMIZED
C
C      SPECIAL CASES:
C      N=1 ;      TREATED AS L=0
C      N=2 ;      TREATED AS L=MIN(L,1)
C      L<0 ;      TREATED AS L=0
C      L>3 ;      TREATED AS L=3
C
C      STORAGE REQUIRED X(N),Y(N),F(5,N); SET BY CALLING PROGRAM
C
C      USAGE:
C      ALL COMPUTATIONS AND REAL VARIABLES ARE DOUBLE PRECISION
C      GIVEN: L,N, (X(I),Y(I),I=1,N)
C      CALL SPLINE (X,Y,F,N,L) ; SETS F
C
C      TO EVALUATE FUNCTION AND DERIVATIVES AT POINT XX
C
C      DO 10 K=1,N
C      IF (K.EQ.N) GO TO 11
C      IF (XX.LT.F(1,K+1)) GO TO 11
C      10 CONTINUE
C      11 DX = XX - F(1,K)
C      YY = F(2,K) + DX*(F(3,K)+DX*(F(4,K)+DX*(F(5,K))))
C      YD = F(3,K) + DX*(2.0*F(4,K)+3.0*DX*F(5,K))
C      YDD = 2.0*F(4,K) + 6.0*DX*F(5,K)

```

C	YDED = 6.0*F(5,K)	SPLINE
C	YDDDD = 0.0	SPLINE
CC		SPLINE
CC	FUNCTIONAL VALUE IN YY, DERIVATIVES IN YD'S	SPLINE
CC	REPEAT FOR NEXT VALUE OF XX	SPLINE
C		SPLINE
C	AUTHOR: DR. JOHN T. FLECK	SPLINE
C		SPLINE
	IMPLICIT REAL*8 (A-H,O-Z)	SPLINE
	DIMENSION X(N),Y(N),F(5,N),C(2,3)	SPLINE
	DO 20 I=1,N	SPLINE
	F(1,I) = X(I)	SPLINE
	DO 10 K=2,5	SPLINE
10	F(K,I) = 0.0	SPLINE
	IF (L.LT.3) F(2,I) = Y(I)	SPLINE
20	IF (L.GT.0 .AND. I.LT.N) F(3,I) = (Y(I+1)-Y(I))/(X(I+1)-X(I))	SPLINE
	IF (L.LT.2 .OR. N.LT.3) GO TO 99	SPLINE
	IF (L.GE.3) GO TO 50	SPLINE
	D1 = X(2) - X(1)	SPLINE
	SS = 0.0	SPLINE
	DS = 0.0	SPLINE
	DO 30 I=3,N	SPLINE
	F(4,I-1) = F(3,I-1) - F(3,I-2) - F(4,I-2)	SPLINE
	DX1 = X(I) - X(I-1)	SPLINE
	DX2 = X(I-1) - X(I-2)	SPLINE
	DD = D1/DX1 + D1/DX2	SPLINE
	SS = SS + DD*DD	SPLINE
	DS = DS + DD*(F(4,I-1)/DX1 - F(4,I-2)/DX2)	SPLINE
30	D1 = -D1	SPLINE
	F(4,1) = DS/SS	SPLINE
	DX = (X(2)-X(1))*F(4,1)	SPLINE
	F(3,1) = F(3,1) - DX	SPLINE
	DO 40 I=3,N	SPLINE
	XX = F(4,I-1) - DX	SPLINE
	F(3,I-1) = F(3,I-1) - XX	SPLINE
	F(4,I-1) = XX/(X(I)-X(I-1))	SPLINE
40	DX = -DX	SPLINE
	GO TO 99	SPLINE
C		SPLINE
C	CUBIC SPLINE	SPLINE
C		SPLINE
50	DO 51 I=2,N	SPLINE
	IF (I.EQ.N) GO TO 51	SPLINE
	F(4,I) = 3.0*(F(3,I)-F(3,I-1))	SPLINE
	F(5,I) = 2.0*(X(I+1)-X(I-1))	SPLINE
51	F(3,I-1) = 0.0	SPLINE
	F(2,N) = -1.0	SPLINE
	F(3,1) = -1.0	SPLINE
	DO 60 I=3,N	SPLINE
	DX = X(I-1) - X(I-2)	SPLINE
	IF (I.GT.3) DX = DX/F(5,I-2)	SPLINE
	DO 60 K=3,5	SPLINE



60	F(K,I-1) = F(K,I-1) - F(K,I-2)*DX**((K-1)/2)	SPLINE
	DO 70 I=3,N	SPLINE
	NI = N-I	SPLINE
	DX = X(NI+3) - X(NI+2)	SPLINE
	DO 70 K=2,4	SPLINE
70	F(K,NI+2) = (F(K,NI+2) - DX*F(K,NI+3))/F(5,NI+2)	SPLINE
	DO 71 J=1,2	SPLINE
	DO 71 K=J,3	SPLINE
	C(J,K) = 0.0	SPLINE
	DO 71 I=3,N	SPLINE
	DX1 = X(I) - X(I-1)	SPLINE
	DX2 = X(I-1) - X(I-2)	SPLINE
71	C(J,K) = C(J,K) + ( (F(J+1,I) - F(J+1,I-1))/DX1	SPLINE
	* - (F(J+1,I-1) - F(J+1,I-2))/DX2)	SPLINE
	* * ( (F(K+1,I) - F(K+1,I-1))/DX1	SPLINE
	* - (F(K+1,I-1) - F(K+1,I-2))/DX2)	SPLINE
	DEN = C(1,1)*C(2,2) - C(1,2)*C(1,2)	SPLINE
	F(4,1) = (C(1,1)*C(2,3) - C(1,2)*C(1,3))/DEN	SPLINE
	F(4,N) = (C(2,2)*C(1,3) - C(1,2)*C(2,3))/DEN	SPLINE
	DO 72 I=3,N	SPLINE
72	F(4,I-1) = F(4,I-1) - F(4,1)*F(3,I-1) - F(4,N)*F(2,I-1)	SPLINE
	D1 = X(2) - X(1)	SPLINE
	F(3,1) = (Y(2)-Y(1))/D1 - (2.0*F(4,1)+F(4,2))*D1/3.0	SPLINE
	F(2,1) = Y(1)	SPLINE
	DO 80 I=2,N	SPLINE
	F(2,I) = Y(I)	SPLINE
	DX = X(I) - X(I-1)	SPLINE
	IF (I.LT.N) F(3,I) = F(3,I-1) + (F(4,I)+F(4,I-1))*DX	SPLINE
80	F(5,I-1) = (F(4,I)-F(4,I-1))/(3.0*DX)	SPLINE
	F(4,N) = 0.0	SPLINE
99	RETURN	SPLINE
	END	SPLINE

```

DOUBLE PRECISION FUNCTION SPRNGF(T,D,ZD,SPR,JSTOP)          SPRNGF
C                                                     REV IV    07/23/86TWOPI
C COMPUTES NONLINEAR SPRING TORQUE FOR JOINTS AS A FUNCTION OF ANGLESPRNGF
C ACTUALLY ROUTINE RETURNS TORQUE/ABS(SIN THETA)          SPRNGF
C                                                     SPRNGF
C ARGUMENTS:                                             SPRNGF
C     T      : COS THETA WHERE THETA IS ANGLE OF JOINT (0<THETA<PI) SPRNGF
C     D      : ABS(SIN THETA)                            SPRNGF
C     ZD     : -THETA DOT * SIN THETA                     SPRNGF
C     SPR    : ARRAY OF 5 VALUES DESCRIBING FUNCTION EVALUATION SPRNGF
C     JSTOP  : INDICATOR TO BE SET TO ONE IF JOINT IS IN STOP SPRNGF
C                                                     SPRNGF
C IMPLICIT REAL*8 (A-H,O-Z)                             SPRNGF
COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),              SPRNGF
*          UNITL,UNITM,UNITT,GRAVITY(3),TWOPI          TWOPI
DIMENSION SPR(5)                                         SPRNGF
C                                                     SPRNGF
C     RESET T=1 IF T>1 (HAD & HBD IN VISPR)             SPRNGF
C                                                     SPRNGF
C IF (T.GT.1.0) T = 1.0                                  SPRNGF
C IF (T.LT.-1.0) T = -1.0                                SPRNGF
C Z = DACOS(T)                                            SPRNGF
C U = EPS(1)*D                                           SPRNGF
C Q = 0.0                                                 SPRNGF
C IF (D.NE.0.0) Q = -ZD/U                                SPRNGF
C IF (Q.GT.1.0) Q = 1.0                                  SPRNGF
C IF (Q.LT.-1.0) Q = -1.0                                SPRNGF
C X = 0.5*(1.0+SPR(4) + Q*(1.0-SPR(4))) )               SPRNGF
C Y = 0.0                                                 SPRNGF
C IF (D.NE.0.0) Y = Z/D                                  SPRNGF
C Q = 1.0                                                 SPRNGF
C IF (DABS(Z).LT.EPS(4)) Y = DSIGN(Q,Z)                 SPRNGF
C SPRNGF = Y*SPR(1)                                       SPRNGF
C JSTOP = 0                                               SPRNGF
C IF (SPR(5).GT.0.0) GO TO 10                             SPRNGF
C SPRNGF = X*SPRNGF                                       SPRNGF
C GO TO 11                                                SPRNGF
10 IF (Z.LT.SPR(5)) GO TO 11                             SPRNGF
C JSTOP = 1                                               SPRNGF
C Z = Z-SPR(5)                                            SPRNGF
C SPRNGF = SPRNGF + X/D*(SPR(2)+Z*SPR(3))*Z**2          SPRNGF
11 CONTINUE                                              SPRNGF
C RETURN                                                  SPRNGF
C END                                                     SPRNGF

```

C

SUBROUTINE TRIGFS	REV 19	08/05/78	TRIGFS
IMPLICIT REAL*8 (A-H,O-Z)			TRIGFS
COMMON/CDINT/ UU(4),GH(3,4),			TRIGFS
* E(3,240), F(5,240),GG(5,240),Y(5,240),U(5,240),			TRIGFS
* H,HPRINT,HS,TPRINT,TSTART,ICNT,IDBL,IFLAG,IDMMY			80386
BETA = 0.0			TRIGFS
IF (HS.NE.0.0) BETA = (H/HS)**2			TRIGFS
R1 = HS/H			TRIGFS
R2 = 1.0+BETA*R1			TRIGFS
GH(3,1) = 2.0/(H*R2)			TRIGFS
GH(2,1) = GH(3,1)*(BETA-1.0)			TRIGFS
GH(1,1) = GH(3,1)* BETA			TRIGFS
GH(1,2) = 4.0*BETA/(R2*H**2)			TRIGFS
GH(3,2) = GH(1,2)* R1			TRIGFS
GH(2,2) = GH(1,2)*(R1+1.0)			TRIGFS
GH(3,3) = 1.0/H			TRIGFS
GH(2,3) = 4.0*GH(3,3)			TRIGFS
GH(1,3) = 3.0*GH(3,3)			TRIGFS
GH(3,4) = 2.0/H**2			TRIGFS
GH(2,4) = 2.0*GH(3,4)			TRIGFS
GH(1,4) = GH(3,4)			TRIGFS
UU(1) = 2.0/H			TRIGFS
UU(2) = 0.0			TRIGFS
UU(3) = 0.5*H			TRIGFS
UU(4) = 0.25*H**2			TRIGFS
IF (HS.EQ.0.0) GO TO 99			TRIGFS
UU(1) = BETA*(4.25+2.25/R1)			TRIGFS
UU(2) = BETA*(2.25+1.25/R1)/R1			TRIGFS
UAU = 1.0+UU(1)+UU(2)			TRIGFS
UU(1) = 2.0*UU(1)/(UAU*H)			TRIGFS
UU(2) = 4.0*UU(2)/(UAU*H**2)			TRIGFS
99 RETURN			TRIGFS
END			TRIGFS



DO 22 K=1,30	UNIT1
DO 22 J=1,3	UNIT1
DO 21 I=1,3	UNIT1
21 XD(I,J,K) = D(I,J,K)	UNIT1
22 XSEGLP(J,K) = SEGLP(J,K)	UNIT1
DO 25 K=1,NSEG	UNIT1
IF (LPMI(K).EQ.0) GO TO 25	UNIT1
CALL DOT33 (DPMI(1,1,K),D(1,1,K),T3)	UNIT1
DO 24 I=1,3	UNIT1
DO 24 J=1,3	UNIT1
24 XD(I,J,K) = T3(I,J)	UNIT1
25 CONTINUE	UNIT1
WRITE (1) XTIME,XSEGLP,XD	UNIT1
99 RETURN	UNIT1
END	UNIT1

	SUBROUTINE UPDATE(I)		UPDATE
C		REV IV	07/24/86SLIP
C	CALL BY SUBROUTINE DINT		UPDATE
C			UPDATE
C	(I=1) AT THE START OF A NEW STEP TO SETUP ANY NEW CONDITIONS		UPDATE
C	TO BE VALID FOR ENTIRE INTEGRATION STEP		UPDATE
C	A. UPDATE FORCE DEFLECTION FUNCTIONS(SUBROUTINE UPDFDC)		UPDATE
C	B. TEST FOR LOCKED JOINTS		UPDATE
C	NOTE: ARGUMENT I WILL BE SET TO -1 TO RESET INTEGRATOR.		UPDATE
C			UPDATE
C	(I=2) AT THE END OF EACH SUCCESSFUL INTEGRATION STEP TO		UPDATE
C	COMPLETE CALCULATIONS FOR OUTPUT (SUBROUTINE AIRBG3).		UPDATE
C			UPDATE
	IMPLICIT REAL*8(A-H,O-Z)		UPDATE
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		UPDATE
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),		UPDATE
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		UPDATE
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),		SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),		UPDATE
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)		UPDATE
	COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),		UPDATE
*	F(3,30),TQ(3,30),WJ(30),A11(3,3,30)		.IP
	COMMON/JBARTZ/ MNPL( 30),MNBLT( 8),MNSEG( 30),MNBAG( 6)		ATE
*	MPL(3,5,30),MBLT(3,5,8),MSEG(3,5,30),MBAG(3,10,6),		UPDATE
*	NTPL( 5,30),NTBLT( 5,8),NTSEG( 5,30)		UPDATE
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)		UPDATE
	COMMON/FORCES/PSF(7,70),BSF(4,20),SSF(10,40),BAGSF(3,20),		NCFORC
*	PRJNT(7,30),NPANEL(5),NPSF,NBSF,NSSF,NBGSF		UPDATE
	COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24),		UPDATE
*	HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12),		UPDATE
*	RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12),		UPDATE
*	KQ1(12),KQ2(12),KQTYPE(12)		UPDATE
	COMMON/TEMPVI/ CREST,TTI(3),R1I(3),R2I(3),JSTOP(4,2,30)		UPDATE
	COMMON/CEULER/ IEULER(30),HIR(3,3,90),ANG(3,30),ANGD(3,30),		JDRIFT
*	FE(3,30),TQE(3,30),CONST(5,30)		JDRIFT
	COMMON/HRNESS/ BAR(15,100),BB(100),BBDOT(100),PLOSS(2,100),		UPDATE
*	XLONG(20),HTIME(2),IBAR(5,100),NL(2,100),		UPDATE
*	NPTSPB(20),NPTPLY(20),NTHRNS(20),NBLTPH(5)		UPDATE
	DIMENSION TQTEST(3),LOCK(8,3),T(3)		UPDATE
	DATA LOCK,-8, 6, 5, 7,-3,-2,-4, 1,		UPDATE
*	6,-8, 4,-3, 7,-1,-5, 2,		UPDATE
*	5, 4,-8,-2,-1, 7,-6, 3/		UPDATE
C			UPDATE
C	CALL AIRBG3 FOR AIRBAG, IF ANY.		UPDATE
C			UPDATE
	IF (NBAG.NE.0) CALL AIRBG3(I)		UPDATE
	IF (I.EQ.2) GO TO 42		UPDATE
	CALL ELTIME (1,7)		UPDATE
	IF (NPL.LE.0) GO TO 13		UPDATE
C			UPDATE
C	CALL UPDFDC FOR EACH ALLOWED PLANE-SEGMENT CONTACT.		UPDATE

C	NPSF = 0	UPDATE
	DO 12 J=1,NPL	UPDATE
	NK = MNPL(J)	UPDATE
	IF (NK.LE.0) GO TO 12	UPDATE
	DO 11 K = 1, NK	UPDATE
	NPSF = NPSF+1	UPDATE
	NT = NTPL(K,J)	UPDATE
	NF = NTAB(NT+5)	UPDATE
	CALL UPDFDC(NT)	UPDATE
	IF (NT.GT.0.OR.TAB(NF+3).EQ.0.0) GO TO 11	UPDATE
	CALL IMPULS(1,K,J)	UPDATE
	I = -1	UPDATE
	11 CONTINUE	UPDATE
	12 CONTINUE	UPDATE
	13 IF (NBLT.LE.0) GO TO 16	UPDATE
C		UPDATE
C	CALL UPDFDC FOR EACH ALLOWED BELT-SEGMENT CONTACT.	UPDATE
C		UPDATE
	DO 15 J=1,NBLT	UPDATE
	NK = MNBLT(J)	UPDATE
	IF (NK.LE.0) GO TO 15	UPDATE
	DO 14 K = 1,NK	UPDATE
	NT = NTBLT(K,J)	UPDATE
	NF = NTAB(NT+5)	UPDATE
	NT6 = NT+6	UPDATE
	CALL UPDFDC(NT)	UPDATE
C		UPDATE
C	AND FOR 2ND FUNCTION, IF FULL BELT FRICTION.	UPDATE
C		UPDATE
	14 IF (NF.NE.0) CALL UPDFDC(NT6)	UPDATE
	15 CONTINUE	UPDATE
C		UPDATE
C	CALL UPDFDC FOR EACH ALLOWED SEGMENT-SEGMENT CONTACT.	UPDATE
C		UPDATE
	16 NSSF = 0	UPDATE
	DO 18 J=1,NSEG	UPDATE
	NK = MNSEG(J)	UPDATE
	IF (NK.LE.0) GO TO 18	UPDATE
	DO 17 K = 1,NK	UPDATE
	NSSF = NSSF+1	UPDATE
	NT = NTSEG(K,J)	UPDATE
	NF = NTAB(NT+5)	UPDATE
	CALL UPDFDC(NT)	UPDATE
	IF (NT.GT.0.OR.TAB(NF+3).EQ.0.0) GO TO 17	UPDATE
	CALL IMPULS(3,K,J)	UPDATE
	I = -1	UPDATE
	17 CONTINUE	UPDATE
	18 CONTINUE	UPDATE
	IF (NHRNSS.LE.0) GO TO 71	UPDATE
C		UPDATE
C	CALL UPDFDC FOR EACH BELT OF HARNESS-BELT SYSTEMS.	UPDATE

```

CALL HPTURB
J1 = 1
K1 = 1
DO 70 II=1,NHRNSS
IF (NBLTPH(II).LE.0) GO TO 70
J2 = J1 + NBLTPH(II) - 1
DO 69 J=J1,J2
IF (NPTPLY(J).LE.0) GO TO 69
NT = NTHRNS(J)
CALL UPDFDC(NT)
K2 = K1 + NPTPLY(J) - 1
DO 68 K=K1,K2
KI = NL(1,K)
NT = IBAR(3,KI)
CALL UPDFDC(NT)
68 CONTINUE
K1 = K2+1
69 CONTINUE
J1 = J2+1
70 CONTINUE
71 IF (NJNT.LE.0) GO TO 37

```

C  
C  
C  
C

```

CHECK FOR IMPULSE ON JOINT STOPS
TO BE CALLED IF IN JOINT STOP (JSTOP(1)-1) THIS TIME STEP
BUT NOT IN IN JOINT STOP (JSTOP(2)=0) AT PREVIOUS TIME.

DO 21 K=1,NJNT
IF (JNT(K).EQ.0) GO TO 21
IF (IABS(IPIN(K)).NE.4 .AND. VISC(7,3*K-2).EQ.0.0) GO TO 20
DO 19 J=1,3
K3J = 3*K-3+J
IF (IABS(IPIN(K)).NE.4) K3J=3*K-2
IF (IABS(IPIN(K)).EQ.4 .AND. VISC(7,K3J).EQ.0.0) GO TO 19
IF (JSTOP(J,1,K).NE.1.OR.JSTOP(J,2,K).NE.0) GO TO 19
CALL IMPULS(4,J,K)
I = -1
19 JSTOP(J,2,K) = JSTOP(J,1,K)
20 IF (IGLOB(K).EQ.0) GO TO 21
NT = IGLOB(K)
MT = NTAB(NT+5)
NT1 = NTAB(NT+2)
NTAB(NT+2) = 0
CALL UPDFDC(NT)
NT = IABS(NT)
NTAB(NT+2) = NT1
IF (TAB(MT+3).EQ.0.0) GO TO 21
IF (JSTOP(4,1,K).NE.1.OR.JSTOP(4,2,K).NE.0) GO TO 21
CALL IMPULS(4,4,K)
I = -1
21 JSTOP(4,2,K) = JSTOP(4,1,K)

```

C

[illegible]



C	TEST TO LOCK OR UNLOCK JOINTS	UPDATE
C		UPDATE
C		UPDATE
C	CONDITIONS TO CHANGE SIGN OF IPIN(J)	UPDATE
C		UPDATE
C	PINNED                  UNPINNED	UPDATE
C	LOCKED (-1) !H.TQ! > T1      (-2) !TQ! > T1	UPDATE
C		UPDATE
C	UNLOCKED (+1) !H.TQ! < T2      (+2) !TQ! < T2	UPDATE
C	OR                                  OR	UPDATE
C	WJ < T3                                  WJ < T3	UPDATE
C		UPDATE
	DO 28 J=1,NJNT	UPDATE
	IF (IABS(IPIN(J)).EQ.4) GO TO 28	UPDATE
	IF (IPIN(J)) 22,28,23	UPDATE
22	T1 = VISC(4,3*J-2)	UPDATE
	IF (T1.EQ.0.0) GO TO 28	UPDATE
	IF (IPIN(J).GT.-1) GOTO 51	SLIP
	IF (IPIN(J).GT.-6.AND.IPIN(J).LT.-1) GOTO 51	SLIP
	TQM = XDY(HB(1,2*J),D(1,1,J+1),TQ(1,J))	UPDATE
	ABSTQM = DABS(TQM)	UPDATE
	IF (ABSTQM.GT.T1) HA(2,2*J-1) = TQM	UPDATE
	TQM = ABSTQM	UPDATE
	GO TO 52	UPDATE
51	TQM = DSQRT(TQ(1,J)**2 + TQ(2,J)**2 + TQ(3,J)**2)	UPDATE
	IF (TQM.GT.T1) CALL DOT31(HIR(1,1,J),TQ(1,J),HA(1,2*J-1))	UPDATE
52	IF (TQM-T1) 28,28,26	UPDATE
23	T2 = VISC(5,3*J-2)	UPDATE
	IF (HA(2,2*J).NE.0.0) GO TO 54	UPDATE
	DO 53 K=1,3	UPDATE
53	HA(K,2*J-1) = 0.0	UPDATE
54	IF (T2.EQ.0.0) GO TO 24	UPDATE
	IF (IPIN(J).GE.2.AND.IPIN(J).LE.5)	SLIP
*	TQM = DSQRT(TQ(1,J)**2+TQ(2,J)**2+TQ(3,J)**2)	SLIP
	IF (IPIN(J).EQ.1.OR.IPIN(J).EQ.6.OR.IPIN(J).EQ.7)	SLIP
*	TQM = DABS(XDY(HB(1,2*J),D(1,1,J+1),TQ(1,J)))	SLIP
	IF (TQM-T2) 25,28,28	UPDATE
24	T3 = VISC(6,3*J-2)	UPDATE
	IF (T3.EQ.0.0) GO TO 28	UPDATE
	IF (WJ(J)-T3) 25,28,28	UPDATE
25	CALL IMPLS2(0,J,HB(1,2*J))	UPDATE
	I = -1	UPDATE
26	IPIN(J) = -IPIN(J)	UPDATE
	TMSEC = 1000.0*TIME	UPDATE
	IPINJ = -IPIN(J)	UPDATE
	WRITE (6,27) TMSEC,J,IPINJ,IPIN(J)	UPDATE
27	FORMAT('0 AT TIME =',F9.3,' MSEC,      IPIN(',I2,	BUTLER1
*	') HAS BEEN CHANGED FROM',I3,' TO',I3)	BUTLER1
28	CONTINUE	UPDATE
C		UPDATE
C	TEST TO LOCK OR UNLOCK EULER JOINTS AXES.	UPDATE
C	USE SAME TEST AS ABOVE BUT ON EACH AXIS SERARATELY.	UPDATE

C		UPDATE
C	IF LOCK(IEULER,K) IS NEGATIVE, AXIS K IS LOCKED;	UPDATE
C	TO UNLOCK AXIS SET IEULER TO -LOCK(IEULER,K).	UPDATE
C		UPDATE
C	IF LOCK(IEULER,K) IS POSITIVE, AXIS K IS UNLOCKED;	UPDATE
C	TO LOCK AXIS SET IEULER TO LOCK(IEULER,K).	UPDATE
C		UPDATE
	DO 36 J=1,NJNT	UPDATE
	IF (IABS(IPIN(J)).NE.4) GO TO 36	UPDATE
	JEULER = IEULER(J)	UPDATE
	CALL DOT31(HIR(1,1,J),TQ(1,J),TQTEST)	UPDATE
	DO 31 K=1,3	UPDATE
	K3J = 3*J-3+K	UPDATE
	NLOCK = LOCK(JEULER,K)	UPDATE
	IF (NLOCK.GT.0) GO TO 29	UPDATE
	IF (VISC(4,K3J).EQ.0.0) GO TO 31	UPDATE
	IF (DABS(TQTEST(K)).LE.VISC(4,K3J)) GO TO 31	UPDATE
	JEULER = -NLOCK	UPDATE
	HA(K,2*J-1) = TQTEST(K)	UPDATE
	GO TO 31	UPDATE
29	IF (HA(K,2*J).EQ.0.0) HA(K,2*J-1) = 0.0	UPDATE
	IF (VISC(5,K3J).EQ.0.0) GO TO 30	UPDATE
	IF (DABS(TQTEST(K)).LT.VISC(5,K3J)) JEULER = NLOCK	UPDATE
	GO TO 31	UPDATE
30	IF (VISC(6,K3J).EQ.0.0) GO TO 31	UPDATE
	IF (DABS(ANGD(K,J)).LT.VISC(6,K3J)) JEULER = NLOCK	UPDATE
31	CONTINUE	UPDATE
	IF (JEULER.EQ.IEULER(J)) GO TO 36	UPDATE
	TMSEC = 1000.0*TIME	UPDATE
	WRITE (6,2) TMSEC,J,IEULER(J),JEULER	UPDATE
32	FORMAT('0 AT TIME =',F9.3,' MSEC, IEULER(' ,I2,	UPDATE
*	' ) HAS BEEN CHANGED FROM',I3,' TO',I3)	BUTLER1
	IF (JEULER.EQ.8) GO TO 35	BUTLER1
	IF (IEULER(J).EQ.7) GO TO 35	UPDATE
	IF (IEULER(J).EQ.6 .AND. (JEULER.EQ.2.OR.JEULER.EQ.1)) GO TO 35	UPDATE
	IF (IEULER(J).EQ.5 .AND. (JEULER.EQ.3.OR.JEULER.EQ.1)) GO TO 35	UPDATE
	IF (IEULER(J).EQ.4 .AND. (JEULER.EQ.3.OR.JEULER.EQ.2)) GO TO 35	UPDATE
	MODE = -1	UPDATE
	K = JEULER	UPDATE
	IF (K.GT.3) GO TO 33	UPDATE
	IF (K.EQ.2) GO TO 34	UPDATE
	K4 = 4-K	UPDATE
	CALL CROSS (HIR(1,K4,J),HIR(1,2,J),T)	UPDATE
	IEULER(J) = 8	UPDATE
	IPIN(J) = 4	UPDATE
	CALL IMPLS2(MODE,J,T)	UPDATE
	I = -1	UPDATE
	GO TO 35	UPDATE
33	MODE = 1	UPDATE
	K = K-3	UPDATE
	IF (K.GT.3) MODE=0	UPDATE
34	IEULER(J) = 8	UPDATE

	IPIN(J) - 4	UPDATE
	CALL IMPLS2(MODE,J,HIR(1,K,J))	UPDATE
	I - -1	UPDATE
35	IEULER(J) = JEULER	UPDATE
	IPIN(J) = 4	UPDATE
	IF (IEULER(J).NE.8) IPIN(J) = -4	UPDATE
C	GET SINE AND COSINE OF NUTATION IF IEULER GOES TO STATE 2	JDRIFT
	CALL EJOINT(-1,J)	JDRIFT
	IF(JEULER.NE.2) GOTO 36	JDRIFT
	TQM=ANG(2,J)+CONST(2,J)	JDRIFT
	CONST(4,J) = DCOS(TQM)	JDRIFT
	CONST(5,J) = DSIN(TQM)	JDRIFT
36	CONTINUE	UPDATE
	DO 90 J = 1,NJNT	SLIP
	IF (IABS(IPIN(J)).IE.4) GO TO 90	SLIP
	IF (IEULER(J).GE.0) GO TO 90	SLIP
	IF (CONST(1,J).EQ.0.0.AND.CONST(2,J).EQ.0.0) GO TO 90	SLIP
	M = JNT(J)	SLIP
	FTEST = XDY(HT(1,3,2*J-1),D(1,1,M),F(1,J))	SLIP
	IF (FTEST.GE.CONST(1,J).AND.FTEST.LE.CONST(2,J)) GO TO 90	SLIP
	IEULER(J) = 0	SLIP
	TMSEC = 1000.0*TIME	SLIP
	WRITE (6,88) TMSEC,J	SLIP
88	FORMAT('/O AT TIME =',F9.3,' MSEC, JOINT ',I3,' HAS BEEN',	SLIP
	* ' UNLOCKED AND ALLOWED TO SLIP.'/)	SLIP
90	CONTINUE	SLIP
C	F IS THE FORCE ON SEGMENT J+1, - F IS ON SEGMENT M	SLIP
C		UPDATE
37	IF (NQ.LE.0) GO TO 41	UPDATE
	DO 40 K=1,NQ	UPDATE
	IF (KQTYPE(K).LT.3) GO TO 40	UPDATE
	IF (KQTYPE(K).GT.4) GO TO 40	UPDATE
	IF (CFQQ(K).LT.0.0) KQTYPE(K) = -KQTYPE(K)	UPDATE
	IF (CFQQ(K).LT.0.0) GO TO 39	UPDATE
C		UPDATE
C	TEST IF ROLLING CONSTRAINT SHOULD BE SLIDING AND VICE VERSA.	UPDATE
C		UPDATE
	QN = -XDY(TQQ(1,K),HHT(1,1,K),QQ(1,K))	UPDATE
	IF (NPRT(24).NE.0) WRITE (6,38) KQTYPE(K),KQ1(K),KQ2(K),	UPDATE
	* (RK1(II,K),II-1,3), (RK2(II,K),II-1,3),	UPDATE
	* ((HHT(II,J,K),J-1,3), II-1,3),	UPDATE
	* (QQ(II,K),II-1,3), (TQQ(II,K),II-1,3), (RQQ(II,K),II-1,3),	UPDATE
	* (HQQ(II,K),II-1,3), SQQ(K), CFQQ(K), QN	UPDATE
38	FORMAT('O UPDATE ROLL-SLIDE TEST'/(2X,9G14.6))	UPDATE
	IF (QN.LT.0.0) KQTYPE(K) = -4	UPDATE
	IF (QN.LT.0.0) GO TO 39	UPDATE
	QDOTQ = QQ(1,K)**2 + QQ(2,K)**2 + QQ(3,K)**2	UPDATE
	QT = DSQRT(QDOTQ-QN**2)	UPDATE
	IF (KQTYPE(K).EQ.3 .AND. QT.LE.CFQQ(K)*QN) GO TO 40	UPDATE
	IF (KQTYPE(K).EQ.4 .AND. QT.GE.0.9*CFQQ(K)*QN) GO TO 40	UPDATE
	KQTYPE(K) = 7-KQTYPE(K)	UPDATE
39	CALL OUTPUT(0)	UPDATE

CALL SETUP2	UPDATE
CALL DAUX(K)	UPDATE
IF (NPRT(24).NE.0) CALL OUTPUT(1)	UPDATE
IF (NPRT( 3).NE.0) CALL PRINT (6HUPDATE)	UPDATE
I = -1	UPDATE
40 CONTINUE	UPDATE
41 CALL ELTIME(2,7)	UPDATE
42 RETURN	UPDATE
END	UPDATE

```

SUBROUTINE UPDFDC (M)                                UPDFDC
C                                                     REV III.2 08/08/84REVIII
C UPDATE FORCE DEFLECTION CURVE DEFINITION THAT IS DEFINED UPDFDC
C IN LOCATION M OF NTAB ARRAY. SUBROUTINE ASSUMES THAT UPDFDC
C A SUCCESSFUL INTEGRATION STEP HAS JUST BEEN COMPLETED AND UPDFDC
C WILL COMPUTE ENTIRE CURVE DEFINITION TO BE VALID FOR NEXT STEP. UPDFDC
C                                                     UPDFDC
IMPLICIT REAL*8(A-H,O-Z)                             UPDFDC
COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)DIMENB
L = NTAB(M)                                           UPDFDC
IF (L.EQ.0) GO TO 99                                  UPDFDC
D = TAB(L)                                           UPDFDC
IF (D.LT.0.0) D = 0.0                                UPDFDC
DLAST = TAB(L+1)                                     UPDFDC
IF (D.EQ.DLAST) GO TO 99                             UPDFDC
DCUBIC = TAB(L+6)                                     UPDFDC
IF (D.EQ.DCUBIC) GO TO 98                            UPDFDC
AREA = TAB(L+2)                                       UPDFDC
RLAST = TAB(L+3)                                       UPDFDC
GLAST = TAB(L+4)                                       UPDFDC
DG = TAB(L+5)                                         UPDFDC
DGO = DG                                              UPDFDC
DREF = TAB(L+7)                                       UPDFDC
DMAX = TAB(L+8)                                       UPDFDC
DINER = TAB(L+9)                                       UPDFDC
FDMAX = TAB(L+10)                                     UPDFDC
DCO = TAB(L+18)                                       UPDFDC
LQ = L+11                                             UPDFDC
LC = L+14                                             UPDFDC
IF (NTAB(M+1).LT.0) GO TO 98                          UPDFDC
IF (D-DCUBIC) 10,98,20                               UPDFDC
C                                                     UPDFDC
C D < DCUBIC, DEFINE NEW CUBIC                       UPDFDC
C  $Y(X) = A0 + A1*(X-X1) + A2*(X-X1)**2 + A3*(X-X1)**3$  UPDFDC
C WHOSE DERIVATIVE IS                                UPDFDC
C  $Y'(X) = A1 + 2*A2*(X-X1) + 3*A3*(X-X1)**2$  UPDFDC
C                                                     UPDFDC
10 X1 = DMAX1 (D,DG)                                  UPDFDC
X2 = DREF                                             UPDFDC
C                                                     UPDFDC
C IF INERTIAL SPIKE EXISTS AND IF DIMAX < DREF , DROP INERTIAL SPIKEUPDFDC
NI = NTAB(M+2)                                       UPDFDC
IF (NI.GT.0.AND.TAB(NI+3).GT.0.0.AND.DREF.GT.TAB(NI+3))NTAB(M+2)=0UPDFDC
DX = X2-X1                                           UPDFDC
X = X1-DG                                            UPDFDC
Y1 = TAB(LQ) +X *(TAB(LQ+1)+X *TAB(LQ+2))          UPDFDC
Y1P = TAB(LQ+1)+2.0*X *TAB(LQ+2)                   UPDFDC
X2DOT = 0.0                                          UPDFDC
CALL FRCDFL (X2,X2DOT,M,0,Y2P,ELOSS)                UPDFDC
CALL FRCDFL (X2,X2DOT,M,1,Y2 ,ELOSS)                UPDFDC
DCUBIC = X1                                          UPDFDC
DCO = DCUBIC                                         UPDFDC

```

C		UPDFDC
C	A0 = Y(X1) (THE VALUE OF THE QUADRATIC AT X1)	UPDFDC
C	A1 = Y'(X1) (THE DERIVATIVE OF THE QUADRATIC AT X1)	UPDFDC
C		UPDFDC
	A0 = Y1	UPDFDC
	A1 = Y1P	UPDFDC
C		UPDFDC
C	SOLVE SIMULTANEOUSLY FOR A2 AND A3	UPDFDC
C	A2*(X2-X1)**2 + A3*(X2-X1)**3 = Y(X2)-A0-A1*(X2-X1)	UPDFDC
C	2*A2*(X2-X1) + 3*A3*(X2-X1)**2 = Y'(X2)-A1	UPDFDC
C		UPDFDC
	R13 = (Y2 - Y1 - Y1P*DX)/DX**2	UPDFDC
	R23 = (Y2P - Y1P)/DX	UPDFDC
	A2 = 3.0*R13 - R23	UPDFDC
	A3 = (R23 - 2.0*R13)/DX	UPDFDC
C		UPDFDC
C	IF LOCAL MINIMUM OF CUBIC (ABSCISSA VALUE WHERE Y'(X) = 0)	UPDFDC
C	LIES BETWEEN DCUBIC AND DREF AND IS NEGATIVE, THEN REPLACE	UPDFDC
C	CUBIC DEFINITION WITH STRAIGHT LINE BETWEEN (X1,Y1) AND (X2,Y2).	UPDFDC
C		UPDFDC
	IF (A3.NE.0.0) GO TO 14	UPDFDC
	R2 = -0.5*A1/A2	UPDFDC
	GO TO 15	UPDFDC
14	A33 = 3.0*A3	UPDFDC
	DISC = A2**2-A1*A33	UPDFDC
	IF (DISC.LT.0.0) GO TO 13	UPDFDC
	SQDISC = DSQRT(DISC)	UPDFDC
	R1 = (-A2+SQDISC)/A33	UPDFDC
	IF (R1.LE.0.0.OR.R1.GE.DX) GO TO 11	UPDFDC
	FR1 = A0+R1*(A1+R1*(A2+R1*A3))	UPDFDC
	IF (FR1.LT.0.0) GO TO 12	UPDFDC
11	R2 = (-A2-SQDISC)/A33	UPDFDC
15	IF (R2.LE.0.0.OR.R2.GE.DX) GO TO 13	UPDFDC
	FR2 = A0+R2*(A1+R2*(A2+R2*A3))	UPDFDC
	IF (FR2.GE.0.0) GO TO 13	UPDFDC
12	A0 = Y1	UPDFDC
	A1 = (Y2-Y1)/DX	UPDFDC
	A2 = 0.0	UPDFDC
	A3 = 0.0	UPDFDC
13	TAB(LC) = A0	UPDFDC
	TAB(LC+1) = A1	UPDFDC
	TAB(LC+2) = A2	UPDFDC
	TAB(LC+3) = A3	UPDFDC
	TAB(L+6) = DCUBIC	UPDFDC
	TAB(L+18) = DCO	UPDFDC
	GO TO 98	UPDFDC
20	IF (D-DREF) 21,21,30	UPDFDC
C		UPDFDC
C	DCUBIC < D < DREF, DEFINE NEW QUADRATIC FROM CUBIC CURVE.	UPDFDC
C		UPDFDC
21	X = D-DCO	UPDFDC
	Y2 = TAB(LC)+X*(TAB(LC+1)+X*(TAB(LC+2)+X*TAB(LC+3)))	UPDFDC

	X1 = DCUBIC - DG	UPDFDC
	AREA = X1*(TAB(LQ)+X1*(TAB(LQ+1)/2.0+X1*TAB(LQ+2)/3.0))	UPDFDC
	* + X*(TAB(LC)+X*(TAB(LC+1)/2.0+X*(TAB(LC+2)/3.0+X*TAB(LC+3)/4.0))	UPDFDC
	X = DCUBIC - DCO	UPDFDC
	IF (X.NE.0.0) AREA = AREA	UPDFDC
	* - X*(TAB(LC)+X*(TAB(LC+1)/2.0+X*(TAB(LC+2)/3.0+X*TAB(LC+3)/4.0))	UPDFDC
	GO TO 31	UPDFDC
C		UPDFDC
C	DREF < D, DEFINE NEW QUADRATIC FROM BASE CURVE.	UPDFDC
C		UPDFDC
C	IF DINER < D , REMOVE INERTIAL SPIKE	UPDFDC
C		UPDFDC
	30 IF (NTAB(M+2).GT.0 .AND. D.GE.DINER) NTAB(M+2) = 0	UPDFDC
	NR = NTAB(M+3)	UPDFDC
	RLAST = 1.0	UPDFDC
	IF (NR.GT.0 ) RLAST = EVALFD(D,NR,1)	UPDFDC
	IF (RLAST.NE.1.0) GO TO 39	UPDFDC
C		UPDFDC
C	R = 1, USE BASE CURVE FOR UNLOADING	UPDFDC
C		UPDFDC
	DG = 0.0	UPDFDC
	DCUBIC = 0.0	UPDFDC
	DREF = 0.0	UPDFDC
	A0 = 0.0	UPDFDC
	A1 = 0.0	UPDFDC
	A2 = 0.0	UPDFDC
	GO TO 32	UPDFDC
	39 NG = NTAB(M+4)	UPDFDC
	GLAST = 0.0	UPDFDC
	IF (NG.GT.0 ) GLAST = EVALFD(D,NG,1)	UPDFDC
	NB = NTAB(M+1)	UPDFDC
	D0 = TAB(NB)	UPDFDC
	DG = D0 + GLAST*(D-D0)	UPDFDC
	Y2 = EVALFD(D, NB,1)	UPDFDC
	NI = NTAB(M+2)	UPDFDC
	IF (NI.GT.0) Y2 = Y2+EVALFD(D,NI,1)	UPDFDC
	AREA = EVALFD(D,NB,2)	UPDFDC
	DREF = D	UPDFDC
	31 DCUBIC = D	UPDFDC
	X1 = DG	UPDFDC
	X2 = D	UPDFDC
	DX = X2-X1	UPDFDC
	Y1 = 0.0	UPDFDC
	RAREA = RLAST*AREA	UPDFDC
C		UPDFDC
C	COMPUTE UNLOADING QUADRATIC COEFFICIENTS SUCH THAT	UPDFDC
C	ENDPOINT DERIVATES ARE NON-NEGATIVE.	UPDFDC
C		UPDFDC
	A0 = 0.0	UPDFDC
	A1 = 2.0/DX*(3.0*RAREA/DX-Y2)	UPDFDC
	IF (A1.LT.0.0) A1 = 0.0	UPDFDC
	A2 = (Y2/DX-A1)/DX	UPDFDC

	IF (A2.GE.0.0) GO TO 32	UPDFDC
	A1 = Y2/DX	UPDFDC
	A2 = 0.0	UPDFDC
C		UPDFDC
C	RESTORE TAB VALUES THAT MAY HAVE BEEN CHANGED	UPDFDC
C		UPDFDC
	. 32 TAB(L+2) = AREA	UPDFDC
	TAB(L+3) = RLAST	UPDFDC
	TAB(L+4) = GLAST	UPDFDC
	TAB(L+5) = DG	UPDFDC
	TAB(L+6) = DCUBIC	UPDFDC
	TAB(L+7) = DREF	UPDFDC
	TAB(LQ) = A0	UPDFDC
	TAB(LQ+1) = A1	UPDFDC
	TAB(LQ+2) = A2	UPDFDC
	98 TAB(L+1) = D	UPDFDC
	IF (D.GT.DG0 .AND. DLAST.LE.DG0) M=-M	UPDFDC
	99 RETURN	UPDFDC
	END	UPDFDC



	SUBROUTINE VEHPOS		REV IV 07/23/86	TWOPI	VEHPOS
C					
C	COMPUTES COMPONENTS OF VEHICLE ACCELERATIONS ONLY AS A FUNCTION				VEHPOS
C	OF TIME USING DATA AND TABLES PRODUCED BY SUBROUTINE VINPUT.				VEHPOS
C					VEHPOS
	IMPLICIT REAL*8 (A-H,O-Z)				VEHPOS
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,				VEHPOS
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG				PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),				VEHPOS
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)				VEHPOS
	COMMON/VPOSTN/ ZPLT(3),SPLT(3),AXV(3,6),VATAB(6,501,6),				VEHICL
*	VTO(6),VDT(6),TIMEV(6),OMEGV(6),NVTAB(6),INDXV(6)				VEHPOS
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),				VEHPOS
*	UNITL,UNITM,UNITT,GRAVTY(3),TWOPI				TWOPI
	DIMENSION AX(3)				VEHPOS
	T = TIME				VEHPOS
	M = 1				VEHPOS
15	DO 16 I=1,3				VEHPOS
16	AX(I) = AXV(I,M)				VEHPOS
	ATO = VTO(M)				VEHPOS
	ADT = VDT(M)				VEHPOS
	VTIME = TIMEV(M)				VEHPOS
	OMEG = OMEGV(M)				VEHPOS
	NATAB = NVTAB(M)				VEHPOS
	K = INDXV(M)				VEHPOS
	IF(NATAB.NE.0) GO TO 20				VEHPOS
C					VEHPOS
C	HALF-SINE WAVE DECELERATION				VEHPOS
C					VEHPOS
	IF(T.GT.VTIME) T=VTIME				VEHPOS
	WT = OMEG*T				VEHPOS
	SWT = DSIN(WT)				VEHPOS
	DO 10 I=1,3				VEHPOS
	AW = AX(I)*OMEG				VEHPOS
	SEGLA(I,K) = -AW*OMEG*SWT				VEHPOS
10	WMEGD(I,K) = 0.0				VEHPOS
	GO TO 99				VEHPOS
20	IF (NATAB.LT.0) GO TO 30				VEHPOS
C					VEHPOS
C	UNIDIRECTIONAL DECELERATION				VEHPOS
C					VEHPOS
	IF (T.LT.VTIME) GO TO 21				VEHPOS
C					VEHPOS
C	TIME POINT EXCEEDS TABLE, USE LAST VALUES OF ACCELERATION.				VEHPOS
C					VEHPOS
	ACO = VATAB(1,NATAB,M)				VEHPOS
	GO TO 25				VEHPOS
C					VEHPOS
C	USE QUADRATIC INTERPOLATION FROM TABLES FOR CURRENT VALUE OF				VEHPOS
C	TIME TO BE CONSISTENT WITH SIMPSON INTEGRATION OF TABLES.				VEHPOS
C					VEHPOS
	21 J= 0.5*(T-ATO)/ADT +1.0				VEHPOS

	XK = T/ADT -DFLOAT(2*J-1)	VEHPOS
	X1 = XK+1.0	VEHPOS
	X3 = XK-1.0	VEHPOS
	ACO = 0.5*XK*X3*VATAB(1,2*J-1,M)	VEHPOS
	* - X3*X1*VATAB(1,2*J ,M)	VEHPOS
	* + 0.5*XK*X1*VATAB(1,2*J+1,M)	VEHPOS
C		VEHPOS
C	COMPONENTS OF VEHICLE ACCELERATION.	VEHPOS
C		VEHPOS
	25 DO 29 I=1,3	VEHPOS
	SEGLA(I,K) = -G*AX(I)*ACO	VEHPOS
	29 WMEGD(I,K) = 0.0	VEHPOS
	GO TO 99	VEHPOS
C		VEHPOS
C	OMNIDIRECTIONAL DECELERATION	VEHPOS
C		VEHPOS
	30 J = (TIME-ATO)/ADT + 1.0	VEHPOS
	IF (J.GE.-NATAB) GO TO 32	VEHPOS
C		VEHPOS
C	INTERPOLATION FROM VINPUT TABLES OF COMPONENTS OF VEHICLE	VEHPOS
C	LINEAR AND ANGULAR ACCELERATION.	VEHPOS
C		VEHPOS
	TJ = ATO + DFLOAT(J-1)*ADT	VEHPOS
	DLT = TIME-TJ	VEHPOS
	R1 = DLT/ADT	VEHPOS
	R2 = 1.0-R1	VEHPOS
	DO 31 I=1,3	VEHPOS
	SEGLA(I,K) = -G*(VATAB(I ,J+1,M)*R1 + VATAB(I ,J,M)*R2)	VEHPOS
	31 WMEGD(I,K) = RADIAN*(VATAB(I+3,J+1,M)*R1 + VATAB(I+3,J,M)*R2)	VEHPOS
	GO TO 99	VEHPOS
C		VEHPOS
C	TIME POINT EXCEEDS TABLE, USE LAST VALUES OF ACCELERATION.	VEHPOS
C		VEHPOS
	32 J = - NATAB	VEHPOS
	DO 33 I=1,3	VEHPOS
	SEGLA(I,K) = -G*VATAB(I ,J,M)	VEHPOS
	33 WMEGD(I,K) = RADIAN*VATAB(I+3,J,M)	VEHPOS
	99 M = M+1	VEHPOS
	IF (M.LE.6 .AND. IND XV(M).NE.0) GO TO 15	VEHPOS
	RETURN	VEHPOS
	END	VEHPOS

	SUBROUTINE VINPUT	REV IV 07/24/86	VINPUT
C		SLIP	
C	PERFORMS CARD INPUT AND COMPUTES DATA AND TABLES REQUIRED BY		VINPUT
C	SUBROUTINE VEHPOS TO INTEGRATE THE CRASH VEHICLE MOTION FOR ONE OF		VINPUT
C	THREE PERMISSABLE OPTIONS:		VINPUT
C	(1) HALF SINE-WAVE LINEAR DECELERATION IMPULSE		VINPUT
C	(2) UNIDIRECTIONAL LINEAR DECELERATION TABULAR INPUT		VINPUT
C	(3) OMNIDIRECTIONAL LINEAR AND ANGULAR ACCELERATION TABULAR		VINPUT
C	INPUT (6 DEGREES OF FREEDOM VEHICLE MOTION)		VINPUT
C			VINPUT
	IMPLICIT REAL*8 (A-H,O-Z)		VINPUT
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,		VINPUT
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG		PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),		VINPUT
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)		VINPUT
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),		SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),		VINPUT
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)		VINPUT
	COMMON/VPOSTN/ ZPLT(3),SPLT(3),AXV(3,6),VATAB(6,501,6),		VEHICL
*	VTO(6),VDT(6),TIMEV(6),OMEGV(6),NVTAB(6),INDXV(6)		VINPUT
	COMMON/TEMPVS/ XO(3),XDOTO(3),XCOMP(3),XVCOMP(3),ANGLE(3),		VINPUT
*	ATAB(15,501),DVEH(3,3),VMEG(3),VMEGD(3),		VEHICL
*	XACOMP(3),THET(3),AX(3),F(5,101),XYZ(103,6),TT(103),		CHGIII
*	VIPS,VMPH,ATO,ADT,VTIME,OMEG,NATAB		VINPUT
*	,SP(5,101,4),Q1(101,4),A1(3),W1(4),QD(4),QC(4)		JTF984
*	,IDMMY,DDMY(23887)		80386
	COMMON/INTEST/ SGTEST(3,4,30),XTEST(3,120),SEGT(120),REGT(120)		VINPUT
	REAL SEGT		VINPUT
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),		VINPUT
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI		TWOPI
	COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),		VINPUT
*	BLTTTL(5,8),PLTTTL(5,30),BAGTTL(5,6),SEG(30),		VINPUT
*	JOINT(30),CGS(30),JS(30)		VINPUT
	REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTTL,BAGTTL,SEG,JOINT		VINPUT
	LOGICAL*1 CGS,JS		VINPUT
	DIMENSION IDYPR(3)		VINPUT
	REAL VEH(6),GRND		VINPUT
	DATA VEH/4HVEH1,4HVEH2,4HVEH3,4HVEH4,4HVEH5,4HVEH /,GRND/4HGRND/		VINPUT
	DATA IDYPR/3,2,1/		VINPUT
	DATA MXTAB2/99/,MXTAB3/501/,MXTAB4/101/		MISC
C			VINPUT
C	READ AND PRINT CONTENTS OF CARDS C.1 AND C.2		VINPUT
C			VINPUT
	NVEH = NSEG		VINPUT
	NVH = 0		VINPUT
	DO 11 I=1,6		VINPUT
11	INDXV(I) = 0		VINPUT
12	READ (5,13) VPSTTL		VINPUT
13	FORMAT (20A4)		VINPUT
	READ(5,14) ANGLE,VIPS,VTIME,XO,NATAB,ATO,ADT,MSEG		VINPUT
14	FORMAT(8F6.0,I6,2F6.0,I6)		VINPUT
	INTAB = IABS(NATAB)		CHGIII

IF (NATAB.GT.0.AND.INTAB.GT.MXTAB2) STOP 79	MISC
WRITE (6,15) NPG,VPSTTL,ANGLE,VIPS,VTIME,X0,NATAB,ATO,ADT,MSEG	PAGE
NPG = NPG+1	PAGE
15 FORMAT('1 VEHICLE DECELERATION INPUTS',94X,'PAGE',I5/120X,	PAGE
* 'CARDS C'/3X,20A4//	PAGE
* 7X,'YAW',9X,'PITCH',7X,'ROLL',8X,'VIPS',8X,'VTIME',7X,'X0(X)',	VINPUT
* 7X,'X0(Y)',7X,'X0(Z)',2X,'NATAB',6X,'ATO',9X,'ADT',4X,'MSEG'/	VINPUT
* 8F12.3,I5,2X,2F12.6,I5)	VINPUT
DA1 = ANGLE(1)*RADIAN	VINPUT
DA2 = ANGLE(2)*RADIAN	VINPUT
AX(3) = DCOS(DA2)	VINPUT
AX(1) = DCOS(DA1)*AX(3)	VINPUT
AX(2) = DSIN(DA1)*AX(3)	VINPUT
AX(3) = DSIN(DA2)	VINPUT
IF(NATAB.NE.0) GO TO 18	VINPUT
C	VINPUT
C HALF-SINE WAVE DECELERATION	VINPUT
C	VINPUT
OMEG = PI/VTIME	VINPUT
AT = 0.5*VIPS/OMEG	VINPUT
IF (VIPS.LT.0.0) VIPS = 0.0	VINPUT
DO 16 I=1,3	VINPUT
XACOMP(I) = 0.0	VINPUT
XDOTO(I) = VIPS*AX(I)	VINPUT
16 AX(I) = AT*AX(I)	VINPUT
WRITE (6,17) VIPS,UNITL,UNITT,ANGLE,VTIME,UNITT	VINPUT
17 FORMAT('0 PASSENGER COMPARTMENT DISPLACEMENT HISTORY'/	VINPUT
* ' ANALYTICAL HALF-SINE WAVE DECELERATION'/	VINPUT
* ' VO= ',F8.3,1X,A4,'/',A4,' , OBLIQUE ANGLES = ',3F7.2,	VINPUT
* ' DEGREES, TIME DURATION = ',F7.3,1X,A4//)	VINPUT
GO TO 28	VINPUT
18 IF (NATAB.LT.0) GO TO 31	VINPUT
C	VINPUT
C FOR UNIDIRECTIONAL VEHICLE MOTION	VINPUT
C READ LINEAR DECELERATION TABLES FROM CARDS C.3	VINPUT
C	VINPUT
READ (5,19) (ATAB(1,I),I=1,NATAB)	VINPUT
19 FORMAT (12F6.0)	VINPUT
C	VINPUT
C EXTEND TABLE IF NECESSARY SUCH THAT NATAB IS ODD AND	VINPUT
C LAST ENTRY NEED NOT BE ZERO. IF TABLE SIZE IS EXCEEDED ON TIME,	VINPUT
C VALUE OF LAST ENTRY WILL BE USED.	VINPUT
C	VINPUT
IF (MOD(NATAB,2).EQ.1) GO TO 20	VINPUT
ATAB(1,NATAB+1) = ATAB(1,NATAB)	VINPUT
NATAB = NATAB+1	VINPUT
20 VTIME = ADT * DFLOAT(NATAB-1)	VINPUT
C	VINPUT
C USING SIMPSON'S INTEGRATION, COMPUTE VELOCITY AND DISPLACEMENT	VINPUT
C TABLE FOR NATAB EQUALLY SPACED (ADT) TIME POINTS.	VINPUT
C FOR I=1,NATAB	VINPUT
C ATAB(1,I) = LINEAR DECELERATION (G'S)	VINPUT

C	ATAB(2,I) = LINEAR VELOCITY (L UNITS/T UNITS)	VINPUT
C	ATAB(3,I) = LINEAR DISPLACEMENT (L UNITS)	VINPUT
C		VINPUT
	ATAB(2,1) = VIPS	VINPUT
	ATAB(3,1) = 0.0	VINPUT
	DA1 = ADT/3.0	VINPUT
	DA2 = ADT/12.0	VINPUT
	UNITS = -G	VINPUT
	DO 22 J=2,3	VINPUT
	DO 21 I=2,NATAB,2	VINPUT
	F1 = ATAB(J-1,I-1) * UNITS	VINPUT
	F2 = ATAB(J-1,I) * UNITS	VINPUT
	F3 = ATAB(J-1,I+1) * UNITS	VINPUT
	ATAB(J,I) = ATAB(J,I-1) + DA2*(5.0*F1+8.0*F2-F3)	VINPUT
21	ATAB(J,I+1) = ATAB(J,I-1) + DA1*(F1+4.0*F2+F3)	VINPUT
22	UNITS = 1.0	VINPUT
C		VINPUT
C	PRINT TABLES	VINPUT
C		VINPUT
	WRITE (6,23) (UNITL,UNITT,UNITL,I-1,2)	VINPUT
23	FORMAT('O UNIDIRECTIONAL VEHICLE POSITION TABLES'//	VINPUT
	* 2(' TIME ACC VELOCITY POSITION ')/	VINPUT
	* 2(' (MSEC) (G) (' ,A4,'/' ,A4,')',5X, '(' ,A4,')',4X)/)	VINPUT
	DO 26 J=1,50	VINPUT
	IF (J.GT.NATAB) GO TO 26	VINPUT
	T1 = (ATO + DFLOAT(J-1)*ADT)*1000.0	VINPUT
	IF (J+50.LE.NATAB) GO TO 25	VINPUT
	WRITE (6,24) T1,(ATAB(I,J),I-1,3)	VINPUT
24	FORMAT(2(F11.5,F10.2,F13.4,F13.5,3X))	VINPUT
	GO TO 26	VINPUT
25	T2 = (ATO + DFLOAT(J+49)*ADT)*1000.0	VINPUT
	WRITE (6,24) T1,(ATAB(I,J),I-1,3),T2,(ATAB(I,J+50),I-1,3)	VINPUT
26	CONTINUE	VINPUT
C		VINPUT
C	INITIALIZATION	VINPUT
C		VINPUT
	DO 27 I=1,3	VINPUT
	XACOMP(I) = -G*AX(I)*ATAB(1,1)	VINPUT
27	XDOTO(I) = VIPS*AX(I)	VINPUT
28	DO 30 I=1,3	VINPUT
	DO 29 J=1,3	VINPUT
29	DVEH(I,J) = 0.0	VINPUT
	DVEH(I,I) = 1.0	VINPUT
	VMEGD(I) = 0.0	VINPUT
30	VMEG(I) = 0.0	VINPUT
	GO TO 64	VINPUT
C		VINPUT
C	FOR OMNIDIRECTIONAL (6 DEGREES OF FREEDOM) VEHICLE MOTION	VINPUT
C	READ LINEAR DECELERATION AND ANGULAR ACCELERATION TABLES	VINPUT
C	FROM CARDS C.2.B AND C.4.	CHGIII
C		VINPUT
	31 MATAB = -NATAB	VINPUT

	READ (5,32) LTYPE,LFIT,NPTS,(VMAG(I),I=1,3)	VINPUT
32	FORMAT (3I6,22X,3F10.0)	VINPUT
	IF (MATAB.GT.MXTAB3) STOP 80	MISC
	IF (LTYPE.EQ.2.AND.LFIT.LT.1) STOP 82	CHGIII
	IF (LTYPE.EQ.1.AND.LFIT.LT.2) STOP 83	VEHICL
	IF (LTYPE.GT.0) GO TO 34	VINPUT
	READ (5,33) ((ATAB(I,J),I=1,3),(ATAB(I,J),I=10,12),J=1,MATAB)	VINPUT
33	FORMAT (10X,6F10.0)	VINPUT
	ISKIP = 0	VINPUT
	GO TO 46	VINPUT
C		CHGIII
C	FOR SPLINE FIT VEHICLE MOTION	CHGIII
C	READ DATA FROM CARDS C.5.	CHGIII
C		CHGIII
34	LPTS = LTYPE-1 + NPTS	VINPUT
	IF (NPTS.GT.MXTAB3) STOP 81	MISC
	READ (5,35) (TT(I),(XYZ(I,J),J=1,6),I=1,LPTS)	VINPUT
35	FORMAT (7F10.0)	VINPUT
	WRITE (6,36) LTYPE,LFIT,NPTS	CHGIII
36	FORMAT ('O SPLINE FIT TABULAR INPUT'//	CHGIII
	* 3X,'LTYPE =',I6,' LFIT =',I6,' NPTS =',I6/)	CHGIII
	IF (LTYPE.EQ.2) WRITE(6,701) UNITL,UNITT,TT(1),(XYZ(1,J),J=1,6)	CHGIII
	IF (LTYPE.EQ.3) WRITE(6,702) UNITL,UNITT,TT(1),(XYZ(1,J),J=1,6),	CHGIII
	* UNITL,UNITT,UNITT,UNITT,TT(2),(XYZ(2,J),J=1,6)	CHGIII
701	FORMAT(32X,'INITIAL LINEAR POSITION (' ,A4,')',17X,'INITIAL ANGULACHGIII	
	*R POSITION (DEG)',/,3X,'TIME(' ,A4,')-',F9.4,3X,2('X-',F10.3,2X,	JTF984
	* 'Y-',F10.3,2X,'Z-',F10.3,8X),/)	CHGIII
702	FORMAT(32X,'INITIAL LINEAR POSITION (' ,A4,')',17X,'INITIAL ANGULACHGIII	
	*R POSITION (DEG)',/,3X,'TIME(' ,A4,')-',F9.4,3X,2('X-',F10.3,2X,	JTF984
	* 'Y-',F10.3,2X,'Z-',F10.3,8X),/.30X,'INITIAL LINEAR VELOCITY (' ,CHGIII	
	* A4,/' ,A4,')',12X,'INITIAL ANGULAR VELOCITY (DEG/' ,A4,')',	CHGIII
	*/,3X,'TIME(' ,A4,')-',F9.4,3X,2('X-',F10.2,2X,'Y-',	CHGIII
	* F10.2,2X,'Z-',F10.2,8X),/)	CHGIII
	IF (LTYPE.EQ.1) WRITE(6,703) UNITL,UNITT	CHGIII
	IF (LTYPE.EQ.2) WRITE(6,704) UNITL,UNITT,UNITT,UNITT	CHGIII
	IF (LTYPE.EQ.3) WRITE(6,705) UNITT,UNITT	VEHICL
703	FORMAT(29X,'LINEAR POSITION (' ,A4,')',21X,'ANGULAR POSITION (DECHGIII	
	*G)',/,5X,'TIME(' ,A4,')',11X,'X',11X,'Y',11X,'Z',18X,'YAW',8X,	VEHICL
	* 'PITCH',8X,'ROLL')	VEHICL
704	FORMAT(26X,'LINEAR VELOCITY (' ,A4,/' ,A4,')',16X,	CHGIII
	* 'ANGULAR VELOCITY (DEG/' ,A4,')',/,5X,'TIME(' ,A4,')',	CHGIII
	* 11X,2('X',11X,'Y',11X,'Z',19X))	CHGIII
705	FORMAT(26X,'LINEAR DECELERATION (G''S)',15X,	VEHICL
	* 'ANGULAR ACCELERATION (DEG/' ,A4, '**2)',/,5X,'TIME(' ,A4,')',	CHGIII
	* 11X,2('X',11X,'Y',11X,'Z',19X))	CHGIII
	IF (LTYPE.EQ.1) WRITE(6,706) (TT(I),(XYZ(I,J),J=1,6),I=1,LPTS)	CHGIII
	IF (LTYPE.EQ.2) WRITE(6,706) (TT(I),(XYZ(I,J),J=1,6),I=2,LPTS)	CHGIII
	IF (LTYPE.EQ.3) WRITE(6,706) (TT(I),(XYZ(I,J),J=1,6),I=3,LPTS)	CHGIII
706	FORMAT(1X,F12.5,6X,3F12.3,8X,3F12.3)	CHGIII
	DO 37 I=1,3	VINPUT
	X0(I) = XYZ(1,I)	VINPUT
	XDOTO(I) = XYZ(2,I)	VINPUT

VMEG(I) = XYZ(2,I+3)	VINPUT
37 ANGLE(I) = XYZ(1,I+3)	JTF984
IMJ = 6	JTF984
IF(LTYPE.EQ.1)IMJ = 3	JTF984
DO 45 II=1,IMJ	JTF984
CALL SPLINE (TT(LTYPE),XYZ(LTYPE,II),F,NPTS,LFIT)	VINPUT
I = II	VINPUT
IF (II.GT.3) I = II + 6	VINPUT
IF(LTYPE.EQ.1) XDOT0(I) = F(3,1)	JTF984
UNITS = 1.0	JTF984
IF (LTYPE.LT.3 .AND. II.LE.3) UNITS = -1.0/G	VINPUT
K1 = 1	VINPUT
DO 45 J=1,MATAB	VINPUT
TTT = ATO + DFLOAT(J-1)*ADT	VINPUT
DO 39 L=K1,NPTS	JTF984
K = L	JTF984
IF (TTT.LT.F(1,L+1)) GO TO 40	VINPUT
39 CONTINUE	VINPUT
40 K1 = K	VINPUT
DX = TTT - F(1,K)	VINPUT
IF (LTYPE-2) 41,42,43	BUTLER1
41 ACC = 2.0*F(4,K) + 6.0*DX*F(5,K)	VINPUT
GO TO 44	VINPUT
42 ACC = F(3,K) + DX*(2.0*F(4,K)+3.0*DX*F(5,K))	VINPUT
GO TO 44	VINPUT
43 ACC = F(2,K) + DX*(F(3,K)+DX*(F(4,K)+DX*F(5,K)))	VINPUT
44 ATAB(I,J) = ACC*UNITS	VINPUT
45 CONTINUE	VINPUT
ISKIP = 1	VINPUT
IF(LTYPE.NE.1)GO TO 46	JTF984
C CODE FOR OMEGA ROUTINE: COMPUTE ATAB(I,J),I=10,11,12 J = 1,MATAB	JTF984
DO 80 I = 1,NPTS	JTF984
DO 91 K = 1,3	JTF984
91 A1(K) = XYZ(I,K+3)	JTF984
CALL QUAT(A1,W1)	JTF984
DO 76 K = 1,4	JTF984
76 Q1(I,K) = W1(K)	JTF984
IF(I.EQ.1)GO TO 80	JTF984
TA = 0.0	JTF984
TB = 0.0	JTF984
DO 77 K = 1,4	JTF984
TA = TA + DABS(Q1(I,K) - Q1(I-1,K))	JTF984
77 TB = TB + DABS(Q1(I,K) + Q1(I-1,K))	JTF984
IF(TA.LE.TB)GO TO 80	JTF984
DO 78 K = 1,4	JTF984
78 Q1(I,K) = -Q1(I,K)	JTF984
80 CONTINUE	JTF984
DO 82 K = 1,4	JTF984
82 CALL SPLINE(TT,Q1(1,K),SP(1,1,K),NPTS,LFIT)	JTF984
DO 90 J = 1,MATAB	JTF984
TTT = ATO + DFLOAT(J-1)*ADT	JTF984
K1 = 1	JTF984

DO 83 L = K1,NPTS	JTF984
K = L	JTF984
83 IF(TTT.LT.SP(1,L+1,1))GO TO 84	JTF984
84 K1 = K	JTF984
DX = TTT - SP(1,K,1)	JTF984
DO 85 L = 1,4	JTF984
W1(L) = SP(2,K,L)+DX*(SP(3,K,L)+DX*(SP(4,K,L)+DX*SP(5,K,L)))	JTF984
QD(L) = 2.0*SP(4,K,L) + 6.0*DX*SP(5,K,L)	JTF984
85 IF(J.EQ.1)QC(L) = SP(3,K,L)+DX*(2.0*SP(4,K,L)+DX*3.0*SP(5,K,L))	MISC
CCC = 2.0/RADIAN	JTF984
IF(J.GT.1)GO TO 88	JTF984
CALL CROSS(QC(2),W1(2),A1)	JTF984
DO 86 K = 1,3	JTF984
86 VMEG(K) = CCC*(W1(1)*QC(K+1) - QC(1)*W1(K+1) + A1(K))	JTF984
CALL DRCQUA(DVEH,W1)	JTF984
CALL YPRDEG(DVEH,ANGLE)	JTF984
88 CALL CROSS(QD(2),W1(2),QC(2))	JTF984
DO 89 K = 2,4	JTF984
89 ATAB(K+8,J) = CCC*(W1(1)*QD(K)-QD(1)*W1(K) + QC(K))	JTF984
90 CONTINUE	JTF984
46 DO 55 J=1,MATAB	VINPUT
IF (MOD(J,45).NE.1) GO TO 49	VINPUT
C	VINPUT
C PRINT PAGE HEADING AT START OF EACH 45 TIME POINTS.	VINPUT
C	VINPUT
IPAGE = (J-1)/45 + 1	VINPUT
IF (ISKIP.EQ.1) WRITE (6,75) NPG	PAGE
IF (ISKIP.EQ.1) NPG=NPG+1	PAGE
75 FORMAT('1',122X,'PAGE',I5)	PAGE
WRITE (6,48) VPSTTL,IPAGE,UNITL,UNITT,UNITL	PAGE
48 FORMAT('0 VEHICLE LINEAR TIME HISTORY',3X,20A4,3X,	PAGE
* 'PAGE NO.',I3//	VINPUT
* 4X,'TIME',12X,'LINEAR DECELERATIONS (G''S)',	VINPUT
* 11X,'LINEAR VELOCITIES (' ,A4,'/' ,A4,' )',	VINPUT
* 11X,'LINEAR DISPLACEMENTS (' ,A4,' )' /	VINPUT
* 3X,'(MSEC)',3(11X,'X',11X,'Y',11X,'Z',3X) / )	VINPUT
ISKIP = 1	VINPUT
49 IF (J.GT.1) GO TO 52	VINPUT
C	VINPUT
C INTEGRATION INITIALIZATION FOR TIME = 0.	VINPUT
C	VINPUT
DO 50 I=1,3	VINPUT
ATAB(I+6,J) = X0(I)	VINPUT
50 ATAB(I+12,J) = VMEG(I)	JTF984
CALL DRCYPR (DVEH,ANGLE,IDYPR)	VINPUT
DO 51 I=1,3	VINPUT
IF (LTYPE.EQ.0) XDOT0(I) = VIPS*DVEH(1,I)	VINPUT
51 ATAB(I+3,J) = XDOT0(I)	VINPUT
GO TO 54	VINPUT
52 DO 53 I=1,3	VINPUT
C	VINPUT
C INTEGRATE LINEAR VELOCITY AND DISPLACEMENT.	VINPUT



C	ATAB(I+3,J) = ATAB(I+3,J-1)-G*ADT/2.0*(ATAB(I,J-1)+ATAB(I,J))	VINPUT
53	ATAB(I+6,J) = ATAB(I+6,J-1)	VINPUT
	* +ADT*(ATAB(I+3,J-1)-G*ADT/6.0*(2.0*ATAB(I,J-1)+ATAB(I,J)))	VINPUT
54	T1 = (ATO + DFLOAT(J-1)*ADT)*1000.0	VINPUT
55	WRITE(6,56) T1,(ATAB(I,J),I=1,9)	VINPUT
56	FORMAT(F9.3,3(3X,3F12.3))	VINPUT
	DO 61 J=1,MATAB	VINPUT
	IF (MOD(J,45).NE.1) GO TO 58	VINPUT
C		VINPUT
C	PRINT PAGE HEADING AT START OF EACH 45 TIME POINTS.	VINPUT
C		VINPUT
	IPAGE = (J-1)/45 + 1	VINPUT
	WRITE (6,57) VPSTTL,NPG,IPAGE,UNITT,UNITT	PAGE
	NPG=NPG+1	PAGE
57	FORMAT('1 VEHICLE ANGULAR TIME HISTORY',3X,20A4,10X,'PAGE',15/	PAGE
	* 116X,'PAGE NO.',13/	PAGE
	* 4X,'TIME', 7X,'ANGULAR ACCELERATIONS (DEG/''A4,'**2)',	VINPUT
	* 7X,'ANGULAR VELOCITIES (DEG/''A4,')',	VINPUT
	* 11X,'ANGULAR DISPLACEMENTS (DEG)' /	VINPUT
	* 3X,'(MSEC)',2(11X,'X',11X,'Y',11X,'Z',3X),	VINPUT
	* 10X,'YAW',8X,'PITCH',8X,'ROLL' /)	VINPUT
58	IF(J.EQ.1) GO TO 60	VINPUT
C		VINPUT
C	INTEGRATE ANGULAR VELOCITY AND DISPLACEMENT.	VINPUT
C		VINPUT
	DO 59 I=1,3	VINPUT
	ATAB(I+12,J) = ATAB(I+12,J-1)+(ATAB(I+9,J-1)+ATAB(I+9,J))*ADT/2.0	VINPUT
59	THET(I) = ADT*(ATAB(I+12,J-1)+(2.0*ATAB(I+9,J-1)+ATAB(I+9,J))*ADT	VINPUT
	*/6.0)*RADIAN	VINPUT
	CALL DSETD(DVEH,THET,THT)	VINPUT
60	CALL YPRDEG(DVEH,THET)	VINPUT
	T1 = (ATO + DFLOAT(J-1)*ADT)*1000.0	VINPUT
61	WRITE (6,56) T1,(ATAB(I,J),I=10,15),THET	VINPUT
C		VINPUT
C	PROGRAM INITIALIZATION FOR TIME = 0.	VINPUT
C		VINPUT
	CALL DRCYPR (DVEH,ANGLE,IDYPR)	VINPUT
	DO 63 I=1,3	VINPUT
	XACOMP(I) = -G*ATAB(I,1)	VINPUT
	VMEG(I) = ATAB(I+12,1)*RADIAN	VINPUT
63	VMEGD(I) = ATAB(I+9,1)*RADIAN	VINPUT
64	J = MSEG	VINPUT
	IF (MSEG.EQ.0) GO TO 65	VINPUT
	IF (MSEG.LE.NSEG) GO TO 66	VINPUT
	IF (MSEG.NE.NVEH+1) STOP 6	VINPUT
65	NVEH = NVEH+1	VINPUT
	J = NVEH	VINPUT
C		VINPUT
C	SETUP FOR ALL PRESCRIBED SEGMENT MOTION.	VINPUT
C		VINPUT
	66 NVH = NVH+1	VINPUT

ISING(J) = -1	VINPUT
IF (MSEG.GT.NSEG) SEG(J) = VEH(NVH)	VINPUT
RW(J) = 0.0	VINPUT
DO 67 I=1,3	VINPUT
RPHI (I,J) = 0.0	VINPUT
SEGLA(I,J) = VMEGD(I)	VINPUT
WMEGD(I,J) = XACOMP(I)	VINPUT
67 AXV(I,NVH) = AX(I)	VINPUT
VTO(NVH) = ATO	VINPUT
VDT(NVH) = ADT	VINPUT
OMEGV(NVH) = OMEG	VINPUT
TIMEV(NVH) = VTIME	VINPUT
NVTAB(NVH) = NATAB	VINPUT
INDXV(NVH) = J	VINPUT
NJ = IABS(NATAB)	VINPUT
IF (NJ.LE.0) GO TO 69	VINPUT
DO 68 K=1,NJ	VINPUT
DO 68 I=1,3	VINPUT
VATAB(I ,K,NVH) = ATAB(I,K)	VINPUT
68 VATAB(I+3,K,NVH) = ATAB(I+9,K)	VINPUT
69 IF (J.LE.NSEG) GO TO 72	VINPUT
C	VINPUT
C SETUP FOR NEW VEHICLE (SEGMENT) MOTION.	VINPUT
C	VINPUT
W(J) = 0.0	VINPUT
RW(J) = 0.0	VINPUT
DO 71 I=1,3	VINPUT
DO 70 K=1,3	VINPUT
D(I,K,J) = DVEH(I,K)	VINPUT
70 SGTEST(I,K,J) = 0.0	VINPUT
SGTEST(I,4,J) = 0.0	VINPUT
SEGLP(I,J) = XO(I)	VINPUT
SEGLV(I,J) = XDOTO(I)	VINPUT
WMEG (I,J) = VMEG(I)	VINPUT
PHI (I,J) = 0.0	VINPUT
71 RPHI (I,J) = 0.0	VINPUT
72 IF (MSEG.NE.0) GO TO 12	VINPUT
SEG(NVEH) = VEH(6)	VINPUT
C	VINPUT
C SET UP SEGMENT DATA FOR GROUND	VINPUT
C	VINPUT
NGRND = NVEH+1	VINPUT
IF (NGRND.GT.30 .OR. NVH.GT.6) STOP 7	VINPUT
SEG(NGRND) = GRND	VINPUT
J = NGRND	VINPUT
ISING(J) = -1	VINPUT
W(J) = 0.0	VINPUT
RW(J) = 0.0	VINPUT
DO 74 I=1,3	VINPUT
DO 73 K=1,3	VINPUT
D(I,K,J) = 0.0	VINPUT
73 SGTEST(I,K,J) = 0.0	VINPUT

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D(I,I,J) = 1.0
SGTEST(I,4,J) = 0.0
SEGLP(I,J) = 0.0
SEGLV(I,J) = 0.0
SEGLA(I,J) = 0.0
WMEG (I,J) = 0.0
WMEGD(I,J) = 0.0
PHI (I,J) = 0.0
74 RPHI (I,J) = 0.0
RETURN
END

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VINPUT
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	DOUBLE PRECISION FUNCTION VISCOS(ZD,VISC,HA)		VISCOS
C		REV 19	10/23/78VISCOS
C	COMPUTES SUM OF COULOMB AND VISCOUS TORQUES		VISCOS
C	AT JOINTS AS A FUNCTION OF THETA DOT.		VISCOS
C	ACTUALLY ROUTINE RETURNS SUM/ZD.		VISCOS
C			VISCOS
C	ARGUMENTS:		VISCOS
C	ZD : !THETA DOT! WHERE THETA IS THE ANGLE OF THE JOINT.		VISCOS
C	VISC: ARRAY OF 5 VALUES DESCRIBING FUNCTION EVALUATION.		VISCOS
C			VISCOS
	IMPLICIT REAL*8 (A-H,O-Z)		VISCOS
	DIMENSION VISC(5)		VISCOS
	Z = ZD		VISCOS
	IF (ZD.LT.VISC(3)) Z = VISC(3)/(2.0-ZD/VISC(3))		VISCOS
	HA = (Z-ZD)/Z		VISCOS
	VISCOS = VISC(1)+VISC(2)/Z		VISCOS
	RETURN		VISCOS
	END		VISCOS

	SUBROUTINE VISPR(IJ,NJ)		REV IV	02/01/88	MISDOT	VISPR
C						VISPR
C	COMPUTES VISCOS AND SPRING TORQUES AT THE JOINTS					VISPR
C	AND ADDS THEM TO THE U2 ARRAY.					VISPR
C	ARGUMENTS:					VISPR
C	NJ = 0 - REGULAR COMPUTATION FOR ALL JOINTS					VISPR
C	# 0 - COMPUTE ONLY FOR JOINT NJ IMPULSE					VISPR
C						VISPR
C	IJ = 1 IMPULSE FOR FLEXURE ONLY					VISPR
C	= 2 IMPULSE FOR TORSION ONLY					VISPR
C	= 4 IMPULSE FOR GLOBALGRAPHIC ONLY					VISPR
C						VISPR
	IMPLICIT REAL*8 (A-H,O-Z)					VISPR
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,					VISPR
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG					PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),					VISPR
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)					VISPR
	COMMON/DESCRP/ PHI(3,30),W(30),RW(30),SR(4,60),HA(3,60),HB(3,60),					SLIP
*	RPHI(3,30),HT(3,3,60),SPRING(5,90),VISC(7,90),					VISPR
*	JNT(30),IPIN(30),ISING(30),IGLOB(30),JOINTF(30)					VISPR
	COMMON/CMATRX/ V1(3,30),V2(3,30),V3(3,12),B12(3,3,60),A22(3,3,60),					VISPR
*	F(3,30),TQ(3,30),WJ(30),A11(3,3,30)					SLIP
	COMMON/FORCES/PSF(7,70),BSF(4,20),SSF(10,40),BAGSF(3,20),					NCFORC
*	PRJNT(7,30),NPANEL(5),NPSF,NBSF,NSSF,NBGSF					VISPR
	COMMON/CEULER/ IEULER(30),HIR(3,3,90),ANG(3,30),ANGD(3,30),					JDRIFT
*	FE(3,30),TQE(3,30),CONST(5,30)					JDRIFT
	COMMON/TEMPVI/ CREST,TTI(3),R1I(3),R2I(3),JSTOP(4,2,30)					VISPR
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),					VISPR
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI					TWOPI
	COMMON/TEMPVS/ T3(3),T6(3),T7(3),T8(3),T9(3),					VISPR
*	WIJ(3),ANGL(3),DH1(3,3),HD3(3,3),					VISPR
*	HAD,HBD,WIJM,CV,CSA,CSB,TQC,DMMY(35067)					80386
	IF (NJNT.LE.0) GO TO 99					VISPR
	CALL ELTIME(1,13)					VISPR
	IF (NPRT(12).NE.0) WRITE (6,11) TIME,NPG					PAGE
	IF (NPRT(12).NE.0) NPG=NPG+1					PAGE
11	FORMAT('1 VISPR COMPUTATIONS FOR TIME =',F12.6,80X,'PAGE',I5)					PAGE
	J1 = 1					VISPR
	J2 = NJNT					VISPR
	IF (NJ.EQ.0) GO TO 13					VISPR
	J1 = NJ					VISPR
	J2 = NJ					VISPR
13	DO 90 J=J1,J2					VISPR
	DO 12 L=1,3					VISPR
	T3(L) = 0.0					VISPR
	T6(L) = 0.0					VISPR
	ANGL(L) = 0.0					VISPR
12	TQ(L,J) = 0.0					VISPR
	WJ(J) = 0.0					VISPR
C						VISPR
C	DO NOT COMPUTE TORQUES FOR NULL, LOCKED OR EUIER JOINTS.					VISPR

C	I = IABS(JNT(J))	VISPR
	IF (I.LE.0) GO TO 90	VISPR
	CALL DOT33 (D(1,1,J+1),HT(1,1,2*J),HIR(1,1,J))	VISPR
	IF (IABS(IPIN(J)).EQ.4) GO TO 90	SLIP
C		VISPR
C	ZERO T1-T9 ARRAYS AND HAD,HBD,WIJM,CV,CS4,CSB AND TQC.	VISPR
C		VISPR
	WIJM = 0.0	VISPR
	HAC = 0.0	BUTLER1
	CV = 0.0	VISPR
	CSA = 0.0	VISPR
	CSB = 0.0	VISPR
	TQC = 0.0	VISPR
	CALL DOT33 (D(1,1,I),HT(1,1,2*J-1),DH1)	VISPR
	CALL DOT33 (DH1,HIR(1,1,J),HD3)	VISPR
	DO 220 L=1,3	TGMOD6
	DO 220 K=1,3	TGMOD6
	IF(DABS(HD3(L,K)).LT.EPS(10)) HD3(L,K) = 0.00	TGMOD6
220	CONTINUE	TGMOD6
	HAD = HD3(3,3)	VISPR
	IF (HAD.GT. 1.0) HAD = 1.0	VISPR
	IF (HAD.LT. -1.0) HAD = -1.0	VISPR
	ANGL(1) = DACOS(HAD)	VISPR
	IF ((HD3(2,3).NE.0.0 .OR. HD3(1,3).NE.0.0).AND. IABS(IPIN(J)).NE.7)SLIP	SLIP
	*ANGL(2) = DATAN2(HD3(2,3),HD3(1,3))	VISPR
	ANGL(3) = DATAN2(HD3(2,1)-HD3(1,2),HD3(1,1)+HD3(2,2))	VISPR
	IF(NPRT(12).NE.0.AND. IPIN(J).LT.0) WRITE (6,739) J,I,ANGL,	TGMOD6
	*((D(L,K,J+1),K-1,3),(HT(L,K,2*J),K-1,3),(HIR(L,K,J),K-1,3),L-1,3),	TGMOD6
	*((D(L,K,I),K-1,3),(HT(L,K,2*J-1),K-1,3),(DH1(L,K),K-1,3),L-1,3),	TGMOD6
	* ((HD3(L,K),K-1,3),L-1,3)	TGMOD6
739	FORMAT(1H0,'J= ',I2,1X,'I= ',I2,3(2X,D14.7),/,	TGMOD6
	* 2(3(9(1X,D13.6),/),/),3(3(2X,D18.12),/))	TGMOD6
	IF (IPIN(J).LT.0) GO TO 41	VISPR
	IF (NJ.NE.0.AND. IJ.EQ.4) GO TO 27	VISPR
C		VISPR
C	CONVERT TO INERTIAL REFERENCE SYSTEM	VISPR
C	T1= D(I)'*HA(NJ) T4=D(J+1)'*HA(MJ)	VISPR
C	T3= D(I)'*WMEG(I) T6=D(J+1)'*WMEG(J+1)	VISPR
C		VISPR
C	HAD = COS TA = T1.T4	VISPR
C	WIJ = T3-T6	VISPR
C	WJ = !WIJ!	VISPR
C		VISPR
	DO 20 L=1,3	VISPR
	DO 15 M=1,3	VISPR
	T3(L) = T3(L)+ D(M,L,I)* WMEG(M,I)	VISPR
15	T6(L) = T6(L)+ D(M,L,J+1)* WMEG(M,J+1)	VISPR
	WIJ(L)= T3(L)-T6(L)	VISPR
20	WIJM = WIJM + WIJ(L)**2	VISPR
	WIJM = DSQRT(WIJM)	VISPR
	IF (WIJM.LE.EPS(12)) WIJM = 0.0	MISDOT

	WJ(J) = WIJM	VISPR
C		VISPR
C	T7 = T1 X T4	VISPR
C	HAC = !T7!	VISPR
C		VISPR
	CALL CROSS (DH1(1,3),HIR(1,3,J),T7)	VISPR
	HACC = T7(1)**2 + T7(2)**2 + T7(3)**2	VISPR
	HAC = DSQRT(HACC)	VISPR
C		VISPR
C	COMPUTE CV, THE MAGNITUDE OF VISCOUS AND COULOMB TORQUE/WIJM	VISPR
C	RA = +SGN TA DOT = -WIJ.T7	VISPR
C	AND CSA, THE MAGNITUDE OF FLEXURE TORQUE/HAC	VISPR
C		VISPR
	CV = VISCOS(WIJM,VISC(1,3*J-2),HA2)	VISPR
	IF (NJ.EQ.0) HA(2,2*J) = HA2	VISPR
	CREST = VISC(7,3*J-2)	VISPR
	RA = -(WIJ(1)*T7(1) + WIJ(2)*T7(2) + WIJ(3)*T7(3))	VISPR
	IF (HAC.LT.EPS(12)) RA=0.0	MISDOT
	IF (HAC.GE.EPS(12)) RA=RA/HAC	MISDOT
	JSTP = 0	VISPR
	IF (IPIN(J).EQ.7) GOTO 25	SLIP
	IF (JOINTF(J).EQ.0) CSA = EFUNCT(ANGL(1),RA,SPRING(1,3*J-2),JSTP)	VISPR
	IF (JOINTF(J).NE.0) CSA = FINTERP(ANGL(1),ANGL(2),JOINTF(J))	VISPR
	IF (HAC.LT.EPS(12)) CSA=0.0	MISDOT
	IF (HAC.GE.EPS(12)) CSA=CSA/HAC	MISDOT
25	IF (NJ.EQ.0) JSTOP(1,1,J) = JSTP	SLIP
	IF (IPIN(J).EQ.1) GO TO 34	VISPR
	IF (IPIN(J).EQ.6) GOTO 34	SLIP
C		VISPR
C	RB = +SGN TB DOT = -WIJ.T8	VISPR
C	COMPUTE CSB, THE MAGNITUDE OF TORSIONAL TORQUE/HBC	VISPR
C		VISPR
	RB = -(WIJ(1)*HIR(1,3,J) + WIJ(2)*HIR(2,3,J) + WIJ(3)*HIR(3,3,J))	VISPR
	CSB = EFUNCT(ANGL(3),RB,SPRING(1,3*J-1),JSTP)	VISPR
	IF (NJ.EQ.0) JSTOP(2,1,J) = JSTP	VISPR
	IF (NJ.GT.0) GO TO 34	VISPR
C		VISPR
C	COMPUTE EFFECT OF GLOBALGRAPHIC JOINT STOP (IPIN=3)	VISPR
C		VISPR
27	IF (IPIN(J).NE.3) GO TO 34	VISPR
	CALL GLOBAL (J,HD3(1,3),DH1,TQC,T9,ANGL)	VISPR
C		VISPR
C	COMPUTE TOTAL TORQUE IN INERTIAL REFERENCE BY	VISPR
C	TQ = -CV*WIJ + CSA*T7 + CSB*T8 + TQC*T9	VISPR
C		VISPR
34	IF (NJ.EQ.0) GO TO 35	JDRIFT
	CV = 0.0	VISPR
	IF (IJ.NE.1) CSA = 0.0	VISPR
	IF (IJ.NE.2) CSB = 0.0	VISPR
	IF (IJ.NE.4) TQC = 0.0	VISPR
35	IF (HA(2,2*J).EQ.0.0) GO TO 36	JDRIFT
	CALL MAT31 (HIR(1,1,J),HA(1,2*J-1),TQ(1,J))	VISPR





	SUBROUTINE WINDY(MMM,MM,N,NN,NT)	WINDY
	REV IV 07/23/86TWOPI	
C	COMPUTES FORCES AND TORQUES ADDING THEM TO THE U1 AND U2 ARRAYS	WINDY
C	OF WIND BLAST FORCES DETERMINED BY FUNCTION STORED IN TAB(NT)	WINDY
C	ON ELLIPSOID (MM) ATTACHED TO BODY SEGMENT (M) WHICH EXTENDS	WINDY
C	THROUGH THE INTERSECTING PLANE (NN) ATTACHED TO SEGMENT (N).	WINDY
C		WINDY
	IMPLICIT REAL*8 (A-H,O-Z)	WINDY
	COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,	WINDY
*	NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36),NPG	PAGE
	COMMON/SGMNTS/ D(3,3,30),WMEG(3,30),WMEGD(3,30),U1(3,30),U2(3,30),	WINDY
*	SEGLP(3,30),SEGLV(3,30),SEGLA(3,30),NSYM(30)	WINDY
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(1250),TAB(4500)	DIMENB
	COMMON/WINDFR/ WTIME(30),QFU(3,5),QFV(3,5),WF(3,30),IWIND(30),	WINDOP
*	MWSEG(7,30),NFWSEG(6),NFWNT(5),MOWSEG(30,30)	WINDOP
	COMMON/CNTRSF/ PL(24,30),BELT(20,8),TPTS(6,8),BD(24,40)	EDGE
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),	WINDY
*	UNITL,UNITM,UNITT,GRAVITY(3),TWOPI	TWOPI
	COMMON/TEMPVS/ DMNT(3,3),XMN(3),XMM(3),TM(3),BET,BTS,P,FT(3),	WINDOP
*	FF(3),AF(3),FAF,TF,BREF,SCALE,TRACER,AREA,RLM(3),	WINDOP
*	TQM(3),RM(3),DD(3,3),DDD(3,3),R(3,3),DVP(3,3),	WINDOP
*	SI(3,15),R2(2,3),TTF(3),FFT(3),AM(3,3),VP(3),	WINDOP
*	SS(3),SM(3),SN1(3),AS(3),BTE,XNORM,TEMP,	WINDOP
*	X,Y,AI(3,3,15),RYC,AMDA1,AMDA2,B1,B2,RXC	WINDOP
*	,DDMY(34805)	80386
		WINDOP
C	MMM=0 CALCULATE NFORCE	WINDOP
C	MMM>0 WIND FORCE CALCULATED USING ENTIRE AREA METHOD	WINDOP
C	MMM<0 WIND FORCE CALCULATED USING GRID METHOD	WINDOP
C	(ALLOWS BLOCKING SEGMENTS)	WINDOP
C		WINDOP
	DATA NSTEPS/4/	WINDOP
	CALL ELTIME(1,37)	WINDY
	M=IABS(MMM)	WINDOP
	IF (MMM.EQ.0) GO TO 50	WINDOP
C		WINDY
C	COMPUTE PENETRATION DISTANCE; IF NEGATIVE, RETURN.	WINDY
C		WINDY
	CALL DOT33 (D(1,1,M),D(1,1,N),DMNT)	WINDY
	DO 10 I=1,3	WINDY
10	XMN(I) = SEGLP(I,M) - SEGLP(I,N)	WINDY
	CALL MAT31 (D(1,1,M),XMN,XMM)	WINDY
	CALL MAT31 (DMNT,PL(1,NN),TM)	WINDY
	BET = PL(4,NN)	WINDY
	DO 11 I=1,3	WINDY
11	BET = BET - TM(I)*(BD(I+3,MM)+XMM(I))	WINDY
	CALL MAT31 (BD(16,MM),TM,RM)	WINDY
	BTS = TM(1)*RM(1) + TM(2)*RM(2) + TM(3)*RM(3)	WINDY
	BTE = -DSQRT(BTS)	WINDY
	P = BET - BTE	WINDY
	IF (P.LT.0.0) GO TO 99	WINDY
C		WINDY

C	FETCH OR STORE INITIAL PENETRATION TIME.	WINDY
C		WINDY
	IWIND(M) = M	WINDY
	IF (TIME.LE.WTIME(M)) WTIME(M) = TIME	WINDY
	FTIME = TIME - WTIME(M)	WINDY
C		WINDY
C	GET DRAG COEFFICIENT CD FROM TABLE NTC FOR TIME = FTIME.	WINDOP
C		WINDOP
	CD=1.0	WINDOP
	NTC=MWSEG(6,M)	WINDOP
	IF (NTC.EQ.0) GOTO 20	WINDOP
	KT=NTI(NTC)	WINDOP
	NENTRY=TAB(KT+5)	WINDOP
	K1=KT+10	WINDOP
	K2=4*NENTRY+KT+2	WINDOP
	IF (NENTRY.EQ.1) GOTO 18	WINDOP
	DO 17 K=K1,K2,4	WINDOP
	IF (FTIME.GT.TAB(K)) GOTO 17	WINDOP
	KK=K	WINDOP
	R1=(TAB(K)-FTIME)/(TAB(K)-TAB(K-4))	WINDOP
	GOTO 19	WINDOP
17	CONTINUE	WINDOP
18	KK=K2	WINDOP
	R1=0.0	WINDOP
19	R22=1.0-R1	WINDOP
	K=KK+1	WINDOP
	CD=R22*TAB(K)+R1*TAB(K-4)	WINDOP
C		WINDOP
C	GET FORCE VECTOR FT	WINDOP
C		WINDOP
C	RK=0    TIME DEPENDENT WIND FORCE FROM TABLE	WINDOP
C	RK#0    VELOCITY DEPENDENT WIND FORCE	WINDOP
C		WINDOP
20	KT = NTI(NT)	WINDOP
	RK=TAB(KT)	WINDOP
	IF (RK.EQ.0.0) GOTO 13	WINDOP
	C=TAB(KT+1)	WINDOP
	PR=TAB(KT+2)	WINDOP
	NSV=IDINT(TAB(KT+3))	WINDOP
	NSR=IDINT(TAB(KT+4))	WINDOP
	DO 12 I=1,3	WINDOP
	V=SEGLV(I,NSV)-SEGLV(I,NSR)	WINDOP
12	FT(I)=DSIGN(0.5DO,-V)*CD*RK*PR*V**2/C**2	WINDOP
	GOTO 14	WINDOP
13	NSR=IDINT(TAB(KT+4))	WINDOP
	NENTRY = TAB(KT+5)	WINDY
	K1 = KT+10	WINDY
	K2 = 4*NENTRY + KT+2	WINDY
	IF (NENTRY.EQ.1) GO TO 31	WINDY
	DO 30 K=K1,K2,4	WINDY
	IF (FTIME.GT.TAB(K)) GO TO 30	WINDY
	KK = K	WINDY

	R1 = (TAB(K)-FTIME)/(TAB(K)-TAB(K-4))	WINDY
	GO TO 32	WINDY
30	CONTINUE	WINDY
31	KK = K2	WINDY
	R1 = 0.0	WINDY
32	R22= 1.0 - R1	WINDOP
	DO 33 I=1,3	WINDY
	K= KK+I	WINDY
33	FT(I)=(R22*TAB(K) + R1*TAB(K-4))*CD	WINDOP
	IF (NSR.EQ.0) GOTO 14	WINDOP
	CALL DOT31(D(1,1,NSR),FT,FF)	WINDOP
	DO 21 I=1,3	WINDOP
21	FT(I)=FF(I)	WINDOP
14	IF (MMM.LT.0) GOTO 15	WINDOP
C		WINDY
C	COMPUTE PRESENTED AREA TO WIND FORCE.	WINDY
C		WINDY
	CALL MAT31 (D(1,1,M),FT,FF)	WINDY
	CALL MAT31 (BD(7,MM),FF,AF)	WINDY
	FAF = FF(1)*AF(1) + FF(2)*AF(2) + FF(3)*AF(3)	WINDY
	IF (FAF.LE.0.0) GO TO 99	WINDY
	TF = TM(1)*FF(1) + TM(2)*FF(2) + TM(3)*FF(3)	WINDY
	BREF=0.0	CCWIND
	TEMP=BTS-TF*TF/FAF	CCWIND
	IF(TEMP.GT.0.0) BREF =DSQRT(TEMP)	CCWIND
	SCALE = (-BET+BREF)/(-BTE+BREF)	WINDY
	IF (SCALE.GE.1.0) GO TO 99	WINDY
	IF (SCALE.LT.0.0) SCALE = 0.0	WINDY
	TRACER = (BD( 7,MM)-AF(1)**2/FAF)*(BD(11,MM)-AF(2)**2/FAF)	WINDY
*	+ (BD( 7,MM)-AF(1)**2/FAF)*(BD(15,MM)-AF(3)**2/FAF)	WINDY
*	+ (BD(11,MM)-AF(2)**2/FAF)*(BD(15,MM)-AF(3)**2/FAF)	WINDY
*	- (BD( 8,MM)-AF(1)*AF(2)/FAF)**2	WINDY
*	- (BD( 9,MM)-AF(1)*AF(3)/FAF)**2	WINDY
*	- (BD(12,MM)-AF(2)*AF(3)/FAF)**2	WINDY
	AREA = (1.0-SCALE**2) * PI / DSQRT(TRACER)	WINDY
C		WINDY
C	ADD FORCE AND TORQUES TO U1 AND U2 ARRAYS FOR SEGMENT M.	WINDY
C		WINDY
	SCALE = SCALE/BTE	WINDY
	DO 36 I=1,3	WINDY
	RLM(I) = RM(I)*SCALE + BD(I+3,MM)	WINDY
	FT (I) = FT(I)*AREA	WINDY
36	FF (I) = FF(I)*AREA	WINDY
	CALL CROSS (RLM,FF,TQM)	WINDY
	DO 39 I=1,3	WINDY
	WF(I,M)=FT(I)	WINDOP
	U1(I,M) = U1(I,M) + FT(I)	WINDY
39	U2(I,M) = U2(I,M) + TQM(I)	WINDY
	IF (NPRT(14).NE.0) WRITE (6,41) TIME,M,P,AREA,FT,TQM	WINDY
41	FORMAT(' WIND FORCE',F14.6,I6,2F10.3,3X,3F12.5,3X,3F12.5)	WINDY
	GO TO 99	WINDY
C		WINDY

C	USE GRID TO CALCULATE WIND FORCE	WINDOP
C	VP - ORIGIN OF WIND	WINDOP
C		WINDOP
15	AREAT=0.0	WINDOP
	DO 16 I=1,3	WINDOP
	TTF(I)=0.0	WINDOP
	TQM(I)=0.0	WINDOP
16	VP(I) = -FT(I)*10000.0	WINDOP
	TEMP=FT(1)**2+FT(2)**2+FT(3)**2	WINDOP
	IF (TEMP.EQ.0.0) GOTO 99	WINDOP
	CALL MAT31(D(1,1,M),FT,FF)	WINDOP
	TEMP = 0.0	WINDOP
	IF (FT(1).NE.0.0.OR.FT(2).NE.0.0) GOTO 150	WINDOP
C		WINDOP
C	CALCULATE DIRECTION COSINE MATRIX FOR VP COORD. SYS.	WINDOP
C		WINDOP
	DO 140 I=1,3	WINDOP
	DO 140 J=1,3	WINDOP
140	DVP(I,J)=0.0	WINDOP
	DVP(1,2)=1.0	WINDOP
	DVP(2,1)=1.0	WINDOP
	DVP(3,3)=-1.0	WINDOP
	GO TO 141	WINDOP
150	CONTINUE	WINDOP
	DO 110 I=1,3	WINDOP
110	TEMP=TEMP+FT(I)*FT(I)	WINDOP
	TEMP = DSQRT(TEMP)	WINDOP
	XNORM = DSQRT(FT(1)*FT(1)/TEMP**2+FT(2)*FT(2)/TEMP**2)	WINDOP
	DVP(1,1) = FT(2)/(XNORM*TEMP)	WINDOP
	DVP(1,2) = -FT(1)/(XNORM*TEMP)	WINDOP
	DVP(1,3) = 0.0	WINDOP
	DVP(2,1) = FT(1)*FT(3)/(XNORM*TEMP*TEMP)	WINDOP
	DVP(2,2) = FT(2)*FT(3)/(XNORM*TEMP*TEMP)	WINDOP
	DVP(2,3) = -XNORM	WINDOP
	DO 130 I=1,3	WINDOP
130	DVP(3,I) = FT(I)/TEMP	WINDOP
141	CONTINUE	WINDOP
	MOELP = MWSEG(7,M)	WINDOP
C		WINDOP
C	PROJECT MM ELLIPSOID UNTO VP-PLANE	WINDOP
C	AS - PROJECTED ELLIPSE MATRIX	WINDOP
C		WINDOP
	CALL DOTT33(D(1,1,M),DVP,DD)	WINDOP
	CALL MAT33(BD(7,MM),DD,DDD)	WINDOP
	CALL DOT33(D(1,1,M),DDD,DD)	WINDOP
	CALL MAT33(DVP,DD,AM)	WINDOP
	DO 101 K=1,3	WINDOP
101	SS(K)=SEGLP(K,M)+BD(K+3,MM)-VP(K)	WINDOP
	CALL MAT31(DVP,SS,SM)	WINDOP
	DO 114 K=1,3	WINDOP
	IF (DABS(SM(K)).LT.EPS(5)) SM(K)=DSIGN(EPS(5),SM(K))	WINDOP
114	CONTINUE	WINDOP

	CALL SOLVR(AM(1,1),AM(2,1),AM(3,1),AM(1,3),AM(2,3),AM(3,3),	WINDOP
	* AM(1,1),AM(1,3),SM,R(1,1),R(3,1))	WINDOP
	CALL SOLVR(AM(1,2),AM(2,2),AM(3,2),AM(1,3),AM(2,3),AM(3,3),	WINDOP
	* AM(2,2),AM(2,3),SM,R(2,2),R(3,2))	WINDOP
	CALL SOLVR(AM(1,1)+AM(1,2),AM(2,1)+AM(2,2),AM(3,1)+AM(3,2),	WINDOP
	* AM(1,3),AM(2,3),AM(3,3),AM(1,1)+2.0*AM(1,2)+AM(2,2),	WINDOP
	* AM(1,3)+AM(2,3),SM,R(1,3),R(3,3))	WINDOP
	R(2,1)=0.0	WINDOP
	R(1,2)=0.0	WINDOP
	R(2,3)=R(1,3)	WINDOP
	DO 102 K=1,3	WINDOP
	DO 102 J=1,2	WINDOP
102	R2(J,K)=R(J,K)	WINDOP
	CALL SOLVA(R2,AS(1),AS(2),AS(3))	WINDOP
C		WINDOP
C	GET MAJOR & MINOR AXES OF PROJECTED ELLIPSE	WINDOP
C		WINDOP
	TEMP=(AS(1)+AS(2))*2-4.0*(AS(1)*AS(2)-AS(3))*2)	WINDOP
	IF (TEMP.LT.0.0) TEMP=0.0	WINDOP
	TEMP = DSQRT(TEMP)	WINDOP
	AMDA1=(AS(1)+AS(2)+TEMP)/2.0	WINDOP
	AMDA2=(AS(1)+AS(2)-TEMP)/2.0	WINDOP
	R2(1,1)=AS(3)	WINDOP
	R2(2,1)=AMDA1-AS(1)	WINDOP
	R2(1,2)=AMDA2-AS(2)	WINDOP
	R2(2,2)=AS(3)	WINDOP
	AMDA1=DABS(AMDA1)	WINDOP
	AMDA2=DABS(AMDA2)	WINDOP
	B1=DSQRT(1.0/(AMDA1*(R2(1,1)**2+R2(1,2)**2)))	WINDOP
	B2=DSQRT(1.0/(AMDA2*(R2(2,1)**2+R2(2,2)**2)))	WINDOP
	R2(1,1)=R2(1,1)*B1	WINDOP
	R2(1,2)=R2(1,2)*B2	WINDOP
	R2(2,1)=R2(2,1)*B1	WINDOP
	R2(2,2)=R2(2,2)*B2	WINDOP
C		WINDOP
C	GET BLOCKING ELLIPSOIDS IN VP COORD. SYS.	WINDOP
C		WINDOP
	DO 103 MI=1,MOELP	WINDOP
	I=MOWSEG(M,MI*2-1)	WINDOP
	II=MOWSEG(M,MI*2)	WINDOP
	CALL DOT33(D(1,1,I),DVP,DD)	WINDOP
	CALL MAT33(BD(7,II),DD,DDD)	WINDOP
	CALL DOT33(D(1,1,I),DDD,DD)	WINDOP
	CALL MAT33(DVP,DD,AI(1,1,MI))	WINDOP
	DO 104 K=1,3	WINDOP
104	SS(K)=SEGLP(K,I)+BD(K+3,II)-VP(K)	WINDOP
	CALL MAT31(DVP,SS,SI(1,MI))	WINDOP
	DO 115 K=1,3	WINDOP
	IF (DABS(SI(K,MI)).LT.EPS(6)) SI(K,MI)=DSIGN(EPS(6),SI(K,MI))	WINDOP
115	CONTINUE	WINDOP
103	CONTINUE	WINDOP
C		WINDOP

C	SET-UP GRID AND CHECK EACH RECTANGLE CENTER POINT	WINDOP
C		WINDOP
	AREA=DSQRT((R2(1,1)**2+R2(2,1)**2)*(R2(1,2)**2+R2(2,2)**2))	WINDOP
	AREA=AREA/NSTEPS**2	WINDOP
	IN=2*NSTEPS+1	WINDOP
	DO 105 I=1,IN	WINDOP
	RXC=R2(1,1)-R2(1,1)*(I-1)/NSTEPS	WINDOP
	RYC=R2(2,1)-R2(2,1)*(I-1)/NSTEPS	WINDOP
	DO 106 J=1,IN	WINDOP
	RM(1)=(RXC-R2(1,2)*(NSTEPS-J+1)/NSTEPS)*0.9999	WINDOP
	RM(2)=(RYC-R2(2,2)*(NSTEPS-J+1)/NSTEPS)*0.9999	WINDOP
	TM(1)=AM(3,3)	WINDOP
	TM(2)=2.0*(RM(1)*AM(1,3)+RM(2)*AM(2,3))	WINDOP
	TM(3)=RM(1)**2*AM(1,1)+RM(2)**2*AM(2,2)+2.0*RM(1)*RM(2)*AM(1,2)-1.	WINDOP
	TEMP=TM(2)**2-4.0*TM(1)*TM(3)	WINDOP
	IF (TEMP.LT.0.0) GOTO 106	WINDOP
	B1=(DSQRT(TEMP)-TM(2))/(2.0*TM(1))	WINDOP
	B2=- (DSQRT(TEMP)+TM(2))/(2.0*TM(1))	WINDOP
	RM(3)=B1	WINDOP
	IF (B2.LT.B1) RM(3)=B2	WINDOP
	SN1(1)=RM(1)+SM(1)	WINDOP
	SN1(2)=RM(2)+SM(2)	WINDOP
	SN1(3)=RM(3)+SM(3)	WINDOP
	CALL DOT31(DVP,SN1,XMM)	WINDOP
C		WINDOP
C	CHECK FOR PENETRATION	WINDOP
C		WINDOP
	DO 107 K=1,3	WINDOP
107	XMN(K)=VP(K)-SEGLP(K,N)+XMM(K)	WINDOP
	CALL MAT31(D(1,1,N),XMN,XMM)	WINDOP
	BET=PL(4,NN)	WINDOP
	BTS=PL(1,NN)*XMM(1)+PL(2,NN)*XMM(2)+PL(3,NN)*XMM(3)	WINDOP
	IF (BTS.GT.BET) GOTO 106	WINDOP
C		WINDOP
C	CHECK FOR BLOCKING ELLIPSOIDS	WINDOP
C		WINDOP
	DO 109 IM=1,MOELP	WINDOP
	X=SN1(1)-SI(1,IM)	WINDOP
	Y=SN1(2)-SI(2,IM)	WINDOP
	TM(1)=AI(3,3,IM)	WINDOP
	TM(2)=2.0*(AI(1,3,IM)*X+AI(2,3,IM)*Y)	WINDOP
	TM(3)=AI(1,1,IM)*X**2+AI(2,2,IM)*Y**2+2.0*AI(1,2,IM)*X*Y-1.0	WINDOP
	TEMP=TM(2)**2-4.0*TM(1)*TM(3)	WINDOP
	IF (TEMP.LT.0.0) GOTO 109	WINDOP
	B1=(-TM(2)+DSQRT(TEMP))/(2.0*TM(1))	WINDOP
	B2=(-TM(2)-DSQRT(TEMP))/(2.0*TM(1))	WINDOP
	IF (B2.LT.B1) B1=B2	WINDOP
	SNZ=B1+SI(3,IM)	WINDOP
	IF (SNZ.LT.SN1(3)) GOTO 106	WINDOP
109	CONTINUE	WINDOP
	CALL DOT31(DVP,RM,SS)	WINDOP
	CALL MAT31(D(1,1,M),SS,RM)	WINDOP

C		WINDOP
C	SUM FORCES & TORQUES	WINDOP
C		WINDOP
	AREAT=AREAT+AREA	WINDOP
	DO 111 K=1,3	WINDOP
	TTF(K)=FT(K)*AREA+TTF(K)	WINDOP
	RM(K)=RM(K)+BD(K+3,MM)	WINDOP
111	FFT(K)=FF(K)*AREA	WINDOP
	CALL CROSS(RM,FFT,TM)	WINDOP
	DO 112 K=1,3	WINDOP
112	TQM(K)=TQM(K)+TM(K)	WINDOP
106	CONTINUE	WINDOP
105	CONTINUE	WINDOP
C		WINDOP
C	ADD FORCE & TORQUE TO U1 & U2 ARRAYS FOR SEGMENT M	WINDOP
C		WINDOP
	IF (NPRT(14).NE.0) WRITE(6,200) TIME,M,AREAT,TTF,TQM	WINDOP
200	FORMAT(' WIND FORCE',F14.6,I6,I3X,F10.3,3F12.5,3X,3F12.5)	WINDOP
	DO 113 I=1,3	WINDOP
	WF(I,M)=TTF(I)	WINDOP
	U1(I,M)=U1(I,M)+TTF(I)	WINDOP
113	U2(I,M)=U2(I,M)+TQM(I)	WINDOP
	GO TO 99	WINDOP
C		WINDOP
C	M = 0: CALCULATE FORCE FUNCTIONS.	WINDOP
C		WINDY
50	NFORCE = NRVSEG(6)	WINDY
	DO 60 J=1,NFORCE	WINDY
	NFS = IABS(NRVSEG(J))	WINDY
	NFT = IABS(NRVNT(J))	WINDY
	KFT = NTI(NFT)	WINDY
	FRCE = EVALFD(TIME,KFT,1)	WINDY
	IF (NRVSEG(J).GT.0) GO TO 52	WINDY
	DO 51 I=1,3	WINDY
51	U2(I,NFS) = U2(I,NFS) + FRCE*QFU(I,J)	WINDY
	GO TO 60	WINDY
52	CALL DOT31 (D(1,1,NFS),QFU(1,J),TM)	WINDY
	DO 53 I=1,3	WINDY
	U1(I,NFS) = U1(I,NFS) + FRCE*TM(I)	WINDY
53	U2(I,NFS) = U2(I,NFS) + FRCE*QFV(I,J)	WINDY
60	CONTINUE	WINDY
99	CALL ELTIME (2,37)	WINDY
	RETURN	WINDY
	END	WINDY

	DOUBLE PRECISION FUNCTION XDY(X,D,Y)		XDY
C		REV IV	07/23/86JTF786
C	FUNCTION ROUTINE TO COMPUTE X.DY OR Y.D'X		XDY
C			XDY
	IMPLICIT REAL*8(A-H,O-Z)		XDY
	DIMENSION X(3),D(3,3),Y(3)		XDY
	XDY = 0.0		XDY
	DO 10 I=1,3		XDY
10	XDY = XDY + X(I)*(D(I,1)*Y(1)+D(I,2)*Y(2)+D(I,3)*Y(3))		JTF786
	RETURN		XDY
	END		XDY



	SUBROUTINE YPRDEG(D,A)		REV IV	11/26/86	YPRDEG
C					YPRFIX
C	COMPUTES YAW PITCH AND ROLL IN DEGREES AND PLACES THEM				YPRDEG
C	INTO THE A ARRAY FOR A GIVEN DIRECTION COSINE MATRIX D.				YPRDEG
C					YPRDEG
C	ASSUMES D = D(R)D(P)D(Y) , WHERE				YPRDEG
C					YPRDEG
C	1 0 0 CP 0 -SP CY SY 0				YPRDEG
C	D(R) = 0 CR SR ,D(P) = 0 1 0 AND D(Y) = -SY CY 0				YPRDEG
C	0 -SR CR SP 0 CP 0 0 1				YPRDEG
C					YPRDEG
	IMPLICIT REAL*8(A-H,O-Z)				YPRDEG
	DIMENSION A(3),D(3,3)				YPRDEG
	COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),				YPRDEG
	* UNITL,UNITM,UNITT,GRAVITY(3),TWOPI				TWOPI
	IF (DABS(D(1,1)).LE.EPS(15).AND.DABS(D(1,2)).LE.EPS(15))GOTO10				YPRFIX
	IF (DABS(D(2,3)).LE.EPS(15).AND.DABS(D(3,3)).LE.EPS(15))GOTO10				YPRFIX
	YAW = DATAN2(D(1,2),D(1,1))				YPRDEG
	ROLL = DATAN2(D(2,3),D(3,3))				YPRDEG
	GO TO 11				YPRDEG
10	YAW = DATAN2(-D(2,1),D(2,2))				YPRDEG
	ROLL = 0.0				YPRDEG
11	PITCH = -DASIN(D(1,3))				YPRDEG
	IF (DABS(ROLL).LE.0.5*PI) GO TO 20				YPRDEG
	IF (DABS(YAW ).LE.0.5*PI) GO TO 20				YPRDEG
	PITCH = DSIGN(PI-DABS(PITCH),PITCH)				YPRDEG
	YAW = DATAN2(-D(1,2),-D(1,1))				YPRDEG
	ROLL = DATAN2(-D(2,3),-D(3,3))				YPRDEG
20	A(1) = YAW/RADIAN				YPRDEG
	A(2) = PITCH/RADIAN				YPRDEG
	A(3) = ROLL/RADIAN				YPRDEG
	RETURN				YPRDEG
	END				YPRDEG

APPENDIX J

386-VIEW Program Listing

	PROGRAM VIEW		V1.1
	COMMON/PLTT/SFACTR,INT,TIME,ICOLOR(91),OFSETX,OFSETY,ZTIME		V1.1
	COMMON/INTERS/ NIE(90),IE(90,90)		V1.1
	COMMON/ELLIPSE/NSTEPS(90),IELP,A(3,3,30),SEGLP(3,90),VP(3),		V1.1
	*D(3,3,90),DVP(3,3),RA(3),NSEG,SEGLPO(3,90)		V1.2
	COMMON/POLYGON/NPLANE,IFLAG,NPPP(90),PO(3,4,60),P(3,4,60),		V1.1
	*CONVEC(2,4,90),POS(2,90),SIGN(90)		V1.1
	COMMON/ATB/PL(17,30)		V1.1
	COMMON/VIEWP/VP0(3),DVP0(3,3),IVP,VP2(3)		V1.1
	COMMON/DEBUG/IDEBUG(80),NISC,DEVFLG,ONLINE,TERM,BDRS,OFFLINE		V1.1
	COMMON/DEVICE/IDEF,IOPORT,MODEL	80386	
	DIMENSION WORK(10000)		V1.1
	CHARACTER*4 ID(10)	80386	
	INTEGER DEVFLG,ONLINE,TERM,BDRS,OFFLINE		V1.1
	DOUBLE PRECISION ZTIME,CTIME,STIME,DTIME,ETIME		V1.1
	CHARACTER*12 FILE1,FILE5,FILE6	80386	
C			V1.1
C	PROGRAM VIEW	VERSION 1.1	LAST MOD. - MARCH 9, 1983
C		VERSION 1.2	LAST MOD. - DECEMBER 18, 1984
C	WRITTEN BY SRL IN SUPPORT OF THE		V1.1
C	MODELING AND ANALYSIS BRANCH OF AMRL		V1.1
C	AT WPAFB.		V1.1
C			80386
C	80386 IMPLEMENTATION BY KETRON, INC.	- OCTOBER 31, 1989	80386
C			V1.1
C	STORED ON TAPE1 THAT IS OUTPUT FROM THE ATBM VERSION V5D.		V1.1
C			V1.1
C	THIS PROGRAM USES CONTOUR LINES TO REPRESENT THE 3-D PROPERTIES OF		V1.1
C	THE DATA ON TAPE1. THE CONTOUR LINES ARE PLOTTED ON PAPER THAT		V1.1
C	REPRESENTS THE PROJECTION PLANE. THE POINTS THAT COMPOSE A CONTOUR		V1.1
C	LINE IN 3-SPACE ARE PROJECTED THROUGH A POINT ON TO THE PROJECTION		V1.1
C	PLANE.		V1.1
C			V1.1
C	CURRENTLY THERE ARE TWO CLASSES OF OBJECTS THAT ARE PLOTTED USING		V1.1
C	CONTOUR LINES.		V1.1
C	CLASS 1 - ELLIPSOIDS		V1.1
C	ELLIPSOIDS ARE USED TO REPRESENT BODY SEGMENTS. THIS PROGRAM ALLOWS		V1.1
C	ELLIPSOIDS TO BE IMBEDDED IN OTHER ELLIPSOIDS.		V1.1
C			V1.1
C	CLASS 2 - CONVEX POLYGONS		V1.1
C	CONVEX POLYGONS ARE USED TO REPRESENT OBJECTS THAT CAN BE DEFINED		V1.1
C	BY A SET OF PLANES. ALL POLYGONS DEFINED BY THE INPUT MUST BE		V1.1
C	CONVEX POLYGONS; CONCAVE POLYGONS CAN BE OBTAINED USING A		V1.1
C	COMBINATION OF CONVEX POLYGONS.		V1.1
C			V1.1
C	THE HIDDEN LINE ROUTINES CHECK FOR POINTS HIDDEN BY		V1.1
C	ELLIPSOIDS OR POLYGONS. THESE ROUTINES MUST CHECK		V1.1
C	FOR ANY POSSIBLE OBJECT THAT MAY BE BLOCKING THE		V1.1
C	CURRENT POINT AS SEEN FROM THE VIEWPOINT.		V1.1
C	IN ORDER TO ELIMINATE CHECKING ALL OBJECTS FOR		V1.1
C	EACH POINT, SUBROUTINES ARE INCLUDED IN THE		V1.1
C	VIEW PROGRAM THAT DETECT OBJECT OVERLAP ON THE		V1.1

C	PROJECTION PLANE. BEFORE THE PLOTTING PHASE OF THE	V1.1
C	VIEW PROGRAM, OBJECTS WHICH OVERLAP EACH OTHER ON	V1.1
C	THE PROJECTION PLANE ARE RECORDED IN THE IE ARRAY.	V1.1
C	DURING THE PLOTTING PHASE OF THE VIEW PROGRAM, THE	V1.1
C	IE ARRAY IS REORDERED TO DECREASE THE SEARCH TIME	V1.1
C	FOR OBJECTS THAT MAY BE BLOCKING THE CURRENT POINT	V1.1
C	BEING PLOTTED. THE ASSUMPTION USED HERE IS - IF AN	V1.1
C	OBJECT BLOCKED THE PREVIOUS POINT ON A CONTOUR LINE	V1.1
C	THEN THAT OBJECT PROBABLY BLOCKS THE NEXT POINT	V1.1
C	ON THE CONTOUR LINE.	V1.1
C		V1.1
	OPEN (UNIT=4,FILE='VIEWPE.DIR',STATUS='OLD')	80386
	READ (4, '(A12/A12/A12)') FILE1, FILE5, FILE6	80386
	READ (4, '(I4/I4/I4)') IDEF, IOPORT, MODEL	80386
	OPEN (UNIT=1,FILE=FILE1,STATUS='OLD',FORM='UNFORMATTED')	80386
	OPEN (UNIT=5,FILE=FILE5,STATUS='OLD')	80386
	OPEN (UNIT=6,FILE=FILE6,STATUS='NEW',CARRIAGE CONTROL='FORTRAN')	80386
C	LUPLOT=8	80386
	ONLINE=1	V1.1
	TERM=2	V1.1
	NF=0	V1.1
	OFLINE=3	V1.1
	BDRS=4	V1.1
	READ(5,130) DEVFLG	V1.1
	DEVFLG=BDRS	80386
	WRITE(6,130) DEVFLG	V1.1
130	FORMAT(I1)	V1.1
C		V1.1
	CALL PLOTS(IDEF,IOPORT,MODEL)	80386
	CALL FACTOR(.75)	80386
C		V1.1
	IFLAG = 0	V1.1
	CALL TITLE	V1.1
	CALL FACTOR(1.0)	80386
	READ(5,200) (ID(I),I=1,10)	V1.1
	WRITE(6,200) (ID(I),I=1,10)	V1.1
200	FORMAT(10A4)	V1.1
	READ(5,150) STIME,DTIME,ETIME	V1.1
150	FORMAT(3D10.0)	V1.1
	CTIME=STIME-DTIME	V1.1
	ITIME=CTIME*1000000.D0	V1.1
	CTIME=ITIME/1000000.D0	V1.1
	READ(5,125) IDEBUG	V1.1
	WRITE(6,125) IDEBUG	V1.1
125	FORMAT(80I1)	V1.1
100	CONTINUE	V1.1
	IFLAG = IFLAG + 1	V1.1
	CTIME=CTIME+DTIME	V1.1
	ITIME=CTIME*1000000.D0	V1.1
	CTIME=ITIME/1000000.D0	V1.1
	IF(CTIME.GT.ETIME) CALL PLOT(0.,0.,999)	V1.1
	IF(CTIME.GT.ETIME) STOP	V1.1

CALL INPUT(CTIME)	V1.1
IF(IFLAG.EQ.10) GO TO 100	V1.1
IF(DEVFLG.EQ.OFFLINE.OR.DEVFLG.EQ.BDRS)	80386
* CALL COLOR(ICOLOR(91),IERR)	80386
XTIME=ZTIME*1000.0	V1.1
NF=NF+1	V1.1
WRITE(6,1000)NF	V1.1
1000 FORMAT(' MAIN - PROCESSING FRAME #',I4)	V1.1
CALL PLOT(0.,0.,-3)	V1.1
CALL SYMBOL(.5, 8.0,.335,ID,0.,35)	80386
CALL SYMBOL(.5,7.0,.335,'TIME(MSEC)',0.,10)	80386
CALL NUMBER(3.85,7.0,.335,XTIME,0.,-1)	80386
CALL MAT(DVP0,D(1,1,IVP),DVP,3,3,3,3,3,3)	V1.1
CALL DOT(D(1,1,IVP),VPO,VP,3,1,3)	V1.1
DO 10 K=1,3	V1.1
10 VP(K)=VP(K)+SEGLP(K,IVP)	V1.1
CALL MAT(DVP,VP,VP2,3,3,1,3,3,3)	V1.1
CALL CONVREC	V1.1
CALL PRJPLY	V1.1
CALL PRJELR	V1.1
CALL POLYD	V1.1
CALL BUILDIE	V1.1
IF(IDEBUG(1).EQ.1) WRITE(6,350) (NIE(I),I=1,90)	V1.1
IF(IDEBUG(2).EQ.1) WRITE(6,350) ((IE(I,J),I=1,90),J=1,90)	V1.1
350 FORMAT(270(30(1X,I2)/))	V1.1
DO 30 IK=1,NSEG	V1.1
IF(DEVFLG.EQ.OFFLINE.OR.DEVFLG.EQ.BDRS) CALL COLOR(ICOLOR(IK),IERR)	80386
IELP=IK	V1.1
INDEX=NSTEPS(IK)+1	V1.1
INDEX2=4*INDEX-3	V1.1
IX1=1	V1.1
IIN=3*INDEX*INDEX+IX1	V1.1
ISEG=IIN+INDEX	V1.1
CALL ELIPSN(INDEX,WORK(IX1),WORK(IIN))	V1.1
CALL PSE(WORK(IX1),WORK(IIN),WORK(ISEG),INDEX,INDEX2,1)	V1.1
CALL PSE(WORK(IX1),WORK(IIN),WORK(ISEG),INDEX,INDEX2,2)	V1.1
30 CONTINUE	V1.1
CALL PLPLN(WORK,INDEX2)	V1.1
IF(DEVFLG.EQ.BDRS) CALL NFRAME	V1.1
IF(DEVFLG.EQ.OFFLINE.OR.DEVFLG.EQ.ONLINE) CALL PLOT (12.,0.0,-3)	V1.1
IF(DEVFLG.EQ.TERM) CALL PLOT(0.,0.,-3)	V1.1
GO TO 100	V1.1
END	V1.1

	SUBROUTINE BUILDIE	V1.1
C		V1.1
C	ONCE THIS SUBROUTINE IS CALLED ALL OBJECTS ARE REPRESENTED BY	V1.1
C	POLYGONS PROJECTED ON THE VIEWPOINT PROJECTION PLANE.	V1.1
C	THIS SUBROUTINE WILL BUILD THE IE AND NIE ARRAYS.	V1.1
C	NEE(K) REPRESENTS THE MEMBER OF ENTRIES IN THE IE(I,K) ARRAY FOR	V1.1
C	OBJECT K.	V1.1
C	THE IE(I,K) ARRAY CONTAINS OBJECT NUMBERS FOR OBJECTS THAT OVERLAP	V1.1
C	IN THE PROJECTION PLANE.	V1.1
C	FOR EXAMPLE, IE(1,2) MIGHT CONTAIN A 3 WHICH MEANS OBJECT 3	V1.1
C	OVERLAPS WITH OBJECT 2.	V1.1
	COMMON/POLYGON/NPLANE, IFLAG, NPPP(90), PO(3,4,60), P(3,4,60),	V1.1
	*CONVEC(2,4,90), POS(2,90), SIGN(90)	V1.1
	COMMON/ELLIPSE/NSTEPS(90), IELP, A(3,3,30), SEGLP(3,90), VP(3),	V1.1
	*D(3,3,90), DVP(3,3), RA(3), NSEG, SEGLPO(3,90)	V1.2
	COMMON/INTERS/ NIE(90), IE(90,90)	V1.1
	COMMON/REMOVE/NPREM, IREMOV(30)	V1.1
	DO 5 I=1,90	V1.1
	NIE(I) = 0	V1.1
	DO 5 K=1,90	V1.1
5	IE(I,K) = 0	V1.1
	IF(NSEG .EQ. 0) GO TO 60	V1.1
	DO 55 I=1,NSEG	V1.1
	IF(NIE(I) .NE. 0) GO TO 10	V1.1
	NIE(I) = 1	V1.1
	IE(1,I) = I	V1.1
10	IOBJ = I + 1	V1.1
	IF(I.EQ.NSEG) GO TO 31	V1.1
	DO 30 K=IOBJ,NSEG	V1.1
	CALL OVERLAP(I,K,MFLAG)	V1.1
	IF(MFLAG .EQ. 0) GO TO 30	V1.1
C		V1.1
C	YES, THERE IS OVERLAP BETWEEN I AND K	V1.1
C		V1.1
	IF(NIE(K) .NE. 0) GO TO 20	V1.1
	NIE(K) = 1	V1.1
	IE(1,K) = K	V1.1
20	NIE(K) = NIE(K) + 1	V1.1
	NIE(I) = NIE(I) + 1	V1.1
	IE(NIE(I),I) = K	V1.1
	IE(NIE(K),K) = I	V1.1
30	CONTINUE	V1.1
31	CONTINUE	V1.1
	IF(NPLANE.EQ.0) GO TO 55	V1.1
	IOBJ = NPLANE + 30	V1.1
	DO 50 K=31,IOBJ	V1.1
	DO 200 LT=1,NPREM	V1.1
	IF(K-30.EQ.IREMOV(LT)) GO TO 50	V1.1
200	CONTINUE	V1.1
	CALL OVERLAP(I,K,MFLAG)	V1.1
	IF(MFLAG .EQ. 0) GO TO 50	V1.1
C		V1.1

C	YES, THERE IS OVERLAP BETWEEN I AND K	V1.1
C		V1.1
	NIE(K) = NIE(K) + 1	V1.1
	NIE(I) = NIE(I) + 1	V1.1
	IE(NIE(I),I) = K	V1.1
	IE(NIE(K),K) = I	V1.1
50	CONTINUE	V1.1
55	CONTINUE	V1.1
C		V1.1
C	NOW CHECK PLANE AGAINST PLANE	V1.1
C		V1.1
60	IF(NPLANE .LE. 1) RETURN	V1.1
	MPLANE=NPLANE+29	V1.1
	KPLANE=NPLANE+30	V1.1
	DO 100 I=31,MPLANE	V1.1
	DO 300 LT=1,NPREM	V1.1
	IF(I-30.EQ.IREMOV(LT)) GO TO 100	V1.2
300	CONTINUE	V1.1
	IOBJ = I + 1	V1.1
	DO 400 K=IOBJ,KPLANE	V1.1
	CALL OVERLAP(I,K,MFLAG)	V1.1
	IF(MFLAG .EQ. 0) GO TO 400	V1.1
C		V1.1
C	YES, THERE IS OVERLAP BETWEEN I AND K	V1.1
C		V1.1
	DO 500 LT=1,NPREM	V1.2
	IF(K-30.EQ.IREMOV(LT)) GO TO 400	V1.2
500	CONTINUE	V1.2
	NIE(K) = NIE(K) + 1	V1.1
	NIE(I) = NIE(I) + 1	V1.1
	IE(NIE(I),I) = K	V1.1
	IE(NIE(K),K) = I	V1.1
400	CONTINUE	V1.1
100	CONTINUE	V1.1
	RETURN	V1.1
	END	V1.1

	SUBROUTINE CLIP(X,Y,XSAV,YSAV,XMIN,XMAX,YMIN,YMAX,IPEN,IPLT)	V1.1
C	*****	V1.1
C		V1.1
C	THIS SUBROUTINE CLIPS PLOTTING OFF BOTH ENDS OF THE CALCOMP DRUM	V1.1
C		V1.1
C	*****	V1.1
C		V1.1
	LOGICAL XOFF,YOFF	V1.1
	DATA LCALL/0/	V1.1
C		V1.1
C	DETERMINE IF X AND/OR Y CLIPPING AND IF OFF TOP,BOTTOM,LEFT,	V1.1
C	OR RIGHT OF PLOTTER	V1.1
C		V1.1
	XOFF=.FALSE.	V1.1
	YOFF=.FALSE.	V1.1
	IF (X.LT.XMIN.OR.X.GT.XMAX) XOFF=.TRUE.	V1.1
	IF (Y.LT.YMIN.OR.Y.GT.YMAX) YOFF=.TRUE.	V1.1
	IF (X.LT.XMIN) XLIMIT=XMIN	V1.1
	IF (X.GT.XMAX) XLIMIT=XMAX	V1.1
	IF (Y.LT.YMIN) YLIMIT=YMIN	V1.1
	IF (Y.GT.YMAX) YLIMIT=YMAX	V1.1
C		V1.1
C	IF PREVIOUS CALL TO CLIP WAS A PEN UP TO 1ST POINT IN SEGMENT,	V1.1
C	INTERPOLATE USING NEW AND SAVED COORD.'S, MOVE PEN, RESET SAVE	V1.1
C	VALUES FOR X+Y POINTS, AND CONTINUE	V1.1
C		V1.1
	IF (LCALL.EQ.0) GO TO 10	V1.1
	IF (XOFF) YLTEMP=YINTCP(X,Y,XSAV,YSAV,XLIMIT)	V1.1
	IF (.NOT.XOFF) YLTEMP=YLIMIT	V1.1
	IF (YOFF) XLTEMP=XINTCP(X,Y,XSAV,YSAV,YLIMIT)	V1.1
	IF (.NOT.YOFF) XLTEMP=XLIMIT	V1.1
	IF (XLTEMP.LT.XMIN) XLTEMP=XMIN	V1.1
	IF (XLTEMP.GT.XMAX) XLTEMP=XMAX	V1.1
	IF (YLTEMP.LT.YMIN) YLTEMP=YMIN	V1.1
	IF (YLTEMP.GT.YMAX) YLTEMP=YMAX	V1.1
	CALL PLOT(XLTEMP,YLTEMP,3)	V1.1
	XSAV=XLTEMP	V1.1
	YSAV=YLTEMP	V1.1
	LCALL=0	V1.1
C		V1.1
C	IF 1ST POINT OF SEGMENT AND PEN UP, SAVE THESE COORD.'S, SET	V1.1
C	FLAG, AND EXIT	V1.1
C		V1.1
10	CONTINUE	V1.1
	IF (IPLT.NE.1.OR.IPEN.NE.3) GO TO 20	V1.1
	XLSAV=X	V1.1
	YLSAV=Y	V1.1
	LCALL=1	V1.1
	IPLT=0	V1.1
	RETURN	V1.1
C		V1.1
C	DO WE WANT TO PLOT?	V1.1



C		V1.1
20	CONTINUE	V1.1
	IF (IPLOT.NE.1) GO TO 30	V1.1
C		V1.1
C	DETERMINE X AND Y COORDINATES TO PLOT TO	V1.1
C		V1.1
	IF (XOFF) YTEMP=YINTCP(X,Y,XSAV,YSAV,XLIMIT)	V1.1
	IF (.NOT.XOFF) YTEMP=YLIMIT	V1.1
	IF (YOFF) XTEMP=XINTCP(X,Y,XSAV,YSAV,YLIMIT)	V1.1
	IF (.NOT.YOFF) XTEMP=XLIMIT	V1.1
C		V1.1
C	PLOT ONLY THE FIRST SEGMENT AFTER CLIPPING DETERMINED, IGNORING	V1.1
C	ALL SEGMENTS AFTER UNLESS PEN TO BE LIFTED.	V1.1
C		V1.1
	CALL PLOT(XTEMP,YTEMP,IPEN)	V1.1
30	CONTINUE	V1.1
	IPLOT=0	V1.1
	RETURN	V1.1
	END	V1.1

	SUBROUTINE CONVREC	V1.1
C		V1.1
C	THIS SUBROUTINE CONVERTS RECTANGLES IN THE ATB	V1.1
C	SIMULATION FORMAT TO POLYGONS IN THE VIEW PLOTTING FORMAT.	V1.1
C		V1.1
	COMMON/ATB/PL(17,30)	V1.1
	DIMENSION R(3)	V1.1
	DIMENSION DX(3)	V1.1
	COMMON/POLYGON/NPLANE, IFLAG, NPPP(90), PO(3,4,60), P(3,4,60),	V1.1
	*CONVEC(2,4,90), POS(2,90), SIGN(90)	V1.1
	COMMON/CONECT/ NP, MPL(3,5,60)	V1.1
	COMMON/DEBUG/IDEBUG(80), NISG, DEVFLG, ONLINE, TERM, BDRS, OFFLINE	V1.1
	COMMON/ELLIPSE/NSTEPS(90), IELP, A(3,3,30), SEGLP(3,90), VP(3),	V1.1
	*D(3,3,90), DVP(3,3), RA(3), NSEG, SEGLPO(3,90)	V1.2
	INTEGER DEVFLG, ONLINE, TERM, BDRS, OFFLINE	V1.1
	IF(NPLANE.EQ.0) RETURN	V1.1
	IF(IDEBUG(4).NE.0) WRITE(6,50)	V1.1
50	FORMAT(1H1, 'PLANE INFORMATION',/, 1H ,17(1H*))	V1.1
	DO 100 J=1, NPLANE	V1.1
	IF(J.GT.NP) GO TO 15	V1.1
	IF(IFLAG.NE.1) GO TO 15	V1.1
	DDD=DET(PL(1,J), PL(2,J), PL(3,J), PL(8,J), PL(9,J), PL(10,J),	V1.1
	- PL(13,J), PL(14,J), PL(15,J))	V1.1
	DX(1) = DET(PL(4,J), PL(2,J), PL(3,J), PL(11,J), PL(9,J), PL(10,J),	V1.1
	- PL(16,J), PL(14,J), PL(15,J))	V1.1
	DX(2) = DET(PL(1,J), PL(4,J), PL(3,J), PL(8,J), PL(11,J), PL(10,J),	V1.1
	- PL(13,J), PL(16,J), PL(15,J))	V1.1
	DX(3) = DET(PL(1,J), PL(2,J), PL(4,J), PL(8,J), PL(9,J), PL(11,J),	V1.1
	- PL(13,J), PL(14,J), PL(16,J))	V1.1
	DO 10 I=1,3	V1.1
	TEMP=DX(I)/DDD	V1.1
	PO(I,1,J)=TEMP	V1.1
	PO(I,2,J)=PL(I+7,J)*PL(12,J)+TEMP	V1.1
	PO(I,3,J)=PL(I+12,J)*PL(17,J)+PO(I,2,J)	V1.1
10	PO(I,4,J)=PL(I+12,J)*PL(17,J)+TEMP	V1.1
15	CONTINUE	V1.1
	ISG=MPL(1,1,J)	V1.1
	IF(ISG.EQ.0) ISG=NISG	V1.1
	IF(IDEBUG(4).NE.0) WRITE(6,200) ISG	V1.1
200	FORMAT(1X, 'ISG=', I2)	V1.1
	DO 20 L=1,4	V1.1
	CALL DOT(D(1,1,ISG), PO(1,L,J), R, 3, 1, 3)	V1.1
	DO 20 I=1,3	V1.1
	P(I,L,J)=R(I)+SEGLP(I,ISG)	V1.1
20	CONTINUE	V1.1
	IF(J.LE.NP) NPPP(J+30)=4	V1.1
	IF(IDEBUG(4).NE.0) WRITE(6,3000)	V1.1
3000	FORMAT(1X, 30(1H*))	V1.1
	IF(IDEBUG(4).NE.0) WRITE(6,2000) J	V1.1
2000	FORMAT(3X, 'PLANE NUMBER = ', I3)	V1.1
	JJ=J	V1.1
	NPPPP=NPPP(J+30)	V1.1

	IF(IDEBUG(4).NE.0) WRITE(6,1000)((P(I,K,JJ),I-1,3),K-1,NPPPP)	V1.1
1000	FORMAT(3X,F7.2,3X,F7.2,3X,F7.2)	V1.1
100	CONTINUE	V1.1
	RETURN	V1.1
	END	V1.1

	SUBROUTINE CROSS(A,B,C)	V1.1
C	COMPUTES VECTOR CROSS PRODUCT C=AXB	V1.1
	DIMENSION A(3),B(3),C(3)	V1.1
	C(1)=A(2)*B(3)-A(3)*B(2)	V1.1
	C(2)=A(3)*B(1)-A(1)*B(3)	V1.1
	C(3)=A(1)*B(2)-A(2)*B(1)	V1.1
	RETURN	V1.1
	END	V1.1

FUNCTION DET(A11,A12,A13,A21,A22,A23,A31,A32,A33)	V1.1
DET=A11*(A22*A33-A23*A32)-A12*(A21*A33-A23*A31)	V1.1
1+A13*(A21*A32-A22*A31)	V1.1
RETURN	V1.1
END	V1.1

	SUBROUTINE DOT(A,B,C,N,M,L)		V1.1
C		REV 03 05/31/73	V1.1
C	PERFORMS MATRIX MULTIPLICATION $C = A'B$ .		V1.1
C	IF A AND B ARE VECTORS, C IS THE DOT PRODUCT A.B		V1.1
C			V1.1
C	ARGUMENTS:		V1.1
C	A: MATRIX OF SIZE (L,N).		V1.1
C	B: MATRIX OF SIZE (L,M).		V1.1
C	C: PRODUCT MATRIX OF SIZE (N,M).		V1.1
C	N,M,L: SIZES OF MATRICES A,B,C.		V1.1
C			V1.1
C	(NOTE: SUBROUTINE ASSUMES THAT THE FIRST DIMENSION		V1.1
C	OF A,B AND C IN THE CALLING PROGRAM IS L,L AND N.)		V1.1
C			V1.1
	DIMENSION A(L,1),B(L,1),C(N,1)		V1.1
	DO 10 I=1,N		V1.1
	DO 10 J=1,M		V1.1
	C(I,J) = 0.0		V1.1
	DO 10 K=1,L		V1.1
10	C(I,J) = C(I,J) + A(K,I)*B(K,J)		V1.1
	RETURN		V1.1
	END		V1.1

	SUBROUTINE DOTT(A,B,C,N,M,L)		V1.1
C		REV 01 11/20/72	V1.1
C	PERFORMS MATRIX MULTIPLICATION $C = AB'$		V1.1
C	WHERE DIMENSIONS ARE A(N,L) , B(M,L) AND C(N,M).		V1.1
C			V1.1
	DIMENSION A(N,1),B(M,1),C(N,1)		V1.1
	DO 10 I=1,N		V1.1
	DO 10 J=1,M		V1.1
	C(I,J)=0.		V1.1
	DO 5 K=1,L		V1.1
	5 C(I,J)= A(I,K)*B(J,K)+C(I,J)		V1.1
10	CONTINUE		V1.1
	RETURN		V1.1
	END		V1.1

	SUBROUTINE DRCYPR (D,A,I1,I2,I3)		V1.1
C		REV 03 07/08/74	V1.1
C	SETS UP 3X3 DIRECTION COSINE MATRIX FOR GIVEN YAW,PITCH AND ROLL.		V1.1
C			V1.1
C	ARGUMENTS:		V1.1
C	D: 3X3 DIRECTION COSINE MATRIX TO BE COMPUTED.		V1.1
C	A: ARRAY OF LENGTH 3 CONTAINING ROTATION ANGLES (DEGREES).		V1.1
C	I1: AXIS OF ROTATION FOR 1ST ANGLE (1,2,3 = X,Y,Z)		V1.1
C	I2: AXIS OF ROTATION FOR 2ND ANGLE (1,2,3 = X,Y,Z)		V1.1
C	I3: AXIS OF ROTATION FOR 3RD ANGLE (1,2,3 = X,Y,Z)		V1.1
C			V1.1
	DIMENSION D(3,3),A(3),T(6,3)		V1.1
	RADIAN=.0174532925199433		V1.1
	Y = A(1)*RADIAN		V1.1
	P = A(2)*RADIAN		V1.1
	R = A(3)*RADIAN		V1.1
	M = 6		V1.1
	N = 3		V1.1
	DO 10 I=1,3		V1.1
	DO 5 J=1,3		V1.1
	D(I,J)=0.		V1.1
5	T(I,J)=0.		V1.1
	T(I,I)=1.		V1.1
10	D(I,I)=1.		V1.1
	IF(Y.EQ.0.)GO TO 20		V1.1
	CALL ROT(T,I1,Y,M)		V1.1
	DO 15 I=1,3		V1.1
	DO 15 J=1,3		V1.1
15	D(I,J)=T(I,J)		V1.1
20	IF(ABS(P).LT.1.E-11)GO TO 30		V1.2
	CALL ROT(T(4,1),I2,P,M)		V1.1
	CALL MAT(T(4,1),T(1,1),D(1,1),3,3,3,M,M,N)		V1.1
	DO 25 I=1,3		V1.1
	DO 25 J=1,3		V1.1
25	T(I,J)=D(I,J)		V1.1
30	IF(ABS(R).LT.1.E-11) GO TO 40		V1.2
	CALL ROT(T(4,1),I3,R,M)		V1.1
	CALL MAT(T(4,1),T(1,1),D(1,1),3,3,3,M,M,N)		V1.1
40	CONTINUE		V1.1
	RETURN		V1.1
	END		V1.1



	SUBROUTINE ELIPSN(INDEX,X1,IN)	V1.1
C	*****	V1.1
C		V1.1
C	THIS SUBROUTINE GENERATES 1/4 OF THE CONTOUR LINES FOR AN ELLIPSOID	V1.1
C		V1.1
C	*****	V1.1
	DIMENSION X1(3,INDEX,INDEX),IN(INDEX)	V1.1
	COMMON/ELLIPSE/NSTEPS(90),IELP,A(3,3,30),SEGLP(3,90),VP(3),	V1.1
	*D(3,3,90),DVP(3,3),RA(3),NSEG,SEGLPO(3,90)	V1.2
	DELTAX=SQRT(1/A(1,1,IELP))/NSTEPS(IELP)	V1.1
	DELTAY=SQRT(1/A(2,2,IELP))/NSTEPS(IELP)	V1.1
	SIMP1 = A(1,1,IELP)	V1.1
	SIMP2 = A(2,2,IELP)	V1.1
	SIMP3 = A(3,3,IELP)	V1.1
	DO 101 L=1,INDEX	V1.1
	X=(L-1)*DELTAX	V1.1
	N=0	V1.1
	DO 50 K=1,INDEX	V1.1
	Y=(K-1)*DELTAY	V1.1
	TEMP = 1-X*X*SIMP1	V1.1
	IF(TEMP.LT.0) TEMP=0	80386
	TEST = TEMP - Y*Y*SIMP2	V1.1
	N=N+1	V1.1
	IF(TEST.LT.0.0) GO TO 100	V1.1
	Z = SQRT(TEST/SIMP3)	V1.1
	X1(1,N,L)=X	V1.1
	X1(2,N,L)=Y	V1.1
	X1(3,N,L)=Z	V1.1
50	CONTINUE	V1.1
	GO TO 101	V1.1
100	Y = SQRT(TEMP/SIMP2)	V1.1
	X1(1,N,L)=X	V1.1
	X1(2,N,L)=Y	V1.1
	X1(3,N,L)=0.0	V1.1
101	IN(L)=N	V1.1
	RETURN	V1.1
	END	V1.1

	SUBROUTINE EXTEND(P,I,J)	V1.1
	COMMON/INTERS/ NIE(90),IE(90,90)	V1.1
	COMMON/ELLIPSE/NSTEPS(90),IELP,A(3,3,30),SEGLP(3,90),VP(3),	V1.1
	*D(3,3,90),DVP(3,3),RA(3),NSEG,SEGLPO(3,90)	V1.2
	DIMENSION P(3,2),P3(3)	V1.1
	COMMON/PLTT/SFACTR,INT,TIME,ICOLOR(91),OFSETX,OFSETY,ZTIME	V1.1
	DOUBLE PRECISION ZTIME	80386
C	*****	V1.1
C		V1.1
C	THIS SUBROUTINE FINDS A MIDPOINT FOR A LINE THAT	V1.1
C	BEGINS ON P(1) AND ENDS ON P(2).	V1.1
C	THIS NEW POINT IS CHECKED BY SUBROUTINE HYDE.	V1.1
C	IF IT IS HIDDEN THEN P(I)=P3	V1.1
C	IF IT IS NOT HIDDEN THEN P(J)=P3	V1.1
C	THIS ALGORITHM IS ITERATED INT TIMES.	V1.1
C	UPON LEAVING EXTEND- P(I) WILL CONTAIN THE RESULT.	V1.1
C		V1.1
C	NOTE: P ARRAY IS CHANGED BY THIS SUBROUTINE.	V1.1
C		V1.1
C	*****	V1.1
	DO 3 IN=1,INT	V1.1
	DO 1 L=1,3	V1.1
1	P3(L)=(P(L,2)+P(L,1))/2.0	V1.1
	NUM=NIE(IELP)	V1.1
	DO 2 IM=1,NUM	V1.1
	KK=IE(IM,IELP)	V1.1
	IF(KK.LE.30) CALL HYDE(KK,P3,IFLAG)	V1.1
	IF(KK.GT.30) CALL HIDE(KK,P3,IFLAG)	V1.1
	IF(IFLAG.EQ.1) GO TO 10	V1.1
2	CONTINUE	V1.1
10	N=I	V1.1
	IF(IFLAG.EQ.1) N=J	V1.1
	DO 3 L=1,3	V1.1
3	P(L,N)=P3(L)	V1.1
	RETURN	V1.1
	END	V1.1

	SUBROUTINE GENDCM(CAMERA, FOCUS, D, ICODE)	V1.2
C	*****	V1.1
C	THIS SUBROUTINE GENERATES A DIRECTION COSINE MATRIX.	V1.1
C		V1.1
	DIMENSION CAMERA(3), FOCUS(3), Z(3), D(3,3)	V1.1
	SUM = 0.0	V1.1
	SI=1.0	V1.2
	IF (FOCUS(1).NE.CAMERA(1).OR.FOCUS(2).NE.CAMERA(2)) GOTO 50	V1.2
	SI=SIGN(1., CAMERA(3)-FOCUS(3))	V1.2
	DO 40 I=1,3	V1.1
	DO 40 J=1,3	V1.1
	D(I,J)=0.0	V1.1
40	CONTINUE	V1.1
	D(1,1)=SI	V1.2
	D(2,2)=1.	V1.2
	D(3,3)=SI	V1.2
	GO TO 999	V1.1
50	IF (ICODE.LT.0) SI=-1.0	V1.2
C		V1.1
	DO 100 I=1,3	V1.1
	Z(I) = FOCUS(I) - CAMERA(I)	V1.1
100	SUM = SUM + Z(I)*Z(I)	V1.1
	SUM = SQRT(SUM)	V1.1
	DO 200 I=1,3	V1.1
200	Z(I) = Z(I)/SUM	V1.1
C		V1.1
	XNORM = SQRT(Z(1)*Z(1) + Z(2)*Z(2))	V1.1
C		V1.1
C	FILL IN FIRST ROW OF D	V1.1
C		V1.1
	D(1,1) = Z(2)/XNORM*SI	V1.2
	D(1,2) = -Z(1)/XNORM*SI	V1.2
	D(1,3) = 0.0	V1.1
C		V1.1
C	FILL IN SECOND ROW OF D	V1.1
C		V1.1
	D(2,1) = Z(1)*Z(3)/XNORM*SI	V1.2
	D(2,2) = Z(2)*Z(3)/XNORM*SI	V1.2
	D(2,3) = -XNORM*SI	V1.2
C		V1.1
C	FILL IN THIRD ROW OF D	V1.1
C		V1.1
	DO 300 I=1,3	V1.1
300	D(3,I) = Z(I)	V1.1
999	CONTINUE	V1.1
	RETURN	V1.1
	END	V1.1

	SUBROUTINE HIDE(KK,P3,IFLAG)	V1.1
	COMMON/POLYGON/NPLANE,KFLAG,NPPP(90),PO(3,4,60),P(3,4,60),	V1.1
	*CONVEC(2,4,90),POS(2,90),SIGN(90)	V1.1
	COMMON/ELLIPSE/NSTEPS(90),IELP,A(3,3,30),SEGLP(3,90),VP(3),	V1.1
	*D(3,3,90),DVP(3,3),RA(3),NSEG,SEGLPO(3,90)	V1.2
	DIMENSION P7(2),PP(3)	V1.1
	DIMENSION P3(3),P4(3)	V1.1
	REAL PPRIME(3),NPRIME(3)	V1.1
	CALL TRANS1(P3,P4)	V1.1
	P7(1)=P4(1)/P4(3)	V1.1
	P7(2)=P4(2)/P4(3)	V1.1
	CALL TPOINT(P7,KK,IFLAG)	V1.1
	IF(IFLAG.EQ.2) RETURN	V1.1
C		V1.1
C	POINT IS INSIDE POLYGON CHECK TO SEE	V1.1
C	IF POLYGON OR POINT IS CLOSER TO VIEWPOINT.	V1.1
C	CALCULATE TAU.	V1.1
C		V1.1
	DO 5 I=1,3	V1.1
	PPRIME(I)=D(1,I,KK)	V1.1
	IF (ABS(PPRIME(I)).LT.1.E-11) PPRIME(I)=.000001	V1.2
5	CONTINUE	V1.1
	CALL MAT(DVP,PPRIME,NPRIME,3,3,1,3,3,3)	V1.1
	DO 10 J=1,3	V1.1
10	PP(J)=P(J,1,KK-30)-VP(J)	V1.1
	CALL MAT(DVP,PP,PPRIME,3,3,1,3,3,3)	V1.1
	CALL DOT(NPRIME,PPRIME,P5,1,1,3)	V1.1
	CALL DOT(NPRIME,P4,P6,1,1,3)	V1.1
	IFLAG=2	V1.1
	IF(P5/P6.GE..99999999) RETURN	V1.1
	IFLAG=1	V1.1
	RETURN	V1.1
	END	V1.1

	SUBROUTINE HYDE(N,R,IFLAG)	V1.1
C		V1.1
C	*****	V1.1
C		V1.1
C	SUBROUTINE HYDE DETERMINES IF A POINT IS HIDDEN BY	V1.1
C	ANOTHER ELLIPSOID.	V1.1
C		V1.1
C	*****	V1.1
C	*****	V1.1
C	N= POSSIBLE HIDING ELLIPSOID NUMBER.	V1.1
C	R= VECTOR TO PLOTTING POINT.	V1.1
C	IFLAG= FLAG THAT INDICATES HIDDEN LINE OR NOT.	V1.1
C	IFLAG = 2 = NOT HIDDEN	V1.1
C	IFLAG = 1 = HIDDEN	V1.1
C	*****	V1.1
	COMMON/ELLIPSE/NSTEPS(90), IELP, AA(3,3,30), SEGLP(3,90), VP(3),	V1.1
	*D(3,3,90), DVP(3,3), RA(3), NSEG, SEGLPO(3,90)	V1.2
	DIMENSION P1(3), P2(3), R2(3), S(3), V(3)	V1.1
	DIMENSION MU(3), M(3,2), P(3), SON(3), SOI(3)	V1.2
	DIMENSION DD(3,3), VP1(3)	V1.1
	DIMENSION R(3)	V1.1
	REAL M, MU, MAG	V1.1
C	ASSUME NOT HIDDEN.	V1.1
	IFLAG=2	V1.1
C		V1.1
C	*****	V1.1
C		V1.1
C	PUT SEGLP(N) IN N'S FRAME.	V1.1
C	PUT SEGLP(M) IN N'S FRAME.	V1.1
C	PUT R2 IN N'S FRAME.	V1.1
C	PUT VIEW POINT IN N'S FRAME.	V1.1
C		V1.1
C	*****	V1.1
	DO 4 I=1,3	V1.2
	SON(I) = SEGLP(I,N) + SEGLPO(I,N)	V1.2
4	SOI(I) = SEGLP(I,IELP) + SEGLPO(I,IELP)	V1.2
	CALL MAT(D(1,1,N),SON,P1,3,3,1,3,3,3)	V1.2
	CALL MAT(D(1,1,N),SOI,P2,3,3,1,3,3,3)	V1.2
	IF(IELP .LE. 30) GO TO 55	V1.1
	DO 56 I=1,3	V1.1
	DO 56 J=1,3	V1.1
56	DD(I,J) = D(I,J,N)	V1.1
	GO TO 57	V1.1
55	CONTINUE	V1.1
	CALL DOTT(D(1,1,N),D(1,1,IELP),DD,3,3,3)	V1.1
57	CONTINUE	V1.1
	CALL MAT(DD,R,R2,3,3,1,3,3,3)	V1.1
	CALL MAT(D(1,1,N),VP,VP1,3,3,1,3,3,3)	V1.1
	MAG = 0.0	V1.1
C		V1.1
C	** *****	V1.1
C		V1.1

C	FIND VECTORS S,V,AND MU.	V1.1
C	MU WILL BECOME A UNIT VECTOR IN VECTOR M'S DIRECTION	V1.1
C	OR IN M'S OPPOSITE DIRECTION.	V1.1
C		V1.1
C	*****	V1.1
C		V1.1
	DO 1 I=1,3	V1.1
	S(I) = P2(I) + R2(I) - P1(I)	V1.1
	V(I) = VP1(I) - P1(I)	V1.1
	MU(I) = S(I) - V(I)	V1.1
	1 MAG = MAG + MU(I)**2	V1.1
	MAG = SQRT(MAG)	V1.1
C		V1.1
C	*****	V1.1
C		V1.1
C	MAKE MU A UNIT VECTOR.	V1.1
C		V1.1
C	*****	V1.1
C		V1.1
	DO 2 I=1,3	V1.1
	2 MU(I) = MU(I) / MAG	V1.1
	A = AA(1,1,N)	V1.1
	B = AA(2,2,N)	V1.1
	C = AA(3,3,N)	V1.1
	IF(ABS(MU(1)).GT..000000001) GO TO 10	V1.1
	IF(ABS(MU(2)).GT..000000001) GO TO 20	V1.1
	CALL Z(MU,A,B,C,S,M,JFLAG)	V1.1
	30 IF(JFLAG.EQ.1) RETURN	V1.1
C		V1.1
C	*****	V1.1
C		V1.1
C	FIND P AND COMPARE M TO P TO DETERMINE WHAT POINT	V1.1
C	IS CLOSER TO THE VIEW POINT.	V1.1
C		V1.1
C	*****	V1.1
C		V1.1
	DO 3 I=1,3	V1.1
	3 P(I)= S(I) - V(I) - M(I,1)	V1.1
	CALL DOT(P,M(1,1),RESLT1,1,1,3)	V1.1
	CALL DOT(P,M(1,2),RESLT2,1,1,3)	V1.1
	IF(N.EQ.IELP) GO TO 400	V1.1
	IF(RESLT1.GT.0.000000001) IFLAG=1	V1.1
	41 IF(RESLT2.GT.0.000000001) IFLAG=1	V1.1
	RETURN	V1.1
	10 CALL XYZ(MU,A,B,C,S,M,JFLAG)	V1.1
	GO TO 30	V1.1
	20 CALL YZ(MU,A,B,C,S,M,JFLAG)	V1.1
	GO TO 30	V1.1
	400 IF(ABS(RESLT2).GT.ABS(RESLT1)) GO TO 41	V1.1
	RESLT2=RESLT1	V1.1
	GO TO 41	V1.1
	RETURN	V1.1

END

V1.1

	SUBROUTINE INPUT(CTIME)	V1.1
	COMMON/PLTT/SFACTR,INT,TIME,ICOLOR(91),OFSETX,OFSETY,ZTIME	V1.1
	COMMON/INTERS/ NIE(90),IE(90,90)	V1.1
	COMMON/ELLIPSE/NSTEPS(90),IELP,A(3,3,30),SEGLP(3,90),VP(3),	V1.1
	*D(3,3,90),DVP(3,3),RA(3),NSEG,SEGLPO(3,90)	V1.2
	COMMON/POLYGON/NPLANE,IFLAG,NPPP(90),PO(3,4,60),P(3,4,60),	V1.1
	*CONVEC(2,4,90),POS(2,90),SIGN(90)	V1.1
	COMMON/ATB/PL(17,30)	V1.1
	DIMENSION BD(24,40)	V1.1
	DIMENSION DD(3)	V1.1
	COMMON/DEBUG/IDEBUG(80),NISG,DEVFLG,ONLINE,TERM,BDRS,OFFLINE	V1.1
	COMMON/VIEWP/VP0(3),DVPO(3,3),IVP,VP2(3)	V1.1
	COMMON/CONECT/ NP,MPL(3,5,60)	V1.1
	COMMON /REMOVE/NPREM,IREMOV(30)	V1.1
	DOUBLE PRECISION CTIME,ZTIME	V1.1
	INTEGER DEVFLG,ONLINE,TERM,BDRS,OFFLINE	80386
	IF(IFLAG.NE.1) GO TO 600	V1.1
	READ(5,70) NFAST,NPREM,NISG	V1.1
	WRITE(6,70) NFAST,NPREM,NISG	V1.1
	READ(5,72)(IREMOV(I),I=1,NPREM)	V1.1
	WRITE(6,72)(IREMOV(I),I=1,NPREM)	V1.1
72	FORMAT(3(40I2/))	V1.1
	READ(1,END=800) NSEG,NP,PL,BD, (((MPL(I,J,K),I=1,3), J=1,5),K	V1
	*=1,30)	V1.1
C		V1.1
39	READ(1,END=700) TIME, ((SEGLP(I,J), I=1,3), J=1,30),	V1.1
	* ((D(I,J,K), I=1,3), J=1,3), K=1,30)	V1.1
	ITIME=TIME*1000000.+5	V1.1
	ZTIME=ITIME/1000000.DO	V1.1
C		V1.1
70	FORMAT(3I2)	V1.1
	IF(ZTIME.LT.CTIME) GO TO 39	V1.1
	READ(5,40) NSP	V1.1
40	FORMAT(I2)	V1.1
	IF(NSP.EQ.0) GO TO 46	V1.1
	DO 45 L=1,NSP	V1.1
	K=NP+L	V1.1
	II=30+NP+L	V1.1
	READ(5,41) NPPP(II),MPL(1,1,K)	V1.1
41	FORMAT(I1,I2)	V1.1
	NSIDES=NPPP(II)	V1.1
	DO 45 J=1,NSIDES	V1.1
	READ(5,42) (PO(I,J,K),I=1,3)	V1.1
42	FORMAT(3F10.0)	V1.1
45	CONTINUE	V1.1
46	NPLANE=NP+NSP	V1.1
	DO 100 J=1,NSEG	V1.1
	DO 100 I=1,3	V1.1
100	A(I,I,J)=1.0/BD(I,J)**2	V1.1
	DO 200 J=1,NSEG	V1.1
	CALL DOT(D(1,1,J),BD(4,J),DD,3,1,3)	V1.1
	DO 200 I=1,3	V1.1



200	SEGLPO(I,J)= DD(I)	V1.2
	IF(IDEBUG(3).EQ.1) WRITE(6,6) NSEG,NPLANE	V1.1
6	FORMAT(1H1,'NUMBER OF SEGMENTS = ',I2,', NUMBER OF PLANES = ',I2)	V1.1
	NSEG = NSEG-NFAST	V1.1
	READ(5,301) (ICOLOR(I),I=1,30)	V1.1
301	FORMAT(8(5X,I5))	V1.1
	II=NPLANE+30	V1.1
	READ(5,301) (ICOLOR(I),I=31,90)	V1.1
	READ(5,301) ICOLOR(91)	V1.1
	IF(IDEBUG(3).EQ.1) WRITE(6,71) NSEG	V1.1
71	FORMAT(1X,'THE NUMBER OF SEGMENTS TO BE PLOTTED = ',I2)	V1.1
	READ(5,1) (NSTEPS(IPP),IPP=1,NSEG)	V1.1
	READ(5,1) (NSTEPS(IPP+30),IPP=1,NPLANE)	V1.1
1	FORMAT(30I2)	V1.1
	IF(IDEBUG(3).EQ.1) WRITE(6,2) (NSTEPS(IPP),IPP=1,NSEG)	V1.1
2	FORMAT(10X,'NUMBER OF DIVISIONS ALONG A RADIUS',/2X,30I3)	V1.1
	IF(IDEBUG(3).EQ.1) WRITE(6,55) (NSTEPS(IPP+30),IPP=1,NPLANE)	V1.1
55	FORMAT(10X,'NUMBER OF DIVISIONS ALONG A SIDE ',/2X,30I3)	V1.1
	READ(5,11) INT,SFACTR	V1.1
11	FORMAT(I3,7X,F10.2)	V1.1
	WRITE(6,11) INT,SFACTR	V1.1
	READ(5,901) OFSETX,OFSETY	V1.1
	WRITE(6,901) OFSETX,OFSETY	V1.1
901	FORMAT(2F10.0)	V1.1
	IF(IDEBUG(3).EQ.1) WRITE(6,902) OFSETX,OFSETY	V1.1
902	FORMAT(1X,'OFSETX= ',F10.3,4X,'OFSETY= ',F10.3)	V1.1
	IF(IDEBUG(3).EQ.1) WRITE(6,12) SFACTR,INT	V1.1
12	FORMAT(1X,'SCALE FACTOR = ',F10.2,2X,' ITERATION NUMBER = ',I3)	V1.1
	READ(5,13) VP,RA,IVP,ICODE	V1.1
13	FORMAT(6F10.0,2I10)	V1.1
C		V1.1
C	ICODE = 0 : ROLL, PITCH, AND YAW ANGLES ARE SUPPLIED IN RA ARRAY.	V1.1
C		V1.1
C	ICODE = 1 : DIRECTION COSINE MATRIX SUPPLIED AS INPUT.RA ARRAY IS 1ST	V1.1
C	ROW OF MATRIX.THE NEXT CARD CONTAINS THE 2ND AND 3RD ROWS	V1.1
C		V1.1
C	ICODE = 2 : POINT AT WHICH VIEWPOINT Z-AXIS IS TO AIM IS SUPPLIED	V1.1
C	IN RA ARRAY.	V1.1
C		V1.1
C	ICODE --2 : SAME AS ICODE=2, EXCEPT THE POSITIVE Z-AXIS IN THE ATB	V1.2
C	SIMULATION IS UP.	V1.2
C		V1.1
	IF(ICODE .NE. 0) GO TO 500	V1.1
	IF(IDEBUG(3).EQ.1) WRITE(6,4) VP,RA	V1.1
4	FORMAT(1X,'VIEWPOINT VECTOR (',F10.1,',',F10.1,',',F10.1,')'/1X	V1.1
	1'ROTATION OF VIEWPOINT RELATIVE TO INERTIAL COORDINATE SYSTEM'/1X	V1.1
	2'THESE ROTATIONS MUST BE DETERMINED BY PERFORMING ROLL MOTION FIRS	V1.1
	3T'/1X'THEN A PITCH MOTION AND THEN THE YAW MOTION'/10X	V1.1
	4'ROLL = ',F10.1,1X,'DEG.',5X,'PITCH = ',F10.1,1X,'DEG.',	V1.1
	55X,'YAW = ',F10.1,1X,'DEG.')	V1.1
	CALL DRCYPR(DVP,RA,1,2,3)	V1.1
	GO TO 550	V1.1

500	IF (IABS(ICODE).EQ.2) CALL GENDCM(VP,RA,DVP,ICODE)	V1.2
	IF (IABS(ICODE).EQ.2) GO TO 550	V1.2
	DO 501 JJJ=1,3	V1.1
501	DVP(1,JJJ) = RA(JJJ)	V1.1
	READ(5,13) ((DVP(I,J),J=1,3),I=2,3)	V1.1
	WRITE(6,13)((DVP(I,J),J=1,3),I=2,3)	V1.1
	IF(IDEBUG(3).EQ.1) WRITE(6,15) (VP(I),I=1,3)	V1.1
15	FORMAT(' VIEW POINT VECTOR (' ,F10.1,' ' ,F10.1,' ' ,F10.1,') .',/,	V1.1
	- ' VIEW POINT ORIENTATION DEFINED IN DIRECTION COSINE MATRIX FORM	V1.1
	- .')	V1.1
550	CONTINUE	V1.1
	DO 80 J=1,3	V1.1
	VPO(J)=VP(J)	V1.1
	DO 80 I=1,3	V1.1
80	DVPO(J,I)=DVP(J,I)	V1.1
	IF(IFLAG.NE.1) RETURN	V1.1
	IF(IDEBUG(3).EQ.1) WRITE(6,60)	V1.1
60	FORMAT(1X,'*****'/,1X,	V1.1
	1'VIEWPOINT DIRECTION COSINE MATRIX')	V1.1
	IF(IDEBUG(3).EQ.1) WRITE(6,53)((DVP(I,J),J=1,3),I=1,3)	V1.1
	IF(IDEBUG(3).EQ.1) WRITE(6,54)	V1.1
	DO 20 IKE=1,NSEG	V1.1
	IF(IDEBUG(3).EQ.1) WRITE(6,50) IKE,(SEGLP(I,IKE),I=1,3)	V1.1
50	FORMAT(1X,'*****'/1X'SEGMENT # ',I3,5X,'SEGLP = ('	V1.1
	-F10.3,2(' ,F10.3),',',/,1X,'A MATRIX',T50,'DIRECTION COSINE MATRIX	V1.1
	- ')/)	V1.1
	DO 400 III=1,3	V1.1
	IF(IDEBUG(3).EQ.1) WRITE(6,51) (A(III,J,IKE),J=1,3),(D(III,J,IKE),	V1.1
	+J=1,3)	V1.1
400	CONTINUE	V1.1
	1 FORMAT(3(2X,F8.5),T50,3(2X,F9.6))	V1.1
53	FORMAT(3(2X,F9.6))	V1.1
	IF(IDEBUG(3).EQ.1) WRITE(6,54)	V1.1
54	FORMAT(1X,/,1X'*****')	V1.1
20	CONTINUE	V1.1
	RETURN	V1.1
600	CONTINUE	V1.1
	IF(ZTIME.LT.CTIME) GO TO 675	V1.1
	IF(ISW1.EQ.0) GO TO 680	V1.1
	DO 650 J=1,NSEG	V1.1
	CALL DOT(D(1,1,J),BD(4,J),DD,3,1,3)	V1.1
	DO 650 I=1,3	V1.1
650	SEGLPO(I,J)= DD(I)	V1.2
	ISW1=0	V1.1
	IFLAG=5	V1.1
	RETURN	V1.1
675	READ(1,END=700) TIME,((SEGLP(I,J),I=1,3),J=1,30),	V1.1
	* (((D(I,J,K), I=1,3), J=1,3), K=1,30)	V1.1
	ITIME=TIME*1000000.+5	V1.1
	ZTIME=ITIME/1000000.DO	V1.1
C		V1.1
	ISW1=1	V1.1

GO TO 600	V1.1
700 WRITE(6,720)	V1.1
720 FORMAT(1X,'END OF DATA REACHED.')	V1.1
ISW1=1	V1.1
STOP	V1.1
800 WRITE(6,820)	V1.1
820 FORMAT(1X,'NO DATA ON TAPE.')	V1.1
STOP	V1.1
680 IFLAG=10	V1.1
RETURN	V1.1
END	V1.1

SUBROUTINE LSEGINT(P1,P2,R1,R2,IFLAG)	V1.1
C	V1.1
C THIS SUBROUTINE DETERMINES IF TWO LINE SEGMENTS, P1P2 AND R1R2,	V1.1
C INTERSECT.	V1.1
C ALL PARALLEL LINE SEGMENTS,WHETHER COINCIDENT OR NOT, ARE	V1.1
C CONSIDERED TO BE NON-INTERSECTING.	V1.1
C CASE 1 IS CONSIDERED TO BE THE REGULAR CONFIGURATION.	V1.1
C THE SPECIAL CASES ARE AS FOLLOWS:	V1.1
C 2) ONE LINE IS VERTICAL	V1.1
C 3) BOTH LINES ARE VERTICAL	V1.1
C 4) BOTH LINES ARE HORIZONTAL	V1.1
C 5) BOTH LINES HAVE THE SAME NON-ZERO SLOPE	V1.1
C 6) ONE LINE IS VERTICAL, THE OTHER IS HORIZONTAL	V1.1
C	V1.1
C	V1.1
C IFLAG = 1 INDICATES INTERSECTION; IFLAG = 0 INDICATES NO INTERSECTION.	V1.1
C	V1.1
DIMENSION P1(2),P2(2),R1(2),R2(2),P(4,2),T(2)	V1.1
REAL M(2)	V1.1
IFLAG=0	V1.1
C	V1.1
C SET UP ARRAYS	V1.1
DO 1 I=1,2	V1.1
P(1,I) = P1(I)	V1.1
P(2,I) = P2(I)	V1.1
P(3,I) = R1(I)	V1.1
1 P(4,I) = R2(I)	V1.1
C	V1.1
C DETERMINE IF CASE 3	V1.1
IF(ABS(P(1,1)-P(2,1)).LT.1.E-11.AND.ABS(P(3,1)-P(4,1)).LT.	V1.1
+1.E-11) RETURN	V1.1
C	V1.1
C DETERMINE IF CASE 4	V1.1
IF(ABS(P(1,2)-P(2,2)).LT.1.E-11.AND.ABS(P(3,2)-P(4,2)).LT.	V1.1
+1.E-11) RETURN	V1.1
C	V1.1
C DETERMINE IF CASE 6	V1.1
DO 2 I=1,2	V1.1
J = 3-I	V1.1
IF(ABS(P(1,I)-P(2,I)).LT.1.E-11.AND.ABS(P(3,J)-P(4,J)).LT.	V1.1
+1.E-11) GO TO 10	V1.1
2 CONTINUE	V1.1
C	V1.1
C DETERMINE IF CASE 2	V1.1
IF(ABS(P(1,1)-P(2,1)).LT.1.E-11.OR.ABS(P(3,1)-P(4,1)).LT.	V1.1
+1.E-11) GO TO 6	V1.1
GO TO 5	V1.1
6 DO 3 I=1,4	V1.1
TEMP = P(I,1)	V1.1
P(I,1) = P(I,2)	V1.1
3 P(I,2) = TEMP	V1.1
C	V1.1

C	REGULAR PROCEDURE	V1.1
	5 DO 4 I=1,2	V1.1
	I1 = 2*I	V1.1
	I2 = 2*I - 1	V1.1
	4 M(I) = (P(I1,2) - P(I2,2))/(P(I1,1) - P(I2,1))	V1.1
C		V1.1
C	CHECK FOR CASE 5	V1.1
	IF(ABS(M(1)-M(2)).LT.1.E-11) RETURN	V1.1
	X = (P(3,2) - P(1,2) + M(1)*P(1,1) - M(2)*P(3,1))/(M(1) - M(2))	V1.1
	DO 7 I=1,2	V1.1
	7 T(I) = (X - P(2*I-1,1))/(P(2*I,1) - P(2*I-1,1))	V1.1
	20 IF(T(1).GT.0 .AND. T(2).GT.0 .AND. T(1).LT.1 .AND. T(2).LT.1)	V1.1
	- IFLAG=1	V1.1
	RETURN	V1.1
C		V1.1
C	CASE 6 PROCEDURE	V1.1
	10 IF(ABS(P(1,1)-P(2,1)).LT.1.E-11) GO TO 11	V1.1
	J=1	V1.1
	I=2	V1.1
	GO TO 12	V1.1
	11 I=1	V1.1
	J=2	V1.1
	12 T(1) = (P(3,J) - P(1,J))/(P(2,J) - P(1,J))	V1.1
	T(2) = (P(1,I) - P(3,I))/(P(4,I) - P(3,I))	V1.1
	GO TO 20	V1.1
	END	V1.1

	SUBROUTINE MAT(A,B,C,LL,MM,NN,JA,JB,JC)		V1.1
C		REV 03 05/31/73	V1.1
C	PERFORMS MATRIX MULTIPLICATION C = AB.		V1.1
C			V1.1
C	ARGUMENTS:		V1.1
C	A: MATRIX OF SIZE (L,M).		V1.1
C	B: MATRIX OF SIZE (M,N).		V1.1
C	C: PRODUCT MATRIX OF SIZE (L,N).		V1.1
C	L,M,N: SIZES OF MATRICES A,B,C.		V1.1
C	LA, LB, LC: 1ST DIMENSION OF A,B,C IN CALLING PROGRAM.		V1.1
C			V1.1
	DIMENSION A(JA,1),B(JB,1),C(JC,1)		V1.1
	DO 20 L=1,LL		V1.1
	DO 10 N=1,NN		V1.1
	S = 0.0		V1.1
	DO 5 M=1,MM		V1.1
	5 S=S+A(L,M)*B(M,N)		V1.1
	C(L,N)=S		V1.1
10	CONTINUE		V1.1
20	CONTINUE		V1.1
	RETURN		V1.1
	END		V1.1

	SUBROUTINE NFRAME	V1.1
C		V1.1
C	THIS ROUTINE PERFORMS THE END OF FRAME HANDLING FOR THE BDRS	V1.1
C		V1.1
	COMMON/DEVICE/IDEF, IOPORT, MODEL	80386
	INTEGER*2 ENDFRA, MASK, STATUS	V1.1
	DATA ENDFRA, MASK/Z'FFFF', Z'FFFF' /	80386
C	CALL DOLWH(8, 1, ENDFRA, MASK, STATUS)	80386
C	CALL PLOTS(M, N, LU)	80386
	CALL PLOT(0.0, 0.0, -999)	80386
	RETURN	V1.1
	END	V1.1

	SUBROUTINE OVERLAP(III, KKK, MFLAG)	V1.1
	DIMENSION P1(2), P2(2), R1(2), R2(2)	V1.1
	DIMENSION PP2(2)	V1.1
	COMMON/POLYGON/NPLANE, IFLAG, NPPP(90), PO(3,4,60), P(3,4,60),	V1.1
	*CONVEC(2,4,90), POS(2,90), SIGN(90)	V1.1
C		V1.1
C	OVERLAP TAKES OBJECTS I AND K AND TESTS FOR ANY OVERLAP ON THE	V1.1
C	PROJECTION PLANE.	V1.1
C	MFLAG WILL BE RETURNED TO INDICATE IF OVERLAP OR NOT.	V1.1
C	MFLAG=0 MEANS NO OVERLAP	V1.1
C	MFLAG=1 MEANS OVERLAP	V1.1
C		V1.1
	I = III	V1.1
	K = KKK	V1.1
	5 CONTINUE	V1.1
	DO 10 J=1,2	V1.1
	10 PP2(J) = POS(J,K)	V1.1
C		V1.1
C	GO AROUND THE RINGS	V1.1
C		V1.1
	NPTS1 = NPPP(I)	V1.1
	NPTS2 = NPPP(K)	V1.1
	DO 200 J=1, NPTS2	V1.1
	CALL TPOINT(PP2, I, MFLAG)	V1.1
	IF(MFLAG.EQ.1) RETURN	V1.1
	DO 200 N=1,2	V1.1
	200 PP2(N) = PP2(N) + CONVEC(N,J,K)	V1.1
C		V1.1
C	CHECKED ALL POINTS AND FOUND THEY WERE ALL OUTSIDE.	V1.1
C		V1.1
C	NEXT, CHECK FOR INTERSECTING LINE SEGMENTS.	V1.1
C		V1.1
	DO 60 II=1,2	V1.1
	P1(II) = POS(II,I)	V1.1
	60 R1(II) = POS(II,K)	V1.1
	DO 61 L=1, NPTS1	V1.1
	DO 62 II=1,2	V1.1
	62 P2(II) = P1(II) + CONVEC(II,L,I)	V1.1
	DO 63 J=1, NPTS2	V1.1
	DO 64 II=1,2	V1.1
	64 R2(II) = R1(II) + CONVEC(II,J,K)	V1.1
	CALL LSEGINT(P1, P2, R1, R2, MFLAG)	V1.1
	IF(MFLAG.EQ. 1) RETURN	V1.1
	R1(1) = R2(1)	V1.1
	63 R1(2) = R2(2)	V1.1
	P1(1) = P2(1)	V1.1
	61 P1(2) = P2(2)	V1.1
	IF(I.NE. III) RETURN	V1.1
	I = KKK	V1.1
	K = III	V1.1
	GO TO 5	V1.1
	END	V1.1



	SUBROUTINE PLPLN(SEG, INDEX2)	V1.1
C	*****	V1.1
C		V1.1
C	THIS SUBROUTINE PLOTS THE PLANES.	V1.1
C		V1.1
C	*****	V1.1
	COMMON/ELLIPSE/NSTEPS(90), IELP, AA(3,3,30), SEGLP(3,90), VP(3),	V1.1
	*D(3,3,90), DVP(3,3), RA(3), NSEG, SEGLPO(3,90)	V1.2
	COMMON/POLYGON/NPLANE, IFLAG, NPPP(90), PO(3,4,60), P(3,4,60),	V1.1
	*CONVEC(2,4,90), POS(2,90), SIGN(90)	V1.1
	COMMON/DEBUG/IDEBUG(80), NISG, DEVFLG, ONLINE, TERM, BDRS, OFFLINE	V1.1
	DIMENSION SEG(3,3333)	V1.1
	INTEGER DEVFLG, ONLINE, TERM, BDRS, OFFLINE	V1.1
	COMMON/PLTT/SFACTR, INT, TIME, ICOLOR(91), OFSETX, OFSETY, ZTIME	V1.1
	COMMON /REMOVE/NPREM, IREMOV(30)	V1.1
	DOUBLE PRECISION ZTIME	80386
	IF(NPLANE .EQ. 0) RETURN	V1.1
	SEG(1,1) = 0.0	V1.1
	SEG(2,1) = 0.0	V1.1
	SEG(3,1) = 0.0	V1.1
	DO 500 LL=1, NPLANE	V1.1
	DO 100 I=1, NPREM	V1.1
	IF (LL.EQ.IREMOV(I)) GO TO 500	V1.1
100	CONTINUE	V1.1
	L = LL + 30	V1.1
	IF(DEVFLG.EQ.OFFLINE.OR.DEVFLG.EQ.BDRS) CALL COLOR(ICOLOR(L), IERR) 80386	
	NUM = NPPP(L)*NSTEPS(L) + 1	V1.1
	A = 1./NSTEPS(L)	V1.1
	NSIDES = NPPP(L)	V1.1
	DO 400 K=1, NSIDES	V1.1
	KK = K + 1	V1.1
	IF(K .EQ. NSIDES) KK=1	V1.1
	I1 = (K-1)*NSTEPS(L) + 2	V1.1
	I2 = I1 + NSTEPS(L) - 1	V1.1
	DO 400 I=I1, I2	V1.1
	DO 400 J=1, 3	V1.1
400	SEG(J, I) = SEG(J, I-1) + A*(P(J, KK, LL) - P(J, K, LL))	V1.1
	IPEN = 3	V1.1
	IELP = L	V1.1
	CALL PNTPLT(SEG(1,1), IPEN, INDEX2, NUM)	V1.1
500	CONTINUE	V1.1
	RETURN	V1.1
	END	V1.1

	SUBROUTINE PNTPLT(SEG, IPEN, INDEX2, NPTS)	V1.1
C	*****	V1.1
C		V1.1
C	POINT PLOT SUBROUTINE.	V1.1
C		V1.1
C	*****	V1.1
	COMMON/PLTT/SFACTR, INT, TIME, ICOLOR(91), OFSETX, OFSETY, ZTIME	V1.1
	COMMON/ELLIPSE/NSTEPS(90), IELP, A(3,3,30), SEGLP(3,90), VP(3),	V1.1
	*D(3,3,90), DVP(3,3), RA(3), NSEG, SEGLPO(3,90)	V1.2
	COMMON/INTERS/ NIE(90), IE(90,90)	V1.1
	DOUBLE PRECISION ZTIME	80386
	DIMENSION P(3), PP(3,2), PPP(3)	V1.1
	DIMENSION SEG(3,3333)	V1.1
	DATA YMIN/0.0/, YMAX/11.0/, IPLOT/1/	V1.1
	DATA IFIRST/0/	V1.1
	DATA ITWO/2/, ITHREE/3/	V1.1
	IF (IFIRST.EQ.0) READ(5,1000)XMIN,XMAX	V1.1
1000	FORMAT(2F10.2)	V1.1
	IF (IFIRST.EQ.0) WRITE(6,1001)XMIN,XMAX	V1.1
1001	FORMAT(' XMIN,XMAX=', 2(1X,F10.3))	V1.1
	IFIRST=1	V1.1
	LFLAG=2	V1.1
	IFLAG=2	V1.1
	NEWPEN=0	V1.1
	DO 100 IPNT=1,NPTS	V1.1
	INUM=NIE(IELP)	V1.1
	IF(INUM.EQ.0) GO TO 61	V1.1
	DO 60 K=1, INUM	V1.1
	KK=IE(K, IELP)	V1.1
	IF(KK.LE.30) CALL HYDE(KK, SEG(1, IPNT), IFLAG)	V1.1
	IF(KK.GT.30) CALL HIDE(KK, SEG(1, IPNT), IFLAG)	V1.1
	IF(IFLAG.EQ.1) GO TO 61	V1.1
60	CONTINUE	V1.1
61	IF(K.GT.INUM .OR. K.EQ.1) GO TO 62	V1.1
	ITEMP = IE(1, IELP)	V1.1
	IE(1, IELP) = IE(K, IELP)	V1.1
	IE(K, IELP) = ITEMP	V1.1
62	IF(IFLAG.NE. LFLAG) THEN	80386
	IF(IPNT.EQ.1) GO TO 70	80386
	DO 250 IJ=1,3	80386
	PP(IJ,1)=SEG(IJ, IPNT-1)	80386
250	PP(IJ,2)=SEG(IJ, IPNT)	80386
	CALL EXTEND(PP, IFLAG, LFLAG)	80386
	DO 260 IJ=1,3	80386
260	P(IJ)=PP(IJ, IFLAG)	80386
	CALL TRANS1(P, PPP)	80386
	X=-PPP(1)*SFACTR/PPP(3)+OFSETX	80386
	Y=PPP(2)*SFACTR/PPP(3)+OFSETY	80386
	IF(LFLAG.EQ.1) GO TO 350	80386
	IF (X.GE.XMIN.AND.X.LE.XMAX.AND.	80386
1	Y.GE.YMIN.AND.Y.LE.YMAX) GO TO 261	80386
	CALL CLIP(X, Y, XSAV, YSAV, XMIN, XMAX, YMIN, YMAX, ITWO, IPLOT)	80386

	NEWPEN=-3	80386
	GO TO 265	80386
261	CONTINUE	80386
	IF (IPNT.NE.1)	80386
1	CALL PREPLT(X,Y,XSAV,YSAV,XMIN,XMAX,YMIN,YMAX,IPEN,NEWPEN)	80386
	CALL PLOT(X,Y,2)	80386
	IPLOT=1	80386
	NEWPEN=3	80386
265	CONTINUE	80386
	IPEN=3	80386
	XSAV=X	80386
	YSAV=Y	80386
	LFLAG=1	80386
	GO TO 100	80386
350	CONTINUE	80386
	IF (X.GE.XMIN.AND.X.LE.XMAX.AND.	80386
1	Y.GE.YMIN.AND.Y.LE.YMAX) GO TO 351	80386
	CALL CLIP(X,Y,XSAV,YSAV,XMIN,XMAX,YMIN,YMAX,ITHREE,IPLOT)	80386
	NEWPEN=-2	80386
	IPEN=3	80386
	GO TO 355	80386
351	CONTINUE	80386
	IF (IPNT.NE.1)	80386
1	CALL PREPLT(X,Y,XSAV,YSAV,XMIN,XMAX,YMIN,YMAX,IPEN,NEWPEN)	80386
	CALL PLOT(X,Y,3)	80386
	IPLOT=1	80386
	NEWPEN=2	80386
	IPEN=2	80386
355	CONTINUE	80386
	XSAV=X	80386
	YSAV=Y	80386
	ENDIF	80386
70	IF (LFLAG.EQ.1) THEN	80386
	IPEN=3	80386
	LFLAG=1	80386
	GO TO 100	80386
	ENDIF	80386
	LFLAG=2	V1.1
	CALL TRANS1(SEG(1,IPNT),PPP)	V1.1
	X=-PPP(1)*SFACTR/PPP(3)+OFSETX	V1.1
	Y=PPP(2)*SFACTR/PPP(3)+OFSETY	V1.1
	IF (X.GE.XMIN.AND.X.LE.XMAX.AND.	V1.1
1	Y.GE.YMIN.AND.Y.LE.YMAX) GO TO 71	V1.1
	CALL CLIP(X,Y,XSAV,YSAV,XMIN,XMAX,YMIN,YMAX,IPEN,IPLOT)	V1.1
	NEWPEN=-2	V1.1
	IPEN=3	V1.1
	GO TO 75	V1.1
71	CONTINUE	V1.1
	IF (IPNT.NE.1)	V1.1
1	CALL PREPLT(X,Y,XSAV,YSAV,XMIN,XMAX,YMIN,YMAX,IPEN,NEWPEN)	V1.1
	CALL PLOT(X,Y,IPEN)	V1.1
	IPLOT=1	V1.1

	NEWPEN=2	V1.1
	IPEN=2	V1.1
75	CONTINUE	V1.1
	XSAV=X	V1.1
	YSAV=Y	V1.1
100	CONTINUE	V1.1
	RETURN	V1.1
	END	V1.1

	SUBROUTINE POLYD	V1.1
C		V1.1
C	POLYD GENERATES DIRECTION COSINE MATRICIES FOR THE POLYGONS.	V1.1
C	THE X AXIS OF THE POLYGON COORDINATE SYSTEM IS THE	V1.1
C	NORMAL VECTOR TO THE POLYGON SURFACE.	V1.1
C	Y VECTOR IS ALIGNED WITH ONE OF THE POLYGON SIDES.	V1.1
C		V1.1
	COMMON/ELLIPSE/NSTEPS(90),IELP,A(3,3,30),SEGLP(3,90),VP(3),	V1.1
	*D(3,3,90),DVP(3,3),RA(3),NSEG,SEGLPO(3,90)	V1.2
	COMMON/POLYGON/NPLANE,IFLAG,NPPP(90),PO(3,4,60),P(3,4,60),	V1.1
	*CONVEC(2,4,90),POS(2,90),SIGN(90)	V1.1
	DIMENSION INDEX(6),D1(810)	V1.1
	EQUIVALENCE (D,D1)	V1.1
	DATA INDEX/3,6,7,1,2,5/	V1.1
	DO 100 L=1,NPLANE	V1.1
	J=9*L+262	V1.1
	DO 20 I=1,3	V1.1
	D1(J+I+2)=P(I,2,L)-P(I,1,L)	V1.1
20	D1(J+I+5)=P(I,3,L)-P(I,1,L)	V1.1
	CALL CROSS(D1(J+3),D1(J+6),D1(J))	V1.1
	SUMD1=0.0	V1.1
	SUMD2=0.0	V1.1
	DO 30 I=1,3	V1.1
	SUMD1=SUMD1+D1(J+I-1)**2	V1.1
30	SUMD2=SUMD2+D1(J+I+2)**2	V1.1
	SUMD1=SQRT(SUMD1)	V1.1
	SUMD2=SQRT(SUMD2)	V1.1
	DO 40 I=1,3	V1.1
	D1(J+I-1)=D1(J+I-1)/SUMD1	V1.1
40	D1(J+I+2)=D1(J+I+2)/SUMD2	V1.1
	CALL CROSS(D1(J),D1(J+3),D1(J+6))	V1.1
	DO 50 I=1,3	V1.1
	TEMP=D1(INDEX(I)+J)	V1.1
	D1(INDEX(I)+J)=D1(INDEX(I+3)+J)	V1.1
50	D1(INDEX(I+3)+J)=TEMP	V1.1
100	CONTINUE	V1.1
	DO 600 J=1,NPLANE	V1.1
	NUM = J + 30	V1.1
	DO 600 K=1,3	V1.1
600	SEGLP(K,NUM) = P(K,1,J)	V1.1
	RETURN	V1.1
	END	V1.1

SUBROUTINE PREPLT(X,Y,XSAV,YSAV,XMIN,XMAX,YMIN,YMAX,IPEN,NEWPEN)	V1.1
C*****	V1.1
C	V1.1
C THIS SUBROUTINE PERFORMS NECESSARY PEN MOVES FOR 1ST PLOT	V1.1
C AFTER CLIPPING	V1.1
C	V1.1
C*****	V1.1
LOGICAL XOFF,YOFF	V1.1
IF (NEWPEN.NE.-2) RETURN	V1.1
C	V1.1
C OUTSIDE X AND/OR Y BOUNDARIES???	V1.1
C	V1.1
XOFF=.FALSE.	V1.1
YOFF=.FALSE.	V1.1
IF (X.LT.XMIN.OR.XSAV.LT.XMIN.OR.	V1.1
1 X.GT.XMAX.OR.XSAV.GT.XMAX) XOFF=.TRUE.	V1.1
IF (Y.LT.YMIN.OR.YSAV.LT.YMIN.OR.	V1.1
1 Y.GT.YMAX.OR.YSAV.GT.YMAX) YOFF=.TRUE.	V1.1
C	V1.1
C DETERMINE IF OFF TOP,BOTTOM,RIGHT,OR LEFT SIDE OF PLOTTER	V1.1
C	V1.1
IF (X.LT.XMIN.OR.XSAV.LT.XMIN) XLIMIT=XMIN	V1.1
IF (X.GT.XMAX.OR.XSAV.GT.XMAX) XLIMIT=XMAX	V1.1
IF (Y.LT.YMIN.OR.YSAV.LT.YMIN) YLIMIT=YMIN	V1.1
IF (Y.GT.YMAX.OR.YSAV.GT.YMAX) YLIMIT=YMAX	V1.1
C	V1.1
C GET X AND Y POINTS DEPENDING ON WHAT BOUNDARIES OVER	V1.1
C	V1.1
IF (XOFF) YTEMP=YINTCP(X,Y,XSAV,YSAV,XLIMIT)	V1.1
IF (.NOT.XOFF) YTEMP=YLIMIT	V1.1
IF (YOFF) XTEMP=XINTCP(X,Y,XSAV,YSAV,YLIMIT)	V1.1
IF (.NOT.YOFF) XTEMP=XLIMIT	V1.1
C	V1.1
C MOVE PEN UP TO THAT SPOT	V1.1
C	V1.1
CALL PLOT(XTEMP,YTEMP,3)	V1.1
IPEN=2	V1.1
RETURN	V1.1
END	V1.1

	SUBROUTINE PRJELR	V1.1
C	*****	V1.1
C		V1.1
C	THIS SUBROUTINE PROJECTS ELLIPSOIDS ONTO THE PROJECTION PLANE.	V1.1
C		V1.1
C	*****	V1.1
	COMMON/ELLIPSE/NSTEPS(90),IELP,A(3,3,30),SEGLP(3,90),VP(3),	V1.1
	*D(3,3,90),DVP(3,3),RA(3),NSEG,SEGLPO(3,90)	V1.2
	COMMON/POLYGON/NPLANE,IFLAG,NPPP(90),PO(3,4,60),P(3,4,60),	V1.1
	*CONVEC(2,4,90),POS(2,90),SIGN(90)	V1.1
	DIMENSION DD(3,3),DDD(3,3),SS(3),S(3)	V1.1
	DIMENSION R(3,3),R2(2,3)	V1.1
	REAL LAMDA1,LAMDA2,M1,M2	V1.1
	IF(NSEG.EQ.0) RETURN	V1.1
	DO 100 I=1,NSEG	V1.1
	CALL DOT(D(1,1,I),DVP,DD,3,3,3)	V1.1
	CALL MAT(A(1,1,I),DD,DDD,3,3,3,3,3,3)	V1.1
	CALL DOT(D(1,1,I),DDD,DD,3,3,3)	V1.1
	CALL MAT(DVP,DD,DDD,3,3,3,3,3,3)	V1.1
	DO 10 K=1,3	V1.1
10	SS(K) = SEGLP(K,I) - VP(K) + SEGLPO(K,I)	V1.2
	CALL MAT(DVP,SS,S,3,3,1,3,3,3)	V1.1
	DO 30 II=1,3	V1.1
	IF (ABS(S(II)).LT.1.E-11) S(II)=1.0	V1.2
30	CONTINUE	V1.1
C		V1.1
	CALL SOLVR(DDD(1,1),DDD(2,1),DDD(3,1),DDD(1,3),DDD(2,3),DDD(3,3),	V1.1
	*DDD(1,1),DDD(1,3),S,R(1,1),R(3,1))	V1.1
	CALL SOLVR(DDD(1,2),DDD(2,2),DDD(3,2),DDD(1,3),DDD(2,3),DDD(3,3),	V1.1
	*DDD(2,2),DDD(2,3),S,R(2,2),R(3,2))	V1.1
	CALL SOLVR(DDD(1,1)+DDD(1,2),DDD(2,1)+DDD(2,2),DDD(3,1)+DDD(3,2),	V1.1
	*DDD(1,3),DDD(2,3),DDD(3,3),DDD(1,1)+2.0*DDD(1,2)+DDD(2,2),	V1.1
	*DDD(1,3)+DDD(2,3),S,R(1,3),R(3,3))	V1.1
	R(2,1)=0.0	V1.1
	R(1,2)=0.0	V1.1
	R(2,3)=R(1,3)	V1.1
	DO 15 IK=1,3	V1.1
	DO 15 IJ=1,2	V1.1
15	R2(IJ,IK)=(S(IJ)+R(IJ,IK))/(S(3)+R(3,IK))-S(IJ)/S(3)	V1.1
	CALL SOLVA(R2,A11,A22,A12)	V1.1
	TEMP=(A11+A22)**2-4.0*(A11*A22-A12**2)	V1.1
	IF(TEMP.LT.0.0) TEMP=0.0	V1.1
	TEMP=SQRT(TEMP)	V1.1
	LAMDA1=(A11+A22+TEMP)/2.0	V1.1
	LAMDA2=(A11+A22-TEMP)/2.0	V1.1
	RX1=A12	V1.1
	RY1=LAMDA1-A11	V1.1
	RX2=LAMDA2-A22	V1.1
	RY2=A12	V1.1
	LAMDA1=ABS(LAMDA1)	V1.1
	LAMDA2=ABS(LAMDA2)	V1.1
	M1=SQRT(1.0/(LAMDA1*(RX1**2+RY1**2)))	V1.1

M2=SQRT(1.0/(LAMDA2*(RX2**2+RY2**2)))	V1.1
RX1=RX1*M1	V1.1
RX2=RX2*M2	V1.1
RY1=RY1*M1	V1.1
RY2=RY2*M2	V1.1
CONVEC(1,1,I)=-2.0*RX1	V1.1
CONVEC(2,1,I)=-2.0*RY1	V1.1
CONVEC(1,2,I)=-2.0*RX2	V1.1
CONVEC(2,2,I)=-2.0*RY2	V1.1
DO 20 IJ=1,2	V1.1
CONVEC(IJ,3,I) = -CONVEC(IJ,1,I)	V1.1
CONVEC(IJ,4,I) = -CONVEC(IJ,2,I)	V1.1
20 POS(IJ,I) = CONVEC(IJ,3,I)/2.0 + CONVEC(IJ,4,I)/2.0+S(IJ)/S(3)	V1.1
NPPP(I)=4	V1.1
SIGN(I)=CONVEC(1,1,I)*CONVEC(2,2,I) -	V1.1
1CONVEC(2,1,I)*CONVEC(1,2,I)	V1.1
100 CONTINUE	V1.1
RETURN	V1.1
END	V1.1



	SUBROUTINE PRJPLY	V1.1
C		V1.1
C	*****	V1.1
C		V1.1
C	THIS SUBROUTINE WILL SETUP THE CONVEC ARRAY.	V1.1
C	IT ALSO SETS UP THE POS AND SIGN ARRAYS.	V1.1
C		V1.1
C	ARRAY P IS THE ORIGINAL POSITION VECTORS FOR THE POLYGONS	V1.1
C	IN THE INERTIAL REFERENCE SYSTEM.	V1.1
C	ARRAY CONVEC WILL CONTAIN THE CONTOUR VECTORS	V1.1
C	FOR PROJECTED POLYGONS.	V1.1
C	ARRAY POS WILL CONTAIN POSITION VECTORS FROM THE	V1.1
C	PROJECTION PLANE ORIGIN TO POLYGON POINT # 1.	V1.1
C	ARRAY SIGN WILL CONTAIN THE SIGN THAT RESULTS FROM	V1.1
C	THE CROSS PRODUCT (P2-P1)X(P3-P2).	V1.1
C		V1.1
C	*****	V1.1
	COMMON/POLYGON/NPLANE, IFLAG, NPPP(90), PO(3,4,60), P(3,4,60),	V1.1
	*CONVEC(2,4,90), POS(2,90), SIGN(90)	V1.1
	COMMON/ELLIPSE/NSTEPS(90), IELP, A(3,3,30), SEGLP(3,90), VP(3),	V1.1
	*D(3,3,90), DVP(3,3), RA(3), NSEG, SEGLPO(3,90)	V1.2
	DIMENSION PPP2(3), PP2(3), PP1(3)	V1.1
	IF(NPLANE.EQ.0) RETURN	V1.1
	DO 40 I=1, NPLANE	V1.1
	II=I+30	V1.1
	NPTS=NPPP(II)	V1.1
	DO 35 K=1, NPTS	V1.1
	DO 10 J=1, 3	V1.1
	PPP2(J)=P(J,K,I)-VP(J)	V1.1
10	CONTINUE	V1.1
	CALL MAT(DVP, PPP2, PP2, 3, 3, 1, 3, 3, 3)	V1.1
	IF(K.NE.1) GO TO 16	V1.1
	DO 15 J=1, 2	V1.1
	POS(J, II)=PP2(J)/PP2(3)	V1.1
15	CONTINUE	V1.1
	GO TO 25	V1.1
16	DO 20 J=1, 2	V1.1
20	CONVEC(J,K-1, II)=PP2(J)/PP2(3)-PP1(J)/PP1(3)	V1.1
25	DO 30 J=1, 3	V1.1
30	PP1(J)=PP2(J)	V1.1
	IF(K.EQ.3) SIGN(II)=CONVEC(1,1, II)*CONVEC(2,2, II)-	V1.1
	1CONVEC(2,1, II)*CONVEC(1,2, II)	V1.1
35	CONTINUE	V1.1
	DO 40 J=1, 2	V1.1
	CONVEC(J, NPTS, II)=POS(J, II)-PP2(J)/PP2(3)	V1.1
40	CONTINUE	V1.1
	RETURN	V1.1
	END	V1.1

	SUBROUTINE PSE(X1,IN,SEG,INDEX,INDEX2,IHALF)	V1.1
	DIMENSION X1(3,INDEX,INDEX),IN(INDEX),SEG(3,3333)	V1.1
C		V1.1
C	THIS SUBROUTINE PLOTS A SEMIELLIPSOID.	V1.1
C	THE HALF OF THE ELLIPSOID PLOTTED DEPENDS UPON IHALF.	V1.1
C	IF IHALF = 1 X .GE. 0 IS PLOTTED.	V1.1
C	IF IHALF = 2 X .LT. 0 IS PLOTTED.	V1.1
	DO 100 I=IHALF,INDEX	V1.1
	LINE=INDEX-I+1	V1.1
	IF(IHALF.EQ.2) LINE=I	V1.1
	NPTS=IN(LINE)	V1.1
	DO 50 K=1,NPTS	V1.1
	DO 50 J=1,3	V1.1
	SEG(J,K)=X1(J,K,LINE)	V1.1
	IF(IHALF.EQ.2.AND.J.EQ.1) SEG(J,K)--SEG(J,K)	V1.1
50	CONTINUE	V1.1
	N=NPTS	V1.1
	IF(LINE.EQ.INDEX) GO TO 71	V1.1
	NPT=NPTS-1	V1.1
	DO 60 K=1,NPT	V1.1
	KK=NPT-K+1	V1.1
	N=N+1	V1.1
	SEG(1,N)=SEG(1,KK)	V1.1
	SEG(2,N)=SEG(2,KK)	V1.1
60	SEG(3,N)--SEG(3,KK)	V1.1
	NPT=N-1	V1.1
	DO 70 K=1,NPT	V1.1
	KK=NPT-K+1	V1.1
	N=N+1	V1.1
	SEG(1,N)=SEG(1,KK)	V1.1
	SEG(2,N)--SEG(2,KK)	V1.1
70	SEG(3,N)=SEG(3,KK)	V1.1
71	IPEN=3	V1.1
	CALL PNTPLT(SEG,IPEN,INDEX2,N)	V1.1
100	CONTINUE	V1.1
	RETURN	V1.1
	END	V1.1

	SUBROUTINE ROT(A,L,TH,M)		V1.1
C		REV 01 08/10/72	V1.1
C	COMPUTES ROTATION MATRIX A FOR ANGLE TH		V1.1
C	ABOUT X,Y OR Z AXIS AS L = 1,2, OR 3.		V1.1
C			V1.1
C	ARGUMENTS:		V1.1
C	A: 3X3 ROTATION MATRIX TO BE COMPUTED.		V1.1
C	L: 1,2 OR 3 TO ROTATE ABOUT X,Y OR Z AXIS.		V1.1
C	TH: ANGLE OF ROTATION IN RADIANS.		V1.1
C	M: 1ST DIMENSION OF A IN CALLING PROGRAM.		V1.1
C			V1.1
	DIMENSION A(M,3)		V1.1
	C= COS(TH)		V1.1
	S= SIN(TH)		V1.1
	IF (L.EQ.2) S = -S		V1.1
	DO 30 I=1,3		V1.1
	IF(I.EQ.3)GO TO 20		V1.1
	DO 10 J=1,2		V1.1
	A(I,J+1)=0.0		V1.1
	A(J+1,I)=0.0		V1.1
	IF(I+J+L.NE.5)GO TO 10		V1.1
	A(I,J+1)=S		V1.1
	A(J+1,I)=-S		V1.1
10	CONTINUE		V1.1
20	A(I,I)= C		V1.1
	IF(I.EQ.L)A(I,I)=1.0		V1.1
30	CONTINUE		V1.1
	RETURN		V1.1
	END		V1.1

SUBROUTINE SOLVA(R,AA11,AA22,AA12)	V1.1
DIMENSION R(2,3)	V1.1
A11=R(1,1)**2	V1.1
A12=2.0*R(2,1)*R(1,1)	V1.1
A13=R(2,1)**2	V1.1
A21=R(1,2)**2	V1.1
A22=2.0*R(2,2)*R(1,2)	V1.1
A23=R(2,2)**2	V1.1
A31=R(1,3)**2	V1.1
A32=2.0*R(2,3)*R(1,3)	V1.1
A33=R(2,3)**2	V1.1
DEL=A11*(A22*A33-A23*A32)-A12*(A21*A33-A23*A31)+	V1.1
1A13*(A21*A32-A22*A31)	V1.1
AA11=((A22-A12)*(A33-A23)-(A23-A13)*(A32-A22))/DEL	V1.1
AA12=((A23-A13)*(A31-A21)-(A21-A11)*(A33-A23))/DEL	V1.1
AA22=((A21-A11)*(A32-A22)-(A22-A12)*(A31-A21))/DEL	V1.1
IF(ABS(AA12).LT.1.E-11) AA12=.000001	V1.2
RETURN	V1.1
END	V1.1

	SUBROUTINE SOLVR(A1,A2,A3,A4,A5,A6,A7,A8,P,RX,RZ)	V1.1
C		V1.1
C	*****	V1.1
C		V1.1
C	THIS SUBROUTINE WILL SOLVE A SET OF SIMULTANEOUS EQUATIONS	V1.1
C	TO FIND COMPONETS OF VECTOR R THAT SATISFY THE PROPERTIES NEEDED	V1.1
C	TO DETURMINE THE EQUATION OF THE PROJECTED ELLIPSE.	V1.1
C		V1.1
C	SEE WRITEUP.	V1.1
C		V1.1
C	*****	V1.1
	DIMENSION P(3)	V1.1
	B=A1*P(1)+A2*P(2)+A3*P(3)	V1.1
	D=A4*P(1)+A5*P(2)+A6*P(3)	V1.1
	T1=A7*(D/B)**2+A6-2.0*A8*D/B	V1.1
	T2=2.0*A7*D/(B)**2-2.0*A8/B	V1.1
	T3=A7*(1/B)**2-1	V1.1
	RZ=(-T2+SQRT(T2**2-4.0*T1*T3))/(2.0*T1)	V1.1
	RX=-D*RZ/B-1.0/B	V1.1
	RETURN	V1.1
	END	V1.1

	SUBROUTINE TITLE	V1.1
	DIMENSION ICOLOR(21)	80386
	CHARACTER*4 ID(10,20)	80386
	COMMON/DEBUG/IDEBUG(80),NISG,DEVFLG,ONLINE,TERM,BDRS,OFLINE	V1.1
	INTEGER ONLINE,DEVFLG,TERM,BDRS,OFLINE	V1.1
	NLINE=20	V1.1
	SIZE=.335	V1.1
	X=1.375	V1.1
	Y=10.0	V1.1
C		V1.1
C	INITIALIZE PLOTTING PACKAGE	V1.1
C		V1.1
	CALL PLOT(0.0,0.0,-3)	V1.1
	READ(5,1) NFRME,ICOLOR(21)	V1.1
1	FORMAT(I2,I2)	V1.1
	IF(NFRME.EQ.0) RETURN	V1.1
	DO 300 K=1,NFRME	V1.1
	DO 50 I=1,NLINE	V1.1
	READ(5,200) (ID(J,I),J=1,8),ICOLOR(I)	V1.1
	WRITE(6,200) (ID(J,I),J=1,8),ICOLOR(I)	V1.1
200	FORMAT(7A4,A2,I2)	V1.1
50	CONTINUE	V1.1
	DO 100 I=1,NLINE	V1.1
	Y=Y-.5	V1.1
	IF(DEVFLG.EQ.OFLINE.OR.DEVFLG.EQ.BDRS) CALL COLOR(ICOLOR(I),IERR) 80386	V1.1
	CALL SYMBOL(X,Y,SIZE,ID(1,I),0.,30)	V1.1
100	CONTINUE	V1.1
	IF(DEVFLG.EQ.ONLINE) CALL PLOT(12.,0.,-3)	V1.1
	IF(DEVFLG.EQ.TERM) CALL PLOT(0.0,0.0,-3)	V1.1
	IF(DEVFLG.EQ.BDRS) CALL NFRAME	V1.1
	IF(DEVFLG.EQ.OFLINE) CALL PLOT (14.,0.,-3)	V1.1
300	CONTINUE	V1.1
	RETURN	V1.1
	END	V1.1

	SUBROUTINE TPOINT(PP2,I,IN)	V1.1
	DIMENSION PP2(3),R(3),PP1(3)	V1.1
	COMMON/POLYGON/NPLANE,IFLAG,NPPP(90),PO(3,4,60),P(3,4,60),	V1.1
	*CONVEC(2,4,90),POS(2,90),SIGN(90)	V1.1
C		V1.1
C	THIS SUBROUTINE TESTS A POINT ON THE PROJECTION PLANE	V1.1
C	DEFINED BY PP2 AGAINST A POLYGON ON THE PROJECTION PLANE	V1.1
C	DEFINED BY I. A FLAG 'IN' IS RETURNED TO INDICATE IF THE	V1.1
C	POINT WAS INSIDE OR OUTSIDE THE POLYGON.	V1.1
C		V1.1
C	IN = 1 POINT WAS INSIDE POLYGON	V1.1
C		V1.1
C	IN = 2 POINT WAS OUTSIDE POLYGON	V1.1
C		V1.1
	IN=1	V1.1
	NPTS1=NPPP(I)	V1.1
	DO 20 JJ=1,2	V1.1
20	PP1(JJ)=POS(JJ,I)	V1.1
	DO 100 L=1,NPTS1	V1.1
	DO 30 N=1,2	V1.1
30	R(N)=PP2(N)-PP1(N)	V1.1
	SIGN2=CONVEC(1,L,I)*R(2)-CONVEC(2,L,I)*R(1)	V1.1
	IF(SIGN2*SIGN(I).LT. 0.) GO TO 150	V1.1
	IF(ABS(SIGN2*SIGN(I)).LT.1.E-11) GO TO 150	V1.1
	DO 100 N=1,2	V1.1
100	PP1(N)=PP1(N)+CONVEC(N,L,I)	V1.1
	RETURN	V1.1
150	IN=2	V1.1
	RETURN	V1.1
	END	V1.1

SUBROUTINE TRANS1(R,P)	V1.1
COMMON/ELLIPSE/NSTEPS(90),IELP,A(3,3,30),SEGLP(3,90),VP(3),	V1.1
*D(3,3,90),DVP(3,3),RA(3),NSEG,SEGLPO(3,90)	V1.2
COMMON/VIEWP/VP0(3),DVPO(3,3),IVP,VP2(3)	V1.1
DIMENSION DD(3,3),P(3),R(3),R2(3),SEGLP2(3),S(3)	V1.2
IF(IELP.GT. 30) GO TO 10	V1.1
CALL DOTT(DVP,D(1,1,IELP),DD,3,3,3)	V1.1
20 CONTINUE	V1.1
CALL MAT(DD,R,R2,3,3,1,3,3,3)	V1.1
DO 2 I=1,3	V1.2
2 S(I) = SEGLP(I,IELP) + SEGLPO(I,IELP)	V1.2
CALL MAT(DVP,S,SEGLP2,3,3,1,3,3,3)	V1.2
DO 1 I=1,3	V1.1
1 P(I)=SEGLP2(I)+R2(I)-VP2(I)	V1.1
RETURN	V1.1
10 DO 11 I=1,3	V1.1
DO 11 J=1,3	V1.1
11 DD(I,J) = DVP(I,J)	V1.1
GO TO 20	V1.1
END	V1.1



	REAL FUNCTION XINTCP(X,Y,XSAV,YSAV,YTEMP)	V1.1
C	*****	V1.1
C		V1.1
C	THIS FUNCTION CALCULATES THE X INTERCEPT AT YTEMP	V1.1
C		V1.1
C	*****	V1.1
	X1=X-XSAV	V1.1
	Y1=Y-YSAV	V1.1
	IF (Y1.NE.0.0) PFACTR=X1/Y1	V1.1
	IF (ABS(Y1).LT.1.E-11) PFACTR=0.0	V1.2
	Y2=YTEMP-YSAV	V1.1
	XINTCP=Y2*PFACTR+XSAV	V1.1
	RETURN	V1.1
	END	V1.1

	SUBROUTINE XYZ(MU,A,B,C,S,M,JFLAG)	V1.1
	DIMENSION MU(3),S(3),M(3,2)	V1.1
	REAL M,MU	V1.1
C		V1.1
C	*****	V1.1
C		V1.1
C	ALPHA AND BETA RELATE THE Y AND Z COMPONENTS OF M TO	V1.1
C	THE X COMPONENT OF M.	V1.1
C	*****	V1.1
C		V1.1
	ALPHA = MU(2) / MU(1)	V1.1
	BETA = MU(3) / MU(1)	V1.1
C		V1.1
C	*****	V1.1
C		V1.1
C	SOLVE THE EQUATION FOR ELLIPSE 'N' TO FIND A POINT ON	V1.1
C	THE ELLIPSE THAT WILL DETERMINE A VECTOR M.	V1.1
C		V1.1
C	*****	V1.1
C		V1.1
	T1=A+B*ALPHA*ALPHA+C*BETA*BETA	V1.1
	T2=2*A*S(1)+2*B*ALPHA*S(2)+2*C*BETA*S(3)	V1.1
	T3=A*S(1)**2+B*S(2)**2+C*S(3)**2-1	V1.1
	TEMP= T2 * T2 - 4 * T1 * T3	V1.1
C		V1.1
C	*****	V1.1
C		V1.1
C	NO SOLUTION MEANS ELLIPSOID 'N' NOT TOUCHED BY LINE OF	V1.1
C	SIGHT RAY.	V1.1
C		V1.1
C	*****	V1.1
C		V1.1
	IF(TEMP.LT.0.0) GO TO 2	V1.1
	TEMP=SQRT(TEMP)	V1.1
C		V1.1
C	*****	V1.1
C		V1.1
C	FIND TWO POSSIBLE M VECTORS BECAUSE A RAY ENTERING A	V1.1
C	SOLID MUST ALSO LEAVE.	V1.1
C		V1.1
C	*****	V1.1
C		V1.1
	M(1,1)=(T2+TEMP)/(2*T1)	V1.1
	M(2,1)=ALPHA*M(1,1)	V1.1
	M(3,1)=BETA*M(1,1)	V1.1
	M(1,2)=(T2-TEMP)/(2*T1)	V1.1
	M(2,2)=ALPHA*M(1,2)	V1.1
	M(3,2)=BETA*M(1,2)	V1.1
	JFLAG=0	V1.1
	RETURN	V1.1
2	JFLAG=1	V1.1
	RETURN	V1.1

END

V1.1

	REAL FUNCTION YINTCP(X,Y,XSAV,YSAV,XTEMP)	V1.1
C	*****	V1.1
C		V1.1
C	THIS FUNCTION CALCULATES THE Y INTERCEPT AT XTEMP	V1.1
C		V1.1
C	*****8	V1.1
	X1=X-XSAV	V1.1
	Y1=Y-YSAV	V1.1
	IF (X1.NE.0.0) PFACTR=Y1/X1	V1.1
	IF (ABS(X1).LT.1.E-11) PFACTR=0.0	V1.2
	X2=XTEMP-XSAV	V1.1
	YINTCP=X2*PFACTR+YSAV	V1.1
	RETURN	V1.1
	END	V1.1

	SUBROUTINE YZ(MU,A,B,C,S,M,JFLAG)	V1.1
	DIMENSION MU(3),S(3),M(3,2)	V1.1
	REAL MU,M	V1.1
C	*****	V1.1
C		V1.1
C	ALPHA RELATES THE Z COMPONET TO THE Y COMPONET	V1.1
C		V1.1
C	*****	V1.1
C	ALPHA=MU(3)/MU(2)	V1.1
C	*****	V1.1
C		V1.1
C	SOLVE THE EQUATION FOR ELLIPSE 'N' WHEN X=0 TO	V1.1
C	FIND A POINT ON THE ELLIPSE THAT WILL DETERMINE A VECTOR M.	V1.1
C		V1.1
C	*****	V1.1
	T1=B+C*ALPHA*ALPHA	V1.1
	T2=2*B*S(2)+2*C*ALPHA*S(3)	V1.1
	T3=A*S(1)**2+B*S(2)**2+C*S(3)**2-1	V1.1
	TEMP=T2*T2-4*T1*T3	V1.1
C	*****	V1.1
C		V1.1
C	NO SOLUTION MEANS ELLIPSOID 'N' NOT TOUCHED BY LINE	V1.1
C	OF SIGHT RAY.	V1.1
C		V1.1
C	*****	V1.1
	IF(TEMP.LT.0.0) GO TO 2	V1.1
	TEMP=SQRT(TEMP)	V1.1
C	*****	V1.1
C		V1.1
C	FIND TWO POSSIBLE M VECTORS BECAUSE A RAY ENTERING	V1.1
C	A SOLID MUST ALSO LEAVE.	V1.1
C		V1.1
C	*****	V1.1
	M(2,1)=(T2+TEMP)/(2*T1)	V1.1
	M(1,1)=0.0	V1.1
	M(3,1)=ALPHA*M(2,1)	V1.1
	M(2,2)=(T2-TEMP)/(2*T1)	V1.1
	M(1,2)=0.0	V1.1
	M(3,2)=ALPHA*M(2,2)	V1.1
	JFLAG=0	V1.1
	RETURN	V1.1
2	JFLAG=1	V1.1
	RETURN	V1.1
	END	V1.1

	SUBROUTINE Z(MU,A,B,C,S,M,JFLAG)	V1.1
	DIMENSION MU(3),S(3),M(3,2)	V1.1
	REAL M,MU	V1.1
C	*****	V1.1
C		V1.1
C	SOLVE THE EQUATION FOR ELLIPSE 'N' WHEN X=0 AND	V1.1
C	Y=0 TO FIND A POINT ON THE ELLIPSE THAT	V1.1
C	WILL DETERMINE A VECTOR M.	V1.1
C		V1.1
C	*****	V1.1
	T1=C	V1.1
	T2=2*C*S(3)	V1.1
	T3=A*S(1)**2+B*S(2)**2+C*S(3)**2-1	V1.1
	TEMP=T2*T2-4*T1*T3	V1.1
C	*****	V1.1
C		V1.1
C	NO SOLUTION MEANS ELLIPSOID 'N' NOT TOUCHED BY LINE	V1.1
C	OF SIGHT RAY.	V1.1
C		V1.1
C	*****	V1.1
	IF(TEMP.LT.0.0) GO TO 2	V1.1
	TEMP=SQRT(TEMP)	V1.1
C	*****	V1.1
C		V1.1
C	FIND TWO POSSIBLE M VECTORS BECAUSE A RAY ENTERING	V1.1
C	A SOLID MUST ALSO LEAVE.	V1.1
C		V1.1
C	*****	V1.1
	M(1,1)=0.0	V1.1
	M(2,1)=0.0	V1.1
	M(3,1)=(T2+TEMP)/(2*T1)	V1.1
	M(1,2)=0.0	V1.1
	M(2,2)=0.0	V1.1
	M(3,2)=(T2-TEMP)/(2*T1)	V1.1
	JFLAG=0	V1.1
	RETURN	V1.1
2	JFLAG=1	V1.1
	RETURN	V1.1
	END	V1.1